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SMITHSONIAN MISCELLANEOUS COLLECTIONS VOLUME 69. NUMBER 1

SMITHSONIAN METEOROLOGICAL TABLES

[BASED ON GUYOT'S METEOROLOGICAL AND PHYSICAL TABLES]

FOURTH REVISED EDITION

(Corrected to January, 1918)



(PUBLICATION 2493)

CITY OF WASHINGTON
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1918

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ADVERTISEMENT TO FOURTH REVISED EDITION.

THE original edition of the Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896, 1897, and 1907. A fourth revised edition is here presented, which has been prepared under the direction of Professor Charles F. Marvin, Chief of the U.S. Weather Bureau, assisted by Professor Herbert H. Kimball. They have had at their disposal numerous notes left by the late Professor Cleveland Abbe, and have consulted with officials of the U.S. Bureau of Standards and of other Government bureaus relative to the value of certain physical constants that have entered into the calculation of the tables.

All errata thus far detected in the earlier editions have here been corrected. New vapor pressure tables, derived from the latest experimental values by means of a modification of Van der Waals interpolation formula devised by Professor Marvin, have been introduced. The table of relative acceleration of gravity at different latitudes has been recomputed from a new equation based upon the latest investigations of the U.S. Coast and Geodetic Survey. These values have been employed in reducing barometric readings to the standard value of gravity adopted by the International Bureau of Weights and Measures, supplementing a table that has been introduced for directly reducing barometer readings from the value of gravity at the place of observation to its standard value.

The new values of vapor pressure and of gravity acceleration thus obtained, together with a recent and more accurate determination of the density of mercury, have called for an extensive revision of numerous other tables, and especially of those for the reduction of psychrometric observations, and the barometrical tables.

Among the new tables added are those for converting barometric inches and barometric millimeters into millibars, for determining heights from pressures expressed in dynamic units, tables of gradient winds, and tables giving the duration of astronomical and civil twilight, and the transmission percentages of radiation through moist air.

The tables of International Meteorological Symbols, of Cloud Classification, of the Beaufort Scale of Winds, of the Beaufort Weather Notation, and the List of Meteorological Stations, are among those extensively revised.

Tables for reducing barometric readings to sea level, and tables of logarithms of numbers, of natural sines and cosines, of tangents and cotangents, and for dividing by 28, 29, and 31, with a few others, have been omitted from this edition.

CHARLES D. WALCOTT,

Secretary.

Smithsonian Institution, *March*, 1918.

ADVERTISEMENT TO THIRD REVISED EDITION

The original edition of Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896 and 1897. A third revised edition is here presented, which has been prepared at the request of the late Professor Langley by the coöperation of Professors Alexander McAdie, Charles F. Marvin, and Cleveland Abbe.

All errata thus far detected have been corrected upon the plates, the Marvin vapor tensions over ice have been introduced, Professor F. H. Bigelow's System of Notation and Formulæ has been added, the List of Meteorological Stations has been revised, and the International Meteorological Symbols, together with the Beaufort Notation, are given at the close of the volume.

R. RATHBUN,

Acting Secretary.

Smithsonian Institution, December, 1906.

ADVERTISEMENT TO SECOND REVISED EDITION.

The edition of the Smithsonian Meteorological Tables issued in 1893 having become exhausted, a careful examination of the work has been made, at my request, by Mr. Alexander McAdie, of the United States Weather Bureau, and a revised edition was published in 1896, with corrections upon the plates and a few slight changes. The International Meteorological Symbols and an Index were also added.

The demand for the work has been so great that it becomes necessary to print a new edition of the revised work, which is here presented with corrections to date.

S. P. LANGLEY,

Secretary.

SMITHSONIAN INSTITUTION, WASHINGTON CITY, October 30, 1897.

PREFACE TO EDITION OF 1893.

In connection with the system of meteorological observations established by the Smithsonian Institution about 1850, a collection of meteorological tables was compiled by Dr. Arnold Guyot, at the request of Secretary Henry, and published in 1852 as a volume of the Miscellaneous Collections.

Five years later, in 1857, a second edition was published after careful revision by the author, and the various series of tables were so enlarged as to extend the work from 212 to over 600 pages.

In 1859 a third edition was published, with further amendments.

Although designed primarily for the meteorological observers reporting to the Smithsonian Institution, the tables obtained a much wider circulation, and were extensively used by meteorologists and physicists in Europe and in the United States.

After twenty-five years of valuable service, the work was again revised by the author; and the fourth edition, containing over 700 pages, was published in 1884. Before finishing the last few tables, Dr. Guyot died, and the completion of the work was intrusted to his assistant, Prof. Wm. Libber, Jr., who executed the duties of final editor.

In a few years the demand for the tables exhausted the edition, and thereupon it appeared desirable to recast entirely the work. After very careful consideration, I decided to publish the new tables in three parts: Meteorological Tables, Geographical Tables, and Physical Tables, each representative of the latest knowledge in its field, and independent of the others; but the three forming a homogeneous series.

Although thus historically related to Dr. Guyot's Tables, the present work is so substantially changed with respect to material, arrangement, and presentation that it is not a fifth edition of the older tables, but essentially a new publication.

In its preparation the advantage of conformity with the recently issued *International Meteorological Tables* has been kept steadily in view, and so far as consistent with other decisions, the constants and methods there employed have been followed. The most important difference in constants is the relation of the yard to the metre. The value provisionally adopted by the Bureau of Weights and Measures of the United States Coast and Geodetic Survey,

I metre = 39.3700 inches,

has been used here in the conversion-tables of metric and English linear measures, and in the transformation of all formulæ involving such conversions.

A large number of tables have been newly computed; those taken from the *International Meteorological Tables* and other official sources are credited in the introduction.

To Prof. Wm. Libber, Jr., especial acknowledgments are due for a large amount of attention given to the present work. Prof. Libber had already completed a revision, involving considerable recomputation, of the meteorological tables contained in the last edition of Guyot's Tables, when it was determined to adopt new values for many of the constants, and to have the present volume set with new type. This involved a large amount of new computation, which was placed under the direction of Mr. George E. Curtis, who has also written the text, and has carefully prepared the whole manuscript and carried it through the press. To Mr. Curtis's interest, and to his special experience as a meteorologist, the present volume is therefore largely due.

Prof. Libber has contributed Tables 38, 39, 55, 56, 61, 74, 77, 89, and 90, and has also read the proof-sheets of the entire work.

I desire to express my acknowledgments to Prof. CLEVELAND ABBE, for the manuscript of Tables 32, 81, 82, 83, 84, 85, 86; to Mr. H. A. HAZEN, for Tables 49, 50, 94, 95, 96, which have been taken from his *Hand-book of Meteorological Tables*; and also to the Superintendent of the United States Coast and Geodetic Survey, the Chief Signal Officer of the Army, and the Chief of the Weather Bureau, for much valuable counsel during the progress of the work.

S. P. LANGLEY.

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INTRODUCTION.

DESCRIPTION AND USE OF TABLES.

THERMOMETRY.

The present standard for exact thermometry is the normal centigrade scale of the constant-volume hydrogen thermometer as defined by the International Bureau of Weights and Measures. The constant volume is one liter and the pressure at the freezing point is one meter of mercury reduced to freezing and standard gravity. The scale is completely defined by designating the temperature of melting ice, o°, and of condensing steam, 100°, both under standard atmospheric pressure. All other thermometric scales that depend upon the physical properties of substances may by definition be made to coincide at the ice point and the boiling point with the normal scale as above defined, but they will diverge more or less from it and from each other at all other points. However, by international consent it is customary in most cases to refer other working scales to the hydrogen scale.

The absolute or thermodynamic scale. To obviate the difficulty which arises because thermometers of different type and substance inherently disagree except at the fixed points, Lord Kelvin proposed that temperatures be defined by reference to certain thermodynamic laws. This course furnishes a scale independent of the nature or properties of any particular substance. The resulting scale has been variously named the absolute, the thermodynamic, and, more recently, in honor of its author, the Kelvin scale. The temperature of melting ice by this scale on the centigrade basis is not as yet accurately known, but it is very nearly 273.13, and that of the boiling point, 373.13.

Many problems in physics and meteorology call for the use of the absolute scale; but it is not convenient, and in many cases not necessary, to adhere strictly to the true thermodynamic scale. In fact, the general requirements of science will very largely be met by the use of an approximate absolute scale which for the centigrade system is defined by the equation

$$T = (273^{\circ} + t^{\circ} \text{ C.})$$

The observed quantity, t° , may be referred to the normal hydrogen centigrade scale or be determined by any acceptable thermometric method.

This scale differs from the true Kelvin scale, first, because 273° is not the exact value of the ice point on the Kelvin scale, second, because each observed value of t° other than 0° or 100° requires a particular correction to

convert it to the corresponding value on the Kelvin scale. These corrections will differ according to the kind of thermometer used in obtaining the value t° , and while they are small for temperatures between 0° and 100° they are large at extreme temperatures and are important in all questions involving thermometric precision.

Since, however, the approximate absolute scale is sufficiently exact for nearly all purposes, and especially since it is most convenient in computations and in the publication of results, much confusion and uncertainty of terminology and meaning will be obviated if scientists will agree to give the approximate absolute scale a particular name of its own.

For the purpose of these tables the name Approximate Absolute will be employed, and in accordance therewith thermometric scales may be designated as follows:—

Scale.	Ice point.	Boiling point.	Symbol.	
Centigrade	o°	100°	<i>C</i> .	
Fahrenheit	32	212	F. or Fahr.	
Reaumur	O	8o	R.	
Thermodynamic	$\begin{cases} 273.13 \ C. \pm \\ 491.6 \ F. \pm \end{cases}$	373.13 <i>C</i> . ± 671.6 <i>F</i> . ±	A. or K .	
Absolute Kelvin	(Names strictly synonymous and strictly one ideal scale.)			
Approximate Absolute	273	373	A.A.	

TABLE 1. Conversion of the Approximate Absolute thermometric scale to the Centigrade, Fahrenheit, and Reaumur scales.

The equivalent values of the four scales are given for every degree on the Approximate Absolute scale from 375° to 0°.

By the help of the table of proportional parts preceding this table, it is also convenient for converting Fahrenheit to Centigrade and Reaumur, and Centigrade to Fahrenheit and Reaumur.

The formulæ expressing the relations between the different scales are also given, in which

$$A.A.^{\circ}$$
 = Temperature — Approximate Absolute Scale.

 $C.^{\circ}$ = Temperature — Centigrade Scale.

 $F.^{\circ}$ = Temperature — Fahrenheit Scale.

 $R.^{\circ}$ = Temperature — Reaumur Scale.

Examples:

To convert 285°5 Approximate Absolute into Centigrade, Fahrenheit, and Reaumur.

From the table,
$$285^{\circ}$$
 $A.A. = 12^{\circ}$ $C. = 53^{\circ}6$ $F. = 9^{\circ}6$ $R.$
From the proportional parts, $0.5 = 0.5 = 0.9 = 0.4$
 285.5 $A.A. = 12.5$ $C. = 54.5$ $F. = 10.0$ $R.$

To convert 16°9 Centigrade to Approximate Absolute, Fahrenheit, and Reaumur.

From the table, I6°.
$$C. = 289^{\circ}. A.A. = 60^{\circ}. 8 F. = 12^{\circ}. 8 R.$$

From the proportional parts $0.9 = 0.9 = 1.6 = 0.7$
 $16.9 C. = 289.9 A.A. = 62.4 F. = 13.5 R.$

Or,
$$16^{\circ}9 \times 2 \left(1 - \frac{1}{10}\right) + 32 = 33.8$$

- 3.4
- $\frac{32.0}{62.4}$

To convert 147°7 Fahrenheit to Approximate Absolute, Centigrade, and Reaumur.

From the table, I40°.
$$F. = 333$$
°. $A.A. = 60$ °. $C. = 48$ °. $R.$ From the proportional parts $7.7 = 4.3 = 4.3 = 3.4$
 147.7 $F. = 337.3$ $A.A. = 64.3$ $C. = 51.4$ $R.$

Or,
$$\frac{147.7 - 32.0}{2} \left(\mathbf{I} + \frac{\mathbf{I}}{10} + \frac{\mathbf{I}}{100} + \frac{\mathbf{I}}{1000} \text{ etc.} \right) = 57.85 + 5.78 + .58 + .06 - 64.27 C$$

Fahrenheit may also be reduced to Approximate Absolute by obtaining its equivalent in Centigrade from Table 2 and adding 273 to the result.

To convert 18.3 Reaumur to Approximate Absolute, Centigrade, and Fahrenheit.

From the table, 16°
$$R$$
. = 293° A . A . = 20° C . = 68° F . From the proportional parts, 2.3 = 2.9 = 2.9 = 5.2

18.3 R . = 295.9 A . A . = 22.9 C . = 73.2 F .

Or,
$$18.3 \times \frac{5}{4} = \frac{91.5}{4} = 22.9 C$$
, and $(18.3 \times \frac{9}{4}) + 32 = \frac{164.7}{4} + 32 = 73.2 F$.

TABLE 2.

TABLE 2. Conversion of readings of the Fahrenheit thermometer to readings Centigrade.

The conversion of Fahrenheit temperatures to Centigrade temperatures is given for every tenth of a degree from $+ 130^{\circ}9$ F. to $- 120^{\circ}9$ F. The side argument is the whole number of degrees Fahrenheit, and the top argument, tenths of a degree Fahrenheit; interpolation to hundredths of a degree, when desired, is readily effected mentally. The tabular values are given to hundredths of a degree Centigrade.

The formula for conversion is

$$C^{\circ} = \frac{5}{9} (F^{\circ} - 32^{\circ})$$

where F° is a given temperature Fahrenheit, and C° the corresponding temperature Centigrade.

Example:

To convert 79°7 Fahrenheit to Centigrade.

The table gives directly 26°50 C.

For conversions of temperatures outside the limits of the table use Table 1.

Table 3. Conversion of readings of the Centigrade thermometer to readings
Fahrenheit.

The conversion of Centigrade temperatures to Fahrenheit temperatures is given for every tenth of a degree Centigrade from $+60^{\circ}9$ to $-90^{\circ}9$ C. The tabular values are expressed in hundredths of a degree Fahrenheit.

The formula for conversion is

$$F^{\circ} = \frac{9}{5} C^{\circ} + 32^{\circ}$$

where C° is a given temperature Centigrade, and F° the corresponding temperature Fahrenheit.

For conversions of temperatures outside the limits of the table, use Table 1 or 4.

TABLE 4. Conversion of readings of the Centigrade thermometer near the boiling point to readings Fahrenheit.

This is an extension of Table 3 from 9000 to 10009 Centigrade.

Example:

To convert 95°74 Centigrade to Fahrenheit.

From the table, 95.70 C = 204.26 F. By interpolation, 0.04 = 0.07

 $\frac{0.04}{95.74} = \frac{0.07}{C} = \frac{0.07}{204.33} F.$

TABLE 5. Conversion of differences Fahrenheit to differences Centigrade.

The table gives for every tenth of a degree from 0° to $20^{\circ}9$ F. the corresponding lengths of the Centigrade scale.

TABLE 6.

TABLE 6. Conversion of differences Centigrade to differences Fahrenheit.

The table gives for every tenth of a degree from 0° to 9.9 C. the corresponding lengths of the Fahrenheit scale.

Example:

To find the equivalent difference in Fahrenheit degrees for a difference of 4.72 Centigrade.

From the table, 4.70 C. = 8.46 F. From the table by moving the decimal point for 0.2, 0.02 = 0.04 = 0.04 0.70 C. = 0.02 = 0.04 = 0.04 0.70 C. = 0.02 = 0.04 = 0.04 0.70 C. = 0.02 = 0.04

TABLES 7, 6.

TABLES 7, 8. Correction for the temperature of the emergent mercurial column of thermometers.

When the temperature of the thermometer stem containing a portion of the mercury column is materially different from that of the bulb, a correction needs to be applied to the observed reading unless the instrument has been previously graduated for the condition of use. This correction frequently becomes necessary in physical experiments where the bulb only, or else the bulb with a portion of the stem, is immersed in a bath whose temperature is to be determined. In meteorological observations the correction may become appreciable in wet-bulb, dew-point, and solar-radiation thermometers, when the temperature of the bulb is considerably above or below the air temperature.

If t' be the average temperature of the emergent mercury column, t the observed reading of the thermometer, n the length of the mercury in the emergent stem in scale degrees, and a the apparent expansion of mercury in glass for 1° , the correction is given by the expression

$$an(t-t')$$
, or $-an(t'-t)$

which latter may be the more convenient form when t' is greater than t.

The value of α varies with the composition of the glass of which the thermometer stem is composed. For glass of unknown composition the best average value for centigrade temperatures appears to be 0.000155, while for stems of Jena 16¹¹¹, or similar glasses, or Jena 59¹¹¹, the values 0.00016 for the former and 0.000165 for the latter may be preferred. (Letter from U.S. Bureau of Standards dated January 5, 1918.)

The use of the formula given above presupposes that the mean temperature of the emergent column has been determined. This temperature may be approximately obtained in one of three ways. (I) By a "fadenthermometer" (Buckingham, Bulletin, Bureau of Standards, 8, 239, 1911, Scientific Paper 170); (2) by exploring the temperature distribution along the stem and calculating the mean temperature; (3) by suspending along the side of, or attaching to the stem, a single thermometer. If properly placed this

thermometer will indicate the temperature of the emergent mercurial column to an accuracy sufficient for many purposes. Under conditions ordinarily met with in practice it is desirable to place the bulb of the auxiliary thermometer at some point below the middle of the emergent column.

It is to be noted that the correction sought is directly proportional to the value of α , and that this may vary for glass stems of different composition from 0.00015 to 0.000165 for Centigrade temperatures. For thermometers ordinarily used in meteorological work, however, 0.000155 appears to be a good average value for Centigrade temperatures (0.000086 for Fahrenheit temperatures), and the correction formulæ, therefore, are,

T = t - 0.000086 n (t' - t) Fahrenheit temperatures. T = t - 0.000155 n (t' - t) Centigrade temperatures.

In the above, T =Corrected temperature.

t =Observed temperature.

t' = Mean temperature of the glass stem and emergent mercury column.

n =Length of mercury in the emergent stem in scale degrees.

When t' is $\begin{cases} \text{higher} \\ \text{lower} \end{cases}$ than t the numerical correction is to be $\begin{cases} \text{subtracted.} \\ \text{added.} \end{cases}$

Table 7 gives corrections computed to 0°01 for Fahrenheit thermometers from the equation C = -0.000086 n (t'-t). The side argument, n, is given for 10° intervals from 10° to 130°; the top argument, t'-t, for 10° intervals from 10° to 100°.

TABLE 8 gives corrections computed to 0.01 for Centigrade thermometers from the equation C = -0.000155 n (t' - t). The side argument, n, is given for 10° intervals from 10° to 100°; the top argument, t' - t, for 10° intervals from 10° to 80°.

Example:

The observed temperature of a black-bulb thermometer is 120.4 F., the temperature of the glass stem is 55.2 F., and the length of mercury in the emergent stem is 130° F. To find the corrected temperature. With $n = 130^{\circ}$ F. and $t' - t = -65^{\circ}$ F., as arguments, Table 7 gives the correction 0.7 F., which by the above rule is to be added to the observed temperature. The corrected temperature is therefore 121.1 F.

CONVERSIONS INVOLVING LINEAR MEASURES.

The fundamental unit of length is the meter, the length of which is equal to the distance between the defining lines on the international prototype meter at the International Bureau of Weights and Measures (near Paris) when this standard is at the temperature of melting ice $(0^{\circ} C)$. The relation

here adopted between the meter and the yard, the English measure of length, is I meter = 39.3700 inches, as legalized by Act of U.S. Congress, July 28, 1866. This U.S. Standard of length must be distinguished from the British Imperial yard, comparisons of which with the international prototype meter give the relation I meter = 39.370113 inches. (See Smithsonian Physical Tables, 1916, p. 7, Table 3.)

TABLE 9. Inches into millimeters.

TABLE 9.

1 inch = 25.40005 millimeters.

The argument is given for every hundredth of an inch up to 32.00 inches, and the tabular values are given to hundredths of a millimeter. A table of proportional parts for thousandths of an inch is added on each page.

Example:

To convert 24.362 inches to millimeters.

The table gives (p. 20).

$$(24.36 + .002)$$
 inches = $(618.75 + 0.05)$ mm. = 618.80 mm.

TABLE 10. Millimeters into inches.

TABLE 10.

From 0 to 400 mm. the argument is given to every millimeter, with subsidiary interpolation tables for tenths and hundredths of a millimeter. The tabular values are given to four decimals. From 400 to 1000 mm., covering the numerical values which are of frequent use in meteorology for the conversion of barometric readings from the metric to the English barometer, the argument is given for every tenth of a millimeter, and the tabular values to three decimals.

Example:

To convert 143.34 mm. to inches.

The table gives

(143 + .3 + .04) mm. = (5.6299 + 0.0118 + 0.0016) inches = 5.6433 inches.

Tables 11, 12. Conversion of barometric readings into standard units of pressure.

The equation for the pressure in millibars, P_{mb} , corresponding to the barometric height, B_{n} , is

$$P_{mb} = B \; \frac{\Delta \; g}{1000}$$

where Δ is the density of mercury and g is the standard value of gravity.

¹ The value of the bar as here defined is a pressure of 1,000,000 dynes per square centimeter, and is that employed by meteorological services, and recommended by inter-

In order that pressures thus derived shall be expressed in C.G.S. units it is evident that the recognized standard values of the constants of the equation must be employed. It therefore becomes necessary to abandon the values for the density of mercury and for standard gravity heretofore employed, which had the sanction of the International Meteorological Committee, in favor of the more recently determined values that have been adopted by the International Bureau of Weights and Measures.

The value adopted for Δ is 13.5951 grams per cubic centimeter; ¹ and for g, 980.665 dynes.²

By the use of these constants in the above equation we obtain

$$P_{mb} = 1.333224 \ B$$
 (millimeters), and $P_{mb} = \frac{1.333224}{0.03937} \ B = 33.86395 \ B$ (inches)

where B is the height of the barometer in the units indicated, after reduction to standard temperature and the standard value of gravity.

TABLE 11. Barometric inches to millibars.

The argument is for 0.01 inch. From 0.00 to 2.49 inches the tabulated values are given to the nearest hundredth of a millibar, so that by removing the decimal one place to the right the value in millibars of every tenth inch from 0.0 to 24.9 inches may be obtained to the nearest tenth of a millibar. From 25.00 to 31.99 inches the tabular values are given to the nearest tenth of a millibar.

The first part of the table may be used as a table of proportional parts for interpolation.

Example:

To convert 23.86 barometric inches into millibars of pressure.

TABLE 12. Barometric millimeters to millibars.

The argument is for each millimeter from 1 to 799, and the tabular values are given to the nearest tenth of a millibar.

This table may also be used to convert millibars into millimeters of mercury.

national meteorological and aerological conferences. It is 1,000,000 times greater than that given in the Smithsonian Physical Tables, 6th ed., 1914, p. 346. The smaller value is generally employed by physicists and chemists. See Marvin, Charles F. Nomenclature of the Unit of Absolute Pressure. Monthly Weather Review, 1918, 46:73-75.

¹ Chappuis, Recueil de Constantes Physiques, Soc. Fr. Phys., 1913, p. 139. Leduc, Trav. et Mém., Bur. Int. Poids et Mes., xvi, p. 36, 1917.

² Comptes Rendus des Séances, Troisième Conférence Générale, p. 68. Trav. et Mém., Bur. Int. Poids et Mes., XII, 1902.

Example:

To convert 1003.5 millibars into millimeters of mercury. 1003.5 mb. = (1002.6 + 0.9) mb. = (752 + 0.68) mm. = 752.68 mm.

TABLE 13. Feet into meters.

TABLE 13.

From the adopted value of the meter, 39.3700 inches—
I English foot = 0.3048006 meter.

Table 13 gives the value in meters and thousandths (or millimeters) for every foot from 0 to 99 feet; the value to hundredths of a meter (or centimeters) of every 10 feet from 100 to 4090 feet; and the value to tenths of a meter of every 10 feet from 4000 to 9090 feet. In using the latter part, the first line of the table serves to interpolate for single feet.

Example:

To convert 47 feet 7 inches to meters. 47 feet 7 inches = 47.583 feet. The table gives 47 feet = 14.326 meters. By moving the decimal point 0.583 " = 0.178 " 47.583 feet = 14.504 meters.

TABLE 14. Meters into feet.

TABLE 14.

I meter = 39.3700 inches = 3.280833 + feet.

From 0 to 509 meters the argument is given for every unit, and the tabular values to two decimals; from 500 to 5090 the argument is given to every 10 meters, and the tabular values to one decimal. The conversion for tenths of a meter is added for convenience of interpolation.

Example:

Convert 4327 meters to feet.

The table gives

(4320 + 7) meters = (14173.2 + 23.0) feet = 14196.2 feet.

TABLE 15. Miles`into kilometers.

TABLE 15.

1 mile = 1.609347 kilometers.

The table extends from 0 to 1009 miles with argument to single miles, and from 1000 to 20000 miles for every 1000 miles. The tabular quantities are given to the nearest kilometer.

TABLE 16. Kilometers into miles.

TABLE 16.

1 kilometer = 0.621370 mile.

The table extends to 1009 kilometers with argument to single kilometers, and from 1000 to 20000 kilometers for every 1000 kilometers. Tabular values are given to tenths of a mile.

Example:

Convert 3957 kilometers into miles.

The table gives

(3000 + 957) kilometers = (1864.1 + 594.7) miles = 2458.8 miles.

TABLE 17. Interconversion of nautical and statute miles.

The nautical mile as defined by the U.S. Coast and Geodetic Survey (Tables for a polyconic projection of maps. U.S. Coast and Geodetic Survey, Special Publication No. 5, page 4) is "A minute of arc of a great circle of a sphere whose surface equals that of the Clarke representative spheroid of 1866," and the value given is 1853.25 meters, or 6080.20 feet.

TABLE 18. Continental measures of length with their metric and English equivalents.

This table gives a miscellaneous list of continental measures of length, alphabetically arranged, with the name of the country to which they belong and their metric and English equivalents.

CONVERSION OF MEASURES OF TIME AND ANGLE.

TABLE 19. Arc into time.

$$1^{\circ} = 4^{m}$$
; $1' = 4^{s}$; $1'' = \frac{1}{15}^{s} = 0.067$.

Example:

Change 124° 15′ 24"7 into time.

From the table,

$$124^{\circ} = 8^{h} \quad 16^{m} \quad 0^{s} \\
15' = I \quad 0 \\
24'' = I.600 \\
0''7 = .047 \\
8^{h} \quad 17^{m} \quad 1^{s}647$$

TABLE 20. Time into arc.

$$I^{h} = I5^{\circ}; I^{m} = I5'; I^{s} = I5''.$$

Example:

Change 8h 17m 1s647 into arc.

From the table,

From the table,
$$8^{h} = 120^{\circ}$$
 $17^{m} = 4 15'$
 $15''$
 $15'' = 0.64 = 9.60$
By moving the decimal point, $0.007 = 0.10$

TABLE 21. Days into decimals of a year and angle.

The table gives for the beginning of each day the corresponding decimal of the year to five places. Thus, at the epoch represented by the beginning of the 15th day, the decimal of the year that has elapsed since January 1.0 is computed from the fraction $\frac{14}{365.25}$. The corresponding value in angle obtained by multiplying this fraction by 360°, is given to the nearest minute. Two additional columns serve to enter the table with the day of the month either of the common or the bissextile year as the argument, and may be used also for converting the day of the month to the day of the year, and vice versa.

Example:

To find the number of days and the decimal of a year between February 12 and August 27 in a bissextile year.

Aug. 27: Day of year = 240; decimal of a year =
$$0.65435$$

Feb. 12: " " = 0.11499
Interval in days = 0.73936

The decimal of the year corresponding to the interval 197 days may also be taken from the table by entering with the argument 198.

Table 22. Hours, minutes and seconds into decimals of a day. Table 22.

The tabular values are given to six decimals.

Example:

Convert 5^h 24^m 23^s4 to the decimal of a day:

$$5^{h} = o^{d}_{.}208333$$

$$24^{m} = o_{.}16667$$

$$23^{s} = 266$$
By interpolation, or by moving the decimal for 4^{s}

$$0.4 = \frac{5}{o^{d}_{.}225271}$$

Table 23. Decimals of a day into hours, minutes and seconds.

TABLE 23.

Example:

Convert 0.225271 to hours, minutes and seconds:

TABLE 24. Minutes and seconds into decimals of an hour.

TABLE 24

The tabular values are given to six decimals.

Example:

Convert 34^m 28^s.7 to decimals of an hour.

$$34^{\text{m}} = 0.566667$$

 $28^{\text{s}} = 7778$
 $0.57 = 194$
 0.574639

TABLE 25. Local mean time at apparent noon.

This table gives the local mean time 1 that should be shown by a clock when the center of the sun crosses the meridian, on the 1st, 8th, 16th, and 24th days of each month. The table is useful in correcting a clock by means of a sundial or noon mark.

Example:

To find the correct local mean time when the sun crosses the meridian on December 15, 1891.

The table gives for December 16, 11^h 56^m. By interpolating, it is seen that the change to December 15 would be only one-half minute; the correct clock time is therefore 4 minutes before 12 o'clock noon.

TABLE 26. Sidereal time into mean solar time.

TABLE 27. Mean solar time into sidereal time.

According to Newcomb, the length of the tropical year is 365.24220 mean solar days,² whence

365.24220 solar days = 366.24220 sidereal days.

Any interval of mean time may therefore be changed into sidereal time

by increasing it by its $\frac{I}{365.24220}$ part, and any interval of sidereal time may

be changed into mean time by diminishing it by its $\frac{I}{366.24220}$ part.

Table 26 gives the quantities to be subtracted from the hours, minutes and seconds of a sidereal interval to obtain the corresponding mean time interval, and Table 27 gives the quantities to be added to the hours, minutes and seconds of a mean time interval to obtain the corresponding sidereal interval. The correction for seconds is sensibly the same for either a sidereal or a mean time interval and is therefore given but once, thus forming a part of each table.

Examples:

Change 14^h 25^m 36^s2 sidereal time into mean solar time.

Given sidereal time
$$14^{h}$$
 25^{m} $36^{s}.2$ Correction for 14^{h} $= -2^{m}$ $17^{s}.61$ $= -4.10$ $36^{s}.2$ $= -10$ -2 21.81 -2 21.8 Corresponding mean time $= 14^{h}$ 25^{m} $36^{s}.2$

¹ Derived from the equation of time for Washington apparent noon for the year 1899. See the American Ephemeris and Nautical Almanac, 1899, pages 377-84.

² The length of the tropical year is not absolutely constant. The value here given is for the year 1900. Its decrease in 100 years is about 0.5s. (See the American Ephemeris and Nautical Almanac 1918, page xvi.)

2. Change 13^h 37^m 22^s.7 mean solar time into sidereal time.

Given mean time =
$$13^{h}$$
 37^{m} $22^{s}.7$
Correction for 13^{h} = $+2^{m}$ $8^{s}.13$
 37^{m} = $+6.08$
 $22^{s}.7$ = $+0.06$
 $+2$ 14.27 $+2$ 14.3
Corresponding sidereal time = 13^{h} 37^{m} $22^{s}.7$

CONVERSION OF MEASURES OF WEIGHT.

TABLE 28.

TABLE 28. Conversion of avoirdupois pounds and ounces into kilograms.

The comparisons of July, 1893, made by the International Bureau of Weights and Measures between the Imperial standard pound and the "kilogram prototype" resulted in the relation:

I pound avoirdupois = 453.592 427 7 grams.

For the conversion of pounds, Table 28 gives the argument for every tenth of a pound up to 9.9, and the tabular conversion values to ten-thousandths of a kilogram.

For the conversion of ounces, the argument is given for every tenth of an ounce up to 15.9, and the tabular values to ten-thousandths of a kilogram.

TABLE 29

TABLE 29. Conversion of kilograms into avoirdupois pounds and ounces.

From the above relation between the pound and the kilogram,

I kilogram = 2.204622 avoirdupois pounds. = 35.274 avoirdupois ounces.

The table gives the value to thousandths of a pound of every tenth of a kilogram up to 9.9; the values of tenths of a kilogram in ounces to four decimals; and the values of hundredths of a kilogram in pounds and ounces to three and two decimals respectively.

TABLE 30. Conversion of grains into grams.

TABLES 30, 31.

TABLE 31. Conversion of grams into grains.

From the above relation between the pound and the kilogram,

I gram = 15.432356 grains. I grain = 0.06479892 gram.

TABLE 30 gives to ten-thousandths of a gram the value of every grain from I to 99, and also the conversion of tenths and hundredths of a grain for convenience in interpolating.

TABLE 31 gives to hundredths of a grain the value of every tenth of a gram from 0.1 to 9.9, and the value of every gram from 1 to 99. The values of hundredths and thousandths of a gram are added as an aid to interpolation.

WIND TABLES.

CONVERSION OF VELOCITIES.

TABLE 32. Synoptic conversion of velocities.

This table,¹ contained on a single page, converts miles per hour into meters per second, feet per second and kilometers per hour. The argument, miles per hour, is given for every half unit from 0 to 78. Tabular values are given to one decimal. For the rapid interconversion of velocities, when extreme precision is not required, this table has proved of marked convenience and utility.

TABLE 33. Conversion of miles per hour into feet per second.

The argument is given for every unit up to 149 and the tabular values are given to one decimal.

TABLE 34. Conversion of feet per second into miles per hour.

The argument is given for every unit up to 199 and the tabular values are given to one decimal.

TABLE 35. Conversion of meters per second into miles per hour.

The argument is given for every tenth of a meter per second up to 60 meters per second, and the tabular values are given to one decimal.

TABLE 36. Conversion of miles per hour into meters per second.

The argument is given for every unit up to 149, and the tabular values are given to two decimals.

TABLE 37. Conversion of meters per second into kilometers per hour.

The argument is given for every tenth of a meter per second up to 60 meters per second, and the tabular values are given to one decimal.

TABLE 38. Conversion of kilometers per hour into meters per second.

The argument is given for every unit up to 200, and the tabular values are given to two decimals.

TABLE 39. Scale of Velocity equivalents of the so-called Beaufort scale of wind.

The personal observation of the estimated force of the wind on an arbitrary scale is a method that belongs to the simplest meteorological

¹ From Hand-Book of Meteorological Tables. By H. A. Hazen. Washington, 1888.

records and is widely practiced. Although anemometers are used at meteorological observatories, the majority of observers are still dependent upon estimates based largely upon their own judgment, and so reliable can such estimates be made that for many purposes they abundantly answer the needs of meteorology as well as of climatology.

A great variety of such arbitrary scales have been adopted by different observers, but the one that has come into the most general use and received the greatest definiteness of application is the duodecimal scale introduced into the British navy by Admiral Beaufort about 1800.

Table 39 is taken from the Observer's Handbook of the Meteorological Office, London, edition of 1917. The velocity equivalents in meters per second and miles per hour are based on extensive observational data collected by Dr. G. C. Simpson and first published by the Meteorological Office in 1906. Several other sets of equivalents have been published in different countries. For a history of this subject see Rept. 10th Meeting International Meteorological Committee, Rome, 1913, Appendix VII. (London, 1914.)

In the Quarterly Journal of the Royal Meteorological Society, volume xxx, No. 132, October, 1904, Prof. A. Lawrence Rotch has described an instrument for obtaining the true direction and velocity of the wind at sea aboard a moving vessel. If a line A B represents the wind due to the motion of a steamer in an opposite direction, and A C the direction of the wind relative to the vessel as shown by the drift of its smoke, then, by measuring the angle D B A that the true wind makes with the vessel — which is easily done by watching the wave crests as they approach it — we obtain the third side, B C, of the triangle. This represents, in direction and also in length, on the scale used in setting off the speed of the ship, the true direction of the wind relative to the vessel and also its true velocity. The method fails when the wind direction coincides with the ship's course and becomes inaccurate when the angle between them is small.

CALCULATION OF THE MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.

Lambert's formula for the eight principal points of the compass is

$$\tan \alpha = \frac{E - W + (NE + SE - NW - SW)\cos 45^{\circ}}{N - S + (NE + NW - SE - SW)\cos 45^{\circ}}.$$

a is the angle of the resultant wind direction with the meridian. E, NE, N, etc., represent the wind movement from the corresponding directions East, Northeast, North, etc. In practice, instead of taking the total wind movement, it is often considered sufficient to take as proportional thereto the number of times the wind has blown from each direction, which is equivalent to considering the wind to have the same mean velocity for all directions.

If directions are observed to sixteen points, half the number belonging to each extra point should be added to the two octant points between which it lies; for example, NNE=6 should be separated into N=3 and NE=3; ESE=4, into E=2 and SE=2. The result will be approximately identical with that obtained by using the complete formula for sixteen points.

Table 40. Multiples of cos 45°; form for computing the numerator and denominator.

TABLE 41. Values of the mean direction (a) or its complement $(90^{\circ} - a)$.

Table 40 gives products of $\cos 45^{\circ}$ by numbers up to 209, together with a form for the computation of the numerator and denominator, illustrated by an example. The quadrant in which α lies is determined by the following rule:

When the numerator and denominator are positive, α lies between N and E.

When the numerator is positive and the denominator negative, α lies between S and E.

When the numerator and denominator are negative, α lies between S and W.

When the numerator is negative and the denominator positive, α lies between N and W.

Table 41^1 combines the use of a division table and a table of natural tangents. It enables the computer, with the numerator and denominator of Lambert's formula (computed from Table 40) as arguments, to take out directly the mean wind direction α or its complement.

The top argument consists of every fifth number from 10 to 200.

The side argument is given for every unit from 1 to 50 and for every two units from 50 to 150. Tabular values are given to the nearest whole degree.

Rule for using the table:

Enter the table with the larger number (either numerator or denominator) as the top argument.

If the denominator be larger than the numerator, the table gives a.

If the denominator be smaller than the numerator, the table gives $90^{\circ} - \alpha$.

a is measured from the meridian in the quadrant determined by the rule given with Table 40.

¹ From Hand-book of Meteorological Tables. By H. A. Hazen. Washington, 1888. A corrected copy of the table was kindly furnished by the author.

Example:

$$\tan \alpha = \frac{-43}{-27}.$$
Table 41 gives
$$90^{\circ} - \alpha = 32^{\circ}$$

$$\alpha = S 58^{\circ} W.$$

Note. — If the numerator and denominator both exceed 150 or if either exceeds 200, the fraction must be divided by some number which will bring them within the limits of the table. The larger the values, provided they are within these limits, the easier and more accurate will be the computation. For example, let $\tan \alpha = \frac{-18}{14}$. The top argument is not given for 18, but if we multiply by 5 or 10 and obtain $\frac{-90}{70}$ or $\frac{-180}{140}$, the table gives, without interpolation, $90^{\circ} - \alpha = 38^{\circ}$ and $\alpha = N 52^{\circ} W$.

GRADIENT WINDS.

When the motions of the atmosphere attain a state of complete equilibrium of flow under definite systems of pressure gradients, the winds blow across the isobars at small angles of inclination depending upon the retarding effects of friction. At the surface of the earth friction is considerable and the angle across the isobars is often great. In the free air, however, the friction is small, and for some purposes may be disregarded entirely. Under an assumption of complete equilibrium of motion and frictionless flow the winds will blow exactly parallel to the isobars, — that is, perpendicular to the gradient which produces and sustains the motion. Such winds are called gradient winds. The anomalous condition of flow of terrestrial winds perpendicular to the moving force is the result of the modifications of atmospheric motions due to the deflective influence of the earth's rotation, and to that other influence due to the inertia reaction of matter when it is constrained to move in a curved path, and commonly called centrifugal force. The equations for gradient wind motions have long been known to meteorologists from the work of Ferrel and others, and may be written in the following form:

For Cyclones

$$V = r \left[\sqrt{\omega^2 \sin^2 \phi + \frac{\Delta P}{\rho r}} - \omega \sin \phi \right]$$
 (1)

For Anticyclones

$$V = r \left[\omega \sin \phi - \sqrt{\omega^2 \sin^2 \phi - \frac{\Delta P}{\rho r}} \right]$$
 (2)

In C. G. S. Units, V = velocity of the gradient wind in centimeters per second; r = radius of curvature of isobars in centimeters; $\Delta P =$ pressure gradient in dynes per square centimeter per centimeter; $\rho =$ density of air in grams per cubic centimeter; $\omega =$ angular velocity of the earth's rotation

per second = $\frac{2\pi}{86164}$, and ϕ = latitude. In the Northern Hemisphere the winds gyrate counterclockwise in cyclones and clockwise in anticyclones. These gyrations are in the reversed direction each to each in the Southern Hemisphere.

In equation (2) the values of V are imaginary for values of $\frac{\Delta P}{\rho r}$ greater than $\omega^2 \sin^2 \phi$. The equality $\frac{\Delta P}{\rho r} = \omega^2 \sin^2 \phi$, or $r = \frac{\Delta P}{\rho \omega^2 \sin^2 \phi}$ defines and fixes an isobar with minimum curvature in anticyclones. Winds cannot flow parallel to the isobars within this critical isobar. For this isobar the gradient wind has its maximum value $V_c = \frac{\Delta P}{\rho \omega \sin \phi}$. For the same gradient and for an isobar with the same curvature in a cyclone the gradient velocity is $V_l = V_c (\sqrt{2} - 1) = 0.414 \ V_c$.

When the isobars are parallel straight lines, a condition very often closely realized in nature, $r = \infty$ and the gradient winds have the value given by either (1) or (2) after squaring, namely,

$$V_{r=\infty} = V_s = \frac{\Delta P}{2 \rho \omega \sin \phi} = \frac{I}{2} V_c.$$

For practical units equation (1) becomes

Units of pressure.

$$V = R \begin{bmatrix} \sqrt{.0053173 \sin^2 \phi + \frac{1}{10 \ K \rho d}} - .07292 \sin \phi \end{bmatrix}$$
 (I) (Millibars)
$$\sqrt{.0053173 \sin^2 \phi + \frac{.13333}{R \rho d}} - .07292 \sin \phi \end{bmatrix}$$
 (II) (Millimeters)
$$\sqrt{.068914 \sin^2 \phi + \frac{1.6946}{R \rho d}} - .26252 \sin \phi \end{bmatrix}$$
 (III) (Inches)

V = velocities in meters per second in (I) and (II) and in miles per hour in (III).

 $R = \text{radius of curvature of isobar (wind path) in kilometers in (I) and (II) and in miles in (III).$

The gradient is to be deduced from isobars drawn for pressure intervals of I millibar in (I), I millimeter in (II) and $\frac{I}{IO}$ inch in (III); d, is the perpendicular distance between isobars (as above defined) in kilometers in (I) and (II), and in miles in (III). $\rho = \text{density of air} = \text{grams per cubic centimeter}$ in all cases.

Units of

Also pressure. $V_c = \begin{bmatrix} \frac{1.3713}{\rho d \sin \phi} \text{ (IV)} \\ \frac{1.8284}{\rho d \sin \phi} \text{ (V)} & \text{and } R_c = \begin{bmatrix} \frac{18.806}{\rho d \sin^2 \phi} \text{ (VII) (Millibars)} \\ \frac{25.073}{\rho d \sin^2 \phi} \text{ (VIII) (Millimeters)} \\ \frac{24.590}{\rho d \sin^2 \phi} \text{ (IX) (Inches)} \end{bmatrix}$

Radius of critical curvature and velocities of gradient winds for frictionless motion in Highs and Lows.

TABLE 42. English Measures.

TABLES 42, 43.

TABLE 43. Metric Measures.

These tables give the radius of curvature of the critical isobar in anticyclones, computed from the equation

$$R_c = \frac{\Delta P}{\rho \omega^2 \sin^2 \phi};$$

the velocity of the wind on this isobar, computed from the equation

$$V_c = \frac{\Delta P}{\rho \omega \sin \phi};$$

the velocity of the wind on a straight isobar, computed from the equation

$$V_s = \frac{\Delta P}{2 \rho \omega \sin \phi} = \frac{I}{2} V_c$$
; and

the velocity of the wind in a cyclone having the same gradient as the anticyclone, and on an isobar having a radius of curvature equal to R_c , computed from the equation

$$V_1 = V_c (\sqrt{2} - 1) = 0.414 V_c$$

Table 42, English measures, gives values of R_c , in miles, and of V_c High, V_s , and V Low, in miles per hour. The side argument is the latitude for 10°, and at 5° intervals from 20° to 90°, inclusive. The top argument, d, is the perpendicular distance in miles between isobars drawn for pressure intervals of $\frac{1}{10}$ inch. For values of d one tenth as great as given in the

heading of the table the values of R_c , V_c High, V_s , and V Low are increased tenfold.

Table 43, metric measures, gives values of R_c in kilometers, and of V_c High, V_s , and V Low, in meters per second. The side argument is the same as in Table 42. The top argument, d, is the perpendicular distance in kilometers between isobars drawn for pressure intervals of 1 millimeter. For values of d one tenth as great as given in the heading of the table the values of R_c , V_c High, V_s , and V Low are increased tenfold.

REDUCTION OF TEMPERATURE TO SEA LEVEL.

TABLE 44. English Measures.

TABLE 45. Metric Measures.

These tables give for different altitudes and for different uniform rates of decrease of temperature with altitude, the amount in hundredths of a degree Fahrenheit and Centigrade, which must be added to observed temperatures in order to reduce them to sea level.

The rate of decrease of temperature with altitude varies from one region to another, and in the same region varies according to the season and the meteorological conditions; being in general greater in warm latitudes than in cold ones, greater in summer than in winter, and greater in areas of falling pressure than in areas of rising pressure. For continental plateau regions, the reduction often becomes fictitious or illusory. The use of the tables therefore requires experience and judgment in selecting the rate of decrease of temperature to be used. Much experimental work is now in progress with kites and balloons to determine average vertical gradients. It must be remembered that the tables here given are not tables giving the data as recently determined for various elevations.

The tables are given in order to facilitate the reduction of temperature either upward or downward in special investigations, but the reduction is not ordinarily applied to meteorological observations.

The tables, 44 and 45, are computed for rates of temperature change ranging from 1° Fahrenheit in 200 feet to 1° Fahrenheit in 900 feet, and from 1° Centigrade in 100 meters to 1° Centigrade in 500 meters; and for altitudes up to 5000 feet and 3000 meters respectively.

Example, Table 44.

Observed temperature at an elevation of 2,500 feet,	52°5 F.
Reduction to sea level for an assumed decrease in tem-	
perature of I° F. for every 300 feet,	+ 8°.3
Temperature reduced to sea level,	60°.8 F.
Example, Table 45.	
Observed temperature at an elevation of 500 meters,	12°5 C.
Reduction to sea level for an assumed decrease in tempera-	
ture of 1° C. for every 200 meters,	+ 2°5
Temperature reduced to sea level,	15°0 C.

BAROMETRICAL TABLES.

REDUCTION TO A STANDARD TEMPERATURE OF OBSERVATIONS MADE WITH MERCURIAL BAROMETERS HAVING BRASS SCALES.

The indicated height of the mercurial column in a barometer varies not only with changes of atmospheric pressure, but also with variations of the temperature of the mercury and of the scale. It is evident therefore that if the height of the barometric column is to be a true relative measure of atmospheric pressure, the observed readings must be reduced to the values they would have if the mercury and scale were maintained at a constant standard temperature. This reduction is known as the reduction for temperature, and combines both the correction for the expansion of the mercury and that for the expansion of the scale, on the assumption that the attached thermometer gives the temperature both of the mercury and of the scale.

The freezing point is universally adopted as the standard temperature of the mercury, to which all readings are to be reduced. The temperature to which the scale is reduced is the normal or standard temperature of the adopted standard of length. For English scales, which depend upon the English yard, this is 62° Fahrenheit. For metric scales, which depend upon the meter, it is 0° Centigrade. As thus reduced, observations made with English and metric barometers become perfectly comparable when converted by the ordinary tables of linear conversion, viz: inches to millimeters and millimeters to inches (see Tables 9, 10), for these conversions refer to the meter at 0° Centigrade and the English yard at 62° Fahrenheit.

Prof. C. F. Marvin in the Monthly Weather Review for July, 1898, has pointed out the necessity of caution in conversion of metric and English barometer readings:

Example:

Attached thermometer, 25.4 C. Barometer reading, 762.15 mm.

If the temperature is converted to Fahrenheit = 77.7 and the reading to 30.006 in., the temperature correction according to table 47 would be -0.133 inch and the reduced reading 29.873. This would be erroneous. The correct conversion is found by taking the correction corresponding to 25.4 C. and 762 mm., i.e., -3.15 mm., which gives a corrected reading of 759 mm., and converted into inches gives 29.882 which is the correct result.

Professor Marvin further remarks that circumstances sometimes arise in which a Centigrade thermometer may be used to determine the temperature of an English barometer, or a Fahrenheit attached thermometer may be used with a metric scale. In all such cases the temperature must be brought into the same system of units as the observed scale reading before corrections can be applied, and the observed reading must then be corrected for temperature before any conversion can be made.

With aneroid barometers corrections for temperature and instrumental error must be determined for each instrument.

The general formula for reducing mercurial barometers with brass scales to the standard temperature is

$$C = -B \frac{m (t-T) - l (t-\theta)}{1 + m (t-T)},$$

in which C =Correction for temperature.

B =Observed height of the barometric column.

t = Temperature of the attached thermometer.

T =Standard temperature of the mercury.

m =Coefficient of expansion of mercury.

l = Coefficient of linear expansion of brass.

 θ = Standard temperature of the scale.

The accepted determination of the coefficient of expansion of mercury is that given by Broch's reduction of Regnault's experiments, viz:

$$m \text{ (for } 1^{\circ} C.) = 10^{-9} (181792 + 0.175t + 0.035116t^2).$$

As a sufficiently accurate approximation, the intermediate value

$$m = 0.0001818$$

has been adopted uniformly for all temperatures in conformity with the usage of the *International Meteorological Tables*.

Various specimens of brass scales made of alloys of different composition show differences in their coefficients of expansion amounting to eight and sometimes ten per cent. of the total amount. The *Smithsonian Tables* prepared by Prof. Guyot were computed with the average value l (for I° C.) = 0.0000188; for the sake of uniformity with the *International Meteorological Tables*, the value

$$l = 0.0000184$$

has been used in the present volume. For any individual scale, either value may easily be in error by four per cent.

A small portion of the tables has been independently computed, but the larger part of the values have been copied from the *International Meteorological Tables*, one inaccuracy having been found and corrected.

TABLE 46. Reduction of the barometer to standard temperature — English measures.

For the English barometer the formula for reducing observed readings to a standard temperature becomes

$$C = -B \frac{m (t - 32^{\circ}) - l (t - 62^{\circ})}{1 + m (t - 32^{\circ})}$$

in which B =Observed height of the barometer in English inches.

t = Temperature of attached thermometer in degrees Fahrenheit.

$$m = 0.0001818 \times \frac{5}{9} = 0.000101$$

$$l = 0.0000184 \times \frac{5}{9} = 0.0000102$$

TABLE 47.

The combined reduction of the mercury to the freezing point and of the scale to 62° Fahrenheit brings the point of no correction to approximately 28.5 Fahrenheit. For temperatures above 28.5 Fahrenheit, the correction is subtractive, and for temperatures below 28.5 Fahrenheit, the correction is additive, as indicated by the signs (+) and (-) inserted throughout the table.

The table gives the corrections for every half degree Fahrenheit from 0° to 100°. The limits of pressure are 19 and 31.6 inches, the corrections being computed for every half inch from 19 to 24 inches, and for every two-tenths of an inch from 24 to 31.6 inches.

Example:

Observed height of barometer = 29.143

Attached thermometer, 54.5 F.

Reduction for temperature = -0.068Barometric reading corrected for temperature = 29.075

Table 47. Reduction of the barometer to standard temperature — Metric measures.

For the metric barometer the formula for reducing observed readings to the standard temperature, o° C., becomes

$$C = -B \frac{(m-l)t}{1+mt}$$

in which C and B are expressed in millimeters and t in Centigrade degrees. m = 0.0001818; l = 0.0000184.

In the table, the limits adopted for the pressure are 440 and 795 millimeters, the intervals being 10 millimeters between 440 and 600 millimeters, and 5 millimeters between 600 and 795 millimeters.

The limits adopted for the temperature are o° and + 35.8, the intervals being 0.5 and 1.0 from 440 to 560 millimeters, and 0.2 from 560 to 795 millimeters.

For temperatures above o° Centigrade the correction is negative, and hence is to be subtracted from the observed readings.

For temperatures below o° Centigrade the correction is *positive*, and from o° C. down to -20° C. the numerical values thereof, for ordinary barometric work, do not materially differ from the values for the corresponding temperatures above o° C. Thus the correction for -9° C is numerically the same as for $+9^{\circ}$ C and is taken from the table. In physical work of extreme precision, the numerical values given for positive temperatures may be used for temperatures below o° C by applying to them the following corrections:

Corrections to be applied to the tabular values of Table 47 in order to use them when the temperature of the attached thermometer is below 0° Centigrade.

Temper-	PRESSURE IN MILLIMETERS.									
ature.	450	500	550	600	650	700	750	800		
C.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.		
— г°	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
- 9	.00	.00	.00	.00	.00	.00	.00	.00		
-10	0.00	0.00	0.00	0.00	0.00	+0.01	+0.01	+0.01		
11	.00	.00	.00	.00	+0.01	.01	.01	.01		
12	.00	.00	.00	+0.01	.01	.01	.01	.01		
13	.00	.00	+0.01	.01	.01	.01	.01	.01		
-14	.00	+0.01	.01	.01	.01	.01	.01	.01		
-15	+001	+001	+0.01	+0.01	+0.01	+0.01	+0.01	+0.01		
16	.01	.01	.01	.01	.01	.01	.01	10,		
17	.01	.01	.01	.01	.01	.oI	.or	.02		
18	.01	.01	.01	.01	.01	.01	.01	.02		
-19	.01	.01	.01	.01	.01	.01	.02	.02		
-20	+0.01	+0.01	+0.01	+0.01	+0.01	+0.02	+0.02	+ 0.02		
21	.01	.01	.01	.02	.02	.02	.02	.02		
22	.oI	.01	.02	.02	.02	.02	.02	.02		
23	.01	.02	.02	.02	.02	.02	.02	.02		
-24	.01	.02	.02	.02	.02	.02	.02	.03		

Example:

Observed height of barometer, 763.17^{mm}: Temperature of the attached thermometer, -12° C.

Numerical value of the reduction for $+ 12^{\circ} C$.	=	1.50
Correction for temperature below o° C.	= +	10.0
Reduction for -12° C.	= +	1.51
Observed height of barometer	=	763.17
Barometer corrected for temperature	. =	764.68

REDUCTION OF THE MERCURIAL BAROMETER TO STANDARD GRAVITY.

TABLES 48, 49, 50.

The mercurial barometer does not directly measure the atmospheric pressure. The latter is proportional to the weight of the mercurial column, and also to its height after certain corrections have been applied. Since the height of the barometric column is easily measured, by common consent the pressures are expressed in terms of this corrected height.

The observed height of the barometer changes with the temperature of the mercury as already shown, and also with the variations in the value of gravity, as well as with the pressure. Therefore, to obtain a height that shall be a true relative measure of the atmospheric pressure, the observed height of the mercurial column must not only be reduced to what its height would be if at a standard temperature, but also to what it would be at a standard value of gravity.

As stated on page xviii, the standard value of gravity adopted is 980.665 dynes. At the time of its adoption this value was assumed to apply for "latitude 45° and sea-level" on the basis of the absolute determination of g at the International Bureau by Defforges, 1887–1890 (Procés-Verbaux, Comité Inter. d. Poids et Mesures, 1887, pp. 27–28, 86; 1891, p. 135).

More recent determinations, 1 based upon numerous measurements in all parts of the world, and assuming a certain ideal figure for the earth, give for the mean value of g at latitude 45° and sea level the value 980.621 dynes. This differs from the standard value by 0.044 dyne. Departures of this magnitude from the mean sea-level gravity of a given latitude are frequently encountered, and in some cases surpassed. They are attributed to topography and isostatic compensation, and to gravity anomalies. For example, according to Bowie,² at Pikes Peak, Colo., the correction for topography and compensation is + 0.187 dyne, while the gravity anomaly³ is +0.021 dyne, giving a total gravity departure of +0.208 dyne. Also, at Seattle, Wash., from the mean of measurements at two stations, the correction for topography and compensation is - 0.19 dyne 4 and the gravity anomaly is -0.093 dyne, giving a total gravity departure of -0.112 dyne. The gravity departure at Pikes Peak is sufficient to cause the barometer to read 0.004 inch or 0.10 mm. low, while the departure at Seattle is sufficient to cause the barometer to read 0.003 inch or 0.09 mm. high, as compared with what the readings would have been with gravity at normal intensity for the latitudes of the respective stations.

From the foregoing it is evident that the value of local gravity, g_l , at the observing station must be determined before the barometer reading can be accurately reduced to standard gravity. In many cases, and especially at sea, it is not practicable to measure g_l . In the United States its value may frequently be determined with sufficient accuracy in the following manner:

(1) Compute g_{ϕ} , mean gravity at sea level for the latitude of the station, from the equation ⁶

```
g_{\phi} = 978.039 \text{ (I} + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi),}
= 980.621 (I - 0.002640 cos 2\phi + 0.000007 cos^2 2\phi)
```

(2) Correct g_{ϕ} for altitude by the equation ⁷ c (dynes) = -0.0003086 h (meters), or c (dynes) = -0.000094 h (feet),

¹ Investigations of gravity and isostasy, by William Bowie. U.S. Coast and Geodetic Survey, Special Publication No. 40, 1917, p. 134.

² Op. cit. p. 50.
³ Op. cit. p. 59.
⁴ Op. cit. p. 50.
⁵ Op. cit. p. 59.

⁶ Bowie, op. cit. p. 134. 7 Bowie, op. cit. p. 93.

where h is the altitude of the station above sea level.

- (3) Correct g_{ϕ} for gravity anomaly.¹
- (4) Finally, g_{ϕ} is to be corrected for topography and isostatic compensation.²

Example:

To determine the value of local gravity g_l , at the Weather Bureau Office, Atlanta, Ga., latitude 33° 45′ N., longitude 84° 23′ W., height of barometer above sea level, 1218 feet.

From Table 83, mean sea level gravity for lat-

itude $33^{\circ} 45'$ = 979.631 dynes.

Correction for height of barometer

 (-0.000094×1218) = - 0.114 "

Correction for gravity anomaly, = -0.023

Correction for topography and compensation =+ 0.014

Local gravity at Weather Bureau Office, Atlanta,

Ga. = 979.508 dynes.

Having determined g_l , the reduction of barometer readings to standard gravity is easily and accurately accomplished by multiplying by the ratio g_l/g , or by applying a correction to the barometer reading, otherwise corrected, derived from the expression $\frac{(g_l-g)}{g}B$. With $g_l< g$ the correction is to be subtracted; with $g_l>g$ the correction is to be added. In general, sufficient accuracy will be attained by computing the gravity correction for a station once for all from the equation $C=B_n\frac{(g_l-g)}{g}$, in which B_n is the normal station barometer pressure, and C is expressed in the same units as B_n .

TABLE 48 gives corrections to reduce barometer readings to standard gravity. The top argument is the barometer reading. The side argument is the difference, $g_l - g$, for each tenth of a dyne up to 4.0 dynes. The relation is a linear function of both $g_l - g$ and B, and for barometer readings 10 or 100 times greater than those given in the argument the correction may be obtained by removing the decimal point in the tabulated values one or two places, respectively, to the right. The correction obtained will be expressed in the same units as the barometer reading to be corrected.

¹ In most cases the gravity anomaly may be obtained from Bowie's paper, op. cit., figure 11.

² In some cases this correction may be obtained from Bowie's paper, op. cit., pp. 50-52, but in many cases, and especially in mountainous districts, it must be separately computed for each station.

Example 1.

The barometer reading corrected for temperature is 29.647 inches, and the local value of gravity is 978.08. The difference, $g_l - g_s$ = -2.585. From the table.

the correction for a barometer reading of 20 inches = -0.0527 in.the correction for a barometer reading of 9 inches = -0.0237 in.the correction for a barometer reading of 0.65 inches = -0.0017 in.Correction for a barometer reading of 29.65 inches = -0.078 in. Corrected barometer reading = 29.647 in. -0.078 in. 29.569 in. Example 2.

The barometer reading reduced to 0° C. is 637.42 mm., and the local value of gravity is 981.51. The difference, $g_t - g = + 0.845$. From the table.

the correction for a barometer reading of 600 mm. = + 0.517 mm.the correction for a barometer reading of 30 mm. = +0.026 mm.the correction for a barometer reading of = + 0.006 mm.Correction for a barometer reading of 637.4 mm. = + 0.55 mm. Corrected barometer reading = 637.42 + 0.55= +637.97 mm.

In the case of barometer readings made at sea, and also at some land stations, it is not practicable to determine local gravity with greater accuracy than it can be computed from the equations for variation with latitude and altitude given above. The reduction to standard gravity, accordingly, consists of two parts — a correction for altitude, and a correction from the computed sea-level gravity for the latitude of the station to standard gravity. The first part of the correction, or the correction for altitude, may be computed once for all from the expression $c = -0.0003086 \ h \ B_n$ (metric measures), or $c = -0.000094 h B_n$ (English measures), and is usually combined with the reduction of the barometer to sea level or to some other reference plane. The second part has heretofore consisted of a correction for the difference between the mean value of gravity for the latitude of the station and for latitude 45°; and, in accordance with the equation given above, it may be derived from the expression

$$(-0.002640 \cos 2 \phi + 0.000007 \cos^2 2 \phi) B$$

where ϕ is the latitude of the station, and B is the barometer reading. The value of the ratio $\frac{g_{45^{\circ}} - g}{g} = \frac{980.621 - 980.665}{980.665} = -0.000045.$ Therefore, the expression for the gravity correction becomes

$$(-0.00264 \cos 2 \phi + 0.000007 \cos^2 2 \phi - 0.000045) B$$

TABLE 49 (English measures) gives the corrections in thousandths of an inch for every degree of latitude and for each inch of barometric pressure from 19 to 30 inches, to reduce barometer readings to standard gravity, computed from the equation

$$C = (-0.00264 \cos 2 \phi + 0.000007 \cos^2 2 \phi - 0.000045) B$$

TABLE 50 (metric measures) gives the same corrections in hundredths of a millimeter for each 20 millimeters barometric pressure from 520 to 780 millimeters.

Example:

Barometric reading (corrected for temperature) at latitude

63° 55', = 27.434 inches
Correction to standard gravity, Table 49, = 0.043 inches
Barometer reduced to standard gravity, = 27.477 inches

The adoption of this new value for standard gravity may require a slight correction to old barometric records in order to make the entire series of readings homogeneous. The amount of this correction will be the difference between the gravity correction computed by these new tables and by the old tables.

Example:

Seattle, Wash., Lat. 47° 38′ N. Long. 122° 20′ W., height of barometer above sea level 125 feet, normal station barometer 29.89 inches.

g_{ϕ} (Table 83)	= 980.859 dynes.
Correction for height (-0.000094×125)	=012 ''
Correction for topography and compensation	=019 "
Correction for gravity anomaly	=093 "
Value of local gravity	980.735 dynes.

Correction to reduce barometer readings to standard gravity, $\frac{980.735 - 980.665}{980.665}$ $B_n = +0.002$ inch. Old correction, +0.007; correction to old records = 0.002 in. -0.007 in. =-0.005 in.

For correcting back records of readings at sea, or at any place where the value of local gravity cannot be determined, the correction is equal to the ratio $\frac{980.599 - 980.665}{980.665} B = -0.000067 B$. The corrections are as follows:

Barometer reading.	Correction.		
From 7 to 22 inches From 23 to 32 inches	- 0.001 in. - 0.002 in.		
From 380 to 520 mm.	- o.o3 mm.		
From 530 to 670 mm.	- 0.04 mm.		
From 680 to 820 mm.	- 0.05 mm.		

THE HYPSOMETRIC FORMULA AND ITS CONSTANTS.

The fundamental formula for reducing the barometer to sea level and for determining heights by the barometer is the original formula of Laplace, amplified into the following form —

(1)
$$Z = K \left(\mathbf{I} + \alpha \theta \right) \left(\frac{\mathbf{I}}{\mathbf{I} - 0.378 \frac{e}{b}} \right) \left(\mathbf{I} + \frac{g - g_I}{g} \right) \left(\mathbf{I} + \frac{h + h_o}{R} \right) \log \frac{p_o}{p}$$

or, where g_l, the value of local gravity is unknown,

or, where
$$g_l$$
, the value of local gravity is unknown,

(2) $Z = K \left(\mathbf{I} + \alpha \theta \right) \left(\frac{h^{\mu m_l k_l}}{\mathbf{I}} \right) \left(\mathbf{I} + k \cos 2 \phi - k' \cos^2 2 \phi + C \right) \left(\mathbf{I} + \frac{h + h_o}{R} \right) \log \frac{p_o}{p}$

in which

h = Height of the upper station.

 h_0 = Height of the lower station.

 $Z = h - h_0$

p = Atmospheric pressure at the upper station.

 p_0 = Atmospheric pressure at the lower station.

R =Mean radius of the earth.

 θ = Mean temperature of the air column between the altitudes h and h_0 .

e =Mean pressure of aqueous vapor in the air column.

b = Mean barometric pressure of the air column.

 ϕ = Latitude of the stations.

K = Barometric constant.

a =Coefficient of the expansion of air.

k and k' = Constants depending on the figure of the earth.

 $C = \text{Constant} = \text{the ratio } \frac{g_{45} \circ - g}{2}$.

g = standard value of gravity = 980.665 dynes.

 $g_l = \text{Local value of gravity.}$

The pressures p_0 and p are computed from the height of the column of mercury at the two stations; the ratio $\frac{B_0}{R}$ of the barometric heights may be substituted for the ratio $\frac{p_0}{h}$, if B_0 and B are reduced to the values that would be measured at the same temperature and under the same relative value of gravity.

The correction of the observed barometric heights for instrumental temperature is always separately made, but the correction for the variation of gravity with altitude is generally introduced into the formula itself.

If B_0 , B represent the barometric heights corrected for temperature only, we have the equation

$$\frac{p_{o}}{p_{o}} = \frac{B_{o}}{B} \left(\mathbf{I} + \mu \frac{Z}{R} \right),$$

 μ being a constant depending on the variation of gravity with altitude $\left(\frac{\mu}{R} = 0.0000003\right)$, and

$$\log \frac{p_o}{p} = \log \frac{B_o}{B} + \log \left(\mathbf{I} + \mu \frac{Z}{R} \right).$$

Since $\frac{\mu Z}{R}$ is a very small fraction, we may write

Nap.
$$\log \left(\mathbf{I} + \frac{\mu Z}{R} \right) = \frac{\mu Z}{R}$$
, and $\log \left(\mathbf{I} + \frac{\mu Z}{R} \right) = \frac{\mu Z}{R} M$,

M being the modulus of common logarithms.

By substituting for Z its approximate value $Z = K \log \frac{B_o}{B}$, we have

$$\log\left(\mathbf{I} + \frac{\mu Z}{R}\right) = \frac{\mu K}{R} M \log \frac{B_o}{B}.$$

With these substitutions the barometric formula becomes

(I)
$$Z = K \left(\mathbf{I} + \alpha \theta \right) \left(\frac{\mathbf{I}}{\mathbf{I} - 0.378_b^e} \right) \left(\mathbf{I} + \frac{g - g_{\text{I}}}{g} \right) \left(\mathbf{I} + \frac{h + h_{\text{o}}}{R} \right) \times \left(\mathbf{I} + \frac{\mu K}{R} M \right) \log \frac{B_{\text{o}}}{B}, \text{ or }$$

(2)
$$Z = K \left(\mathbf{I} + \alpha \theta \right) \left(\frac{\mathbf{I}}{\mathbf{I} - 0.378_b^e} \right) \left(\mathbf{I} + k \cos 2\phi - k' \cos^2 2\phi + C \right) \left(\mathbf{I} + \frac{k + h_o}{R} \right) \times \left(\mathbf{I} + \frac{\mu K}{R} M \right) \log \frac{B_o}{B}.$$

As a further simplification we shall put

$$\beta = 0.378 \frac{e}{h}$$
, $\gamma = k \cos 2\phi - k' \cos^2 2\phi + C$ and $\eta = \frac{\mu K}{R} M$,

and write for the second form, (2), the formula -

$$Z = K(\mathbf{I} + \alpha\theta) \left(\frac{\mathbf{I}}{\mathbf{I} - \beta}\right) (\mathbf{I} + \gamma) \left(\mathbf{I} + \frac{h + h_o}{R}\right) (\mathbf{I} + \eta) \log \frac{B_o}{B}.$$

Values of the constants. — The barometric constant K is a complex quantity defined by the equation

$$K = \frac{\Delta \times B_n}{\delta \times M}.$$

 B_n is the normal barometric height of Laplace, 760 mm.

 Δ is the density of mercury at the temperature of melting ice. The value adopted by the International Meteorological Committee, and which has been employed in previous editions of these tables is $\Delta = 13.5956$. The

most probable value, taking into account the recently determined relation between the liter and the cubic decimeter, 1 is as already stated, $\Delta = 13.5951$ and this value is here adopted.

 δ is the density of dry air at $0^{\circ}C$ under the pressure of a column of mercury B_n at the sea level and under standard gravity. The value adopted by the International Bureau of Weights and Measures for air under the above conditions and free from CO_2 is $\delta = 0.0012928$ grams per cubic centimeter.² This is in close agreement with the value ($\delta = 0.00129278$) used in previous editions of these tables. For air containing 4 parts in 10000 of CO_2 it gives a density of 0.00129307, and for air containing 3 parts in 10000 of CO_2 , the proportion adopted by Hann,³ it gives a density of 0.00129301. Therefore, the value adopted for the density of air containing an average amount of CO_2 is

$$\delta = 0.0012930$$

M (Modulus of common logarithms) = 0.4342945. These numbers give for the value of the barometric constant

$$K = 18400$$
 meters.

For the remaining constants, the following values have been used:

 α = 0.00367 for 1° Centigrade. (International Bureau of Weights and Measures: Travaux et Mémoires, t. I, p. A. 54.)

 $\lambda = k \cos 2\phi - k' \cos^2 2\phi + C = 0.002640 \cos 2\phi - 0.000007 \cos^2 2\phi + 0.000045$

R = 6367324 meters. (A. R. Clarke: Geodesy, 8°, Oxford, 1880.)

$$\eta = \frac{\mu KM}{R} = 0.002396$$
. (Ferrel: Report Chief Signal Officer, 1885, pt. 2, pp. 17 and 393.)

TABLES 51, 52, 53, 54, 56.

THE DETERMINATION OF HEIGHTS BY THE BAROMETER.

TABLES 51, 52, 53, 54, 55.

English Measures.

Since a barometric determination of the height will rarely be made at a place where g_l is known, the discussion which follows will be confined to the second form of the barometric formula developed in the preceding section (see page xxxix). For convenience in computing heights it is arranged in the following form:

bllowing form:
$$Z = K (\log B_{0} - \log B) \begin{bmatrix} (\mathbf{I} + \alpha \theta) & -\frac{1}{4} & -\frac{1}{4} \\ (\mathbf{I} + \beta) & -\frac{1}{4} & -\frac{1}{4} \\ (\mathbf{I} + k \cos 2\phi - k' \cos^{2} 2\phi + C) (\mathbf{I} + \eta) \\ \left(\mathbf{I} + \frac{Z + 2h_{0}}{R}\right) & \text{gravity with alt.} \end{bmatrix} qravity$$

¹ Comptes Rendus, Quatrième Conférence Générale Poids et Mesures, 1907, pp. 60-61.

² Leduc, 1.c.

³ Lehrbuch der Meteorologie, dritte Auflage, 1915, s. 5.

in which K (log B_{\circ} - log B) is an approximate value of Z and the factors in the brackets are correction factors depending respectively on the air temperature, the humidity, the variation of gravity with latitude, the variation of gravity with altitude in its effect on the weight of mercury in the barometer, and the variation of gravity with altitude in its effect on the weight of the air. With the constants already given, the formula becomes in English measures:

in English measures:
$$Z(\text{feet}) = 60368^{1} (\log B_{\circ} - \log B) \begin{bmatrix} [1 + 0.002039 (\theta - 32^{\circ})] \\ (1 + \beta) \\ (1 + 0.002640 \cos 2\phi - 0.000007 \cos^{2} 2\phi \\ + 0.000045) (1 + 0.00239) \end{bmatrix}$$

In order to make the temperature correction as small as possible for average air temperatures, 50° F. will be taken as the temperature at which the correction factor is zero. This is accomplished by the following transformation:

$$I + 0.002039 (\theta - 32^{\circ}) = [I + 0.002039 (\theta - 50^{\circ})][I + 0.0010195 \times 36^{\circ}].$$

The second factor of this expression combines with the constant, and gives $60368 (1 + 0.0010195 \times 36^{\circ}) = 62583.6$.

The first approximate value of Z is therefore

$$62583.6 (\log B_0 - \log B).$$

In order further to increase the utility of the tables, we shall make a further substitution for $\log B_{\circ} - \log B$, and write

$$62583.6 \left(\log B_{\circ} - \log B\right) = 62583.6 \left(\log \frac{29.9}{B} - \log \frac{29.9}{B_{\circ}}\right).$$

TABLE 51 contains values of the expression

$$62583.6 \log \frac{29.9}{B}$$

for values of B varying by intervals of 0.01 inch from 12.00 inches to 30.90 inches.

The first approximate value of Z is then obtained by subtracting the tabular value corresponding to B_o from the tabular value corresponding to B (B and B_o being the barometric readings observed and corrected for temperature at the upper and lower stations respectively).

TABLE 52 gives the temperature correction

$$Z \times 0.002039 (\theta - 50^{\circ}).$$

¹ In accordance with the relation between the meter and the foot given on p. xix, this constant should be 60367. (See Table 14.)

The side argument is the mean temperature of the air column (θ) given for intervals of 1° from 0° to 100° F. The top argument is the approximate difference of altitude Z obtained from Table 51.

For temperatures above 50° F., the correction is to be added, and for temperatures below 50° F., the correction is to be subtracted. It will be observed that the correction is a linear function of Z, and hence, for example, the value for Z = 1740 is the sum of the corrections in the columns headed 1000, 700, and 40.

In general, accurate altitudes cannot be obtained unless the temperature used is freed from diurnal variation.

Table 53 gives the correction for gravity, and for the effect of the variation of gravity with altitude on the weight of the mercury. When altitudes are determined with aneroid barometers the second factor does not enter the formula. In this case the effect of the latitude factor can be obtained by taking the difference between the tabular value for the given latitude and the tabular value for latitude 45° 29'. The side argument is the latitude of the station given for intervals of 2° . The top argument is the approximate difference of height Z.

Table 54 gives the correction for the average humidity of the air at different temperatures. In evaluating the humidity factor as a function of the air temperature, the tables given by Prof. Ferrel have been adopted (Meteorological researches. Part iii. — Barometric hypsometry and reduction of the barometer to sea level. Report, U.S. Coast Survey, 1881. Appendix 10.) These tables by interpolation, and by extrapolation below $0^{\circ}F$, give the following values for β :

For Fahrenheit temperatures,

θ	β	θ	β	θ	β	θ	β
F20° -16 -12 ° -8 -6 -4 -2 4 6 8	0.00008 .00020 .00032 .00044 0.00050 .00056 .00062 .00068 .00075 .00082 .00089	F. 10° 12 14 16 18 20 22 24 26 28 30 32 34	0.00104 .00111 .00118 .00126 .00134 .00143 .00153 .00163 .00174 .00187 .00203 .00222	F. 368 388 442 446 488 552 546 558 60	0.00267 .00203 .00322 .00353 .00386 .00421 .00458 .00496 .00534 .00572 .00610 .00648	F. 62° 64 66 68 70 72 76 80 84 88 92 96	0.00724 .00762 .00801 .00839 .00877 .00914 0.00990 .01065 .01141 .01217 .01293

This correction could have been incorporated with the temperature factor in Table 52, but it is given separately in order that the magnitude of the correction may be apparent, and in order that, when the actual hu-

midity is observed, the correction may be computed if desired, by the expression

$$Z\left(0.378 \frac{e}{\bar{b}}\right)$$

where e is the mean pressure of vapor in the air column, and b the mean barometric pressure.

The side argument is the mean temperature of the air column, varying by intervals of 2° from -20° F. to 96° F., except near the extremities of the table where the interval is 4° . The top argument is the approximate difference of altitude Z.

Table 55 gives the correction for the variation of gravity with altitude in its effect on the weight of the air. The side argument is the approximate difference of altitude Z, and the top argument is the elevation of the lower station h_0 .

The corrections given by Tables 53, 54, and 55 are all additive.

Example:

Let the barometric pressure observed, and corrected for temperature, at the upper and lower stations be, respectively, B = 23.61 and $B_o = 29.97$. Let the mean temperature of the air column be 35° F., and the latitude 44° 16′. To determine the difference of height.

Feet.
6420
- 64
$= \overline{6484}$
- 198
+ (16)
+ 16
+ 2
= 6320

If in this example the barometric readings be observed with aneroid barometers, the correction to be obtained from Table 53 will be simply the portion due to the latitude factor, and this will be obtained by subtracting the tabular value for 45° 29' from that for 44° , the top argument being Z = 6300. This gives 16 - 15 = 1.

TABLES 56, 67, 58, 59, 60, 61, 62, 63.

Metric and Dynamic Measures.

The barometric formula developed on page xli is, in metric and dynamic units,

$$Z \text{ (meters)} = 18400 \text{ (log } B_{\text{o}} - \log B) \boxed{ (1 + 0.00367 \ \theta \ C.) \\ (1 + 0.378_{\bar{b}}^{e}) \\ (1 + 0.002640 \cos 2 \phi - 0.000007 \cos^{2} 2 \phi + 0.000045) (1 + 0.00239) \\ \left(1 + \frac{Z + 2 h_{\text{o}}}{6.367.324}\right) }$$

The approximate value of Z (the difference of height of the upper and lower station) is given by the factor 18400 (log $B_{\rm o}$ – log B). This expression is computed by means of two entries of a table whose argument is the barometric pressure. In order that the two entries may result at once in an approximate value of the elevation of the upper and lower stations, a transformation is made, which gives the following identities:

18400 (log
$$B_{\rm o}$$
 – log B) = 18400 (log $\frac{760}{B}$ – log $\frac{760}{B_{\rm o}}$) — Metric measures, and 18400 (log $B_{\rm o}$ – log B) = 18400 (log $\frac{1013.3}{B}$ – log $\frac{1013.3}{B_{\rm o}}$) — Dynamic measures.

TABLE 56 gives values of the expression 18400 $\log \frac{760}{B}$ for values of B

varying by intervals of 1 mm. from 300 mm. to 779 mm. The first approximate value of Z is then obtained by subtracting the tabular value corresponding to B_0 from the tabular value corresponding to B (B and B_0 being the barometric readings observed and reduced to O C at the upper and lower stations respectively). The first entry of Table 56 with the argument B gives an approximate value of the elevation of the upper station above sea level, and the second entry with the argument B_0 gives an approximate value of the elevation of the lower station.

Table 57 gives values of the expression 18400 log $\frac{1013.3}{B}$ for values of

B varying by intervals of 1 mb. from 0 mb. to 1049 mb. The approximate value of Z is then obtained by subtracting the tabular value corresponding to B_0 from the tabular value corresponding to B (B and B_0 being the barometric readings observed and reduced to O C. at the upper and lower stations respectively). The first entry of Table 57 with the argument B gives an approximate value of the elevation of the upper station above sea level, and the second entry with the argument B_0 gives an approximate value of the elevation of the lower station.

Table 58 gives the temperature correction factor, $a = 0.00367\theta$, for each tenth of a degree centigrade, from 0° C. to 50.9° C. To find the correction corresponding to any mean temperature of the air column, θ , multiply the approximate altitude as determined from Table 56 or 57 by the value of a obtained from this table, and add the result if θ is above 0° C.; subtract, if below 0° C.

Attention is called to the fact that the formula is linear with respect to θ , and hence that the correction, for example, for 59.8 C. equals the correction for 50.8 plus the correction for 9° or .186 + .033 = .219, and is to be added.

Table 59 is an amplification of Table 58 and gives the temperature correction 0.00367 $\theta \times Z$.

The side argument is the approximate difference of elevation Z and the top argument is the mean temperature of the air column. The values of Z vary by intervals of 100 m. from 100 to 4000 meters and the temperature varies by intervals of 1° from 1° C. to 10° C. with additional columns for 20°, 30°, and 40° C. This formula also is linear with respect to θ , and hence the correction, for example, for 27° equals the correction for 20° plus the correction for 7°. When the table is used for temperatures below 0° C. the tabular correction must be subtracted from, instead of added to, the approximate value of Z.

Table 60 (pp. 149 and 150) gives the correction for humidity resulting from the factor 0.378 $\frac{e}{h} \times Z = \beta Z$.

Page 149 gives the value of 0.378 $\frac{e}{b}$ multiplied by 10000. The side argument is the mean pressure of aqueous vapor, e, which serves to represent the mean state of humidity of the air between the two stations. $e = \frac{1}{2}(e_1 + e_0)$ (e_1 and e_0 being the vapor pressures observed at the two stations) has been written at the head of the table, but the value to be assigned to e is in reality left to the observer, independently of all hypothesis. The top argument is the mean barometric pressure $\frac{1}{2}$ ($B + B_0$).

The vapor pressure varies by millimeters from 1 to 40, and the mean barometric pressure varies by intervals of 20 mm. from 500 mm. to 760 mm.

The tabular values represent the humidity factor β , or 0.378 $\frac{e}{b}$, multiplied by 10000.

Page 150 gives the correction for humidity, with Z and 10000 \times 0.378 $\frac{e}{b}$ (derived from page 149) as arguments.

The approximate difference of altitude is given by intervals of 100 meters from 100 to 4000 meters, with additional lines for 5000, 6000, and 7000 meters. The values of 10000 β vary by intervals of 25 from 25 to 300. The tabular values are given in tenths of meters to facilitate and increase the accuracy of interpolation.

Table 61. Humidity correction: Value of $\frac{1}{2} \left(\frac{0.378_b^e}{0.00367} \right)$. It has been found advantageous to express the humidity term, βZ , as a correction to the temperature term, $\alpha \theta Z$.

Let
$$\alpha \Delta \theta Z = \beta Z$$
; then,
$$\Delta \theta = \frac{\beta}{\alpha} = \frac{0.378\frac{\epsilon}{b}}{0.00367}.$$

For convenience in computing, the tabulated values of $\Delta \theta$ are for $\frac{1}{2} \left(\frac{0.378_b^e}{0.00367} \right)$. The side and top arguments are air and vapor pressures, respectively, in mm. on p. 151 and in mb. on p. 152. Instead of computing $\Delta \theta$ from the mean of the values of B and e at the upper and lower stations it is computed for each station separately, and the sum of the two determinations is added to θ .

TABLE 62 gives the correction for gravity, and for the effect of the variation of gravity with altitude on the weight of the mercurial column. When altitudes are determined with aneroid barometers the <u>latter factor</u> does not enter the formula. In this case the effect of the latitude factor can be obtained by subtracting the tabular value for latitude 45° 29′ from the tabular value for the latitude in question. ←

The side argument is the approximate difference of elevation Z varying by intervals of 100 meters from 100 to 4000, and by 500 meters from 4000 to 7000. The top argument is the latitude, varying by intervals of 5° from 0° to $75.^{\circ}$

Table 63 gives the correction for the variation of gravity with altitude in its effect on the weight of the air. \prec

The side argument is the same as in Table 62; the top argument is the height of the lower station, varying by intervals of 200 meters from 0 to 2000, with additional columns for 2500, 3000 and 4000 meters.

The corrections given in Table 62 and Table 63 apply to the approximate heights computed from metric or dynamic measures by the use of Tables 56 to 61, inclusive, and are additive.

Example: (Metric Measures.)

Let the barometric reading (reduced to 0° C.) at the upper station be 655.7 mm.; at the lower station, 772.4 mm. Let the mean temperature of the air column be $\theta = 12^{\circ}3$ C., the mean vapor pressure e = 9 mm. and the latitude $\phi = 32^{\circ}$.

Table 56, with argument 655.7, gives	1179 meters.		
Table 56, " " 772.4, "	- 129		
Approximate value of Z	= 1308		
Table 59, with $Z = 1308$ and $\theta = 12.3$ C, gives	59		
Table 60, with $e = 9$ mm. and $Z = 1370$, gives	7		
Table 62, with $Z = 1370$ and $\phi = 32^{\circ}$, gives	5		
Table 63, with $Z = 1370$ and $h_0 = 0$, gives	0		
Corrected value of Z	= 1379 meters.		

Example: (Dynamic Measures.)

Let the barometer reading (reduced to 0° C.) at the upper station be 448.6 mb.; at the lower station, 1000.3 mb. Let the vapor pres-

sure at the upper station be 2.4 mb.; at the lower station 7.3 mb. Let the mean temperature of the air column be $\theta = 5.8$ C. and the latitude $\phi = 39^{\circ} 25'$ N.

Table 57, with argument 448.6, gives

Table 57, with argument 1000.3, gives

Approximate value of Z6511 meters.

104

6407 meters.

Table 61, with arguments 449 and 2.4 gives $\Delta \theta = 0.3$ Table 61, with arguments 1000 and 7.3 gives $\Delta \theta = 0.4$

Table 58, with $\theta = 5.8 + 0.7 = 6.5$, and Z = 6407 gives

 $6407 \times 0.024 =$ 154
Table 62 with Z = 6561 and $\phi = 39^{\circ} 25'$, gives 19
Table 63 with Z = 6561 and $h_{\circ} = 0$, gives 7

Corrected value of Z = $6\overline{587}$ meters.

TABLE 64. Difference of height corresponding to a change of O.1 inch in the barometer — English measures.

If we differentiate the barometric formula, page xlii, we shall obtain, neglecting insensible quantities,

$$dZ = -26281 \frac{dB}{B} \left(1 + 0.002039 \left(\theta - 32^{\circ} \right) \right) (1 + \beta),$$

in which B represents the mean pressure of the air column d Z.

Putting dB = 0.1 inch,

$$dZ = -\frac{2628.1}{B} \left(1 + 0.002039 \left(\theta - 32^{\circ} \right) \right) (1 + \beta).$$

The second member, taken positively, expresses the height of a column of air in feet corresponding to a tenth of an inch in the barometer under standard gravity. Since the last factor $(1 + \beta)$, as given on page xliii, is a function of the temperature, the function has only two variables and admits of convenient tabulation.

Table 64, containing values of dZ for short intervals of the arguments B and θ , has been taken from the Report of the U.S. Coast Survey, 1881, Appendix 10, — Barometric hypsometry and reduction of the barometer to sea level, by Wm. Ferrel.¹

The temperature argument is given for every 5° from 30° F. to 85° F., and the pressure argument for every 0.2 inch from 22.0 to 30.8 inches.

This table may be used in computing small differences of altitude, and, up to a thousand feet or more, very approximate results may be obtained.

$$dZ = -\frac{2628.4}{B} \left(1 + 0.002034 (\theta - 32^{\circ})\right) (1 + \beta).$$

¹ Due to the use of a slightly different value for the coefficient of expansion, Prof. Ferrel's formula, upon which the table is computed, is

Example:

Mean pressure at Augusta, October, 1891, 29.94; temperature, 60.8 F Mean pressure at Atlanta, October, 1891, 28.97; temperature, 59.4 Mean pressure of air column B = 29.455; $\theta = 60.1$

Entering the table with 29.455 and 60°1 as arguments, we take out 94.95 as the difference of elevation corresponding to a tenth of an inch difference of pressure. Multiplying this value by the number of tenths of inches difference in the observed pressures, viz. 97, we obtain the difference of elevation 921 feet.

TABLE 65

Table 65. Difference of height corresponding to a change of one millimeter in the barometer — Metric measures.

This table has been computed by converting Table 64 into metric units. The temperature argument is given for every 2° from -2° C. to $+36^{\circ}$ C.; the pressure argument is given for 10-mm. intervals from 760 to 560 mm.

TABLE 66.

TABLE 66. Babinet's formula for determining heights by the barometer.

Babinet's formula for computing differences of altitude ¹ represents the formula of Laplace quite accurately for differences of altitude up to 1000 meters, and within one per cent for much greater altitudes. As it has been quite widely disseminated among travelers and engineers, and is of convenient application, the formula is here given in English and metric measures. It might seem desirable to alter the figures given by Babinet so as to conform to the newer values of the barometrical constants now adopted; but this change would increase the resulting altitudes by less than one-half of one per cent without enhancing their reliability to a corresponding degree, on account of the outstanding uncertainty of the assumed mean temperature of the air.

The formula is, in English measures,

$$Z ext{ (feet)} = 52494 \left[1 + \frac{t_o + t - 64^{\circ}}{900} \right] \frac{B_o - B}{B_o + B};$$

and in metric measures,

$$Z ext{ (meters)} = 16000 \left[1 + \frac{2 (t_0 + t)}{1000} \right] \frac{B_0 - B}{B_0 + B},$$

in which Z is the difference of elevation between a lower and an upper station at which the barometric pressures corrected for all sources of instrumental error are B_o and B, and the observed air temperatures are t_o and t, respectively.

For ready computation the formula is written

$$Z = C \times \frac{B_{\circ} - B}{B_{\circ} + B},$$

¹ Comptes Rendus, Paris, 1850, vol. xxx., page 309.

and the factor C, computed both in English and metric measures, has been kindly furnished by the late Prof. Cleveland Abbe. The argument is $\frac{1}{2}(t_0+t)$ given for every 5° Fahrenheit between 10° and 100° F., and for every 2° Centigrade between - 10° and 36° Centigrade.

In using the table, it should be borne in mind that on account of the uncertainty in the assumed temperature, the last two figures in the value of C are uncertain, and are here given only for the sake of convenience of interpolation. Consequently one should not attach to the resulting altitudes a greater degree of confidence than is warranted by the accuracy of the temperatures and the formula. The table shows that the numerical factor changes by about one per cent of its value for every change of five degrees Fahrenheit in the mean temperature of the stratum of air between the upper and lower stations; therefore the computed difference of altitude will have an uncertainty of one per cent if the assumed temperature of the air is in doubt by $5^{\circ}F$. With these precautions the observer may properly estimate the reliability of his altitudes whether computed by Babinet's formula or by more elaborate tables.

Example:

Let the barometric pressure observed and corrected for temperature at the upper and lower stations be, respectively, B = 635 mm. and $B_o = 730$ mm. Let the temperatures be, respectively, $t = 15^{\circ}$ C., $t_o = 20_{\circ}$ C. To find the approximate difference of height.

With
$$\frac{1}{2}(t_0 + t) = \frac{20^\circ + 15^\circ}{2} = 17^\circ 5$$
 C., the table in metric measures gives $C = 17120$ meters. $\frac{B_0 - B}{B_0 + B} = \frac{95}{1365}$.

The approximate difference of height = $17120 \times \frac{95}{1365} = 1191.5$ meters.

THERMOMETRICAL MEASUREMENT OF HEIGHTS BY OBSERVATION OF THE TEMPERATURE OF THE BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of its vapor gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles and the water boils. The temperature at which water boils in the open air thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the *higher* the station where an observation is made, the *lower* will be the temperature of the boiling point.

The difference of elevation between two places therefore can be de-

duced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and from these to compute the difference of height by the tables given herein for computing heights from barometric observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometric observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water is a less accurate measurement of the atmospheric pressure than is the height of the barometer. In the present state of thermometry it would hardly be safe, indeed, to rely, in the most favorable circumstances, upon quantities so small as hundredths of a degree, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and substance of the vessel containing the water, the purity of the water itself, the position at which the bulb of the thermometer is placed, whether in the current of the steam or in the water, - all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric pressure. Owing to these various causes, an observation of the boiling point, differing by one-tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one-tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimeters in the barometric pressure, or of from 70 to 80 feet in the final result, while with a good barometer the error of pressure will hardly ever exceed one-tenth of a millimeter, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer is of the greatest utility to travellers and explorers in rough countries, on account of its being more conveniently transported and much less liable to accidents than the mercurial barometer. A suitable form for it, designed by Regnault (Annales de Chimie et de Physique, Tome xiv, p. 202), consists of an accurate thermometer with long degrees, subdivided into tenths. For observation the bulb is placed about 2 or 3 centimeters above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp.

TABLES 67, 66.

Barometric pressures at standard gravity corresponding to the temperature of boiling water.

TABLE 67. English Measures.

TABLE 68. Metric Measures.

Table 67 is copied directly from Table 70. The argument is the temperature of boiling water for every tenth of a degree from 1850 to 21409 Fahrenheit. The tabular values are given to the nearest 0.001 inch.

Table 68 is copied directly from Table 72. The argument is given for every tenth of a degree from 80°0 to 100°9 C. The tabular values are given to the nearest 0.01 mm.

HYGROMETRICAL TABLES.

PRESSURE OF SATURATED AQUEOUS VAPOR.

In former editions of these tables the values of aqueous vapor pressures at temperatures between -29° and 100° C. were based upon Broch's reduction of the classic observations of Regnault. (Travaux et Mémoires du Bureau international des Poids et Mesures, t. I, p. A 19-39). In these computations the same continuous mathematical function was employed to calculate the values of vapor pressure both above and below the point of change of state on freezing. This resulted in a systematic disagreement between observed and computed vapor pressures below the freezing point, and confirmed the inference from the laws of diffusion following from the kinetic theory of gases, namely, that the pressure of the vapor is different according as it is in contact with its liquid or its solid.

Seeking to remove the uncertainty of the values of vapor pressures at temperatures below freezing, Marvin (Annual Report Chief Signal Officer, 1891, Appendix No. 10) made direct experimental determinations thereof, in the course of which the specimens of water were cooled to temperatures of from -10° to -12° C. while still retaining the liquid state, thus affording opportunity for measurements of vapor pressure over ice and over water at various temperatures below the freezing point. The results of these investigations, confirmed by similar independent studies by Juhlin, were printed in the third revised edition of these tables.

Since 1907, especially, several extended series 1 of entirely new determinations, together covering the whole range of temperature from - 70° C. to + 374° C., have been made at the Physikalische-Technischen Reichsanstalt. Because of the elaborate instrumental means available and the extreme effort to eliminate all possible errors these results may be presumed to represent the most accurate series of experimental values of this important physical datum available to science.

Hitherto no satisfactory mathematical equation has been offered adequate to give computed values of vapor pressures with an order of precision comparable to the systematic self consistency of the observations

¹ Scheel, Karl und Heuse, Wilhelm. Bestimmung des Sättigungsdrucks von Wasserdampf unter 0°. Annalen der Physik, 1909, 29: 723–737.

Bestimmung des Sättigungsdrucks von Wasserdampf zwischen o° und + 50°. Annalen der Physik, 1910, 31: 715-736.

Holborn, L. und Henning, F. Über das Platinthermometer und den Sättigungsdruck des Wasserdampfes zwischen 50 und 200°. Annalen der Physik, 1908, 26:833-883.

Holborn, L. und Baumann, A. Über den Sättigungsdruck des Wasserdampfes oberhalb 200°. Annalen der Physik, 1910, 31: 945-970.

themselves. This is particularly the case with the more recent data over the whole range of temperature from 0° to the critical temperature at about 374° Centigrade. Two remedies have been utilized to overcome this difficulty. First, the employment of separate equations of interpolation adjusted to fit the observations accurately over a short range of temperature, 0° to 100° for example, as in the case of Broch's computations. (It has already been mentioned that theory requires the function for vapor pressures over ice to differ from the one for pressures over water, so that the values for ice offer no difficulty.) The second remedy sometimes employed consists in fitting any reasonably accurate equation as closely as possible to the observations. The differences between the observed and computed values are then charted and a smooth curve drawn by hand through the points thus located. This method has been employed notably by Henning¹ and others, using an empirical equation proposed by Thiesen.

For the purpose of these tables it has been found possible from among a multitude of equations to develop a modification of the theoretical equation of Van der Waals which fits the whole range of observations much better than any hitherto offered and with an order of precision quite comparable to the data itself. In fact, the equation serves to disclose inconsistencies in the observations, more particularly between 50° and 80° C., which seem to suggest the need for further experimental determination of values possibly over the range between 0° and 100°.

Although it is not difficult to show, as Cederberg ² has done, that the simple form of general theoretical equation for all vapors developed by Van der Waals is inadequate to represent experiments on water vapor with sufficient accuracy for practical requirements, nevertheless a somewhat simple elaboration of its single constant suffices to remove this limitation in a very satisfactory manner.

The resulting equation is:

log
$$e = \log \pi - [A - bX + mX^2 - nX^3 + sX^4] \frac{\theta - T}{T}$$
, where $X = \frac{T - 453}{10}$. (1)

The quantity within the square brackets in this equation replaces a single term of the Van der Waals equation which was regarded by him as a constant.

In Van der Waals's original equation π and θ are respectively the critical pressure and temperature (absolute). In the present state of physical science, and from the very nature of the data, these quantities cannot be evaluated exactly. Moreover it is unnecessary to do so for the mere purpose of accurately fitting a mathematical curve to the observational data,

¹ Annalen der Physik, 1907, 22: 609-630.

² Cederberg, Ivar W. Über eine exakte Dampfdruckberechnungsmethode. Physik. Zeitschr. xv: 697, 1914; Über die Temperaturabhängigkeit einiger physikalischen Eigenschaften des Wassers in seinen vershiedenen Aggregatzuständen. Physik. Zeitschr. xv: 824, 1914.

because the same result is attained by simply passing the curve through a point more accurately known and as near as may be to the critical point. This is equivalent to defining π and θ by an "equation of condition." Another "equation of condition" fixes the pressure at the boiling point which by definition must be 760 mm. From the considerations given on page xi computations are greatly facilitated by taking all temperatures on the approximate absolute scale represented by $T = 273 + \ell^{\circ}$.

A careful preliminary analysis of the observational data in the vicinity of the critical temperature resulted in assigning values to θ and π as follows:

$$\theta = 643^{\circ}, \log \pi = 5.1959000$$

It is emphasized here again that these data do not represent critical temperature conditions, but simply a convenient point on the pressure curve slightly below the critical temperature, the value of which is fixed with considerable accuracy by the observational data.

The value of the constant A was fixed by the equation of condition, e = 760 mm. when T = 373 (X = -8). The remaining constants (b, m, n, s) are computed by the method of least squares. The results are as follows:

$$A = 3.1473172$$
 $b = .00295944$
 $m = .0004191398$
 $n = .0000001829924$
 $s = .00000008243516$

The number of significant figures in the constants is obviously greater than the accuracy of the data justifies; but is justified to facilitate computation and to secure accuracy in the interpolation of values which should themselves be as accurate as the data.

Thiesen¹ has shown that the observed values of vapor pressure over ice can be reproduced by the equation

Log
$$e = \log e_0 + 9.632 (1 - 0.00035t) \frac{t}{T}$$

 $e_0 = 4.5785$, and $T = 273 + t$.

where

For convenience in computing this equation, for metric units it may be written

$$\text{Log } e = 0.66072 + \left(\frac{9.632 - 0.0033712 \, t}{273 + t}\right) t. \tag{2}$$

For English units the equation becomes

$$\operatorname{Log} e = \overline{1}.255888 + \left(\frac{9.69193 - 0.00187289 t_{1}}{459.4 + t_{1}}\right) (t_{1} - 32). \tag{3}$$

t =degrees Centigrade; $t_r =$ degrees Fahrenheit.

¹ Thiesen M. Die Dampfspannung über Eis. (Mitteilung aus der Physikalisch-Technischen Reichsanstalt.) Annalen der Physik, 1909; 29: 1057.

The vapor pressures in the tables here given are expressed in standard manametric units.

TABLE 69.

Table 69. Pressure of aqueous vapor over ice. English measures.

The pressures, computed by equation (3) above, are given to 0.00001 inch for each degree of temperature from -60° to -15° , for each half degree from -15 to $\pm 0^{\circ}$, and for each tenth of a degree from $\pm 0^{\circ}$ 0 to $+32^{\circ}$ 0.

TABLE 70.

TABLE 70. Pressure of aqueous vapor over water. English measures.

This table has been computed by converting Table 72 into English units. The temperature argument is given for every 0.1 from 32.0 to 214.9 F. The vapor pressures are to 0.0001 inch from 32.0 to 130.9, F., and to 0.001 inch from 130.0 to 214.9 F.

TABLE 71,

Table 71. Pressure of aqueous vapor over ice. Metric measures.

The pressures, computed by equation (2) above, are given to the nearest 0.0001 mm. for each degree of temperature from -70° to -50° , for each half degree from -50° to -35° , and each tenth of a degree from -35° 0 to $\pm 0^{\circ}$ 0.

TABLE 72.

Table 72. Pressure of aqueous vapor over water. Metric measures.

The pressures, computed by equation (1) above, are given for each tenth of a degree to 0.001 mm. from 0.0 to 50.9, and to 0.01 mm. from 50.0 to 100.9. They are given for each degree to 0.1 mm. from 100° to 189°, and in millimeters from 190° to 374°.

TABLES 72 74

Table 73. Weight of cubic foot of saturated aqueous vapor — English measures.

Table 74. Weight of a cubic meter of saturated aqueous vapor — Metric measures.

For many years it has been customary to assume that the specific gravity of water vapor relative to dry air is a constant whose theoretical value computed from the accurately known densities of its constituent gases is 0.6221. Direct experimental determinations of the specific volume of dry saturated steam (as yet but few observations are available at moderate temperatures) show conclusively (I) that this theoretical specific gravity is true only for saturated vapor at very low temperatures or when the vapor is in a very attenuated state of partial saturation; (2) that at increasingly higher temperatures the specific gravity is increasingly greater than 0.6221. These assertions are in accord with the values of weight per cubic foot of

water vapor tabulated by Marks & Davis ¹ from the most recent determinations of the specific volume of water vapor. However, owing to the paucity of data, and its inaccuracy for the range of atmospheric temperatures and conditions, the values derived from densities given by Marks and Davis between 10° and 50° are probably too low and require revision. The basis on which this assertion is made is the generalization that the theoretical value 0.6221 is probably a minimum specific gravity towards which actual values asymptotically tend at low temperature and low relative humidity in the meteorological sense, or high super heats in the steam engineering sense. This generalization affords a very helpful "control" in harmonizing and combining experimental determinations of specific volume. It was thus employed in a recomputation, from the original experimental data on specific volumes, of the accompanying table of specific gravities, δ , of saturated water vapor.

$T. (C^{\circ})$	δ	$T. (C^{\circ})$	δ
– 60	0.6226	60	0.6273
50	0.6227	70	0.6283
40	0.6229	8o ·	0.6296
30	0.6230	90	0.6311
20	0.6232	100	0.6329
– 10	0.6235	I IO	0.6351
\pm o	0.6238	120	0.6377
+ 10	0.6241	130	0.6408
20	0.6246	140	o.6446
30	0.6251	150	0.6491
40	0.6257	160	0.6545
50	0.6264	170	0.6609
		180	0.6687

The weight of a cubic meter of saturated vapor is given by the expression

$$W = \frac{a\delta}{1 + at} \cdot \frac{e}{760},$$

a is the weight of a cubic meter of dry air (free from carbonic acid) at temperature of C, and pressure of 760 millimeters of mercury of standard density under standard gravity: a = 1.29278 kg. (Bureau International des Poids et Mesures: Travaux et Mémoires, t. I, p. A 54.)

 δ is the density of aqueous vapor relative to dry air: $\delta = 0.6221$.

While, as stated above, there is reason for believing that this value is too low, for atmospheric temperatures the error is less than one per cent. For practical work in meteorology and at moderate temperatures, it seems best to retain the theoretical value until the actual value has been determined

¹ Marks, Lionel S., and Davis, Harvey N. Tables and diagrams of the thermal properties of saturated and superheated steam. New York, 1909.

with greater accuracy. For all important calculations except those at low temperatures the values of δ in the Table on page lvi should be employed.

e is the pressure of saturated aqueous vapor at temperature t, taken from Tables 71 and 72.

 α is the coefficient of expansion of air for 1° C.: $\alpha = 0.003670$. ϵ 173 t is the temperature in Centigrade degrees.

Whence we have

$$W ext{(grams)} = 1.05821 \times \frac{e}{1 + 0.003670 t}$$

TABLE 74 is computed from this formula and gives the weight of saturated vapor in grams in a cubic meter for dew-points from -29° to $+40^{\circ}9$ C., the intervals from 6° to $40^{\circ}9$ C., being $0^{\circ}1$ C. The tabular values are given to three decimals.

The weight W_{I} of a *cubic foot* of saturated vapor is obtained by converting the foregoing constants into English measures.

The weight of a cubic foot of dry air at temperature $32^{\circ}F$, and at a pressure of 760 mm. or 29.921 inches is

$$a_1(\text{grains}) = \frac{1292.78 \times 15.43235}{(3.280833)^3} = 564.94.$$

We have therefore.

$$W_1 \text{ (grains)} = \frac{a_1 \delta}{29.921} \times \frac{e_1}{1 + a_1 (t_1 - 32^\circ)} = 11.7459 \frac{e_1}{1 + 0.002039 (t_1 - 32^\circ)}$$

The temperature $t_{\rm r}$ is expressed in degrees Fahrenheit; the vapor pressure $e_{\rm r}$, expressed in inches, is obtained from Tables 69 and 70.

Table 73 gives the weight of saturated aqueous vapor in grains per cubic foot for dew points given to every degree from -30° to $+20^{\circ}$, to each half degree from $+20^{\circ}$ to $+70^{\circ}$, and for every 0.2 from 70.0 to 119.8 F, the values being computed to the thousandth of a grain.

REDUCTION OF OBSERVATIONS WITH THE PSYCHROMETER AND DETERMINATION OF RELATIVE HUMIDITY.

The psychrometric formula derived by Maxwell, Stefan, August, Regnault and others is, in its simplest form,

$$e = e' - AB (t - t'),$$

in which t = Air temperature.

t' = Temperature of the wet-bulb thermometer.

e =Pressure of aqueous vapor in the air.

e' = Vapor pressure, saturated, at temperature t'.

B = Barometric pressure.

A = A quantity which, for the same instrument and for certain conditions, is a constant, or a function depending in a small measure on t'.

All pressures are expressed in heights of mercurial column under standard gravity.

The important advance made since the time of Regnault consists in recognizing that the value of A differs materially according to whether the wet-bulb is in quiet or moving air. This was experimentally demonstrated by the distinguished Italian physicist, Belli, in 1830, and was well known to Espy, who always used a whirled psychrometer. The latter describes his practice as follows: "When experimenting to ascertain the dew-point by means of the wet-bulb, I always swung both thermometers moderately in the air, having first ascertained that a moderate movement produced the same depression as a rapid one."

The principles and methods of these two pioneers in accurate psychrometry have now come to be adopted in the standard practice of meteorologists, and psychrometric tables are adapted to the use of a whirled or ventilated instrument.

The factor A depends in theory upon the size and shape of the thermometer bulb, largeness of stem and velocity of ventilation, and different formulæ and tables would accordingly be required for different instruments. But by using a ventilating velocity of three meters or more per second, the differences in the results given by different instruments vanish, and the same tables can be adapted to any kind of a thermometer and to all changes of velocity above that which gives sensibly the greatest depression of the wet-bulb temperature; and with this arrangement there is no necessity to measure or estimate the velocity in each case further than to be certain that it does not fall below the assigned limit.

The formula and tables here given for obtaining the vapor pressure and dew-point from observations of the whirled or ventilated psychrometer are those deduced by Prof. Wm. Ferrel (Annual Report Chief Signal Officer, 1886, Appendix 24) from a discussion of a large number of observations.

Taking the psychrometric formula in metric units, pressures being expressed in millimeters and temperatures in centigrade degrees, Prof. Ferrel derived for A the value

$$A = 0.000656 (1 + 0.0019 t').$$

In this expression for A, the factor depending on t' arises from a similar term in the expression for the latent heat of water, and the theoretical value of the coefficient of t' is 0.00115. Since it would require a very small change in the method of observing to cause the difference between the theoretical value and that obtained from the experiments, Prof. Ferrel adopted the theoretical coefficient 0.00115 and then recomputed the observations, obtaining therefrom the final value

$$A = 0.000660 (1 + 0.00115 t').$$

With this value the psychrometric formula in metric measures becomes e = e' - 0.000660 B (t - t') (1 + 0.00115 t').

$$e = e' - 0.000367 B (t - t') [I + 0.00064 (t' - 32^{\circ})]$$

= $e' - 0.000367 B (t - t') \left(I + \frac{t' - 32}{157I}\right)$

in which e = Vapor pressure in inches.

e' = Pressure of saturated aqueous vapor at temperature t'.

t = Temperature of the air in Fahrenheit degrees.

t' = Temperature of the wet-bulb thermometer in Fahrenheit degrees.

B = Barometric pressure in inches.

TABLE 75.

Table 75. Reduction of Psychrometric Observations — English measures.

Values of
$$e = e' - 0.000367 B (t - t') \left(I + \frac{t' - 32}{1571} \right)$$

This table provides for computing the vapor pressure, e, from observations of ventilated wet- and dry-bulb Fahrenheit thermometers. From the vapor pressure thus computed the dew-point and relative humidity of the atmosphere may be obtained.

The tabular values of the vapor pressure, e, are computed for degree intervals of t' from -20° to $+110^{\circ}$ F. Below $+10^{\circ}$ the interval for t-t' is 0°2, and above 10° the interval is 1°. The computation has been made for B=30.0 inches, but at the bottom, and usually, also, at the top of each page of the table is given a correction, $\Delta e \times \Delta B$, computed for B=29.0 inches or $\Delta B=1$ inch, and for the value of t' indicated. The correction is a linear function of ΔB . For atmospheric pressures less than 30.0 inches, it is to be added to the tabular values of e, while for atmospheric pressures greater than 30.0 inches it is to be subtracted.

The values of e are given to 0.0001 inch for t' less than 10°, and to 0.001 inch for t' greater than 10°.

Examples:

- 1. Given, t = 84.3; t' = 66.7, and B = 30.00 inches. With t' = 66.7 and t t' = 17.6 as arguments, Table 75 gives for e the value 0.462 inch. On page 174, for t t' = 0.0 it is seen that a vapor presure of 0.462 inch corresponds to a temperature $t' = t = 57^{\circ}$, which is the saturation, or dew-point temperature for the data given.
- 2. Given, t = 34.5; t' = 29.4; B = 22.3 inches. With t' = 29.4 and t t' = 5.1 as arguments, Table 75 gives for e the value 0.104. $\Delta B = 30.0 22.3 = 7.7$, and $\Delta e \times \Delta B = 0.0018 \times 7.7 = 0.014$. Correct value of e

For t - t' = 0.0 a vapor pressure of 0.118 inch corresponds to a temperature $t' = t = 23^{\circ}$ (see page 174), which is the saturation or dewpoint temperature for the data given.

Table 76. Relative humidity — Temperature Fahrenheit.

The table gives the vapor pressure corresponding to air temperatures from -30° to $+120^{\circ}$ at degree intervals (side argument) and for percentages of saturation at 10 per cent intervals (top argument). It is computed from the formula

$$e = e_s \times \text{relative humidity}$$
,

where e_s is the saturation vapor pressure at the given air temperature. Below a temperature of 20° the values of e are given to 0.0001 inch; above 20° they are given to 0.001 inch.

Examples:

1. In dew-point example 1, above, the computed vapor pressure is 0.462 inch. Entering Table 76 with air temperature 84°3 as side argument, we obtain vapor pressure

0.462 inch - 0.356 inch = 0.106 inch = "
$$\frac{90}{10}$$
 = 9
therefore, vapor pressure - 0.462 inch with $t = 84.3$ F. = " " 39

2. In dew-point example 2, above, the computed vapor pressure is 0.118 inch. Entering Table 76 with air temperature 34.5 as side argument, we obtain, vapor pressure

0.118 inch - 0.100 inch = 0.018 inch = "
$$\frac{90}{10} = 9$$

therefore, vapor pressure - 0.118 inch with $t = 34.5 F$. = " 59

Reduction of Psychrometric Observations — Metric measures.

Table 77. Values of
$$e = e' - 0.000660 B (t - t') (1 + 0.00115 t')$$

This table provides for computing the vapor pressure from observations of ventilated wet- and dry-bulb Centigrade thermometers. From the vapor pressure thus computed the dew-point and relative humidity of the atmosphere may be obtained.

The tabular values of the vapor pressure, e, are computed for degree intervals of t' from -30° to $+45^{\circ}$ C. Below -5° 0 the interval for t-t'

is 0°1, and above -5°0 the interval is 1°. The computation has been made for B=760 mm. but on each page of the table is given a correction, $\Delta e \times \Delta B$, computed for B=660, or $\Delta P=100$ mm., and for the values of t' indicated. The correction is a linear function of ΔB . For atmospheric pressures less than 760 mm. it is to be added to the tabular values of e, while for atmospheric pressures greater than 760 mm. it is to be subtracted. The values of e are given to 0.001 mm. for t' less than -5°0, and to 0.01 mm. for t' greater than -5°0.

Example:

Given, t = 10.4 C.; t' = 8.3 C., and B = 740 mm. With t' = 8.3 and t - t' = 2.1 as arguments, Table 77 gives for e the value 7.15 mm.

$$\Delta B = \frac{760 - 740}{100} = 0.2.$$
 $\Delta e \times \Delta B = 0.14 \times 0.2$ = 0.03.

Corrected value of e = 7.18 mm.

For t - t' = 0 a vapor pressure of 7.18 mm. corresponds to a temperature t' = t = 6.3 C., which is the saturation, or dew-point temperature for the data given.

TABLE 78.

Table 78. Relative humidity — Temperature Centigrade.

This table gives the vapor pressure corresponding to air temperatures from -45° C. to $+55^{\circ}$ C. at degree intervals (side argument) and for percentage of saturation at 10 per cent intervals (top argument). It is computed from the same formula as Table 76, namely,

$$e = e_s \times \text{relative humidity}.$$

Below a temperature of $+5^{\circ}$ 0 the values of e are given to 0.01 mm.; above 5° 0 they are given to 0.1 mm.

Example:

In the dew-point example given above, the computed vapor pressure is 7.18 mm. Entering Table 78 with air temperature 10.4 as side argument, we obtain vapor pressure

6.6 mm. = relative humidity 70 and
$$7.18 - 6.6 = 0.58$$
 mm. = " $\frac{60}{10} = 6$

7.18 mm. with t = 10.4 C. = " = 76

TABLE 79.

TABLE 79. Rate of decrease of vapor pressure with altitude for mountain stations.

From hygrometric observations made at various mountain stations on the Himalayas, Mount Ararat, Teneriffe, and the Alps, Dr. J. Hann (*Lehrbuch der Meteorologie Dritte Auflage*, S. 230) has deduced the following empirical formula showing the average relation between the vapor

pressure e_0 at a lower station and e the vapor pressure at another station at an altitude h meters above it:

$$\frac{e}{e_{\circ}} = 10^{-\frac{h}{6300}}.$$

This is of course an average relation for all times and places from which the actual rate of decrease of vapor pressure in any individual case may widely differ.

Table 79 gives the values of the ratio $\frac{e}{e_o}$ for values of h from 200 to 6000 meters. An additional column gives the equivalent values of h in feet.

REDUCTION OF SNOWFALL MEASUREMENT.

The determination of the water equivalent of snowfall has usually been made by one of two methods: (a) by dividing the depth of snow by an arbitrary factor ranging from 8 to 16 for snow of different degrees of compactness; (b) by melting the snow and measuring the depth of the resulting water. The first of these methods has always been recognized as incapable of giving reliable results, and the second, although much more accurate, is still open to objection. After extended experience in the trial of both these methods, it has been found that the most accurate and most convenient measurement is that of weighing the collected snow, and then converting the weight into depth in inches. The method is equally applicable whether the snow as it falls is caught in the gage, or a section of the fallen snow is taken by collecting it in an inverted gage.

Table 80. Depth of water corresponding to the weight of a cylindrical snow core, 2.655 inches in diameter.

This table is prepared for convenience in making surveys of the snow layer on the ground, particularly in the western mountain sections of the country. The weighing method is the only one found to be practicable. Present Weather Bureau practice is to take out a sample by means of a special tube, whose diameter, 2.655 inches, has been selected by reason of convenience in manipulation and simplicity in relation to the pound. Table 80 gives the depth of water in inches and hundredths corresponding to given weights. The argument is given in hundredths of a pound from 0.01 pound to 2.99 pounds.

Table 81. Depth of water corresponding to the weight of snow (or rain) collected in an 8-inch gage.

The table gives the depth to hundredths of an inch, corresponding to the weight of snow or rain collected in a gage having a circular collecting mouth 8 inches in diameter — this being the standard size of gage used throughout the United States. The argument is given in hundredths of a pound from 0.01 pound to 0.99 pound. When the weight of the collected snow or rain is one pound or more, the depth corresponding to even pounds may be obtained from the equivalent of one pound given in the heading of the table.

Example:

The weight of the snow collected in a gage having a circular collecting mouth 8 inches in diameter is 3.48 pounds. Find the corresponding depth of water.

A weight of 2 the corresponds to a depth of water of

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	0.55	507	× 3,	equ	als						1.65 in.
Αv	veigh	t of	0.48	lbs.	corres	ponds	to a	depth	of wat	ter of	0.26
Α	"	"	3.48	"	"		"	"	4	4	T.OT in.

TABLE 82. Quantity of rainfall corresponding to given depths.

TABLE 82.

This table gives for different depths of rainfall in inches over an acre the total quantity of water expressed in cubic inches, cubic feet, gallons, and tons. (See Henry, A. J. "Quantity of Rainfall corresponding to Given Depths." *Monthly Weather Review*, 1898, 26: 408-09.)

GEODETICAL TABLES.

Table 83. Value of apparent gravity on the earth at sea level. 1 Table 83.

The value of apparent gravity on the earth at sea level is given for every twenty minutes of latitude from 5° to 86°, and for degree intervals near the equator and the poles. It is computed to 0.001 dyne from the equation ²

$$g_{\phi} = 978.039 \text{ (I } + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2 \phi)$$

= 980.621 (I - 0.002640 \cos^2 \phi + 0.000007 \cos^2 2 \phi)

in which g_{ϕ} is the value of the gravity at latitude ϕ .

The second form of the equation is the more convenient for the computation.

TABLE 84.

TABLE 84. Relative acceleration of gravity at sea level at different latitudes.

The formula adopted for the variation with latitude of apparent gravity

The formula adopted for the variation with latitude of apparent gravity at sea level is that of the U.S. Coast and Geodetic Survey, given above.

The table gives the values of the ratio $\frac{g_{\phi}}{g_{45^{\circ}}}$ to six decimals for every 10' of latitude from the equator to the pole.

¹ Gravity is here considered in terms of force (expressed in dynes) that is exerted on a mass of one gram rather than its numerical equivalent, acceleration (expressed in centimeters and seconds), for which there is no convenient expression.

² See Bowie, William, *Investigations of Gravity and Isostasy*. U.S. Coast and Geodetic Survey, Special Publication No. 40, 1917, page 134.

LENGTH OF A DEGREE OF THE MERIDIAN AND OF ANY PARALLEL.

The dimensions of the earth used in computing lengths of the meridian and of parallels of latitude are those of Clarke's spheroid of 1866.¹ This spheroid undoubtedly represents very closely the true size and shape of the earth, and is the one to which nearly all geodetic work in the United States is now referred.

The values of the constants are as follows:

a, semi-major axis = 20926062 feet; $\log a = 7.3206875$. b, semi-minor axis = 20855121 feet; $\log b = 7.3192127$.

$$e^2 = \frac{a^2 - b^2}{a^2} = 0.00676866$$
; $\log e^2 = 7.8305030 - 10.$

With these values for the figure of the earth, the formula for computing any portion of a quadrant of the meridian is

Meridional distance in feet = $[5.5618284] \Delta \phi$ (in degrees), - $[5.0269880] \cos 2 \phi \sin \Delta \phi$, + $[2.0528] \cos 4 \phi \sin 2 \Delta \phi$, in which $2\phi = \phi_2 + \phi_1$, $\Delta \phi = \phi_2 - \phi_1$; ϕ_1 , ϕ_2 = end latitudes of arc.

For the length of I degree, the formula becomes:

I degree of the meridian, in feet = 364609.9 - 1857.1 cos 2 ϕ + 3.94 cos 4 ϕ .

The length of the parallel is given by the equation

I degree of the parallel at latitude ϕ , in feet = 365538.48 cos ϕ - 310.17 cos 3 ϕ + 0.39 cos 5 ϕ .

TABLE 85. Length of one degree of the meridian at different latitudes.

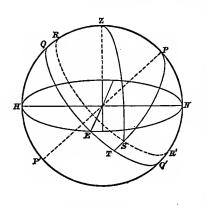
This gives for every degree of latitude the length of one degree of the meridian in statute miles to three decimals, in meters to one decimal, and in geographic miles to three decimals—the geographic mile being here defined to be one minute of arc on the equator. The values in meters are computed from the relation: I meter = 39.3700 inches. The tabular values represent the length of an arc of one degree, the middle of which is situated at the corresponding latitude. For example, the length of an arc of one degree of the meridian, whose end latitudes are 29° 30′ and 30° 30′, is 68.879 statute miles.

Table 86. Length of one degree of the parallel at different latitudes.

This table is similar to Table 85.

¹ Comparisons of Standards of Length, made at the Ordnance Survey Office, Southampton, England, by Capt. A. R. Clarke, R. E., 1866.

TABLE 87. Duration of sunshine at different latitudes for different values of the sun's declination.



Let Z be the zenith, and NH the horizon of a place in the northern hemisphere.

P the pole;

QEQ' the celestial equator;

RR' the parallel described by the sun on any given day;

S the position of the sun when its upper limb appears on the horizon;

PN the latitude of the place, ϕ .

ST the sun's declination, δ .

PS the sun's polar distance, $90^{\circ} - \delta$.

ZS the sun's zenith distance, z.

ZPS the hour angle of the sun from meridian, t.

r the mean horizontal refraction = 34' approximately.

s the mean solar semi-diameter = 16'

$$z = 90^{\circ} + r + s = 90^{\circ} 50'$$

In the spherical traingle ZPS, the hour angle ZPS may be computed from the values of the three known sides by the formula

$$\sin \frac{1}{2} ZPS = \sqrt{\frac{\sin \frac{1}{2} (ZS + PZ - PS) \sin \frac{1}{2} (ZS + PS - PZ)}{\sin PZ \sin PS}}$$
or
$$\sin \frac{1}{2} t = \sqrt{\frac{\sin \frac{1}{2} (z + \delta - \phi) \sin \frac{1}{2} (z - \delta + \phi)}{\cos \phi \cos \delta}}$$

The hour angle t, converted into mean solar time and multiplied by $\boldsymbol{2}$ is the duration of sunshine.

Table 87 has been computed for this volume by Prof. Wm. Libbey, Jr. It is a table of double entry with arguments δ and ϕ . For north latitudes northerly declination is considered positive and southerly declination as negative. The table may be used for south latitudes by considering southerly declination as positive and northerly declination as negative.

The top argument is the latitude, given for every 5° from 0° to 40°, for every 2° from 40° to 60°, and for every degree from 60° to 80°.

The side argument is the sun's declination for every 20' from S 23° 27' to N 23° 27'.

The duration of sunshine is given in hours and minutes.

To find the duration of sunshine for a given day at a place whose latitude is known, find the declination of the sun at mean noon for that day in the *Nautical Almanac*, and enter the table with the latitude and declination as arguments.

Example:

To find the duration of sunshine, May 18, 1892, in latitude 49° 30' North.

From the Nautical Almanac, $\delta = 19^{\circ} 43' N$.

From the table, with $\delta = 19^{\circ} 43' N$ and $\phi = 49^{\circ} 30'$, the duration of sunshine is found to be $15^{h} 31^{m}$.

TABLE 88. Declination of the sun for the year 1899.

This table is an auxiliary to Table 87, and gives the declination of the sun for every third day of the year 1899. These declinations may be used as approximate values for the corresponding dates of other years when the exact declination cannot readily be obtained. Thus, in the preceding example, the declination for May 18, 1892, may be taken as approximately the same as that for the same date in 1899, viz. 19° 37'.

THE DURATION OF TWILIGHT.

A review of the literature ¹ indicates that from an early date astronomical twilight has been considered to end in the evening and begin in the morning when the true position of the sun's center is 18° below the horizon. At this time stars of the sixth magnitude are visible near the zenith, and generally there is no trace on the horizon of the twilight glow.

It also appears that *civil* twilight ends in the evening and begins in the morning when the true position of the sun's center is 6° below the horizon. At this time stars and planets of the first magnitude are just visible. In the evening the first purple light has just disappeared, and darkness compels the suspension of outdoor work unless artificial lighting is provided. In the morning the first purple light is beginning to be visible, and the illumination is sufficient for the resumption of outdoor occupations.

Some confusion has arisen in the computation of tables of the duration of both astronomical and civil twilight, due to the fact that in some instances the time of sunrise or sunset has been considered to be that instant when the *center* of the sun is on the true horizon; in others, when its center *appears* to be on the true horizon; and in still others when the *upper limb* of the sun appears to coincide with the true horizon. In the United States this latter is regarded as defining the time of sunrise and sunset.

In the tables here presented the duration of astronomical twilight is the interval between sunrise or sunset, according to this latter definition, and the instant the true position of the sun's center is 18° below the horizon. Likewise, the duration of civil twilight is the interval from sunrise or sunset to the instant the true position of the sun's center is 6° below the horizon.

¹ Kimball, Herbert H. "Duration and Intensity of Twilight," Monthly Weather Review, 1916, 44: 614–620.

The computations may be made from the equation

$$\cos t = \frac{\sin a - \sin \phi \sin \delta}{\cos \phi \cos \delta}$$

where t is the sun's hour angle from the meridian, a is the sun's altitude, considered minus below the horizon, δ is the solar declination, and ϕ is the latitude of the place of observation.

The solar declinations employed are those given in the American Ephemeris and Nautical Almanac, 1899, pp. 377-384, Solar Ephemeris for Washington.

The atmospheric refraction with the sun on the horizon has been assumed to be 34', and 16' has been allowed for the sun's semi-diameter, so that at the instant of sunrise or sunset, as defined above, the true position of the sun's center is about 50' below the horizon. The difference between this value of t and its value with the sun 6° and 18° below the horizon gives, respectively, the duration of civil and astronomical twilight.

The computations have been simplified by the use of Ball's Altitude Tables, from which the value of t has been determined for true altitudes of the sun of -50', -6° , and -18° .

TABLE 89. Duration of astronomical twilight.

TABLE 89.

The duration of astronomical twilight is given to the nearest minute for the 1st, 11th, and 21st day of each month for north latitudes, 0°, 10°, 20°, 25°, and at 2° intervals from 30° to 50°, inclusive. The absence of data for latitude 50° from June 1 to July 11, inclusive, indicates that between these dates at this latitude astronomical twilight continues throughout the night.

TABLE 90. Duration of civil twilight.

TABLE 90.

The duration of civil twilight is given to the nearest minute for the 1st, 11th and 21st day of each month for north latitudes 0°, 10°, 20°, 25°, and at 2° intervals from 30° to 50°, inclusive.

RELATIVE INTENSITY OF SOLAR RADIATION AT DIFFERENT LATITUDES. TABLE 94.

Table 91. Mean intensity for 24 hours of solar radiation on a horizontal surface at the top of the atmosphere.

This table is that of Prof. Wm. Ferrel, published in the Annual Report of the Chief Signal Officer, 1885, Part 2, p. 427, and computed from formulæ and constants given in Chapter II of the above publication, pages 75 to 82. It gives the mean intensity, J, for 24 hours of solar radiation received by a horizontal surface at the top of the atmosphere, in terms of the mean solar

¹ Ball, Frederick. Altitude Tables for lat. 31° to 60°. London, 1907; [same] for lat. 0° to 30°, London, 1910.

constant A_o , for each tenth parallel of latitude of the northern hemisphere, and for the first and sixteenth day of each month; also the values of the solar constant A in terms of A_o , and the longitude of the sun for the given dates.

Table 92. Relative amounts of solar radiation received on a horizontal surface during the year at different latitudes.

The second column of this table is obtained from the last line of Table 91 by multiplying by 1440, the number of minutes in 24 hours. It therefore gives the average daily amount of radiation that would be received from the sun on a horizontal surface at the surface of the earth if none were absorbed or scattered by the atmosphere, expressed in terms of the mean solar constant. The following columns give similar data, except that the atmospheric transmission coefficient is assumed to be 0.9, 0.8, 0.7 and 0.6, respectively, and have been computed by utilizing Angot's work (Recherches théoretiques sur la distribution de la chaleur à la surface du globe, par M. Alfred Angot, Annales du Bureau Central Météorologique de France, Année 1883. v. 1. B 121-B 169), which leads to practically the same values as Ferrel's when expressed in the same units.

The vertical argument of the table is for 10° intervals of latitude from the equator to the north pole, inclusive.

TABLE 93. Air mass, m, corresponding to different zenith distances of the sun.

For homogenous rays, the intensity of solar energy after passing through an air mass, m, is expressed by the equation $I = I_o a^m$, where I_o is the intensity before absorption, a is the atmospheric transmission coefficient, or the proportion of the energy transmitted by unit air mass, and m is the air mass passed through. If we take for unit air mass the atmospheric mass passed through by the rays when the sun is in the zenith, then for zenith distances of the sun less than 80° the air mass is nearly proportional to the secant of the sun's zenith distance. In general, the secant gives air masses that are too high by an increasing amount as the zenith distance of the sun increases.

The equation by which air masses are sometimes computed is $m = \frac{atmospheric\ refraction}{K\sin Z}$

where Z is the sun's zenith distance and K is a constant. The uncertain factor in this equation is the atmospheric refraction. Table 93 gives values of m computed by Bemporad (*Rend. Acc. Lincei.*, Roma, Ser. 5, V. 16, 2 Sem. 1907, pp. 66–71) from the above formula, using for K the value $58^{\prime\prime}.36$. The argument is for each degree of Z from 20° to 89° , with values of M added for $Z = 0^{\circ}$, 10° , and 15° . The values of M are given to two decimal places.

TABLE 94. Relative illumination intensities.

TABLE 94.

The table gives illumination intensities in foot-candles for zenithal sun, sky at sunset, sky at end of civil twilight, zenithal full moon, quarter moon, and starlight, and the ratio of these intensities to the illumination from the zenithal full moon. For the sources of the data see Kimball, Herbert H., "Duration and Intensity of Twilight," *Monthly Weather Review*, 1916, 44: 614–620.

MISCELLANEOUS TABLES.

WEIGHT IN GRAMS OF A CUBIC CENTIMETER OF AIR.

The following tables (95 to 100) give the factors for computing the weight of a cubic centimeter of air at different temperatures, humidities and pressures.

$$\delta = \frac{0.00129305}{1 + 0.00367 t} \left(\frac{B - 0.378 e}{760} \right)$$

in which δ is the weight of a cubic centimeter of air expressed in grams, under the standard value of gravity (g = 980.665)

B is the atmospheric pressure in millimeters, under standard gravity;

e is the pressure of aqueous vapor in millimeters, under standard gravity;

t is the temperature in Centigrade degrees.

For dry atmospheric air (containing 0.0004 of its weight of carbonic acid) at a pressure of 760 mm. and temperature o° C., the absolute density, or the weight of one cubic centimeter, is 0.00129305 gram. (International Bureau of Weights and Measures. *Travaux et Mémoires*, t. I, p. A 54.) See also these Tables, p. xli.

The weight of a cubic centimeter may also be written as follows:

$$\delta = \frac{0.00129305}{1 + 0.0020389 \ (t - 32^{\circ})} \left(\frac{B - 0.378 \ e}{29.921}\right)$$

where δ is defined as before, but B and e are expressed in inches and t in Fahrenheit degrees. Thus by the use of tables based on these two formulæ, lines of equal atmospheric density may be drawn for the whole world, no matter whether the original observations are in English or metric measures.

ENGLISH MEASURES.

TABLES 95, 96, 97.

TABLE 95. Temperature Term.

This table gives the values and logarithms of the expression

$$\delta_{t, 29.921} = \frac{0.00129305}{1 + 0.0020389 \ (t - 32^{\circ})}$$

for values of t extending from $-45^{\circ} F$. to $+140^{\circ} F$., the intervals between $0^{\circ} F$. and $110^{\circ} F$. being 1° .

The tabular values are given to five significant figures.

TABLE 96. Term for humidity; auxiliary to Table 95.

Table 97. Humidity and pressure term.
$$\frac{h}{29.921} = \frac{B - 0.378 e}{29.921}$$

TABLE 96 gives values of 0.378 e to three decimal places as an aid to the use of Table 97. The argument is the dew-point given for every degree from $-60^{\circ} F$. to $+140^{\circ} F$. The second column gives the corresponding values of the vapor pressure (e) derived from Tables 69 and 70.

Table 97 gives values and logarithms of
$$\frac{h}{29.921} = \frac{B - 0.378 e}{29.921}$$
 for values

of h extending from 10.0 to 31.7 inches. The logarithms are given to five significant figures and the corresponding numbers to four decimals.

Example:

The air temperature is 68° F., the pressure is 29.36 inches and the dewpoint 51° F. Find the logarithm of the density.

Table 95, for
$$t = 68^{\circ}$$
 F., gives 7.08085 – 10

Table 96, for dew-point 51° , gives 0.378 e = 0.142 inch,

Table 97, for
$$h = B - 0.378 e = 29.36 - 0.14 = 29.22$$
, gives 9.98941 - 10

Logarithm of density =

30 7.07056 - 10

METRIC MEASURES.

TABLE 98. Temperature term.

This table gives values and logarithms of the expression

$$\delta_{t, 760} = \frac{0.00129305}{1 + 0.00367 t}$$

for values of t extending from -34° C. to $+69^{\circ}$ C. The tabular values are given to five significant figures.

Table 99. Term for humidity; auxiliary to Table 100.

Table 100. Humidity and pressure terms.
$$\frac{h}{760} = \frac{B - 0.378 e}{760}$$
.

Table 99 gives the values of 0.378 e to hundredths of a millimeter for dew-points extending from -50° C. to $+60^{\circ}$ C. Above -25° C. the interval is one degree. The values of the vapor pressure, e, corresponding to these dew-points, given in the second column, are taken from tables 71 and 72.

Table 100 gives values and logarithms of
$$\frac{h}{760} = \frac{B - 0.378 e}{760}$$
 for

values of h extending from 300 to 799 mm. The atmospheric pressure B is the barometer reading corrected for gravity and 0.378 e is the term for

humidity obtained from Table 99. The logarithms are given to five significant figures and the corresponding numbers to four decimal places.

TABLE 101. Atmospheric water-vapor lines in the visible spectrum. TABLE 101.

Table 101, prepared by the Astrophysical Observatory at Washington, gives a summary of lines in Rowland's "Preliminary Table of Solar Spectrum Wave Lengths," recorded as of atmospheric water vapor origin. There are more than 400 such lines in Rowland's table, but an abridgment is here made as follows:

Only lines of intensity "I" or greater are here separately given, but the total number and average intensity of the fainter lines lying between these are inserted. Rowland's scale of intensities is such that a line of intensity "I" is "just clearly visible" on Rowland's map; the H and K lines are of intensity, 1,000; $D_{\rm I}$ (the sodium line of greater wave length), 20; $C_{\rm I}$, 40. "Lines more and more difficult to see" are distinguished by 0, 00, 000, and 0000.

Table 102. Absorption by atmospheric water-vapor bands in the infra-red.

The values of Table 102 relate to the transmission of energy in the minima of various water-vapor bands, when there is 1 cm. of precipitable water in the path through the air. For other amounts of water-vapor, the depths of these minima may be taken as equal to a^{δ} , where a is the coefficient taken from the third column of Table 102 and δ is the amount of precipitable water in the path. For average conditions in the transmission of radiation through the atmosphere, δ may be determined by the modification of Hann's formula $\delta = 2.0 \, e$ sec. Z, where e is the vapor pressure in cms. as determined by wet and dry thermometers and Z is the angle which the path makes with the vertical.

For the use of the transmissions observed in such bands for the inverse process of determining the amount of water-vapor in the atmosphere, see Fowle, *Astrophysical Journal*, 35, p. 149, 1912; 37, p. 359, 1913.

Table 103. Transmission percentages of radiation through moist air.

The values of Table 103 will be of use when the transmission of energy through the atmosphere containing a known amount of water-vapor is under consideration. An approximate value for the energy transmitted may be had if the amount of energy from the source between the wavelengths of the first column is known and is multiplied by the corresponding transmission coefficients of the subsequent columns of the table. The table is compiled from Fowle, "Water-vapor Transparency," Smithsonian Miscellaneous Collections, 68, No. 8, 1917; see also, Fowle, "The Transparency of Aqueous Vapor," Astrophysical Journal, 42, p. 394, 1915.

TABLE 104. International meteorological symbols.

The information under this heading has been compiled for the present

edition by the librarian of the United States Weather Bureau, and represents current practice in the use of the symbols approved by the International Meteorological Organization. For further information on the subject of meteorological symbols, see *Monthly Weather Review* (Wash., D.C.), May, 1916, pp. 265–274.

TABLE 105. International cloud classification.

The text under this heading is condensed from the International Cloud Atlas, 2d edition, Paris, 1910.

TABLE 106. Beaufort weather notation.

This table has been revised in the library of the United States Weather Bureau, and represents the current practice of American and British observers in the use of the Beaufort letters.

TABLE 107. List of meteorological stations.

This list has been extensively revised in the library of the Weather Bureau, and has been enlarged to include all the stations for which data appear in the "Réseau Mondial" of the British Meteorological Office for 1912 (published 1917). The stations of the Réseau Mondial were selected to represent, so far as available data permitted, the meteorology of all land areas of the globe, on the basis of two, or in some cases three, stations for each ten-degree square of latitude and longitude.

No attempt has been made in this edition of the Smithsonian Tables to indicate the "order" of the several stations, according to the definitions adopted at the Vienna Congress of 1873; as, owing to the present widespread use of self-recording instruments, the old distinction between first and second order stations has lost much of its importance.

Several stations included in the list are no longer in operation. Data concerning the locations and altitudes of these stations are still valuable, in view of the frequent use made of their records in meteorological and climatological studies.

In general, the spellings of names are those most frequently met with in existing compilations of meteorological data, without regard to the practice of English-speaking countries. In a majority of cases the native orthography has been followed.

THERMOMETRICAL TABLES

Con	version of thermometric scales —	
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	Centigrade scale to Fahrenheit	TABLE 3
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TABLE 1.
APPROXIMATE ABSOLUTE, CENTIGRADE, FAHRENHEIT, AND REAUMUR SCALES.

Conversion Formulæ for Approximate Absolute (A.A), Centigrade (C), Fahrenheit (F), and Reaumur (R) Scales.

	1	/o (F		- C		./. D. I					
A	C = 5	/9 (F - 3)	3^{2}) $+ ^{2}$ 7 3^{2}) $= ^{5}$ /	3 = C - 4R =	+ 273 = A.A − :	$5/4 K + 273 = \frac{I}{2}$	F - 32	$(1+\frac{1}{2})$	<u>-+-</u>	+ 1	+)
		/5 C + 3									/
		/9 (F —					37 1 3	(10,) · °	
			,			ONAL PAI	RTS.				
A.A	} r	2	3		4	5	6	7		8	9
F R	1.8		5	4 :	7.2	9.0	10.8	12.6	14		
		3 1.6	2.,	4 3	3.2	4.0	4.8	5.6			.2
F C A.A			_* _ 4		4	5	6	7 3.88*		8 g	
A.A	·5	5* 1. 1 4* .8		_	.22 * ·77*	2.77* 2.22*	3·33* 2.66*	3.00			00* 00*
-				-							
R C A.A	} 1.2		3 0 3.7		.4 .00	5 6.25	ຸ6 7∙5 ○	7 8.75	8 10.	,	.25
A.A F	2.2			-		·	13.50	15.75	18.		-
						s repeated					
A.A.	C,	F.	R.	A.A.	c.	F.	R.	A.A.	c.	F.	R.
375°	1020	215.6	8 1 .6	350°	77°	170°.6	61.6	325°	52°	125°.6	41°.6
374	101	213.8	80.8 80.0	349 348	76 75	168.8 167.0	60.8 60.0	324 323	51 50	123.8 122.0	40.8 40.0
372	99.	210.2	79.2	347	74	165.2	59.2	322	49	120.2	39.2
371	98	208.4	78.4	346	73	163.4	58.4	321	48	118.4	38.4
370 369	97. 96	206.6	77.6 76.8	345 344	72 71	161.6 159.8	57.6 56.8	320 319	47	116.6 114.8	37.6 36.8
368	95	203.0	76.0	343	70	158.0	56.0	318	46 45	114.0	36.0
367	94	201.2	75.2	342	69 68	156.2	55.2	317	44	111.2	35.2
366	93	199.4	74-4	341	00	154.4	54-4	316	43	109.4	34.4
365	92	197.6	73.6 72.8	340	67 66	152.6 150.8	53.6	315	42	107.6	33.6
364 363	91. 90	195.8	72.0	339 338	65	140.0	52.8 52.0	314	41 40	105.8 104.0	32.8 32.0
362	89	192.2	71.2	337	64	147.2	51.2	312	39	102,2	31.2
361	88	190.4	70.4	336	63	145.4	50.4	311	38	100.4	30.4
360	87	188.6 186.8	69.6 68.8	335	62 61	143.6	49.6	310	37	98.6	20.6
359 358	86 85	185.0	68.o	334 333	60	141.8	48.8 48.0	309 308	36 35	96.8 95.0	28.8 28.0
357	84	183.2	67.2	332	59	138.2	47.2	307	34	93.2	27.2
356	83	181.4	66.4	331	58	136.4	46.4	306	33	91.4	26.4
355	82 81	179.6 177.8	65.6 64.8	330	57 56	134.6 132.8	45.6	305	32	89.6	25.6
354 353	80	177.0	64.0	329 328	56 55	132.0	44.8	304 303	31 30	87.8 86.0	24.8 24.0
352	79 78	174.2 172.4	63.2 62.4	327 326	54	129.2	43.2	302	29	84.2	23.2
351	.	172.4	61.6	320 325	53 52	127.4	42.4	301 300	28	82.4 80.6	22.4
350	77 C.	F.	R.	325 A.A.	C.	F.	41.6 R.		$-\frac{^{27}}{\mathbf{C}.}$	80.0 F.	21.6
A.A.	<u>. </u>	F.	п.	7.4.	٠.	r.	ır.	A.A.		г.	R.

TABLE 1
APPROXIMATE ABSOLUTE, CENTIGRADE, FAHRENHEIT, AND REAUMUR
SCALES.

A.A.	с.	F.	R.	Α.Α.	c.	F.	R.	A.A.	c.	F.	R.
300°	27°	80°.6	21°.6	250°	-23°	- 9°.4	-18.°4	200°	-73°	- 99°4	-58.4
299	26	78.8	20.8	249	24	11.2	19.2	199	74	101.2	59.2
298	25	77.0	20.0	248	25	13.0	20.0	198	75	103.0	60.0
297	24	75.2	19.2	247	26	14.8	20.8	197	76	104.8	60.8
296	23	73.4	18.4	246	27	16.6	21.6	196	77	106.6	61.6
295	22	71.6	17.6	245	-28	-18.4	-22.4	195	-78	-108.4	-62.4
294	21	69.8	16.8	244	29	20.2	23.2	194	-70 79	110.2	63.2
293	20	68.0	16.0	243	30	22.0	24.0	193	80	112.0	64.0
292	19	66.2	15.2	242	31	23.8	24.8	192	81	113.8	64.8
291	18	64.4	14.4	241	32	25.6	25.6	191	82	115.6	65.6
290	17	62.6	13.6	240	-33	-27.4	-26.4	190	-83	-117.4	-66.4
280	16	60.8	12.8	239	34	29.2	27.2	180	84	110.2	67.2
288	15	59.0	12.0	238	35	31.0	28.0	188	85	121.0	68.0
287	14	57-2	11.2	237	36	32.8	28.8	187	86	122.8	68.8
286	13	55-4	10.4	236	37	34.6	29.6	186	87	124.6	69.6
285	12	53.6	9.6	235	<i>∸</i> 38	-36.4	-30.4	185	-88	-126.4	-70.4
284	11	51.8	8.8	234	39	38.2	31.2	184	89	128.2	71.2
283	10	50.0	8.0	233	40	40.0	32.0	183	90	130.0	72.0
282	9 8	48.2	7.2	232	41	41.8	32.8	182	91	131.8	72.8
281	8	46.4	6.4	231	42	43.6	33.6	181	92	133.6	73.6
280	7	44.6	5.6	230	-43	-45.4	-34.4	180	-93	-135.4	-74-4
279	6	42.8	4.8	220	44	47.2	35.2	179	94	137.2	75.2
278	5	41.0	4.0	228	45	49.0	36.0	178	95	139.0	76.0
277	4	39.2	3.2	227	46	50.8	36.8	177	96	140.8	76.8
276	3	37.4	2.4	226	47	52.6	37.6	176	97	142.6	77.6
275	+ 2	35.6	+ 1.6	225	_ ₄₈	 −54.4	-38.4	175	- 98	-144.4	-78.4
274	+ 1	33.8	+ 0.8	224	49	56.2	39.2	174	99	146.2	79.2
273	\pm \circ	32.0	± 0.0	223	50	58.0	40.0	173	100	148.0	80.0
272	- I	30.2	- 0.8	222	51	59.8	40.8	172	101	149.8	80.8
271	- 2	28.4	- 1.6	221	52	61.6	41.6	171	102	151.6	81.6
270	- 3	26.6	- 2.4	220	-53	-63.4	-42.4	170	-103	-153.4	-82 4
269	4	24.8	3.2	219	54	65.2	43.2	169	104	155.2	83.2
268	5 6	23.0	4.0	218	55	67.0	44.0	168	105	157.0	84.0
267		21.2	4.8	217	56	68.8	44.8	167	106	158.8	84.8
266	7	19.4	5.6	216	57	70.6	45.6	166	107	160.6	85.6
265	- 8	17.6	- 6.4	215	-58	-72.4	-46.4	165	-108	-162.4	-86.4
264	9	15.8	7.2	214	59	74.2	47.2	164	109	164.2	87.2
263	10	14.0	8.0	213	60	76.0	48.0	163	110	166.0	88.0
262	11	12.2	8.8	212	61	77.8	48.8	162	111	167.8	88.8
261	12	10.4	9.6	211	62	79.6	49.6	161	112	169.6	89.6
260	-13	8.6	-10.4	210	-63	-81.4	-50.4	160	-113	-171.4	-90.4
259	14	6.8	11.2	209	64	83.2	51.2	159	114	173.2	91.2
258	15	5.0	12.0	208	65	85.0	52.0	158	115	175.0	92.0
257	16	3.z	12.8	207	66	86.8	52.8	157	116	176.8	92.8
256	17	+ 1.4	13.6	206	67	88.6	53.6	156	117	178.6	93.6
255	-18	-0.4	-14.4	205	-68	-90.4	-54.4	155	-118	-180.4	-94.4
254	19	2.2	15.2	204	69	92.2	55-2	154	119	182.2	95.2
253	20	4.0	16.0	203	70	94.0	56.0	153	120	184.0	96.0
252	21	5.8	16.8	202	71	95.8	56.8	152	121	185.8	96.8
251	22	7.6	17.6	201	72	97.6	57.6	151	122	187.6	97.6
250	-23	-9.4	-18.4	200	-73_	-99.4	-58.4	150	-123	-189.4	-98.4
A.A.	c.	F.	R.	A.A.	C.	F.	R.	A.A.	C.	F.	R.

SMITHSONIAN TABLES.

TABLE 1
APPROXIMATE ABSOLUTE, CENTIGRADE, FAHRENHEIT, AND REAUMUR
SCALES.

						ALES.					
A.A.	C.	F.	R.	A.A.	C.	F.	R.	Α.Α.	c.	F.	ι R.
150°	-123°	-189.4	- 98.4	100°	~173°	-279°4	-138.4	50°	-223°	-369°4	-178.4
149	124	191.2	99.2	99	174	281.2	139.2	40	224	371.2	179.2
148	125	193.0	100.0	98	175	283.0	140.0	48	225	373.0	180.0
147	126	194.8	100.8	97	176	284.8	140.8	47	226	374.8	180.8
146	127	196.6	101.6	96	177	286.6	141.6	46	227	376.6	181.6
145	-128	-198.4	-102.4	95	-178	-288.4	-142.4	45	-228	-378.4	-182.4
144	120	200.2	103.2	94	179	200.2	143.2	44	220	380.2	183.2
143	130	202.0	104.0	93	180	202.0	144.0	43	230	382.0	184.0
142	131	203.8	104.8	92	181	293.8	144.8	42	231	383.8	184.8
141	132	205.6	105.6	91	182	295.6	145.6	41	232	385.6	185.6
140	-133	-207.4	-106.4	90	-183	-207.4	-146.4	40	-233	-387.4	-186.4
139	134	200.2	107.2	80	184	299.2	147.2	39	234	389.2	187.2
138	135	211.0	108.0	88	185	301.0	148.0	38	235	391.0	188.0
137	136	212.8	108.8	87	186	302.8	148.8	37	236	392.8	188.8
136	137	214.6	109.6	86	187	304.6	149.6	36	237	394.6	189.6
135	-138	-216.4	-110.4	85	-188	-306.4	-150.4	35	-238	-396.4	-190.4
134	139	218.2	111.2	84	189	308.2	151.2	34	239	398.2	191.2
133	140	220.0	112,0	83	190	310.0	152.0	33	240	400.0	192.0
132	141	221.8	112.8	82	191	311.8	152.8	32	241	401.8	192.8
131	142	223.6	113.6	81	192	313.6	153.6	31	242	403.6	193.6
130	-143	-225.4	-114.4	80	-193	-315.4	-154.4	30	-243	-405.4	-194.4
129	144	227.2	115.2	79	194	317.2	155.2	29	244	407.2	195.2
128	145	229.C	116.0	78	195	319.0	156.0	28	245	409.0	196.0
127	146	230.8	116.8	77	196	320.8	156.8	27	246	410.8	196.8
126	147	232.6	117.6	76	197	322.6	157.6	26	247	412.6	197.6
125	-148	-234.4	-118.4	75	-198	-324.4	-158.4	25	-248	-414.4	-198.4
124	149	236.2	119.2	74	199	326.2	159.2	24	249	416.2	199.2
123	150	238.0	120.0	73	200	328.0	160.0	23	250	418.0	200.0
122	151	239.8	120.8	72	201	329.8	160.8	22	251	419.8	200.8
121	152	241.6	121.6	71	202	331.6	161.6	21	252	421.6	201.6
120	-153	-243.4	-122.4	70	-203	-333-4	-162.4	20	-253	-423.4	-202.4
119	154	245.2	123.2	69	204	335.2	163.2	10	254	425.2	203.2
118	155	247.0	124.0	68	205	337.0	164.0	18	255	427.0	204.0
117	156	248.8	124.8	67	206	338.8	164.8	17	256	428.8	204.8
116	157	250.6	125.6	66	207	340.6	165.6	16	257	430.6	205.6
115	-158	-252.4	-126.4	65	-208	-342.4	-166.4	15	-258	-432.4	-206.4
114	159	254.2	127.2	64	209	344.2	167.2	14	259	434.2	207.2
113	160	256.0	128.0	63	210	346.0	168.0	13	260	436.0	208.0
II2	161	257.8	128.8	62	211	347.8	168.8	12	261	437.8	208.8
III	162	259.6	129.6	61	212	349.6	169.6	11	262	439.6	209.6
110	-163	-261.4	-т30.4	60	-213	-351.4	-170.4	10	-263	-441.4	-210.4
100	164	263.2	131.2	59	214	353.2	171.2	9	264	443.2	211.2
108	165	265.0	132.0	58	215	355.0	172.0	8	265	445.0	212.0
107	166	266.8	132.8	57	216	356.8	172.8	7	266	446.8	212.8
106	167	268.6	133.6	56	217	358.6	173.6	6	267	448.6	213.6
105	-168	-270.4	-134.4	55	-218	-360.4	-174.4	5	-268	-450.4	-214.4
104	169	272.2	135.2	54	219	362.2	175.2	4	269	452.2	215.2
103	170	274.0	136.0	53	220	364.0	176.0	3	270	454.0	216.0
102	171	275.8	136.8	52	221	365.8	176.8	2	271	455.8	216.8
101	172	277.6	137.6	51	222	367.6	177.6	1	272	457.6	217.6
100	-173	-279-4	-138.4	50	-223	-369.4	-178.4	0	-273	-459.4	-218.4
A.A.	c.	F.	R.	A.A.	c.	F.	R.	A.A.	c.	F.	R.

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
+130° 129 128 127 126	c.	c.	c.	c.	C.	c.	c.	c.	c.	c.
	+54°44	+54.50	+54°,56	+54.66	+54.67	+54°72	+54.78	+54.83	+54.89	+54.94
	53.89	53.94	54.00	54.06	54.11	54.17	54.22	54.28	54.33	54.39
	53.33	53.39	53.44	53.50	53.56	53.61	53.67	53.72	53.78	53.83
	52.78	52.83	52.89	52.94	53.00	53.06	53.11	53.17	53.22	53.28
	52.22	52.28	52.33	52.39	52.44	52.50	52.56	52.61	52.67	52.72
+125	+51.67	+ 51.72	+51.78	+51.83	+51.89		+52.00	+52.06	+52.11	+52.17
124	51.11	51.17	51.22	51.28	51.33		51.44	51.50	51.56	51.61
123	50.56	50.61	50.67	50.72	50.78		50.89	50.94	51.00	51.06
122	50.00	50.06	50.11	50.17	50.22		50.33	50.39	50.44	50.50
121	49.44	49.50	49.56	49.61	49.67		49.78	49.83	49.89	49.94
+120	+48.89	+43.94	+49.00	+49.06	+49.11	+49.17	+49.22	+49.28	+49.33	+49.39
119	48.33	48.39	48.44	48.50	48.56	48.61	48.67	48.72	48.78	48.83
118	47.78	47.83	47.89	47.94	48.00	48.06	48.11	48.17	48.22	48.28
117	47.22	47.28	47.33	47.39	47.44	47.50	47.56	47.61	47.67	47.72
116	46.67	46.72	46.78	46.83	46.89	46.94	47.00	47.06	47.11	47.17
+115	+46.11	+46.17	+46.22	+46.28	+46.33	+46.39	+46.44	+46.50	+46.56	+46.61
114	45.56	45.61	45.67	45.72	45.78	45.83	45.89	45.94	46.00	46.06
113	45.00	45.06	45.11	45.17	45.22	45.28	45.33	45.39	45.44	45.50
112	44.44	44.50	44.56	44.61	44.67	44.72	44.78	44.83	44.89	44.94
111	43.89	43.94	44.00	44.06	44.11	44.17	44.22	44.28	44.33	44.39
+ IIO 109 108 107 106	+43.33 42.78 42.22 41.67 41.11	+43.39 42.83 42.28 41.72 41.17	+43.44 42.89 42.33 41.78 41.22	+43.50 42.94 42.39 41.83 41.28	+43.56 43.00 42.44 41.89 41.33	43.06 42.50	+43.67 43.11 42.56 42.00 41.44	+43.72 43.17 42.61 42.06 41.50	+43.78 43.22 42.67 42.11 41.56	+43.83 43.28 42.72 42.17 41.61
→105	+40.56	+40.61	+40.67	+40.72	+40.78	+40.83	+40.89	+40.94	+41.00	+41.06
104	40.00	40.06	40.11	40.17	40.22	40.28	40.33	40.39	40.44	40.50
103	39.44	39.50	39.56	39.61	39.67	39.72	39.78	39.83	39.89	39.94
102	38.89	38.94	39.00	39.06	39.11	39.17	39.22	39.28	39.33	39.39
101	38.33	38.39	38.44	38.50	38.56	38.61	38.67	38.72	38.78	38.83
+100	+37.78	+37.83	+37.89	+37.94	+38.00	+38.06	+38.11	+38.17	+38.22	+38.28
99	37.22	37.28	37.33	37.39	37.44	37.50	37.56	37.61	37.67	37.72
98	36.67	36.72	36.78	36.83	36.89	36.94	37.00	37.06	37.11	37.17
97	36.11	36.17	36.22	36.28	36.33	36.39	36.44	36.50	36.56	36.61
96	35.56	35.61	35.67	35.72	35.78	35.83	35.89	35.94	36.00	36.06
+ 95	+35.00	+35.06	+35.11	+35.17	+35.22	+35.28	+35.33	+35.39	+35.44	+35.50
94	34.44	34.50	34.56	34.61	34.67	34.72	34.78	34.83	34.89	34.94
93	33.89	33.94	34.00	34.06	34.11	34.17	34.22	34.28	34.33	34.39
92	33.33	33.39	33.44	33.50	33.56	33.61	33.67	33.72	33.78	33.83
91	32.78	32.83	32.89	32.94	33.00	33.06	33.11	33.17	33.22	33.28
+ 90 89 88 87 86	+32.22	+32.28	+32.33	+32.39	+32.44	+32.50	+32.56	+32.61	+32.67	+32.72
	31.67	31.72	31.78	31.83	31.89	31.94	32.00	32.06	32.11	33.17
	31.11	31.17	31.22	31.28	31.33	31.39	31.44	31.50	31.56	31.61
	30.56	30.61	30.67	30.72	30.78	30.83	30.89	30.94	31.00	31.06
	30.00	30.06	30.11	30.17	30.22	30.28	30.33	30.39	30.44	30.50
+ 85 84 83 82 81 + 80	+29.44 28.89 28.33 27.78 27.22	+29.50 28.94 28.39 27.83 27.28	+29.56 29.00 28.44 27.89 27.33	+29.61 29.06 28.50 27.94 27.39	+29.67 29.11 28.56 28.00 27.44	29.17 28.61 28.06 27.50	+29.78 29.22 28.67 28.11 27.56	+29.83 29.28 28.72 28.17 27.61	+29.89 29.33 28.78 28.22 27.67	+29.94 29.39 28.83 28.28 27.72
T 6U	+26.67 .0	+26.72 .1	+26.78 .2	+26.83 .3	+26.89	+26.94 . 5	+27.00 .6	+27.06 . 7	+27.11 .8	+27.17 .9

			KENH		ALE	O CE	NIIGH			-
Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
+ 80° 79 78	c. +26.67 26.11 25.56	c. +26°72 26.17 25.61	c. +26°.78 26.22 25.67	c. +26.83 26.28 25.72	c. +26.89 26.33 25.78	c. +26.94 26.39 25.83	c. +27°.00 26.44 25.89	c. +27:06 26.50 25.94	c. +27:11 26.56 26.00	c. +27°.17 26.61 26.06 25.50
77	25.00	25.06	25.11	25.17	25.22	25.28	25.33	25.39	25.44	24.94
76	24.44	24.50	24.56	24.61	24.67	24.72	24.78	24.83	24.89	
+ 75 74 73 72 71	+23.89	+23.94	+24.00	+24.06	+24.11	+24.17	+24.22	+24.28	+24.33	+24.39
	23.33	23.39	23.44	23.50	23.56	23.61	23.67	23.72	23.78	23.83
	22.78	22.83	22.89	22.94	23.00	23.06	23.11	23.17	23.22	23.28
	22.22	22.28	22.33	22.39	22.44	22.50	22.56	22.61	22.67	22.72
	21.67	21.72	21.78	21.83	21.89	21.94	22.00	22.06	22.11	22.17
+ 70 69 68 67 66	+21.11 20.56 20.00 19.44 18.89	+21.17 20.61 20.06 19.50 18.94	+21.22 20.67 20.11 19.56 19.00	+21.28 20.72 20.17 19.61 19.06	+21.33 20.78 20.22 19.67 19.11		+21.44 20.89 20.33 19.78 19.22	+21.50 20.94 20.39 19.83 19.28	+21.56 21.00 20.44 19.89 19.33	+21.61 21.06 20.50 19.94 19.39
+ 65 64 63 62 61	+18.33	+18.39	+18.44	+18.50	+18.56	+18.61	+18.67	+18.72	+18.78	+18.83
	17.78	17.83	17.89	17.94	18.00	18.06	18.11	18.17	18.22	18.28
	17.22	17.28	17.33	17.39	17.44	17.50	17.56	17.61	17.67	17.72
	16.67	16.72	16.78	16.83	16.89	16.94	17.00	17.06	17.11	17.17
	16.11	16.17	16.22	16.28	16.33	16.39	16.44	16.50	16.56	16.61
+ 60 59 58 57 56	+15.56	+15.61	+15.67	+15.72	+15.78	+15.83	+15.89	+15.94	+16.00	+16.06
	15.00	15.06	15.11	15.17	15.22	15.28	15.33	15.39	15.44	15.50
	14.44	14.50	14.56	14.61	14.67	14.72	14.78	14.83	14.89	14.94
	13.89	13.94	14.00	14.06	14.11	14.17	14.22	14.28	14.33	14.39
	13.33	13.39	13.44	13.50	13.56	13.61	13.67	13.72	13.78	13.83
+55	+12.78	+12.83	+12.89	+12.94	+13.00	+13.06	+13.11	+13.17	+13.22	13.28
54	12.22	12.28	12.33	12.39	12.44	12.50	12.56	12.61	12.67	12.72
53	11.67	11.72	11.78	11.83	11.89	11.94	12.00	12.06	12.11	12.17
52	11.11	11.17	11.22	11.28	11.33	11.39	11.44	11.50	11.56	11.61
51	10.56	10.61	10.67	10.72	10.78	10.83	10.89	10.94	11.00	11.06
+50	+10.00	+10.06	+10.11	+10.17	+10.22	+10.28	+10.33	+10.39	+10.44	+10.50
49	9.44	9,50	9.56	9.61	9.67	9.72	9.78	9.83	9.89	9.94
48	8.89	8.94	9.00	9.06	9.11	9.17	9.22	9.28	9.33	9.39
47	8.33	8.39	8.44	8.50	8.56	8.61	8.67	8.72	8.78	8.83
46	7.78	7.83	7.89	7.94	8.00	8.06	8.11	8.17	8.22	8.28
+45	+ 7.22	+ 7.28	+ 7.33	+ 7.39 6.83 6.28 5.72 5.17	+ 7.44	+ 7.50	+ 7.56	+ 7.61	+ 7.67	+ 7.72
44	6.67	6.72	6.78		6.89	6.94	7.00	7.06	7.11	7.17
43	6.11	6.17	6.22		6.33	6.39	6.44	6.50	6.56	6.61
42	5.56	5.61	5.67		5.78	5.83	5.89	5.94	6.00	6.06
41	5.00	5.06	5. 11		5.22	5.28	5.33	5.39	5.44	5.50
+40 39 38 37 36	+ 4.44 3.89 3.33 2.78 2.22	+ 4.50 3.94 3.39 2.83 2.28	+ 4.56 4.00 3.44 2.89 2.33	+ 4.61 4.06 3.50 2.94 2.39	+ 4.67 4.11 3.56 3.00 2.44	4.17 3.61 3.06	+ 4.78 4.22 3.67 3.11 2.56	4.28 3.72 3.17	+ 4.89 4.33 3.78 3.22 2.67	+ 4.94 4.39 3.83 3.28 2.72
+35 34 33 32 31 +30	+ 1.11 + 0.56 0.00	+ 1.72 + 1.17 + 0.61 + 0.06 - 0.50 - 1.06	+ 1.22 + 0.67 + 0.11	+ 1.28	+ 1.33 + 0.78 + 0.22 - 0.33	+ 0.83 + 0.28 - 0.28	+ 1.44 + 0.89	+ 1.50 + 0.94 + 0.39 - 0.17	+ 2.11 + 1.56 + 1.00 + 0.44 - 0.11 - 0.67	+ 1.06 + 0.50
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9

Fahren- heit.	.0	.ì	.2	.3	.4	.5	.6	.7	.8	.9
+30° 29 28 27 26	C.	c.	c.	C.						
	- 1°11	- 1.06	- 1.00	- 0°.94	- 0.89	- 0.83	- 0°78	- 0°.72	- 0.67	- 0.61
	1.67	1.61	1.56	1.50	1.44	1.39	1.33	1.28	1.22	1.17
	2.22	2.17	2.11	2.06	2.00	1.94	1.89	1.83	1.78	1.72
	2.78	2.72	2.67	2.61	2.56	2.50	2.44	2.39	2.33	2.28
	3.33	3.28	3.22	3.17	3.11	3.06	3.00	2.94	2.89	2.83
+25	- 3.89	- 3.83	- 3.78	- 3.72	- 3.67	- 3.61	- 3.56	- 3.50	- 3.44	- 3.39
24	4.44	4.39	4.33	4.28	4.22	4.17	4.11	4.06	4.00	3.94
23	5.00	4.94	4.89	4.83	4.78	4.72	4.67	4.61	4.56	4.50
22	5.56	5.50	5.44	5.39	5.33	5.28	5.22	5.17	5.11	5.06
21	6.11	6.06	6.00	5.94	5.89	5.83	5.78	5.72	5.67	5.61
+20	- 6.67	- 6.61	- 6.56	- 6.50	- 6.44	- 6.39	- 6.33	- 6.28	- 6.22	- 6.17
19	7.22	7.17	7.11	7.06	7.00	6.94	6.89	6.83	6.78	6.72
18	7.78	7.72	7.67	7.61	7.56	7.50	7.44	7.39	7.33	7.28
17	8.33	8.28	8.22	8.17	8.11	8.06	8.00	7.94	7.89	7.83
16	8.89	8.83	8.78	8.72	8.67	8.61	8.56	8.50	8.44	8.39
+ 15	- 9.44	- 9.39	- 9.33	- 9.28	- 9.22	- 9.17	- 9.11	- 9.06	- 9.00	- 8.94
14	10.00	9.94	9.89	9.83	9.78	9.72	9.67	9.61	9.56	9.50
13	10.56	10.50	10.44	10.39	10.33	10.28	10.22	10.17	10.11	10.06
12	11.11	11.06	11.00	10.94	10.89	10.83	10.78	10.72	10.67	10.61
11	11.67	11.61	11.56	11.50	11.44	11.39	11.33	11.28	11.22	11.17
+ 10 9 7 6	12.22	-12.17	-12.11	-12.06	-12.00	—11.94	-11.89	-11.83	-11.78	-11.72
	12.78	12.72	12.67	12.61	12.56	12.50	12.44	12.39	12.33	12.28
	13.33	13.28	13.22	13.17	13.11	13.06	13.00	12.94	12.89	12.83
	13.89	13.83	13.78	13.72	13.67	13.61	13.56	13.50	13.44	13.39
	14.44	14.39	14.33	14.28	14.22	14.17	14.11	14.06	14.00	13.94
+ 5 4 3 2 1 + 0	-15.00 15.56 16.11 16.67 17.22 17.78	14.94 15.50 16.06 16.61 17.17 17.72	-14.89 15.44 16.00 16.56 17.11 17.67	14.83 15.39 15.94 16.50 17.06	-14.78 15.33 15.89 16.44 17.00	-14.72 15.28 15.83 16.39 16.94 17.50	-14.67 15.22 15.78 16.33 16.89 17.44	-14.61 15.17 15.72 16.28 16.83 17.39	-14.56 15.71 15.67 16.22 16.78 17.33	-14.50 15.06 15.61 16.17 16.72 17.28
- 0 1 2 3 4	-17.78 18.33 13.89 19.44 20.00	-17.83 18.39 18.94 19.50 20.06	-17.89 18.44 19.00 19.56 20.11	-17.94 18.50 19.06 19.61 20.17	-18.00 18.56 19.11 19.67 20.22	18.61 19.17 19.72 20.28	-18.11 18.67 19.22 19.78 20.33	-18.17 18.72 19.28 19.83 20.39	-18.22 18.78 19.33 19.89 20.44	-18.28 18.83 10.39 19.94 20.50
- 5 6 7 8 9	-20.56	-20.61	-20.67	-20.72	-20.78	-20.83	-20.89	-20.94	-21.00	-21.06
	21.11	21.17	21.22	21.28	21.33	21.39	21.44	21.50	21.56	21.61
	21.67	21.72	21.78	21.83	21.89	21.94	22.00	22.06	22.11	22.17
	22.22	22.28	-22.33	22.39	22.44	22.50	22.56	22.61	22.67	22.72
	22.78	22.83	22.89	22.94	23.00	23.06	23.11	23.17	23.22	23.28
- 10 11 12 13 14	-23.33 23.89 24.44 25.00 25.56	-23.39 23.94 24.50 25.06 25.61	-23.44 24.00 24.56 25.11 25.67	-23.50 24.06 24.61 25.17 25.72	-23.56 24.11 24.67 25.22 25.78	24.17 24.72 25.28 25.83	-23.67 24.22 24.78 25.33 25.89	-23.72 24.28 24.83 25.39 25.94	-23.78 24.33 24.89 25.44 26.00	-23.83 24.39 24.94 25.50 26.06
- 15 16 17 18 19 -20	-26.11 26.67 27.22 27.78 28.33 -28.89	-26.17 26.72 27.28 27.83 28.39 -28.94	-26.22 26.78 27.33 27.89 28.44 -29.00	-26.28 26.83 27.39 27.94 28.50 -29.06	-26.33 26.89 27.44 28.00 28.56 -29.11	-26.39 26.94 27.50 28.06 28.61 -29.17	-26.44 27.00 27.56 28.11 28.67 -29.22	-26.50 27.61 28.17 28.72 -29.28	-26.56 27.11 27.67 28.22 28.78 -29.33	-26.61 27.17 27.72 28.28 28.83 -29.39
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9

r —	-				JALE	O CE	NIIGH			
Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	c.	c.	c.	c.	c.	c.	c.	С.	c.	c.
-20°	-28.89	-28.94	-29 00	29.06	-29°11	-20°17	-29°22	-29.28	-29°33	-29°39
21	29.44	29.50	29.56	29.61	29.67	29.72	29.78	29.83	29.89	29.94
22	30.00	30.06	30.11	30.17	30.22		30.33	30.39	30.44	30.50
23	30.56	30.61	30.67	30.72	30.78		30.89	30.94	31.00	31.06
24	31.11	31.17	31.22	31.28	31.33	31.39	31.44	31.50	31.56	31.61
-25	-31.67	-31.72	-31.78	-31.83	31.89	- 31.94	-32.00	-32.06	-32.11	-32.17
26	32.22	32.28	32.33	32.39	32.44		32.56	32,61	32.67	32.72
27	32.78	32.83	32.89	32.94	33.00		33.11	33.17	33.22	33.28
28	33.33	33.39	33.44	33.50	33.56		33.67	33.72	33.78	33.83
29	33.89	33.94	34.00	34.06	34.11	34.17	34.22	34.28	34.33	34-39
–30	-34-44	-34.50	- 34.56	-34.6 1	- 34.67	-34.72	-34.78	-34.83	-34.89	-34.94
31	35.00	35.06	35.11	35-17	35.22	35.28	35-33	35.39	35.44	35.50
32	35.56	35.61	35.67	35.72	35.78	35.83	35.89	35.94	36.00	36.06
33 34	36.11 36.67	36.17 36.72	36.22 36.78	36.28 36.83	36.33 36.89		36.44 37.00	36.50	36.56	36,61
11 1					ا آ	0).		37.06	37.11	37.17
-35	-37.22	-37.28	-37.33	-37.39	-37.44	-37.50	-3 7.56	-37.6 1	-37.67	-37.72
36	37.78	37.83	37.89	37.94	38.00		38.11	38.17	38.22	38.28
37 38	38.33 38.89	38.39 38.94	38.44 39.00	38.50 39.06	38.56	38.61 39.17	38.67	38.72 39.28	38.78	38.83
39	39.44	39.50	39.56	39.61	39.11 39.67	39.72	39.22 39.78	39.83	39·33 39·89	39·39 39·94
								1		
-40	-40.00	-40.06	-40.11	-40.17			-40.33	-40.39	-40.44	-40.50
41 42	40.56 41.11	40.61	40.67 41.22	40.72 41.28	40.78	40.83	40.89	40.94	41.00	41.06
43	41.67	41.72	41.78	41.83	41.33 41.89		41.44 42.00	41.50 42.06	41.56 42.11	41.61 42.17
44	42.22	42.28	42.33	42.39	42.44		42.56	42.61	42.67	42.72
-45	40.79	40.00								
-45 46	-42.78 43.33	-42.83	-42.89				- 43.11 43.67	-43.17	-43.22	-43.2 ⁹
	43.89	43-39 43-94	43.44 44.00	43.50 44.06	43.56 44.11	44.17	44.22	43.72 44.28	43.78 44.33	43.83 44.39
47 48	44.44	44.50	44.56	44.61	44.67	44.72	44.78	44.83	44.89	44.94
49	45.00	45.06	45.11	45.17	45.22		45.33	45.39	45-44	45.50
-50	-45.56	-45.6 1	-45.67	-45.72	-45.78	-45.83	-45. 89	-45 •94	-46.00	-46. 06
51	46.11	46.17	46.22	46.28	46.33	46.39	46.44	46.50	46.56	46.61
52	46.67	46.72	46.78	46.83	46.89		47.00	47.06	47.11	47.17
53	47.22	47.28	47.33	47.39	47.44		47.56	47.61	47.67	47.72
54	47.78	47.83	47.89	47-94	48.00	48.06	48.11	48.17	48.22	48.28
-55	-48.33	-48.39	-48.44	-48.5 0	-48.56	- 48.61	-48.67	-48.72	-48.78	-48.83
56	48.89	48.94	49.00	49.06	49.11	49.17	49.22	49.28	49.33	49.39
57	49.44	49.50	49.56	49.61	49.67	49.72	49.78	49.83	49.89	49.94
58	50.00	50.06	50.11	50.17	50.22		50.33	50.39	50.44	50.50
59	50.56	50.61	50.67	50.72	50.78	50.83	50.89	50.94	51.00	51.06
–60	-51.11	-51.17	-51.22	-51.28	-51.33	-51.39	-51.44	-51.50	-51.56	- 51.61
67	51.67	51.72	51.78	51.83	51.89	51.94	52.00	52.06	52.11	52.17
62	52.22	52.28	52.33	52.39	52.44	52.50	52.56	52.61	52.67	52.72
63	52.78	52.83	52.89	52.94	53.00	53.06	53.11		53.22	53.28
64	53-33	53-39	53-44	53.50	53.56	53.61	53.67	53.72	53.78	53.83
–65	-53.89	-53.94	-54.00	-54. 06	-54.11	-54.17	-54.22	-54.28	-54-33	-54.39
66	54.44	54.50	54.56	54.61	54.67	54.72	54.78	54.83	54.89	54.94
67	55.00	55.06	55.11	55.17	55.22	55.28	55-33	55:39	55.44	55.50
68	55.56	55.61	55.67	55.72	55.78	55.83	55.89	55.94	56.00	56.06
69	56.11	56.17	56.22	56.28	56.33	56.39	56.44	56.50	56.56	56.61
-70	- 56.67	-56.72	-56.78	- 56.83	- 56.89	-56.94	−57.00	-57.06	-57.11	-57.17
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
1	<u> </u>									

T										
Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
700	C.	C.	C.	C.	C.	C.	C.	C.	C.	C. -57.17
-70°	-56°.67	-56.72 57.28	−56.78 57·33	-56:83 57-39	-56°.89	-56°.94 57.50	−57.°30 57.56	-57.°06 57.61	-57.°11 57.67	57.72
71 72	57.78	57.83	57.89	57·94	58.00	58.06	58.11	58.17	58.22	58.28
73	58.33	58.39	58.44	58.50	58.56	58.61	58.67	58.72	58.78	58.83
74	58.89	58.94	59.00	59.06	59.11	59.17	59.22	59.28	59.33	59.39
-75 -6	-59.44	-59.50	-59.56	-59.61	-59.67	-59.72	-59.78	-59.83	-59.89	-59.94
76 77	60.56	60.06 60.61	60.11 60.67	60.17 60.72	60.22 60.78	60,28 60,83	60.33 60.89	60.39 60.94	60.44 61.00	60.50 61.06
78	61.11	61.17	61.22	61.28	61.33	61.39	61.44	61.50	61.56	61.61
79	61.67	61.72	61.78	61.83	61.89	61.94	62.00	62.06	62.11	62.17
-80	-62.22	-62.28	-62.33	-62.39	-62.44	-62.50	-62.56	-62.61	-62.67	-62.72
81	62.78	62.83	62.89	62.94	63.00	63.06	63.11	63.17	63.22	63.28
8 ₂ 8 ₃	63.33 63.89	63.39 63.94	63.44	63.50 l 64.06	63.56 64.11	63.61 64.17	63.67 64.22	63.72 64.28	63.78 64.33	63.83 64.39
84	64.44	64.50	64.56	64.61	64.67	64.72	64.78	64.83	64.89	64.94
-85	-65.00	-65.06	-65.11	-65.17	-65.22	-65.28	-65.33	-65.39	-65.44	-65.50
86	65.56	65.61	65.67	65.72	65.78	65.83	65.89	65.94	66.00	66.06
87	66.11	66.17	66.22	66.28	66.33	66.39	66.44	66.50	66.56	66.61
88 89	66.67 67.22	66.72 67.28	66.78 67.33	66.83 67.39	66 . 89	66.94 67.50	67.00 67.56	67.06 67.61	67.11 67.67	67.17 67.72
-90	-67.78	-67.83	-67.8g	-67.94	68.00	-68.06	-68.11	-68.17	-68.22	-68.28
91	68.33	68.39	68.44	68.50	68.56	68.61	68.67	68.72	68.78	68.83
92	68.89	68.94	69.00	69.06	69.11		69.22	69.28	69.33	69.39
93	69.44	69.50	69.56	69.61	69.67	69.72 70.28	69.78	69.83 70.39	69.89 70.44	69.94 70.50
94	70.00	70.06	70.11	70.17		,				
-95 96	-70.56	-70.61	-70.67 71.22	-70.72 71.28	-70.78	-70.83 71.39	-70.89 71.44	-70.94 71.50	-71.00 71.56	-71.06 71.61
97	71.11 71.67	71.17 71.72	71.78	71.83	71.33	71.94	72.00	72.06	72.11	72.17
98	72.22	72.28	72.33	72.39	72.44		72.56	72.61	72.67	72.72
99	72.78	72.83	72.89	72.94	73.00	73.06	73.11	73.17	73.22	73.28
-100	-73·33	-73.39	-73.44	-73.50	-73.56	-73.61	-73.67 74.22	-73.72 74.28	-73.78	-73.83
101	73.89 74.44	73.94 74.50	74.00 74.56	74.06 74.61	74.11 74.67	74.17 74.72	74.78	74.28	74.33 74.89	74·39 74·94
103	75.00	75.06	75.11	75.17	75.22	75.28	75-33	75.39	75.44	75.50
104	75.56	75.61	75.67	75.72	75.78	75.83	75.89	75.94	76.00	76.06
-105	-76.11	-76.17	-76.22	-76.28	-76.33	-76.39	-76.44	-76.50	-76.56	-76.61
106	76.67	76.72 77.28	76.78 77.33	76.83 77.39	76.89 77.44	76.94 77.50	77.00 77.56	77.06 77.61	77.11 77.67	77.17 77.72
107	77.22 77.78	77.26	77.89	77.39	78.00	78.06	78.11	78.17	78.22	78.28
100	78.33	78.39	78.44	78.50	78.56	78.61	78.67	78.72	78.78	78.83
-110	-78.89	-78.94	-79.00	-79.06	-79.11		-79.22	-79.28	-79-33	-79.39
111	79.44	79.50	79.56	79.61	79.67	79.72	79.78	79.83	79.89	79.94
112	80.00	80.06 80.61	80.11 80.67	80.17	80.22 80.78	80.28 80.83	80.33 80.89	80.39 80.94	80.44 81.00	80.50 81.06
113	80.56 81.11	81.17	81.22	81.28	81.33	81.39	81.44	81.50	81.56	81.61
-115	-81.67	-81.72	-81.78	-81.83	-81.89	-81.94	-82.00	-82.06	-82.11	-82.17
116	82.22	82.28	82.33	82.39	82.44		82.56	82.61	82.67	82.72
117	82.78	82.83	82.89	82.54	83.00		83.11	83.17	83.22	83.28
118	83.33	83.39	83.44	83.50 84.06	83.56 84.11		83.67	83.72 84.28	83.78	83.83 84.39
119	83.89	83.94				-84.72	-84.78	-84.83	-84.89	-84.94
-120	-84.44	-84.50	-84.56	-84.61	<u>-84.67</u>	-04.72	.6	-04.03 . 7	-04.09	-04.94 .9
	.0	1.1	.2	.3	.4	1 .5				.9

CENTIGRADE SCALE TO FAHRENHEIT.

Centi-	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
grade.										———— F.
+60°	F. +140°00	F. +140°18	F. +140°26	F. +140°54	F. +140°72	F. +t40°00	F. +141.08	+141°26	+141.44	
50	138.20	138.38	138.56	138.74	138.92	139.10	139.28	139.46	139.64	139.02
59 58	136.40		136.76	136.94					137.84	
57	134.60	134.78	134.96	135.14	135.32		135.68	135.86		
56	132.80	132.98	133.16	133.34	133.52	133.70	133.88	134.06	134.24	134.42
+55	+131.00	+131.18	+131.36	+131.54	+131.72	+131.90	+132.08	+132.26	+132.44	+132.62
54	129.20	129.38	129.56	129.74	129.92	130.10	130.28	130.40	130.04	130.82
53	127.40			127.94						129.02
52 51	125.60 123.80									125.42
II I	l * '							` -		- 1
							+123.08	+123.26	+123.44 121.64	+123.62 121.82
49	120.20 118.40	120.38 118.58	120.56 118.76	120.74	120.92 119.12	121.10	121.28	121.46 119.66		120.02
48 47	116.40		116.70	118.94 117.14						118.22
46	114.80			115.34						116.42
il .							•			1 77 . 6
			+113.36				+114.08	T114.20	+114.44 112.64	+114.62 112.82
44	111.20	111.38	111.56 109.76	111.74		112.10				111.02
43 42	109.40 107.60			109.94						100.22
41	105.80				106.52					107.42
1 40		1 - 0 4 - 78	1 704 06	1.504.54	J. T. O. 4.70	+ 104.00	1 TOT 08	±105 26	+105 44	+105.62
+40	102.20		102.56	102.74		103.10	103.28	103.46	103.44	103.82
39 38	100.40			100.94				101.66		102.02
37	98.60			99.14			99.68	99.86	100.04	100.22
36	96.80	96.98	97.16	97.34	97.52	97.70	97.88	98.06	98.24	98.42
+35	+ 95.00	+ 95.18	+ 95.36	+ 95.54	+ 95.72	+ 95.90	+ 96.08	+ 96.26	+ 96.44	+ 96.62
34	93.20		93.56	93.74	93.92	94.10	94.28	94.46	94.64	94.82
33	91.40		91.76	91.94	92.12				92.84	93.02
32	89.60		89.96 88.16	90.14			90.68 88.88	90.86 89.06	91.04 89.24	91.22 89.42
31	87.80	87.98	55,10	88.34	00.52	00.70	00.00	9.00	09.24	09.42
t I										+ 87.62
29	84.20	84.38		84.74		85.10				85.82
28 27	82.40 80.60	82.58 80.78	82.76 80.96	82.94 81.14	83.12 81.32					
26	78.80			79.34						
	1	, ,								
+25	+ 77.00		+ 77.36		+ 77.72					
24	75.20 73.40	75.38 73.58	75.56 73.76	75·74 73·94						
23 22	71.60		71.96	73.94						
21	69.80		70.16	70.34						
+20	+ 68.00	± 68.±8	+ 68.26	+ 68.54	+ 68 72	+ 68 00	+ 60.08	+ 60.26	+ 60 44	+ 69.62
10	66.20	66.38	66.56	66.74	66.92	67.10				
18	64.40		64.76	64.94	65.12	65.30	65.48	65.66		
17	62.60	62.78	62.96	63.14		63.50	63.68	63.86	64.04	64.22
16	60.80	60.98	61.16	61.34	61.52	61.70	61.88	62.06	62.24	62.42
+15	+ 59.00	+ 59.18	+ 59.36	+ 59.54	+ 59.72	+ 59.00	+ 60.08	+ 60.26	+ 60.44	+ 60.62
14	57.20	57.38	57.56	57.74	57.92	58.10	58.28	58.46	58.64	58.82
13	55.40	55.58	55.76	55.94						
12 11	53.60 51.80			54.14 5 2.34						
	i -				l		*	"	1	
+10	+ 50.00	+ 50.18	+ 50.36	+ 50.54	+ 50.72	+ 50.90	+ 51.08	+ 51.26	+ 51.44	+ 51.62
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9

CENTIGRADE SCALE TO FAHRENHEIT.

Genti- grade.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
+10°	F. +50.∞	F. +50 . 18	F. +50°.36	F. +50°.54	F. +50°∙72	F. +50.90	F. +51 .0 8	F. +51.26	F. +51,44	F. +51.62
+ 9 7 6 5	+48.20 46.40 44.60 42.80 41.00	+48.38 46.58 44.78 42.98 41.18	+48.56 46.76 44.96 43.16 41.36	+48.74 46.94 45.14 43.34 41.54	+48.92 47.12 45.32 43.52 41.72	+49.10 47.30 45.50 43.70 41.90	+49.28 47.48 45.68 43.88 42.08	+49.46 47.66 45.86 44.06 42.26		+49.82 48.02 46.22 44.42 42.62
+ 4 3 2 1 + 0	+39.20 37.40 35.60 33.80 32.00	+39.38 37.58 35.78 33.98	+39.56 37.76 35.96 34.16 32.36	+39.74 37.94 36.14 34.34 32.54	+39.92 38.12 36.32 34.52 32.72	+40.10 38.30 36.50		+40.46 38.66 36.86 35.06 33.26	+40.64 38.84 37.04 35.24	+40.82 39.02 37.22 35.42 33.62
- 0 1 2 3 4	+32.00 30.20 28.40 26.60 24.80	30.02 28.22 26.42	+31.64 29.84 28.04 26.24 24.44	+31.46 29.66 27.86 26.06 24.26	+31.28 29.48 27.68 25.88 24.08	+31.10 29.30 27.50 25.70 23.90		+30.74 28.94 27.14 25.34 23.54		+30.38 28.58 26.78 24.98 23.18
- 5 6 7 8 9	+23.00 21.20 19.40 17.60 15.80	21.02 19.22 17.42	+22.64 20.84 19.04 17.24 15.44	+22.46 20.66 18.86 17.06 15.26	+22.28 20.48 18.68 16.88	+22.10 20.30 18.50 16.70 14.90	+21.92 20.12 18.32 16.52 14.72	+21.74 19.94 18.14 16.34 14.54	+21.56 19.76 17.96 16.16 14.36	+21.38 19.58 17.78 15.98 14.18
-10 11 12 13 14	+14.00 12.20 10.40 8.60 6.80	12.02 10.22 8.42	+13.64 11.84 10.04 8.24 6.44	+13.46 11.66 9.86 8.06 6.26	+13.28 11.48 9.68 7.88 6.08	+13.10 11.30 9.50 7.70 5.90	+12.92 11.12 9.32 7.52 5.72	+12.74 10.94 9.14 7.34 5.54	+12.56 10.76 8.96 7.16 5.36	+12.38 10.58 8.78 6.98 5.18
-I5 16 17 18	+ 5.00 + 3.20 + 1.40 - 0.40 - 2.20	+ 3.02 + 1.22 - 0.58	+ 4.64 + 2.84 + 1.04 - 0.76 - 2.56	+ 4.46 + 2.66 + 0.86 - 0.94 - 2.74	+ 4.28 + 2.48 + 0.68 - 1.12 - 2.92	+ 4.10 + 2.30 + 0.50 - 1.30 - 3.10		+ 3.74 + 1.94 + 0.14 - 1.66 - 3.46	+ 3.56 + 1.76 - 0.04 - 1.84 - 3.64	+ 3.38 + 1.58 - 0.22 - 2.02 - 3.82
-20 21 22 23 24	- 4.00 5.80 7.60 9.40 11.20	5.98 7.78 9.58	- 4.36 6.16 7.96 9.76 11.56	- 4.54 6.34 8.14 9.94 11.74	- 4.72 6.52 8.32 10.12 11.92	- 4.90 6.70 8.50 10.30 12.10	- 5.08 6.88 8.68 10.48 12.28	- 5.26 7.06 8.86 10.66 12.46	- 5.44 7.24 9.04 10.84 12.64	- 5.62 7.42 9.22 11.02 12.82
-25 26 27 28 29	-13.00 14.80 16.60 18.40 20.20	14.98 16.78 18.58	-13.36 15.16 16.96 18.76 20.56	-13.54 15.34 17.14 18.94 20.74	-13.72 15.52 17.32 19.12 20.92	15.70 17.50 19.30	-14.08 15.88 17.68 19.48 21.28	-14.26 16.06 17.86 19.66 21.46	-14.44 16.24 18.04 19.84 21.64	-14.62 16.42 18.22 20.02 21.82
- 30 31 32 33 34	-22.00 23.80 25.60 27.40 29.20	23.98 25.78 27.58	25.96 27.76	24.34 26.14 27.94	-22.72 24.52 26.32 28.12 29.92	26.50 28.30	-23.08 24.88 26.68 28.48 30.28	-23.26 25.06 26.86 28.66 30.46	-23.44 25.24 27.04 28.84 30.64	-23.62 25.42 27.22 29.02 30.82
- 35 36 37 38 39	-31.00 32.80 34.60 36.40 38.20	32.98 34.78 36.58	-31.36 33.16 34.96 36.76 38.56		-31.72 33.52 35.32 37.12 38.92	33.70 35.50 37.30	-32.08 33.88 35.68 37.48 39.28	-32.26 34.06 35.86 37.66 39.46	-32.44 34.24 36.04 37.84 39.64	-32.62 34.42 36.22 38.02 39.82
-40	-40.00 .0	-40.18	-40.36 .2	-4°.54	-40.72	-40.90 .5	-41.08 .6	-41.26 - 7	-41.44 .8	-41.62 .9

CENTIGRADE SCALE TO FAHRENHEIT.

Centi- grade.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.
– 40°	– 4°°.∞	- 40°.18	- 40°.36	- 40°.54	- 40°.72	– 4 0 .90	- 41°.08	- 41.26		- 41°.62
41	41.80	41.98	42.16	42.34	42.52	42.70	42.88	43.06	43.24	43.42
42	43.60		43.96	44.14	44-32			44.86	45.04	45.22
43	45.40						46.48 48.28	46.66 48.46	46.84 48.64	47.02 48.82
44	47.20	47.38	47.56	47.74	47.92	48.10	40.20	40.40	40.04	40.02
- 45	- 49.00		- 49.36	- 49.54	- 49.72			- 50.26		- 50.62
46	50.80		51.16	51.34	51.52	51.70	51.88	52.06	52.24	52.42
47	52.60		52.96	53.14	53.32	53.50	53.68	53.86	54.04 55.84	54.22 56.02
48 49	54.40 56.20		54.76 56.56	54.94 56.74	55.12 56.92		55.48 57.28	55.66 57.46	57.64	57.82
ļ	30.20									
- 50	- 58.00		- 58.36				- 59.08	- 59.26	- 59.44	- 59.62
51	59.80	59.98	60.16	60.34	60.52	60.70	60.88 62.68	61.06 62.86	61.24 63.04	61.42
52	61.60 63.40		61.96 63.76	62.14 63.94	62.32 64.12	62.50 64.30	64.48	64.66	64.84	65.02
53 54	65.20		65.56	65.74	65.92		66.28	66.46	66.64	66.82
								· '		60.6
- 55	- 67.00							- 68.26	- 68.44	- 68.62
56	68.80	/_	69.16	69.34	69.52	69.70	69.88 71.68	70.06 71.86	70.24 72.04	70.42
57 58	70.60 72.40		70.96 72.76	71.14 72.94	71.32 73.12	71.50 73.30	73.48	73.66	73.84	74.02
59	74.20		74.56		74.92		75.28	75.46	75.64	75.82
- 60	- 76.00				- 76.72		- 77.08	- 77.26	- 77.44	- 77.62
61	77.80		78.16		78.52	78.70	78.88	79.06	79.24	79.42 81.22
62 63	79.60 81.40		79.96 81.76	80.14 81.04	80.32 82.12	80.50 82.30	82.48	80.86 82.66	81.04 82.84	83.02
64	83.20		83.56	83.74	83.92		84.28	84.46	84.64	84.82
			1	-						
- 65	- 85.00		- 85.36		- 85.72		- 86.08	- 86.26	- 86.44	- 86.62
66	86.8o		87.16		87.52	87.70	87.88	88.06	88.24	88.42
67 68	88.60 90.40		88.96 90.76	89.14 90.94	89.32	89.50 91.30	89.68 91.48	89.86 91.66	90.04	90.22
69	90.40		92.56				93.28	93.46	93.64	93.82
- 70	- 94.00	- 94.18	- 94.36			- 94.90	- 95.08	- 95.26	- 95.44	- 95.62
71	95.80					96.70 98.50	96.88 98.68	97.06 98.86	97.24 99.04	97.42 99.22
72 73	97.60 99.40		97.96 99.76		, ,		100.48	100.66	100.84	101.02
74	101.20		101.56		101.92		102.28	102.46	102.64	102.82
			_							
- 75	-103.00				-103.72			-104.26 106.06	-104.44	106.42
76	104.80 106.60		105.16 106.96	105.34	105.52 107.32	105.70	105.88		106.24	100.42
77 78	108.40		108.76		107.32	107.30	' -	100.66	100.84	110.02
79	110.20		110.56		110.92	111.10	111.28	111.46	111.64	111.82
			****				TT0 60			
- 80	-112.00 113.80		-112.36 114.16					-113.26 115.06	-113.44 115.24	-113.62 115.42
82	113.60		114.10				114.68	116.86	115.24	117.22
83	117.40								118.84	119.02
84	119.20		119.56					120.46	120.64	120.82
0.5			_ 101 06	- 121 5	_ 101 55	_ Tat a-	0	_ 122.04		T02 62
- 85 86	→121.00 122.80		-121.36 123.16		-121.72 123.52		-122.08 123.88		-132.44 124.24	-122.62 124.42
87	122.60									
88	126.40									
89	128.20				128.92					129.82
- 90	-130.00	-130.18	-130.36	-130.54	-130.72	-130.90	-131.08	-131.26	-131.44	-131.62
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
L	<u>u</u>	. 1		3	• •			1 •/		

Table 4. CENTIGRADE SCALE TO FAHRENHEIT - Near the Boiling Point.

Centi- grade.	۰.0	.1	.2	.з	.4	.5	.6	.7	.8	.9
100° 99	F. 212.00 210.20	F. 212°18 210.38	F. 212°36 210.56	F. 212.54 210.74	F. 212.72 210.92	F. 212.90 211.10	F. 213.08 211.28	F. 213.26 211.46	F. 213.44 211.64	F. 213.62 211.82
98	208.40	208.58	208.76	208.94	209.12	209.30	209.48	209.66	209.84	210.02
97	206.60	206.78	206.96	207.14	207.32	207.50	207.68	207.86	208.04	208.22
96	204.80	204.98	205.16	205.34	205.52	205.70	205.88	206.06	206.24	206.42
95	203.00	203.18	203.36	203.54	203.72	203.90	204.08	204.26	204.44	204.62
94	201.20	201.38	201.56	201.74	201.92	202.10	202.28	202.46	202.64	202.82
93	199.40	199.58	199.76	199.94	200.12	200.30	200.48	200.66	200.84	201.02
92	197.60	197.78	197.96	198.14	198.32	198.50	198.68	198.86	199.04	199.22
91	195.80	195.98	196.16	196.34	196.52	196.70	196.88	197.06	197.24	197.42
90	194.00	194.18	194.36	194.54	194.72	194.90	195.08	195.26	195.44	195.62

TABLE 5. DIFFERENCES FAHRENHEIT TO DIFFERENCES CENTIGRADE.

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
0° 1 2 3 4	C. 0.00 0.56 I.II 1.67 2.22	c. o.o6 o.61 I.17 1.72 2.28	c. 0.11 0.67 1.22 1.78 2.33	c. 0.17 0.72 1.28 1.83 2.39	C. 0.22 0.78 1.33 1.89 2.44	c. o.28 o.83 1.39 1.94 2.50	c. 0°33 0.89 1.44 2.00 2.56	c. 0°39 0.94 1.50 2.06 2.61	C. 0.44 1.00 1.56 2.11 2.67	c. 0°50 1.06 1.61 2.17 2.72
5 6 7 8	2.78 3.33 3.89 4.44 5.00	2.83 3.39 3.94 4.50 5.06	2.89 3.44 4.00 4.56 5.11	2.94 3.50 4.06 4.61 5.17	3.00 3.56 4.11 4.67 5.22	3.06 3.61 4.17 4.72 5.28	3.11 3.67 4.22 4.78 5.33	3.17 3.72 4.28 4.83 5.39	3.22 3.78 4.33 4.89 5.44	3.28 3.83 4.39 4.94 5.50
10 11 12 13 14	5.56 6.11 6.67 7.22 7.78	5.61 6.17 6.72 7.28 7.83	5.67 6.22 6.78 7.33 7.89	5.72 6.28 6.83 7.39 7.94	5.78 6.33 6.89 7.44 8.00	5.83 6.39 6.94 7.50 8.06	5.89 6.44 7.00 7.56 8.11	5.94 6.50 7.06 7.61 8.17	6.00 6.56 7.11 7.67 8.22	6.06 6.61 7.17 7.72 8.28
15 16 17 18 19 20	8.33 8.89 9.44 10.00 10.56	8.39 8.94 9.50 10.06 10.61	8.44 9.00 9.56 10.11 10.67	8.50 9.06 9.61 10.17 10.72 11.28	8.56 9.11 9.67 10.22 10.78 11.33	8.61 9.17 9.72 10.28 10.83	8.67 9.22 9.78 10.33 10.89	8.72 9.28 9.83 10.39 10.94	8.78 9.33 9.89 10.44 11.00 11.56	8.83 9.39 9.94 10.50 11.06

TABLE 6. DIFFERENCES CENTIGRADE TO DIFFERENCES FAHRENHEIT.

Centi- grade.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
0° 1 2 3 4	F.									
	0.00	0.18	0°.36	0°54	0.72	0.90	1.08	1°26	1°44	1°62
	1.80	1.98	2.16	2.34	2.52	2.70	2.88	3.06	3.24	3.42
	3.60	3.78	3.96	4.14	4.32	4.50	4.68	4.86	5.04	5.22
	5.40	5.58	5.76	5.94	6.12	6.30	6.48	6.66	6.84	7.02
	7.20	7.38	7.56	7.74	7.92	8.10	8.28	8.46	8.64	8.82
5	9.00	9.18	9.36	9.54	9.72	9.90	10.08	10.26	10.44	10.62
6	10.80	10.98	11.16	11.34	11.52	11.70	11.88	12.06	12.24	12.42
7	12.60	12.78	12.96	13.14	13.32	13.50	13.68	13.86	14.04	14.22
8	14.40	14.58	14.76	14.94	15.12	15.30	15.48	15.66	15.84	16.02
9	16.20	16.38	16.56	16.74	16.92	17.10	17.28	17.46	17.64	17.82

CORRECTION FOR THE TEMPERATURE OF THE EMERGENT MERCURIAL COLUMN OF THERMOMETERS.

 $T=t-0.000086 \ n(t'-t)$ — Fahrenheit temperatures. $T=t-0.000155 \ n(t'-t)$ — Centigrade temperatures. T= Corrected temperature.

t =Observed temperature. t' = Mean temperature of the glass stem and emergent mercury column.

n = Length of mercury in the emergent stem in scale degrees.

 $\left\{\frac{\text{higher}}{t_{\text{const}}}\right\}$ than t the numerical correction is to be $\left\{\frac{\text{subtracted.}}{t_{\text{const}}}\right\}$ When t' is

TABLE 7. CORRECTION FOR FAHRENHEIT THERMOMETERS.

Values of $0.000086 \cdot n(t'-t)$

n					t'-t					
	10°	20°	30°	40°	50°	60°	70°	80°	90°	100°
F.	F,	F.	F.	F.	F.	* F.	F.	F.	F.	F.
100	10.0	0.02	0.03	0.03	0.04	0.05	o:°06	0.07	0.08	ဝ.၀၀
20	0.02	0.03	0.05	0.07	0.00	0.10	0.12	0.14	0.15	0.17
30	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.21	0.23	0.26
40	0.03	0.07	0.10	0.14	0.17	0.21	0.24	0.28	0.31	0.34
50	0.04	0.09	0.13	0.17	0.22	0.26	0.30	0.34	0.39	0.43
60	0.05	0.10	0.15	0.21	0.26	0.31	0.36	0.41	0.46	0.52
70	0.06	0.12	0.18	0.24	0.30	0.36	0.42	0.48	0.54	0.60
80	0.07	0.14	0.21	0.28	0.34	0.41	0.48	0.55	0.62	0.69
90	0.08	0.15	0.23	0.31	0.39	0.46	0.54	0.62	0.70	0.77
100	0.09	0.17	0.26	0.34	0.43	0.52	0.60	0.69	0.77	0.86
110	0.00	0.10	0.28	0.38	0.47	0.57	0.66	0.76	0.85	0.95
120	0.10	0.21	0.31	0.41	0.52	0.62	0.72	0.83	0.93	1.03
130	11.0	0.22	0.34	0.45	0.56	0.67	0.78	0.90	1.01	1.12

TABLE 8. CORRECTION FOR CENTIGRADE THERMOMETERS.

Values of 0.000155 n(t'-t)

n				t'-t				
	1 O°	20°	30°	40°	50°	60°	·70°	80°
С.	c.	c.	c.	c.	c.	c.	c.	c.
100	0.02	o:°o3	0.05	0.06	80.0	0.09	0.11	0.12
20	0.03	0.06	0.09	0.12	0.16	0.19	0.22	0.25
30	0.05	0.09	0.14	0.19	0.23	0.28	0.33	0.37
40	0.06	0.12	0.19	0.25	0.31	0.37	0.43	0.50
50	0.08	0.16	0.23	0.31	0.39	0.46	0.54	0.62
60	0.00	0.10	0.28	0.37	0.46	0.56	0.65	0.74
	0.11	0.22	0.33	0.43	0.54	0.65	0.76	0.87
70 80	0.12	0.25	0.37	0.50	0.62	0.74	0.87	0.99
90	0.14	0.28	0.42	0.56	0.70	0.84	0.98	1.12
100	0.16	0.31	0.46	0.62	0.78	0.93	1.08	1.24

SMITHSONIAN TABLES.

. CONVERSIONS INVOLVING LINEAR MEASURES.

Inches into millimeters		•	•	•	•	•	•	•				TABLE 9
Millimeters into inches								•				TABLE 10
Barometric inches into	mil	liba	ars									TABLE 11
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Meters into feet								•				Table 14
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Kilometers into miles												TABLE 16
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Continental measures of		_									_	T
equivalents												I ABLE 18

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
0.00	0.00	0.25	0.51	0.76	1.02	1.27	1.52	1.78	2.03	2.29
0.10 0.20	2.54 5.08	2.79	3.05	3.30	3.56 6.10	3.81	4.06 6.60	4.32 6.86	4.57	4.83
0.30	7.62	5.33 7.87	5.59 8.13	5.84 8.38	8.64	6.35 8.89	9.14	9.40	7.11 9.65	7.37 9.91
0.40	10.16	10.41	10.67	10.92	11.18	11.43	11.68	11.94	12.19	12.45
0.50	12.70	12.95	13.21	13.46	13.72	13.97	14.22	14.48	14.73	14.99
0.60	15.24	15.49	15.75	16.00	16.26	16.51	16.76	17.02	17.27	17.53
0.70	17.78	18.03	18.29	18.54	18.80	19.05	19.30	19.56	19.81	20.07
0.80	20,32	20.57	20.83	21.08	21.34	21.59	21.84	22.10	22.35	22.61
0.90	22.86	23.11	23.37	23.62	23.88	24.13	24.38	24.64	24.89	25.15
1.00	25.40	25.65	25.91	26.16	26.42	26.67	26.92	27.18	27.43	27.69
I.IO I.20	27.94 30.48	28.19	28.45 30.99	28.70	28.96	29.21	29.46	29.72 32.26	29.97	30.23
1.30	33.02	33.27	33.53	33.78	31.50	31.75	32.00	34.80	32.51 35.05	32.77 35.31
1.40	35.56	35.81	36.07	36.32	36.58	36.83	37.08	37.34	37.59	37.85
1.50	38.10	38.35	38.61	38.86	39.12	39-37	39.62	39.88	40.13	40.39
1.60	40.64	40.89	41.15	41.40	41.66	41.91	42.16	42.42	42.67	42.93
1.70	43.18	43.43	43.69	43.94	44.20	44.45	44.70	44.96	45.21	45.47
1.80 1.90	45.72 48.26	45.97 48.51	46.23	46.48	46.74	46.99	47.24	47.50	47.75	48.01
-			1	49.02	1	49.53	49.78	50.04	50.29	50.55
2.00 2.10	50.80	51.05	51.31	51.56	51.82	52.07	52.32	52.58	52.83	53.09
2.20	53.34 55.88	53.59 56.13	53.85	54.10	54.36	54.61 57.15	54.86	55.12 57.66	55.37	55.63 58.17
2.30	58.42	58.67	58.93	59.18	59.44	59.69	59.94	60.20	57.91 60.45	60.71
2.40	60.96	61.21	61.47	61.72	61.98	62.23	62.48	62.74	62.99	63.25
2.50	63.50	63.75	64.01	64.26	64.52	64.77	65.02	65.28	65.53	65.79
2.60	66.04	66.29	66.55	66.8o	67.06	67.31	67.56	67.82	68.07	68.33
2.70 2.80	68.58	68.83	69.09	69.34	69.60	69.85	70.10	70.36	70.61	70.87
2.90	71.12 73.66	71.37 73.91	71.63 74.17	71.88 74.42	72.14	72.39 74.93	72.64	72.90 75.44	73.15	73.41
3.00	76.20	76.45	76.71	76.96	-			_	75.69	75.95
3.10	78.74	78.99	79.25	79.50	77.22	77.47 80.01	77.72 80.26	77.98 80.52	78.23 80.77	78.49 81.03
3.20	81.28	81.53	81.79	82.04	82.30	82.55	82.80	83.06	83.31	83.57
3.30	83.82	84.07	84.33	84.59	84.84	85.09	85.34	85.60	85.85	86.11
3.40	86.36	86.61	86.87	87.12	87.38	87.63	87.88	88.14	88.39	88.65
3.50	88.90	89.15	89.41	89.66	89.92	90.17	90.42	90.68	90.93	91.19
3.60	91.44 93.98	91.69	91.95	92.20	92.46	92.71	92.96	93.22	93.47	93.73
3.70 3.80	96.52	94.23 96.77	94·49 97.03	94.74	95.00 97.54	95.25 97.79	95.50 98.04	95.76 98.30	96.01 98.55	96.27 98.81
3.90	99.06	99.31	99-57	99.82	100.08	100.33	100.58	100.84	101.09	101.35
4.00	101.60	101.85	102.11	102.36	102.62	102.87	103.12	103.38	103.63	103.89
4.10	104.14	104.39	104.65	104.90	105.16	105.41	105.66	105.92	106.17	106.43
4.20	106.68	106.93	107.19	107.44	107.70	107.95	108.20	108.46	108.71	108.97
4.30 4.40	109.22	109.47	109.73	109.98	110.24	110.49	110.74	111.00	111.25	111.51
li l	•					113.03	113.28		113.79	114.05
4.50 4.60	114.30	114.55	114.81	115.06	115.32	115.57 118.11	115.82	116.08	116.33	116.59
4.70	119.38	119.63	119.89	120.14	120.40	120.65	120.90	121.16	121.41	119.13
4.80	121.92	122.17	122.43	122.68	122.94	123.19	123.44	123.70	123.95	124.21
4.90	124.46	124.71	124.97	125.22	125.48	125.73	125.98	126.24	126.49	126.75
5.00	127.00	127.25	127.51	127.76	128.02	128.27	128.52	128.78	129.03	129.29
Proporti •	onal Parts	Inch.				0.00	-	0.007 0.178		.009

Inches.	.00	10.	.02	.03	.04	.05	.06	.07	.08	.09
5.00 5.10 5.20 5.30 5.40	mm. 127.00 129.54 132.08 134.62 137.16	mm. 127.25 129.79 132.33 134.87 137.41	mm. 127.51 130.05 132.59 135.13 137.67	mm. 127.76 130.30 132.84 135.38 137.92	mm. 128.02 130.56 133.10 135.64 138.18	mm. 128.27 130.81 133.35 135.89 138.43	mm. 128.52 131.06 133.60 136.14 138.68	mm. 128.78 131.32 133.86 136.40 138.94	mm. 129.03 131.57 134.11 136.65	mm. 129.29 131.83 134.37 136.91 139.45
5.50	139.70	139.95	140.21	140.46	140.72	140.97	141.22	141.48	141.73	141.99
5.60	142.24	142.49	142.75	143.00	143.26	143.51	143.76	144.02	144.27	144.53
5.70	144.78	145.03	145.29	145.54	145.80	146.05	146.30	146.56	146.81	147.07
5.80	147.32	147.57	147.83	148.08	148.34	148.59	148.84	149.10	149.35	149.61
5.90	149.86	150.11	150.37	150.62	150.88	151.13	151.38	151.64	151.89	152.15
6.00	152.40	152.66	152.91	153.16	153.42	153.67	153.92	154.18	154.43	154.69
6.10	154.94	155.19	155.45	155.70	155.96	156.21	156.46	156.72	156.97	157.23
6.20	157.48	157.73	157.99	158.24	158.50	158.75	159.00	159.26	159.51	159.77
6.30	160.02	160.27	160.53	160.78	161.04	161.29	161.54	161.80	162.05	162.31
. 6.40	162.56	162.81	163.07	163.32	163.58	163.83	164.08	164.34	164.59	164.85
6.50	165.10	165.35	165.61	165.86	166.12	166.37	166.62	166.88	167.13	167.39
6.60	167.64	167.89	168.15	168.40	168.66	168.91	169.16	169.42	169.67	169.93
6.70	170.18	170.43	170.69	170.94	171.20	171.45	171.70	171.96	172.21	172.47
6.80	172.72	172.97	173.23	173.48	173.74	173.99	174.24	174.50	174. 7 5	175.01
6.90	175.26	175.51	175.77	176.02	176.28	176.53	176.78	177.04	177.29	177.55
7.00	177.80	178.05	178.31	178.56	178.82	179.07	179.32	179.58	179.83	180.09
7.10	180.34	180.59	180.85	181.10	181.36	181.61	181.86	182.12	182.37	182.63
7.20	182.88	183.13	183.39	183.64	183.90	184.15	184.40	184.66	184.91	185.17
7.30	185.42	185.67	185.93	186.18	186.44	186.69	186.94	187.20	187.45	187.71
7.40	187.96	188.21	188.47	188.72	188.98	189.23	189.48	189.74	189.99	190.25
7.50	190.50	190.75	191.01	191.26	191.52	191.77	192.02	192.28	192.53	192.79
7.60	193.04	193.29	193.55	193.80	194.06	194.31	194.56	194.82	195.07	195.33
7.70	195.58	195.83	196.09	196.34	196.60	196.85	197.10	197.36	197.61	197.87
7.80	198.12	198.37	198.63	198.88	199.14	199.39	199.64	199.90	200.15	200.41
7.90	200.66	200.91	201.17	201.42	201.68	201.93	202.18	202.44	202.69	202.95
8.00	203.20	203.45	203.71	203.96	204.22	204.47	204.72	204.98	205.23	205.49
8.10	205.74	205.99	206.25	206.50	206.76	207.01	207.26	207.52	207.77	208.03
8.20	208.28	208.53	208.79	209.04	209.30	209.55	209.80	210.06	210.31	210.57
8.30	210.82	211.07	211.33	211.58	211.84	212.09	212.34	212.60	212.85	213.11
8.40	213.36	213.61	213.87	214.12	214.38	214.63	214.88	215.14	215.39	215.65
8.50	215.90	216.15	216.41	216.66	216.92	217.17	217.42	217.68	217.93	218.19
. 8.60	218.44	218.69	218.95	219.20	219.46	219.71	219.96	220.22	220.47	220.73
8.70	220.98	221.23	221.49	221.74	222.00	222.25	222.50	222.76	223.01	223.27
8.80	223.52	223.77	224.03	224.28	224.54	224.79	225.04	225.30	225.55	225.81
8.90	226.06	226.31	226.57	226.82	227.08	227.33	227.58	227.84	228.09	228.35
9.00	228.60	228.85	229.11	229.36	229.62	229.87	230.12	230.38	230.63	230.89
9.10	231.14	231.39	231.65	231.90	232.16	232.41	232.66	232.92	233.17	233.43
9.20	233.68	233.93	234.19	234.44	234.70	234.95	235.20	235.46	235.71	235.97
9.30	236.22	236.47	236.73	236.98	237.24	237.49	237.74	238.00	238.25	238.51
9.40	238.76	239.01	239.27	239.52	239.78	240.03	240.28	240.54	240.79	241.05
9.50	241.30	241.55	241.81	242.06	242.32	242.57	242.82	243.08	243.33	243.59
9.60	243.84	244.09	244.35	244.60	244.86	245.11	245.36	245.62	245.87	246.13
9.70	246.38	246.63	246.89	247.14	247.40	247.65	247.90	248.16	248.41	248.67
9.80	248.92	249.17	249.43	249.68	249.94	250.19	250.44	250.70	250.95	251.21
9.90	251.46	251.71	251.97	252.22	252.48	252.73	252.98	253.24	253.49	253.75
Propo	254.00 rtional Pa	rts. Incl	-	0.002 0.051		.004 0.0 .102 0.1	-	•		0.009

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
10.00	mm.	mm.	mm,	mm.	mm.	mm.	mm.	mm. 255.78	mm. 256.03	mm. 256.29
10.00	254.00 256.54	254.25 256.79	254.51 257.05	254.76	255.02	255.27	255.52 258.06	258.32	258.57	258.83
10.10	259.08	259.33	259.59	257.30 259.84	257.56	257.81 260.35	260.60	260.86	261.11	261.37
10.30	261.62	261.87	262.1	262.38	262.64	262.89	263.14	263.40	263.65	263.91
10.40	264.16	264.41	264.67	264.92	265.18	265.43	265.68	265.94	266.19	266.45
10.50	266.70	266.95	267.21	267.46	267.72		268,22	268.48	268.73	268.99
10.60	269.24	269.49	269.75	270.00	270.26	267.97	270.76	271.02	271.27	271.53
10.70	271.78	272.03	272.29	272.54	272.80	270.51 273.05	273.30	273.56	273.81	274.07
10.80	274.32	274.57	274.93	275.08	275.34	275.59	275.84	276.10	276.35	276.61
10.90	276.86	277.11	277.37	277.62	277.88	278.13	278.38	278.64	278.89	279.15
11.00	279.40	279.65	279.91	280,16	280,42	280.67	1 : -	281.18	281.43	281.69
11.10	281.94	282.19	282.45	282.70	282.96	283.21	283.46	283.72	283.97	284.23
11,20	284.48	284.73	284.99	285.24	285.50	285.75	286.00	286.26	286.51	286.77
11.30	287.02	287.27	287.53	287.78	288.04	288.29	288.54	288.80	289.05	289.31
11.40	289.56	289.81	290.07	290.32	290.58	290.83	291.08	291.34	291.59	291.85
11.50	292.10	292.35	292.61	292.86	293.12	293-37	293.62	293.88	294.13	294.39
11.60	294.64	294.89	295.15	295.40	295.66	295.91	296.16	296.42		296.93
11.70	297.18	297.43	297.69	297.94	298.20	298.45	298.70	298.96	299.21	299.47
11.80	299.72	299.97	300.23	300.48	300.74	300.99	301.24	301.50	301.75	302.01
11.90	302.26	302.51	302.77	303.02	303.28	303.53	303.78	304.04	304.29	304.55
12.00	304.80	305.05	305.31	305.56	305.82	306.07	306.32	306.58	306.83	307.09
12.10	307.34	307.59	307.85	308.10	308.36	308.61	308.86	309.12	309.37	309.63
12,20	309.88	310.13	310.39	310.64	310.90	311.15	311.40	311.66	311.91	312.17
12.30	312.42	312.67	312.93	313.18	313.44	313.69	313.94	314.20	314.45	314.71
12.40	314.96	315.21	315.47	315.72	315.98	316.23	316.48	316.74	316.99	317.25
12.50	317.50	317.75	318.01	318.26	318.52	318.77	319.02	319.28	319.53	319.79
12.60	320.04	320.29	320.55	320.80	321.06	321.31	321.56	321.82	322.07	322.33
12.70	322.58	322.83	323.09	323.34	323.60	323.85	324.10	324.36	324.61	324.87
12.80	325.12	325.37	325.63	325.88	326.14	326.39	326.64	326.90	327.15	327.41
12.90	327.66	327.91	328.17	328.42	328.68	328.93	329.18	329.44	329.69	329.95
13.00	330.20	330.45	330.71	330.96	331.22	331.47	331.72	331.98	332.23	332.49
13.10	332.74	332.99	333-25	333.50	333.76	334.01	334.26	334.52	334.77	335.03
13.20	335.28	335.53	335.79	336.04	336.30	336.55	336.80	337.06	337.31	337.57
13.30	337.82	338.07	338.33	338.58	338.84	339.09	339.34	339.60	339.85	340.11
13.40	340.36	340.61	340.87	341.12	341.38	341.63	341.88	342.14	342.39	342.65
13.50	342.90	343.15	343.41	343.66	343.92	344.17	344.42	344.68	344.93	345.19
13.60	345.44	345.69	345.95	346.20	346.46	346.71	346.96	347.22	347-47	347.73
13.70	347.98	348.23	348.49	348.74	349.00	349.25	349.50	349.76	350.01	350.27
13.80	350.52	350.77	351.03	351.28	351.54	351.79	352.04	352.30	352.55	352.81
13.90	353.06	353.31	353-57	353.82	354.08	354-33	354-58	354.84	355.09	355-35
14.00	355.60	355.85	356.11	356.36	356.62	356.87	357.12	357.38	357.63	357.89
14.10	358.14	358.39	358.65	358.90	359.16	359.41	359.66	359.92	360.17	360.43
14.20	360.68	360.93	361.19	361.44	361.70	361.95	362.20	362.46	362.71	362.97
14.30	363.22	363.47	363.73	363.98	364.24	364.49	364.74	365.00	365.25	365.51
14.40	365.76	366.01	366.27	366.52	366.78	367.03	367.28	367.54	367.79	368.05
14.50	368.30	368.55	368.81	369.06	369.32	369.57	369.82	370.08	370.33	370.59
14.60	370.84		371.35	371.60	371.86		372.36	372.62		373.13
14.70	373.38	373.63	373.89	374.14	374.40	374.65	374.90	375.16	375.41	375.67
14.80	375.92	376.17	376.43	376.68	376.94	377.19	377.44	377.70	377.95	378.21
14.90	378.46	378.71	378.97	379.22	379.48	379.73	379.98	380.24	380.49	380.75
15.00	381.00	381.25	381.51	381.76	382.02	382.27	382.52	382.78	383.03	383.29
Propor	rtional Par	rts. Inch			-	.004 0,0	-	-		0.009
		mm	. 0.025	0.051	o.o76 o.	102 0.12	27 0.152	0.178	0.203	0.229

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
15.00 15.10. 15.20 15.30 15.40	mm. 381.00 383.54 386.08 388.62 391.16	mm. 381.25 383.79 386.33 388.87 391.41	mm. 381.51 384.05 386.59 389.13 391.67	mm. 381.76 384.30 386.84 389.38 391.92	mm. 382.02 384.56 387.10 389.64 392.18	mm. 382.27 384.81 387.35 389.89 392.43	mm. 382.52 385.06 387.60 390.14 392.68	mm. 382.78 385.32 387.86 390.40 392.94	mm. 383.03 385.57 388.11 390.65 393.19	mm. 383.29 385.83 388.37 390.91 393.45
15.50	393.70	393-95	394.21	394.46	394.72	394.97	395.22	395.48	395.73	395.99
15.60	396.24	39.649	396.75	397.00	397.26	397.51	397.76	398.02	398.27	398.53
15.70	398.78	399-03	399.29	399.54	399.80	400.05	400.30	400.56	400.81	401.07
15.80	401.32	401.57	401.83	402.08	402.34	402.59	402.84	403.10	403.35	403.61
15.90	403.86	404.11	404.37	404.62	404.88	405.13	405.38	405.64	405.89	406.15
16.00	406.40	406.65	406.91	407.16	407.52	407.67	407.92	408.18	408.43	408.69
16.10	408.94	409.19	409.45	409.70	409.96	410.21	410.46	410.72	410.97	411.23
16.20	411.48	411.73	411.99	412.24	412.50	412.75	413.00	413.26	413.51	413.77
16.30	414.02	414.27	414.53	414.78	415.04	415.29	415.54	415.80	416.05	416.31
16.40	416.56	416.81	417.07	417.32	417.58	417.83	418.08	418.34	418.59	418.85
16.50	419.10	419.35	419.61	419.86	420.12	420.37	420.62	420.88	421.13	421.39
16.60	421.64	421.89	422.15	422.40	422.66	422.91	423.16	423.42	423.67	423.93
16.70	424.18	424.43	424.69	424.94	425.20	425.45	425.70	425.96	426.21	426.47
16.80	426.72	426.97	427.23	427.48	427.74	427.99	428.24	428.50	428.75	429.01
16.90	429.26	429.51	429.77	430.02	430.28	430.53	430.78	431.04	431.29	431.55
17.00	431.80	432.05	432.31	432.56	432.82	433.07	433.32	433.58	433.83	434.09
17.10	434.34	434.59	434.85	435.10	435.36	435.61	435.86	436.12	436.37	436.63
17.20	436.88	437.13	437.39	437.64	437.90	438.15	438.40	438.66	438.91	439.17
17.30	439.42	439.67	439.93	440.18	440.44	440.69	440.94	441.20	441.45	441.71
17.40	441.96	442.21	442.47	442.72	442.98	443.23	443.48	443.74	443.99	444.25
17.50	444.50	444.75	445.01	445.26	445.52	445.77	446.02	·446.28	446.53	446.79
17.60	447.04	447.29	447.55	447.80	448.06	448.31	448.56	448.82	449.07	449.33
17.70	449.58	449.83	450.09	450.34	450.60	450.85	451.10	451.36	451.61	451.87
17.80	452.12	452.37	452.63	452.88	453.14	453.39	453.64	453.90	454.15	454.41
17.90	454.66	454.91	455.17	455.42	455.68	455.93	456.18	456.44	456.69	456.95
18.00	457.20	457.45	457.71	457.96	458.22	458.47	458.72	458.98	459.23	459.49
18.10	459.74	459.99	460.25	460.50	460.76	461.01	461.26	461.52	461.77	462.03
18.20	462.28	462.53	462.79	463.04	463.30	463.55	463.80	464.06	464.31	464.57
18.30	464.82	465.07	465.33	465.58	465.84	466.09	466.34	466.60	466.85	467.11
18.40	467.36	467.61	467.87	468.12	468.38	468.63	468.88	469.14	469.39	469.35
18.50	469.90	470.15	470.41	470.66	470.92	471.17	471.42	471.68	471.93	472.19
18.60	472.44	472.69	472.95	473.20	473.46	473.71	473.96	474.22	474.47	474.73
18.70	474.98	475.23	475.49	475.74	476.00	476.25	476.50	476.76	477.01	477.27
18.80	477.52	477.77	478.03	478.28	478.54	478.79	479.04	479.30	479.55	479.81
18.90	480.06	480.31	480.57	480.82	481.08	481.33	481.58	481.84	482.09	482.35
19.00	482.60	482.85	483.11	483.36	483.62	483.87	484.12	484.38	484.63	484.89
19.10	485.14	485.39	485.65	485.90	486.16	486.41	486.66	486.92	487.17	487.43
19.20	487.68	487.93	488.19	488.44	488.70	488.95	489.20	489.46	489.71	489.97
19.30	490.22	490.47	490.73	490.98	491.24	491.49	491.74	492.00	492.25	492.51
19.40	492.76	493.01	493.27	493.52	493.78	494.03	494.28	494.54	494.79	495.05
19.50 19.60 19.70 19.80 19.90	495.30 497.84 500.38 502.92 505.46	495.55 498.09 500.34 503.18 505.72	495.81 498.35 500.89 503.43 505.97	496.06 498.60 501.14 503.68 506.22	506.48	504.19 506.73	496.82 499.36 501.91 504.45 506.99	497.08 499.62 502.16 504.70 507.24	497.33 499.87 502.41 504.95 507.49	497.59 500.13 502.67 505.21 507.75
Propo	508.00	508.26	508.51 1. 0.001 1. 0.025			509.27 004 0.00 102 0.12		0.007 0.178		510.29 0.009 0.229

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
-	mm.	mm.		mm.	mm.	mm.	mm,	mm.	mm.	mm.
20.00	508.00	508.26	508.51	508.76	509.02	509.27	509.53	509.78	510.03	510.29
20.10	510.54	510.80	511.05	511.30	511.56	511.81	512.07	512.32	512.57	512.83
20.20	513.08	513.34	513.59	513.84	514.10	514.35	514.61	514.86	515.11	515.37
20.30	515.62	515.88	516.13	516.38	516.64	516.89	517.15	517.40	517.65	517.91
20.40	518.16	518.42	518.67	518.92	519.18	519.43	519.69	519.94	520.19	520.45
	ľ]		-	1 -			1	-	
20.50	520.70	520.96	521.21	521.46	521.72	521.97	522.23	522.48	522.73	522.99
20.60	523.24	523.50	523.75	524.00	524.26	524.51	524.77	525.02	525. 27	525.53
20.70 20.80	525.78	526.04	526.29	526.54	526.80	526.95	527.31	527.56	527.81	528.07
20.90	528.32 530.86	528.58	528.83	529.08	529.34	529.59	529.85	530.10	530.35	530.61
1	550.00	531.12	531.37	531.62	531.88	532.13	532.39	532.64	332.09	533.15
21.00	533.40	533.66	533.91	534.16	534.42	534.67	534-93	535.18	535-43	535.69
21.10	535.94	536.20	536.45	536.70	536.96	537.21	537-47	537.72	537.98	538.23
21.20	538.48	538.74	538.99	539.24	539.50	539-75	540.01	540.26	540.51	540.77
21.30	541.02	541.28	541.53	541.78	542.04	542.29	542.55	542.80	543.05	543.31
21.40	543.56	543.82	544.07	544.32	544.58	544.83	545.09	545.34	545.59	545.85
21.50	546.10	546.36	546.61	546.86	547.12	547-37	547.63	547.88	548.13	548.39
21.60	548.64	548.90	549.15	549.40	549.66	549.91	550.17	550.42	550.67	550.93
21.70	551.18	551.44	551.69	551.94	552.20	552.45	552.71	552.96	553.21	553-47
21.80	553.72	553.98	554.23	554.48	554.74	554.99	555-25	555.50	555.75	556.01
21.90	556.26	556.52	556.77	557.02	557.28	557.53	557-79	558.04	558.29	558.55
22.00	558.80	559.06	559.31	559.56	559.82	560.07	560.03	560.58	560.83	561.09
22,10	561.34	561.60	561.85	562.10	562.36	562.61	562.87	563.12	563.37	563.63
22,20	563.88	564.14	564.39	564.64	564.90	565.15	565.41	565.66	565.91	566.17
22.30	566.42	566.68	566.93	567.18	567.44	567.69	567.95	568.20	568.45	568.71
22.40	568.96	569.22	569.47	569.72	569.98	570.23	570.49	570.74	570.99	571.25
22.50	577.50	- 7 76								
22.60	571.50	571.76	572.01	572.26	572.52	572.77	573.03	573.28	573·53 576.07	573.79
22.70	574.04 576.58	574.30 576.84	574·55 577 · 09	574.80 577.34	575.06 577.60	575.31	575.57 578.11	575.82 578.36	578.61	576.33 578.87
22,80	579.12	579.38	579.63	579.88	580.14	577·95 580.39	580.65	580.90	581.15	581.41
22,90	581.66	581.92	582.17	582.42	582.68	582.93	583.19	583.44	583.69	583.95
1 1	Ĭ				_			- 1, 1, 1		
23.00	584.20	584.46	584.71	584.96	585.22	585.47	585.73	585.98	586.23	586.49
23.10	586.74	587.00	587.25	587.50	587.76	588.01	588.27	588.52	588.77	589.03
23.20 23.30	589.28 591.82	589.54	589.79	590.04	590.30 592.84	590.55	590.81	591.06	591.31	591.57
23.4 0		592.08 594.62	592.33	592.58	595.38	593.09	593.35	593.60 596.14	593.85	594.11 596.65
	594.36		594.87	595.12		595.63	595.89		596.39	390.03
23.50	596.90	597.16	597.41	597.66	597.92	598.17	598.43	598.68	598.93	599.19
23.60	599-44	599.70	599.95	600.20	600.46	600.71	600.97	601.22	601.47	601.73
23.70	601.98	602.24	602.49	602.74	603.00	603.25	603.51	603.76	604.01	604.27
23.80	604.52	604.78	605.03	605.28	605.54	605.79	606.05	606.30	606.55	606.81
23.90	607.06	607.32	607.57	607.82	608.08	608.33	608.59	608.84	609.09	609.35
24.00	609.60	609.86	610.11	610.36	610.62	610.87	611.13	611.38	611.63	611.89
24.10	612.14	612.40	612.65	612.90.	613.16	613.41	613.67	613.92	614.17	614.43
24.20	614.68	614.94	615.19	615.44	615.70	615.95	616.21	616.46	616.71	616.97
24.30	617.22	617.48	617.73	617.98	618.24	618.49	618.75	619.00	619.25	619.51
24. 40	619.76	620,02	620.27	620.52	620.78	621.03	621.29	621.54	621.79	622.05
24.50	622.30	622,56	622.81	623.06	623.32	623.57	623.83	624.08	624.33	624.59
24.60	624.84	625 10	625.35	625.60	625.86	626.11	626.37	626.62	626.87	627.13
24.70	627.38	627.64	627.89	628.14	628.40	628.65	628.91	629.16	629.41	629.67
24 .80	629.92	630.18	630.43	630.68	630.94	631.19	631.45	631.70	631.95	632.21
24.90	632.46	632.72	632.97	633.22	633.48	633.73	633.99	634.24	634.49	634.75
25.00	635.00	635.26	635.51	635.76	636.02	636.27	636.53	636.78	637.03	637.29
	00.23	00	00.0-	00.75	<u> </u>		0.00	J 1, 2	5,3	
		Inch	. 0,001	0.002	0.003 0.0	004 0.00	5 0.006	0 007	0.008	0.000
Propor	tional Par	ts. mm				102 0. 12	-	0.178		0.229
					,.					

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
25.00 25.10 25.20 25.30 25.40	mm. 635.00 637.54 640.08 642.62 645.16	mm, 635.26 637.80 640.34 642.88 645.42	mm. 635.51 638.05 640.59 643.13 645.67	mm. 635.76 638.30 640.84 643.38 645.92	mm. 636.02 638.56 641.10 643.64 646.18	mm. 636.27 638.81 641.35 643.89 646.43	mm. 636.53 639.07 641.61 644.15 646.69	mm. 636.78 639.32 641.86 644.40 646.94	mm. 637.03 639.57 642.11 644.65 647.19	mm. 637.29 639.83 642.37 644.91 647.45
25.50	647.70	647.96	648.21	648.46	648.72	648.97	649.23	649.48	649.73	649.99
25.60	650.24	650.50	650.75	651.00	651.26	651.51	651.77	652.02	654.27	652.53
25.70	652.78	653.04	653.29	653.54	653.80	654.05	654.31	654.56	654.81	655.07
25.80	655.32	655.58	655.83	656.08	656.34	656.59	656.85	657.10	657.35	657.61
25.90	657.86	658.12	658.37	658.62	658.88	659.13	659.39	659.64	659.89	660.15
26.00	660.40	660.66	660.91	661.16	661.42	661.67	661.93	662.18	662.43	662.69
26.10	662.94	663.20	663.45	663.70	663.96	664.21	664.47	664.72	664.97	665.23
26.20	665.48	665.74	665.99	666.24	666.50	666.75	667.01	667.26	667.51	667.77
26.30	668.02	668.28	668.53	668.78	669.04	669.29	669.55	669.80	670.05	670.31
26.40	670.56	670.82	671.07	671.32	671.58	671.83	672.09	672.34	672.59	672.85
26.50	673.10	673.36	673.61	673.86	674.12	674.37	674.63	674.88	675.13	675.39
26.60	675.64	675.90	676.15	676.40	676.66	676.91	677.17	677.42	677.67	677.93
26.70	678.18	678.44	678.69	678.94	679.20	679.45	679.71	679.96	680.21	680.47
26.80	680.72	680.98	681.23	681.48	681.74	681.99	682.25	682.50	682.75	683.01
26.90	683.26	683.52	683.77	684.02	684.28	684.53	684.79	685.04	685.29	685.5 5
27.00	685.80	686.06	686.31	686.56	686.82	687.07	687.33	687.58	687.83	688.09
27.10	688.34	688.60	688.85	689.10	689.36	689.61	689.87	690.12	690.37	690.63
27.20	690.88	691.14	691.39	691.64	691.90	692.15	692.41	692.66	692.91	693.17
27.30	693.42	693.68	693.93	694.18	694.44	694.69	694.95	695.20	695.45	695.71
27.40	695.96	696.22	696.47	696.72	696.98	697.23	697.49	697.74	697.99	698.25
27.50	698.50	698.76	699.01	699.26	699.52	699.77	700.03	700.28	700.53	700.79
27.60	701.04	701.30	701.55	701.80	702.06	702.31	702.57	702.82	703.07	703.33
27.70	703.58	703.84	704.09	704.34	704.60	704.85	705.11	705.36	705.61	705.87
27.80	706.12	706.38	706.63	706.88	707.14	707.39	707.65	707.90	708.15	708.41
27.90	708.66	708.92	709.17	709.42	709.68	709.93	710.19	710.44	710.69	710.95
28.00	711.20	711.46	711.71	711.96	712.22	712.47	712.73	712.98	713.23	713.49
28.10	713.74	714.00	714.25	714.50	714.76	715.01	715.27	715.52	715.77	716.03
28.20	716.28	716.54	716.79	717.04	717.30	717.55	717.81	718.06	718.31	718.57
28.30	718.82	719.08	719.33	719.58	719.84	720.09	720.35	720.60	720.85	721.11
28.40	721.36	721.62	721.87	722.12	722.39	722.63	722.89	723.14	723.39	723.65
28.50	723.90	724.16	724.41	724.66	724.92	725.17	725.43	725.68	725.93	726.19
28.60	725.44	726.70	726.95	727.20	727.46	727.71	727.97	728.22	728.47	728.73
28.70	728.98	729.24	729.49	729.74	730.00	730.25	730.51	730.76	731.01	731.27
28.80	731.52	731.78	732.03	732.28	732.54	732.79	733.05	733.30	733.55	733.81
28.90	734.06	734:32	734.57	734.82	735.08	735.33	735.59	735.84	736.09	736.35
29.00	736.60	736.86	737.11	737.36	737.62	737.87	738.13	738.38	738.63	738.89
29.10	739.14	739.40	739.65	739.90	740.16	740.41	740.67	740.92	741.17	741.43
29.20	741.68	741.94	742.19	742.44	742.70	742.95	743.21	743.46	743.71	743.97
29.30	744.22	744.48	744.73	744.98	745.24	745.49	745:75	746.00	746.25	746.51
29.40	746.76	747.02	747.27	747.52	747.78	748.03	748.29	748.54	748.79	749.05
29.50	749.30	749.56	749.81	750.06	750.32	750.57	750.83	751.08	751.33	751.59
29.60	751.84	752.10	752.35	752.60	752.86	753.11	753.37	753.62	753.87	754.13
29.70	754.38	754.64	754.89	755.14	755.40	755.65	755.91	756.16	756.41	756.67
29.80	756.92	757.18	757.43	757.68	757.94	758.19	758.45	758.70	758.95	759.21
29.90	759.46	759.72	759.97	760.22	760.48	760.73	760.99	761.24	761.49	761.75
Propos	762.00 tional Par	762.26 ts. Inch			_	763.27 004 0. 00 102 0.12	-	763.78 0.007 0.178		764.29 0.009 0.229

1 inch = 25.40005 mm.

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
30.00	762.00	762.26	762.51	762.76	763.02	763.27	763.53	763.78	764.03	764.29
30.10	764.54	764.80	765.05	765.30	765.56	765.81	766.07	766.32	766.57	766.83
30.20	767.08	767.34	767.59	767.84	768.10	768.35	768.61	768.86	769.11	769.37
30.30	769.62	769.88	770.13	770.38	770.64	770.89	771.15	771.40	771.65	771.91
30.40	772.16	772.42	772.67	772.92	773.18	773.43	773.69	773.94	774.19	774.45
30.50	774.70	774.96	775.21	775.46	775.72	775-97	776.23	776.48	776.73	776.99
30.60	777.24	777.50	777.75	778.00	778.26	778.51	778.77	779.02	779.27	779.53
30.70	779.78	780.04	780.29	780.54	780.80	781.05	781.31	781.56	781.81	782.07
30.80	782.32	782.58	782.83	783.08	783.34	783.59	783.85	784.10	784.35	784.61
30.90	784.86	785.12	785.37	785.62	785.88	786.13	786.39	786.64	786.89	787.15
31.00	787.40	787.66	787.91	788.16	788.42	788.67	788.93	789.18	789.43	789.69
31.10	789.94	790.20	790.45	790.70	790.96	791.21	791.47	791.72	791.97	792.23
31.20	792.48	792.74	792.99	793.24	793.50	793.75	794.01	794.26	794.51	794.77
31.30	795.02	795.28	795.53	795.78	796.04	796.29	796.55	796.80	797.05	797.31
31.40	797.56	797.82	798.07	798.32	798.58	798.83	799.09	799.34	799.59	799.85
31.50	800.10	800.36	800.61	800.86	801.12	801.37	801.63	801.88	802.13	802.39
31.60	802.64	802.90	803.15	803.40	803.66	803.91	804.17	804.42	804.67	804.93
31.70	805.18	805.44	805.69	805.94	806.20	806.45	806.71	806.96	807.21	807.47
31.80	807.72	807.98	808.23	808.48	808.74	808.99	809.25	809.50	809.75	810.01
31.90	810.26	810.52	810.77	811.02	811.28	811.53	811.79	812.04	812.29	812.55
32.00	812.80									
Propor	tional Par	ts. Inch			-	004 0.00 102 0.12	-	o.ao7 o.178		0.009 7.229

SMITHSONIAN TABLES

Milli- msters.	0	ı	2	3	4	5	6	7	8	9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
0	0.0000	0.0394	0.0787	0.1181	0.1575	0.1968	0.2362	0.2756	0.3150	0.3543
10	0.3937	0.4331	0.4724	0.5118	0.5512	0.5906	0.6299	0.6693	0.7087	0.7480
20	0.7874	0.8268	0.8661	0.9055		0.9842	1.0236	1.0630	1.1024	1.1417
30	1.1811	1.2205	1.2598	1.2992		1.3780	1.4173	1.4567	1.4961	1.5354
40	1.5748	1.6142	1.6535	1.6929	1.7323	1.7716	1.8110	1.8504	1.8898	1.9291
50	1.9685	2.0079	2.0472	2.0866	2.1260	2.1654	2.2047	2.2441	2.2835	2.3228
60	2,3622	2.4016	2.4409	2.4803		2.5590	2.5984	2.6378	2.6772	2.7165
70	2.7559	2.7953	2.8346	2.8740		2.9528	2.9921	3.0315	3.0709	3.1102
8o	3.1496	3.1890	3.2283	3.2677	3.3071	3.3464	3.3858	3.4252	3.4646	3.5039
90	3.5433	3.5828	3.6220	3.6614	3.7008	3.7402	3.7795	3.8189	3.8583	3.8976
100	3.9370	3.9764	4.0157	4.0551		4.1338	4.1732	4.2126	4.2520	4.2913
110	4.3307	4.3701	4.4094	4.4488	4.4882	4.5276	4.5669	4.6063	4.6457	4.6850
120	4.7244	4.7638	4.8031	4.8425		4.9212	4.9606	5.0000	5.0394	5.0787
130	5.1181	5.1575	5.1968	5.2362		5.3150	5.3543	5.3937	5.4331	5.4724
140	5.5118	5.5512	5.5905	5.6299	5.6693	5.7086	5.7480	5.7874	5.8268	5.8661
150	5.9055	5.9449	5.9842	6.0236	6.0630	6.1024	6.1417	6.1811	6.2205	6.2598
160	6.2992	6.3386	6.3779	6.4173	6.4567	6.4960	6.5354	6.5748	6.6142	6.6535
170	6.6929	6.7323	6.7716	6.8110	6.8504	6.8898	6.9291	6.9685	7.0079	7.0472
180	7.0866	7.1260	7.1653	7.2047		7.2834	7.3228	7.3622	7.4016	7.4409
190	7.4803	7.5197	7.5590	7.5984	7.6378	7.6772	7.7165	7.7559	7.7953	7.8346
200	7.8740	7.9134	7.9527	7.9921	8.0315	8.0708	8.1102	8.1496	8.1890	8.2283
210	8.2677	8.3071	8.3464	8.3858	8.4252	8.4646	8.5039	8.5433	8.5827	8.6220
220	8.6614	8.7008	8.7401	8.7795		8,8582	8.8976	8.9370	8.9764	
230	9.0551	9.0945	9.1338	9.1732			9.2913	9.3307	9.3701	
240	9.4488	9.4882	9.5275	9.5669	9.6063	9.6456	9.6850	9.7244	9.7638	9.8031
250	9.8425	9.8819	9.9212	9.9606	10.0000	10.0394	10.0787	10.1181	10.1575	10.1968
260	10.2362		10.3149	10.3543	10.3937	10.4330	10.4724	10.5118	10.5512	10.5905
270					10.7874					
280					11.1811					
, 290	11.4173	11.4568	11.4960	11.5354	11.5748	11.6142	11.6535	11.6929	11.7323	11.7716
300	11.8110	11.8504	11.8897	11.9291	11.9685	12.0078	12.0472	12.0866	12.1260	12.1653
310	12.2047	12.2441	12.2834	12.3228	12.3622	12.4016	12.4409	12.4803	12.5197	12.5590
320	12.5984	12.6378	12.6771	12.7165	12.7559	12.7952	12.8346	12.8740	12.9134	
330	12.9921	13.0315	13.0708	13.1102	13.1496	13.1890	13.2283	13.2677	13.3071	13.3464
340	13.3858	13.4252	13.4645	13.5039	13.5433	13.5826	13.0220	13.0014	13.7008	13.7401
350					13.9370					14.1338
360	14.1732	14.2126	14.2519	14.2913	14.3307	14.3700	14.4094	14.4488	14.4882	14.5275
370					14.7244					
380	14.9606	15.0000	15.0393	15.0787	15.1181	15.1574	15.1908	15.2302	15.2750	15.3149
390		i	1	1	15.5118		1	i .	1	
400	15.7480	15.7874	15.8267	15.8661	15.9055	15.9448	15.9842	16.0236	16.0630	16.1023
		Tenth	s of a mill	lmeter.			Hundred	ths of a n	nillimster.	
	mm.	Incl	ı. 11	m.	Inch.	mm.	Incl	ı. m	m.	Inch.
	1.0	0.003	9 0	.6	0.0236	0.01	0.000	' 1	.06	0.0024
	.2	.007		.7	.0076	.02	,000		.07	.0028
	-3	,011		.5	.0315	.03	.001		.08	.0031
	-4	.015		.9	.0354	.04	.001		.09	.0035
	.5	.019	"	0.1	.0394	.05	,002		.10	.0039

Mill]- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.						
400	15.748	15.752	15.756	15.760	15.764	15.768	15.772	15.776	15.779	15.783
401	15.787	15.791	15.795	15.799	15.803	15.807	15.811	15.815	15.819	15.823
402	15.827	15.831	15.835	15.839	15.842	15.846	15.850	15.854	15.858	15.862
403	15.866	15.870	15.874	15.878	15.882	15.886	15.890	15.894	15.898	15.902
404	15.905	15.909	15.913	15.917	15.921	15.925	15.929	15.933	15.937	15.941
405	15.945	15.949	15.953	15.957	15.961	15.965	15.968	15.972	15.976	15.980
406	15.984	15.988	15.992	15.996	16.000	16.004	16.008	16.012	16.016	16.020
407	16.024	16.028	16.031	16.035	16.039	16.043	16.047	16.051	16.055	16.059
408	16.063	16.067	16.071	16.075	16.079	16.083	16.087	16.091	16.094	16.098
409	16.102	16.106	16.110	16.114	16.118	16.122	16.126	16.130	16.134	16.138
410	16.142	16.146	16.150	16.154	16.157	16.161	16.165	16.169	16.173	16.177
411	16.181	16.185	16.189	16.193	16.197	16.201	16.205	16.209	16.213	16.217
412	16.220	16.224	16.228	16.232	16.236	16.240	16.244	16.248	16.252	16.256
413	16.260	16.264	16.268	16.272	16.276	16.279	16.283	16.287	16.291	16.295
414	16.299	16.303	16.307	16.311	16.315	16.319	16.323	16.327	16.331	16.335
415	16.339	16.342	16.346	16.350	16.354	16.358	16.362	16.366	16.370	16.374
416	16.378	16.382	16.386	16.390	16.394	16.398	16.402	16.405	16.409	16.413
417	16.417	16.421	16.425	16.429	16.433	16.437	16.441	16.445	16.449	16.453
418	16.457	16.461	16.465	16.468	16.472	16.476	16.480	16.484	16.488	16.492
419	16.496	16.500	16.504	16.508	16.512	16.516	16.520	16.524	16.528	16.531
420	16.535	16.539	16.543	16.547	16.551	16.555	16.559	16.563	16.567	16.571
421	16.575	16.579	16.583	16.587	16.591	16.594	16.598	16.602	16.606	16.610
422	16.614	16.618	16.622	16.626	16.630	16.634	16.638	16.642	16.646	16.650
423	16.654	16.657	16.661	16.665	16.669	16.673	16.677	16.681	16.685	16.689
424	16.693	16.697	16.701	16.705	16.709	16.713	16.717	16.720	16.724	16.728
425	16.732	16.736	16.740	16.744	16.748	16.752	16.756	16.760	16.764	16.768
426	16.772	16.776	16.779	16.783	16.787	16.791	16.795	16.799	16.803	16.807
427	16.811	16.815	16.819	16.823	16.827	16.831	16.835	16.839	16.842	16.846
428	16.850	16.854	16.858	16.862	16.866	16.870	16.874	16.878	16.882	16.886
429	16.890	16.894	16.898	16.902	16.905	16.909	16.913	16.917	16.921	16.925
430 431 432 433 434	16.929 16.968 17.008 17.047 17.087	16.933 16.972 17.012 17.051 17.091	16.937 16.976 17.016 17.055 17.094	16.941 16.980 17.020 17.059 17.098	16.945 16.984 17.024 17.063 17.102	16.949 16.988 17.028 17.067 17.106	16.953 16.992 17.031 17.071 17.110	16.957 16.996 17.035 17.075	16.961 17.000 17.039 17.079 17.118	16.965 17.004 17.043 17.083 17.122
435	17.126	17.130	17.134	17.138	17.142	17.146	17.150	17.154	17.157	17.161
436	17.165	17.169	17.173	:7.177	17.181	17.185	17.189	17.193	17.197	17.201
437	17.205	17.209	17.213	17.217	17.220	17.224	17.228	17.232	17.236	17.240
438	17.244	17.248	17.252	17.256	17.260	17.264	17.268	17.272	17.276	17.279
439	17.283	17.287	17.291	17.295	17.299	17.303	17.307	17.311	17.315	17.319
440	17.323	17.327	17.331	17.335	17.339	17.342	17.346	17.350	17.354	17.358
441	17.362	17.366	17.370	17.374	17.378	17.382	17.386	17.390	17.394	17.398
442	17.402	17.405	17.409	17.413	17.417	17.421	17.425	17.429	17.433	17.437
443	17.441	17.445	17.449	17.453	17.457	17.461	17.465	17.468	17.472	17.476
444	17.480	17.484	17.488	17.492	17.496	17.500	17.504	17.508	17.512	17.516
445	17.520	17.524	17.528	17.531	17.535	17.539	17.543	17.547	17.551	17.555
446	17.559	17.563	17.567	17.571	17.575	17.579	17.583	17.587	17.591	17.594
447	17.598	17.602	17.606	17.610	17.614	17.618	17.622	17.626	17.630	17.634
448	17.638	17.642	17.646	17.650	17.654	17.657	17.661	17.665	17.669	17.673
449	17.677	17.681	17.685	17.689	17.693	17.697	17.701	17.705	17.709	17.713
450	17.717	17.720	17.724	17.728	17.732	17.736	17.740	17.744	17.748	17.752

Milli- meters.	.0	.I	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
450	17.717	17.720	17.724	17.728	17.732	17.736	17.740	17.744	17.748	17.752
451	17.756	17.760	17.764	17.768	17.772	17.776	17.779	17.783	17.787	17.791
452	17.795	17.799	17.803	17.807	17.811	17.815	17.819	17.823	17.827	17.831
453	17.835	17.839	17.842	17.846	17.850	17.854	17.858	17.862	17.866	17.870
454	17.874	17.878	17.882	17.886	17.890	17.894	17.898	17.902	17.905	17.909
455	17.913	17.917	17.921	17.925	17.929	17.933	17.937	17.941	17.945	17.949
456	17.953	17.957	17.961	17.965	17.968	17.972	17.976	17.980	17.984	17.988
457	17.992	17.996	18.000	18.004	18.008	18.012	18.016	18.020	18.024	18.028
458	18.031	18.035	18.039	18.043	18.047	18.051	18.055	18.059	18.063	18.067
459	18.071	18.075	18.079	18.083	18.087	18.091	18.094	18.098	18.102	18.106
4 60	18.110	18.114	18.118	18.122	18.126	18.130	18.134	18.138	18.142	18.146
461	18.150	18.154	18.157	18.161	18.165	18.169	18.173	18.177	18.181	18.185
462	18.189	18.193	18.197	18.201	18.205	18.209	18.213	18.216	18.220	18.224
463	18.228	18.232	18.236	18.240	18.244	18.248	18.252	18.256	18.260	18.264
464	18.268	18.272	18.276	18.279	18.283	18.287	18.291	18.295	18.299	18.303
465	18.307	18.311	18.315	18.319	18.323	18.327	18.331	18.335	18.339	18.342
466	18.346	18.350	18.354	18.358	18.362	18.366	18.370	18.374	18.378	18.382
467	18.386	18.390	18.394	18.398	18.402	18.405	18.409	18.413	18.417	18.421
468	18.425	18.429	18.433	18.437	18.441	18.445	18.449	18.453	18.457	18.461
469	18.465	18.468	18.472	18.476	18.480	18.484	18.488	18.492	18.496	18.500
470	18.504	18.508	18.512	18.516	18.520	18.524	18.528	18.531	18.535	18.539
471	18.543	18.547	18.551	18.555	18.559	18.563	18.567	18.571	18.575	18.579
472	18.583	18.587	18.591	18.594	18.598	18.602	18.606	18.610	18.614	18.618
473	18.622	18.626	18.630	18.634	18.638	18.642	18.646	18.650	18.654	18.657
474	18.661	18.665	18.669	18.673	18.677	18.681	18.685	18.689	18.693	18.697
475	18.701	18.705	18.709	18.713	18.716	18.720	18.724	18.728	18.732	18.736
476	18.740	18.744	18.748	18.752	18.756	18.760	18.764	18.768	18.772	18.776
477	18.779	18.783	18.787	18.791	18.795	18.799	18.803	18.807	18.811	18.815
478	18.819	18.823	18.827	18.831	18.835	18.839	18.842	18.846	18.850	18.854
479	18.858	18.862	18.866	18.870	18.874	18.878	18.882	18.886	18.890	18.894
480 481 482 483 484	18.898 18.937 18.976 19.016	18.902 18.941 18.980 19.020	18.905 18.945 18.984 19.024 19.063	18.909 18.949 18.988 19.028 19.067	18.913 18.953 18.992 19.031 19.071	18.917 18.957 18.996 19.035 19.075	18.921 18.961 19.000 19.039 19.079	18.925 18.965 19.004 19.043 19.083	18.929 18.968 19.008 19.047 19.087	18.933 18.972 19.012 19.051
485	19.094	19.098	19.102	19.106	19.110	19.114	19.118	19.122	19.126	19.130
486	19.134	19.138	19.142	19.146	19.150	19.154	19.157	19.161	19.165	19.169
4 87	19.173	19.177	19.181	19.185	19.189	19.193	19.197	19.201	19.205	19.209
488	19.213	19.216	19.220	19.224	19.228	19.232	19.236	19.240	19.244	19.248
489	19.252	19.256	19.260	19.264	19.268	19.272	19.276	19.279	19.283	19.287
490	19.291	19.295	19.299	19.303	19.307	19.311	19.315	19.319	19.323	19.327
491	19.331	19.335	19.339	19.342	19.346	19.350	19.354	19.358	19.362	19.366
492	19.370	19.374	19.378	19.382	19.386	19.390	19.394	19.398	19.402	19.405
493	19.409	19.413	19.417	19.421	19.425	19.429	19.433	19.437	19.441	19.445
494	19.449	19.453	19.457	19.461	19.465	19.468	19.472	19.476	19.480	19.484
495	19.488	19.492	19.496	19.500	19.504	19.508	19.512	19.516	19.520	19.524
496	19.528	19.531	19.535	19.539	19.543	19.547	19.551	19.555	19.559	19.563
497	19.567	19.571	19.575	19.579	19.583	19.587	19.591	19.594	19.598	19.602
498	19.606	19.610	19.614	19.618	19.622	19.626	19.630	19.634	19.638	19.642
499	19.646	19.650	19.654	19.657	19.661	19.665	19.669	19.673	19.677	19.681
500	19.685	19.689	19.693	19.697	19.701	19.705	19.709	19.713	19.716	19.720

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
500	19.685	19.689	19.693	19.697	19.701	19.705	19.709	19.713	19.716	19.720
501	19.724	19.728	19.732	19.736	19.740	19.744	19.748	19.752	19.756	19.760
502	19.764	19.768	19.772	19.776	19.779	19.783	19.787	19.791	19.795	19.799
503	19.803	19.807	19.811	19.815	19.819	19.823	19.827	19.831	19.835	19.839
504	19,842	19.846	19.850	19.854	19.858	19.862	19.866	19.870	19.874	19.878
505	19.882	19.886	19.890	19.894	19.898	19.902	19.905	19.909	19.913	19.917
506	19.921	19.925	19.929	19.933	19.937	19.941	19.945	19.949	19.953	19.957
507	19.961	19.965	19.968	19.972	19.976	19.980	19.984	19.988	19.992	19.996
508	20,000	20.004	20.008	20.012	20.016	20,023	20.024	20.028	20.031	20.035
509	20.039	20.043	20.047	20,051	20.055	20.059	20.063	20.067	20.071	20.075
510	20.079	20.083	20.087	20.091	20.094	20.098	20, 102	20.106	20.110	20.114
511	20.118	20.122	20.126	20.130	20.134	20.138	20.142	20.146	20.150	20.154
512	20.157	20.161	20,165	20.169	20.173	20.177	20.181	20.185	20.189	20.193
513	20.197	20,201	20.205	20,209	20.213	20.216	20,220	20.224	20.228	20.232
514	20.236	20.240	20.244	20,248	20.252	20.256	20,260	20.264	20.268	20.272
515	20.276	20.279	20.283	20.287	20.291	20.295	20.299	20.303	20.307	20.311
516	20.315	20.319	20.323	20.327	20.331	20.335	20.339	20.342	20.346	20.350
517	20.354	20.358	20.362	20.366	20.370	20.374	20.378	20.382	20.386	20.390
518 519	20.394	20.398	20.402 20.441	20.405 20.445	20.409 20.449	20.413	20.417 20.457	20.421 20.461	20.425	20.429 20.468
1								-		
520	20.472	20.476	20.480	20.484	20.488	20.492	20.496	20.500	20.504	20.508
521 522	20.512	20.516	20.520 20.559	20.524	20.528	20.531 20.571	20.535	20.539	20.543	20.547
523	20.591	20.594	20.598	20.602	20.606	20.610	20.575	20.579 20.618	20,583	20.587 20.626
524	20.630	20.634	20.638	20.642	20.646	20.650	20.654	20.657	20.661	20.665
525	20.669	20.673	20.677	20.681	20.685	20.689	20.693	20.697	20.701	20.705
526	20.709	20.713	20.716	20.720	20.724	20.728	20.732	20.736	20.740	20.744
527	20.748	20.752	20.756	20.760	20.764	20.768	20.772	20.776	20.779	20.783
528	20.787	20.791	20.795	20.799	20.803	20.807	20.811	20.815	20.819	20.823
529	20.827	20.831	20.835	20.839	20.842	20.846	20.850	20.854	20,858	20.862
530	20.866	20.870	20.874	20.878	20.882	20.886	20.890	20.894	20.898	20.902
531	20.905	20.909	20.913	20.917	20.921	20.925	20.929	20.933	20.937	20.941
532	20.945	20.949	20.953	20.957	20.961	20.965	20.968	20.972	20.976	20.980
533	20.984	20.988 21.028	20.992 21.031	20.996	21,000	21.004	21.008	21.012 21.051	21.016	21.020
534		_		• •	21.039			_	21.055	21.059
535	21.063	21.067	21.071	21.075	21.079	21.083	21.087	21.091	21.094	21.098
536	21.102	21.106 21.146	21.110	21.114	21.118	21.122 21.161	21.126	21.130	21.134	21.138
537 538	21.142 21.181	21.140	21.150	21.154	21.157 21.197	21.101	21.105	21.169	21.173	21.177
539	21.220	21.224	21.228	21.232	21.236	21.240	21.244	21.248	21.213 21.252	21.216
540	21.260	21.264	21.268	21.272	21.276	21.279	21.283	21.287	21.291	21.295
54I	21.299	21.303	21.307	21.311	21.315	21.319	21.323	21.327	21.331	21.335
542	21.339	21.342	21.346	21.350	21.354	21.358	21.362	21.366	21.370	21.374
543	21.378	21.382	21.386	21.390	21.394	21.398	21.402	21.405	21.409	21.413
544	21.417	21.421	21.425	21.429	21.433	21.437	21.441	21.445	21.449	21.453
545	21.457	21.461	21.465	21.468	21.472	21.476	21.480	21.484	21.488	21.492
546	21.496	21.500	21.504	21.508	21.512	21.516	21.520	21.524	21.528	21.531
547 548	21.535	21.539	21.543	21.547	21.551	21.555	21.559	21.563	21.567	21.571
549	21.575	21.579	21.503	21.507	21.630	21.594	21.598	21.602	21.606 21.646	21.610
550	21.654	21.657	21.661	21.665	21.669	21.673	21.677	21.681	21.685	21.689
	04		21.501			-2.073	21.0//	21.001	21.005	21.009

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
550	21.654	21.657	21.661	21.665	21.669	21.673	21.677	21.681	21.685	21.689
551	21.693	21.697	21.701	21.705	21.709	21.713	21.716	21.720	21.724	21.728 21.768
552 553	21.732 21.772	21.736 21.776	21.740 21.779	21.744	21.748 21.787	21.752 21.791	21.756	21.760	21.764 21.803	21.807
554	21.811	21.815	21.819	21.823	21.827	21.831	21.835	21.839	21.842	21.846
555	21.850	21.854	21.858	21.862	21.866	21.870	21.874	21.878	21.882	21.886
556	21.890	21.894	21.898	21.902	21.905	21.909	21.913	21.917	21.921	21.925
557 558	21.929	21.933	21.937	21.941	21.945 21.984	21.949	21.953	21.957 21.996	21.961	21.965 22.004
559	22.008	21.972	21.976 22.016	22.020	22.024	21.988	22.031	22,035	22.039	22.043
560	22.047	22.051	22.055	22.059	22,063	22.067	22.071	22.075	22.079	22.083
561	22.087	22.091	22.094	22.098	22.102	22.106	22. I IO	22.114	22,118	22.122
562 563	22.126	22.130	22.134 22.173	22.138 22.177	22.142 22.181	22.146 22.185	22.150 22.189	22.153	22.157 22.197	22.161 22.201
564	22.205	22.109	22.213	22.216	22.220	22.105	22.228	22.232	22.236	22.240
565	22.244	22.248	22.252	22.256	22.260	22.264	22.268	22.272	22.276	22.279
566	22.283	22.287	22.291	22.295	22.299	22.303	22.307	22.311	22.315	22.319
567 568	22.323	22.327	22.331	22.335 22.374	22.339 22.378	22.342 22.382	22.346	22.350	22.354	22.358
569	22.402	22.405	22.409	22.413	22.417	22.421	22.425	22,429	22.433	2 2. 437
570	22.441	22.445	22.449	22.453	22.457	22.461	22.465	22.468	22.472	22.476
571	22.480	22.484	22.488	22.492	22.496	22.500	22.504	22.508	22.512	22.516
572 573	22.520	22.524	22.528 22.567	22.53I 22.57I	22.535	22.539 22.579	22.543	22.547 22.587	22.551 22.591	22.555 22.594
574	22.598	22.602	22,606	22.610	22.614	22.618	22.622	22.626	22.630	22.634
575	22.638	22.642	22.646	22.650	22.653	22,657	22.661	22.665	22.669	22.673
576	22.677 22.716	22.681	22.685	22.689 22.728	22.693	22.697 22.736	22.701	22.705 22.744	22.709	22.713
577 578	22.756	22.760	22.764	22.768	22.732 22.772	22.776	22.779	22.783	22.787	22.791
579	22.795	22.799	22.803	22.807	22.811	22.815	22.819	22.823	22.827	22.831
580	22.835	22.839	22.842	22.846	22.850	22.854	22.858	22.862	22.866	22.870
581 582	22.874	22.878	22.882	22.886	22.890	22.894	22.898	22.902 22.941	22.905	22.909 22.949
583	22.913	22.917	22.961	22.965	22.968	22.972	22.976	22.980	22.984	22.988
584	22.992	22.996	23.000	23.004	23.008	23.012	23.016	23.020	23.024	23.028
585	23.031	23.035	23.039	23.043	23.047	23.051	23.055	23.059	23.063	23.067
586 587	23.071 23.110	23.075	23.079 23.118	23.083	23.087	23.091 23.130	23.094	23.098	23.102	23.106 23.146
588	23.110	23.153	23.157	23.161	23.165	23.169	23.173	23.177	23.181	23.185
589	23.189	23.193	23.197	23.201	23.205	23.209	23.213	23.216	23.220	23.224
590	23.228	23.232	23.236	23.240	23.244	23.248	23.252	23.256	23.260	23.264
591	23.268	23.272	23.276	23.279	23.283	23.287	23.291	23.295	23.299	23.303
592 593	23.307 23.346	23.311	23.315	23.319 23.358	23.323	23.327 23.366	23.331	23.335	23.339	23.342
593 594	23.386	23.390	23.394	23.398	23.402		23.409	23.413	23.417	23.421
595	23.425	23.429	23.433	23.437	23.441		23.449	23.453	23.457	23.461
596	23.465	23.468	23.472	23.476	23.480	23.484	23.488	23.492	23.496	23.500
597 508	23.504	23.508	23.512	23.516	23.520	23.524 23.563	23.528	23.531	23.535 23.575	23.539 23.579
598 599	23.543 23.583	23.547 23.587	23.551	23.555 23.594	23.598	23.602	23.606	23.610	23.614	23.618
600	23.622	23.626	23.630	23.634	23.638	23.642	23.646	23.650	23.653	23.657
L	<u> </u>	I	ŀ	<u> </u>	<u> </u>	<u>'</u>	<u> </u>	J		I

600 23.622 23.626 23.636 23.634 23.638 23.642 23.646 23.650 23.653 23.673 23.677 23.767 23.685 23.685 23.689 23.693 23.736 23.766 23.685 23.685 23.689 23.732 23.732 23.732 23.732 23.732 23.732 23.732 23.742 23.742 23.768 23.772 23.772 23.766 23.760 23.760 23.764 23.768 23.772 23.772 23.763 23.760 23.760 23.764 23.768 23.772 23.772 23.760 23.764 23.768 23.772 23.760 23.764 23.768 23.772 23.772 23.760 23.764 23.789 23.799 23.803 23.881 23.879 23.883 23.883 23.883 23.884 23.886 23.886 23.886 23.992 23.984 23.992 23.917 23.921 23.925 23.929 23.986 23.992 23.984 23.992 23.965 23.992 23.965 <th>.9 3.657 3.697 3.736 3.776 3.815 3.854 3.894 3.972 1.012</th>	.9 3.657 3.697 3.736 3.776 3.815 3.854 3.894 3.972 1.012
600 23.622 23.626 23.636 23.634 23.638 23.642 23.646 23.650 23.653 23.673 23.677 23.767 23.685 23.685 23.689 23.693 23.736 23.761 23.762 23.766 23.681 23.685 23.685 23.689 23.732 23.732 23.728 23.772 23.728 23.772 23.773 23.772 23.766 23.760 23.760 23.762 23.768 23.772 23.768 23.772 23.768 23.772 23.760 23.760 23.764 23.768 23.772 23.760 23.760 23.764 23.768 23.772 23.760 23.764 23.768 23.772 23.760 23.764 23.768 23.779 23.783 23.8799 23.803 23.880 23.881 23.881 23.883 23.883 23.885 23.885 23.886 23.886 23.937 23.941 23.945 23.9499 23.953 23.957 23.950 23.953 23.953 23.957 23.955 23.965 </th <th>3.657 3.697 3.736 3.776 3.815 3.854 3.894 3.933 3.972 1.012</th>	3.657 3.697 3.736 3.776 3.815 3.854 3.894 3.933 3.972 1.012
601 23.661 23.665 23.669 23.773 23.771 23.762 23.724 23.728 23.732 23.876 23.766 23.764 23.786 23.772 23.861 23.876 23.879 23.833 23.832 23.827 23.831 23.835 23.878 23.878 23.842 23.886 23.890 23.990 23.993 23.991 23.921 23.925 23.929 23.993 23.991 23.965 23.965 23.968 23.968 23.992 23.988 23.992 23.988 23.992 23.968 23.965 23.968 23.968 23.968 23.968 23.968 23.965 <td>3.697 3.736 3.776 3.815 3.854 3.894 3.972 1.012 1.051 1.091 1.130</td>	3.697 3.736 3.776 3.815 3.854 3.894 3.972 1.012 1.051 1.091 1.130
602 23.701 23.705 23.709 23.713 23.716 23.720 23.724 23.728 23.732 23.765 603 23.764 23.768 23.778 23.752 23.755 23.756 23.760 23.764 23.768 23.772 23.801 23.807 23.803 23.803 23.807 23.811 23.765 23.799 23.803 23.807 23.811 23.811 23.866 23.879 23.879 23.879 23.878 23.882 23.866 23.886 23.890 23.866 23.870 23.874 23.878 23.882 23.886 23.890 23.995 23.990 23.913 23.977 23.921 23.922 23.866 23.892 23.994 23.945 23.945 23.945 23.945 23.945 23.945 23.940 23.957 23.961 23.965 23.968 23.929 23.955 23.992 23.957 23.961 23.965 23.968 23.929 23.957 23.961 23.966 23.953 23.953 23.953 23.957	3.736 3.776 3.815 3.854 3.894 3.933 3.972 1.012 1.051 1.091 1.130
603 23.740 23.744 23.748 23.779 23.799 23.760 23.764 23.768 23.772 23.811 23.765 63.799 23.803 23.867 23.811 23.811 23.803 23.879 23.879 23.799 23.803 23.867 23.811 23.866 23.879 23.878 23.879 23.884 23.886 23.880 23.886 23.879 23.879 23.878 23.878 23.886 23.889 23.992 23.991 23.921 23.922 23.996 23.995 23.995 23.995 23.995 23.995 23.995 23.995 23.996 23.957 23.961 23.965 23.968 23.968 23.988 23.992 23.996 24.000 24.002 24.024 24.028 24.031 24.035 24.039 24.0408 24.0404 24.028 24.031 24.035 24.039 24.047 24.071 24.075 24.079 24.031 24.072 24.071 24.071 24.075 24.071 24.075 24.079 24.032 </th <td>3.776 3.815 3.854 3.894 3.933 3.972 4.012 4.051 4.091 4.130</td>	3.776 3.815 3.854 3.894 3.933 3.972 4.012 4.051 4.091 4.130
605 23.819 23.823 23.827 23.831 23.837 23.837 23.837 23.837 23.837 23.878 23.874 23.878 23.842 23.846 23.850 23.922 23.866 23.876 23.874 23.878 23.878 23.842 23.846 23.850 23.922 23.905 23.905 23.972 23.917 23.921 23.925 23.929 23.965 23.953 23.941 23.945 23.945 23.945 23.945 23.945 23.949 23.953 23.996 24.000 24.004 24.008 24.031 24.035 24.039 24.044 24.008 24.012 24.067 24.071 24.075 24.079 24.083 24.087 24.075 24.079 24.083 24.087 24.114 24.118 24.124 24.106 24.107 24.106 24.114 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.127 24.181 24.185 24.189 24.219 24.220 24.224 24.228 <td>3.854 3.894 3.972 1.012 1.051 1.091 1.130</td>	3.854 3.894 3.972 1.012 1.051 1.091 1.130
606 23.858 23.862 23.866 23.870 23.874 23.878 23.882 23.886 23.890 23.905 23.909 23.913 23.917 23.921 23.965 23.965 23.968 23.984 23.988 23.995 23.957 23.961 23.965 23.968 23.968 23.988 23.998 23.996 23.968 23.988 23.995 23.966 24.002 24.024 24.028 24.031 24.035 24.039 24.040 24.047 24.071 24.075 24.079 24.083 24.047 24.071 24.075 24.079 24.083 24.087 24.071 24.075 24.079 24.083 24.087 24.086 24.110 24.110 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.118 24.119 24.221 24.228 24.223 24.236 24.240 24.244 24.248 24.232 24.236 24.243 24.352 <td>3.894 3.933 3.972 4.012 4.051 4.091 4.130</td>	3.894 3.933 3.972 4.012 4.051 4.091 4.130
607 23.898 23.902 23.905 23.909 23.913 23.917 23.921 23.925 23.929 23.968 23.937 23.941 23.945 23.949 23.953 23.957 23.961 23.965 23.968 23.968 23.988 23.998 23.996 24.000 24.004 24.008 24.008 24.008 24.008 24.004 24.008 24.031 24.035 24.039 24.043 24.047 24.075 24.079 24.083 24.087 24.071 24.114 24.114 24.114 24.114 24.115 24.114 24.114 24.115 24.113 24.112 24.126 24.213 24.142 24.146 24.153 24.177 24.181 24.185 24.189 24.193 24.197 24.201 24.205 24.206 24.216 24.224 24.228 24.232 24.236 24.240 24.2424 24.288 24.272 24.276 24.279 24.233 24.331 24.331 24.333 24.332 24.2424 24.2428 24.232<	3.933 3.972 4.012 4.051 4.091 4.130
608 23.937 23.941 23.945 23.945 23.953 23.953 23.961 23.965 23.968 23.988 23.988 23.998 23.996 24.000 24.004 24.008 24.004 24.008 24.008 24.004 24.008 24.004 24.008 24.047 24.028 24.031 24.035 24.039 24.043 24.047 24.087 24.071 24.075 24.079 24.083 24.087 24.087 24.075 24.079 24.083 24.087 24.087 24.075 24.079 24.083 24.087 24.087 24.071 24.075 24.079 24.083 24.087 24.087 24.106 24.110 24.114 24.118 24.122 24.126 24.146 24.155 24.153 24.177 24.181 24.185 24.189 24.193 24.197 24.201 24.220 24.224 24.228 24.232 24.236 24.240 24.244 24.246 24.256 24.256 24.256 24.256 24.256 24.2424 24.31 <td>3.972 1.012 1.051 1.091 1.130</td>	3.972 1.012 1.051 1.091 1.130
610 24.016 24.020 24.024 24.028 24.031 24.035 24.039 24.043 24.047 24.057 611 24.055 24.059 24.063 24.067 24.071 24.075 24.039 24.043 24.047 24.067 612 24.054 24.068 24.102 24.106 24.110 24.114 24.118 24.118 24.121 24.126 24.126 24.126 24.127 24.181 24.185 24.189 24.193 24.197 24.201 24.205 24 24.228 24.232 24.236 24.240 24.244 24 24.268 24.272 24.276 24.279 24.283 24.249 24.288 24.272 24.276 24.279 24.283 24.247 24.276 24.272 24.276 24.272 24.276 24.272 24.276 24.272 24.276 24.272 24.276 24.272 24.276 24.279 24.233 24.331 24.331 24.331 24.331 24.331 24.331 24.331 <td>1.051 1.091 1.130</td>	1.051 1.091 1.130
611	1.091 1.130
612	1.130
613	
615 24.213 24.216 24.220 24.224 24.268 24.238 24.236 24.240 24.244 24.266 24.268 24.276 24.276 24.279 24.243 24.268 24.272 24.276 24.279 24.283 24.283 24.276 24.276 24.279 24.283 24.286 24.272 24.276 24.279 24.283 24.383 24.331 24.355 24.339 24.342 24.346 24.350 24.354 24.358 24.362 24.366 24.390 24.354 24.358 24.362 24.362 24.390 24.374 24.378 24.378 24.382 24.386 24.390 24.394 24.398 24.402 24.402 24.402 24.402 24.402 24.402 24.433 24.437 24.441 24.425 24.429 24.433 24.437 24.441 24.425 24.429 24.433 24.437 24.441 24.425 24.468 24.472 24.476 24.472 24.476 24.472 24.476 24.472 24.476 <td></td>	
616	.209
617	.248
618	1.287 1.327
620 24.409 24.413 24.417 24.421 24.425 24.426 24.433 24.437 24.441 24.456 24.468 24.433 24.437 24.441 24.456 24.468 24.472 24.436 24.480 24.456 24.468 24.472 24.476 24.480 24.502 24.502 24.502 24.502 24.502 24.516 24.520 24.520 24.543 24.547 24.551 24.555 24.559 24.559 24.547 24.587 24.551 24.555 24.559 24.548 24.567 24.579 24.583 24.587 24.587 24.594 24.594 24.598 24.594 24.630 24.634 24.638 24.659 24.650 24.661 24.661 24.662 24.665 24.663 24.673 24.751 24.752 24.752 24.752 24.752 24.752 24.752 24.657 24.665 24.666 24.666 24.666 24.650 24.653 24.657 24.7667 24.705 24.770 24.705 24.705 <td>1.366</td>	1.366
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622 24.488 24.492 24.596 24.500 24.504 24.508 24.512 24.516 24.520 24.526 24.526 24.526 24.526 24.526 24.526 24.526 24.526 24.527 24.575 24.579 24.583 24.587 24.591 24.594 24.598 24.596 24.666 24.660 24.610 24.614 24.618 24.622 24.626 24.630 24.634 24.638 24.650 24.646 24.650 24.653 24.657 24.657 24.666 24.666 24.656 24.669 24.650 24.653 24.657 24.701 24.705 24.709 24.713 24.716 24.628 24.724 24.728 24.732 24.736 24.740 24.748 24.752 24.756 24.75	1.445
623	1.484 1.524
625 24.666 24.610 24.614 24.658 24.622 24.626 24.630 24.634 24.638 24 626 24.646 24.650 24.653 24.657 24.661 24.665 24.669 24.673 24.677 24.677 24.705 24.709 24.713 24.716 24 628 24.724 24.728 24.732 24.736 24.740 24.748 24.748 24.752 24.756 24	1.563
626 24.646 24.650 24.653 24.657 24.661 24.665 24.669 24.673 24.677 24 627 24.685 24.689 24.693 24.697 24.701 24.705 24.709 24.713 24.716 24 628 24.724 24.728 24.732 24.736 24.740 24.744 24.748 24.752 24.756 24	.602
627 24.685 24.689 24.693 24.697 24.701 24.705 24.709 24.713 24.716 24 628 24.728 24.728 24.732 24.736 24.740 24.744 24.748 24.752 24.756 24	.642
628 24.724 24.728 24.732 24.736 24.740 24.744 24.748 24.752 24.756 24	,.681 .720
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600 000 000 000 000 000 000 000 000 000	.878 .917
633 24.921 24.925 24.929 24.933 24.937 24.941 24.945 24.949 24.953 24	-957
035 037 0	.996
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627 25 270 25 282 25 287 25 25 25 25 25 25 25 25 25 25 25 25 25	.075
638 25.118 25.122 25.126 25.130 25.134 25.138 25.142 25.146 25.150 25	.153
	.193
	.232
640 07 076 07 070 05 000 07 070 070 070 070 070 07	.272 .311
643 25.315 25.319 25.323 25.327 25.331 25.335 25.339 25.342 25.346 25	3.350
044 25.354 25.358 25.362 25.366 25.370 25.374 25.378 25.382 25.386 25	390
645 25.394 25.398 25.402 25.405 25.409 25.413 25.417 25.421 25.425 25.466 25.433 25.437 25.441 25.445 25.449 25.453 25.457 25.461 25.465	
647 05 470 05 476 05 400 05 100 05 100 100 100 100 100 100 100	.429
648 25.512 25.516 25.520 25.524 25.528 25.531 25.535 25.539 25.543 25	.468
049 25.551 25.555 25.559 25.563 25.567 25.571 25.575 25.579 25.583 25	
650 25.591 25.594 25.598 25.602 25.606 25.610 25.614 25.618 25.622 25	5.468 5.508

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
650	25.591	25·594	25.598	25.602	25.606	25.610	25.614	25.618	25.622	25.626
651 652	25.630 25.669	25.634 25.673	25.638 25.677	25.642 25.681	25.646 25.685	25.650 25.689	25.653 25.693	25.657 25.697	25.661 25.701	25.665 25.705
653	25.709	25.713	25.716	25.720	25.724	25.728	25.732	25.736	25.740	25.744
654	25.748	25.752	25.756	25.760	25.764	25.768	25.772	25.776	25.779	25.783
655	25.787	25.791	25.795	25.799 25.839	25.803	25.807	25.811	25.815	25.819	25.823
656	25.827	25.831	25.835	25.839	25.842	25.846	25.850	25.854	25.858	25.862
657 658	25.866 25.905	25.870 25.909	25.874 25.913	25.878 25.917	25.882 25.921	25.886 25.925	25.890 25.929	25.894 25.933	25.898 25.937	25.902 25.941
659	25.945	25.949	25.953	25.957	25.961	25.965	25.968	25.972	25.976	25.980
660	25.984	25.988	25.992	25.996	26,000	26.004	26.008	26.012	26.016	26,020
661 662	26.024 26.063	26.028 26.067	26.031 26.071	26.035 26.075	26.039 26.079	26.043 26.083	26.047 26.087	26.051 26.090	26.055 26.094	26.059 26.098
663	26.102	26.106	26.110	26.114	26.118	26.122	26.126	26.130	26.134	26.138
664	26.142	26.146	26.150	26.153	26.157	26.161	26.165	26.169	26.173	26.177
665	26.181	26.185	26.189	26.193	26.197	26.201	26.205	26.209	26.213	26.216
666	26,220 26,260	26.224 26.264	26.228 26.268	26.232 26.272	26.236 26.276	26.240 26.279	26.244 26.283	26.248 26.287	26.252 26.291	26.256 26.295
667 668	26.299	26.303	26.307	26.311	26.315	26.319	26.323	26.327	26.331	26.335
669	26.339	26.342	26.346	26.350	26.354	26.35 8	26.362	26.366	26.370	26.374
670	26.378	26.382	26.386	26.390	26.394	26.398	26.402	26.405	26.409	26.413
671	26.417 26.457	26.421 26.461	26.425 26.465	26.429 26.468	26.433 26.472	26.437 26.476	26.441 26.480	26.445 26.484	26.449 26.488	26.453 26.492
672 673	26.496	26.500	26.504	26.508	26.512	26.516	26.520	26.524	26.528	26.531
674	26.535	26.539	26.543	26.547	26.551	26.555	26.559	26.563	26.567	26.571
675	26.575	26.579	26.583	26.587	26.590	26.594	26.598	26.602	26.606	26.610
676	26.614 26.653	26.618 26.657	26.622 26.661	26.626	26.630 26.669	26.634 26.673	26.638 26.677	26.642 26.681	26.646 26.685	26.650 26.689
677 678	26.693	26.697	26.701	26.705	26.709	26.713	26.716	26.720	26.724	26.728
679	26.732	26.736	26.740	26.744	26.748	26.752	26.756	26.760	26.764	26.768
680	26.772	26.776	26.779	26.783	26.787	26.791	26.795	26.799	26.803	26.807
681 682	26.811 26.850	26.815 26.854	26.819 26.858	26.823 26.862	26.827 26.866	26.831 26.870	26.835 26.874	26.838 26.878	26.842 26.882	26.846 26.886
683	26.890	26.894	26.898	26.902	26.905	26.909	26.913	26.917	26.921	26.925
684	26.929	26.933	26.937	26.941	26.945	26.949	26.953	26.957	26.961	26.965
685	26.968	26.972	26.976	26.980	26.984	26.988	26.992	26.996	27.000	27.004
686 687	27.008 27.047	.27.012 27.051	27.016 27.055	27.020 27.059	27.024 27.063	27.028 27.067	27.031 27.071	27.035 27.075	27.039 27.079	27.043 27.083
688	27.047	27.090	27.094	27.098	27.102	27.106	27.110	27.114	27.118	27.122
689	27.126	27.130	27.134	27.138	27.142	27.146	27.150	27.153	27.157	27.161
690	27.165	27.169	27.173	27.177	27.181		27.189	27.193	27.197	27.201
691 692	27.205 27.244	27.209 27.248	27.213 27.252	27.216 27.256	27.220 27.260	27.224 27.264	27.228 27.268	27.232	27.236 27.276	27.240 27.279
693	27.244	27.240	27.291	27.295	27.299	27.303	27.307	27.311	27.315	27.319
694	27.323	27.327	27.331	27.335	27.339	27.342	27.346	27.350	27.354	27.358
695	27.362	27.366	27.370	27.374	27.378	27.382	27.386	27.390	27.394	27.398
696	27.402	27.405	27.409	27.413	27.417	27.421 27.461	27.425 27.465	27.429 27.468	27.433	27.437
697 698	27.441 27.480	27.445 27.484	27.449 27.488	27.453 27.492	27.457	27.500	27.504	27.408	27.512	27.476
699	27.520	27.524	27.528	27.531	27.535	27.539	27.543	27.547	27.551	27.555
700	27.559	27.563	27.567	27.571	27.575	27.57 9	27.583	27.587	27.590	27.594

1 mm. = 0.03937 inch.

Mill-	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
meters.										
700	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
701	27.559 27.598	27.563 27.602	27.567 27.606	27.571 27.610	27.575 27.614	27.579 27.618	27.583 27.622	27.587 27.626	27.590	27.594 27.634
702 703	27.638 27.677	27.642 27.681	27.646	27.650 27.689	27.653	27.657 27.697	27.661 27.701	27.665	27.669	27.673
704	27.716	27.720	27.724	27.728	27.732	27.736	27.740	27.744	27.748	27.752
705 706	27.756	27.760	27.764 27.803	27.768	27.772	27.776	27.779 27.819	27.783 27.823	27.787 27.827	27.791 27.831
707	27.795 27.835	27.799 27.839	27.842	27.807 27.846	27.811	27.815	27.858	27.862	27.866	27.870
708 709	27.874 27.913	27.878 27.917	27.882 27.921	27.886	27.890 27.929	27.894	27.898	27.902 27.941	27.905 27.945	27.909 27.949
710	27.953	27.957	27.961	27.965	27.929	27.933 27.972	27.937 27.976	27.980	27.984	27.988
711	27.992	27.996	28,000	28.004	28.008	28.012	28.016	28.020	28.024	28.028
712 713	28.031 28.071	28.035 28.075	28.039 28.079	28.043 28.083	28.047 28.087	28.051 28.090	28.055 28.094	28.059 28.098	28.063 28.102	28.067 28.106
714	28.110	28.114	28.118	28.122	28.126	28.130	28.134	28.138	28.142	28.146
715 716	28.150 28.189	28.153 28.193	28.157 28.197	28.161 28.201	28.165 28.205	28.169 28.209	28.173 28.213	28.177 28.216	28.181 28.220	28.185 28.224
717	28.228	28.232	28.236	28.240	28.244	28.248	28.252	28.256	28.260	28.264
718 719	28.268 28.307	28.272 28.311	28.276 28.315	28.279 28.319	28.283 28.323	28.287 28.327	28.291 28.331	28.295 28.335	28.299 28.339	28.303 28.342
720	28.346	28.350	28.354	28.358	28.362	28.366	28.370	28.374	28.378	28.382
72I	28.386	28.390	28.394	28.398	28.402	28.405	28.409	28.413	28.417	28.421
722 723	28.425 28.465	28.429 28.468	28.433 28.472	28.437 28.476	28.441 28.480	28.445 28.484	28.449 28.488	28.453 28.492	28.457 28.496	28.461 28.500
724	28.504	28.508	28.512	28.516	28.520	28.524	28.528	28.531	-28.535	28.539
725 726	28.543 28.583	28.547 28.587	28.551 28.590	28.555 28.594	28.559 28.598	28.563 28.602	28.567 28.606	28.571 28.610	28.575 28.614	28.579 28.618
727	28.622	28.626	28.630	28.634	28.638	28.642	28.646	28.650	28.653	28.657
728 729	28.661 28.701	28.665 28.705	28.669 28.709	28.673 28.713	28.677 28.716	28.681 28.720	28.685 28.724	28.689 28.728	28.693 28.732	28.697 28.736
730	28.740	28.744	28.748	28.752	28.756	28.760	28.764	28.768	28.772	28.776
731 732	28.779 28.819	28.783 28.823	28.787 28.827	28.791 28.831	28.795 28.835	28.799 28.839	28.803 28.842	28.807 28.846	28.811 28.850	28.815 28.854
733	28.858 28.898	28.862 28.902	28.866 28.905	28.870	28.874	28.878	28.882	28.886	28.890	28.894
734 735	28.937	28.941	28.945	28.909	28.913 28.953	28.917	28.921	28.925 28.965	28.929 28.968	28.933 28.972
736	28.976	28.980	28.984	28.988	28.992	28.996	29.000	29.004	29.008	29.012
737 738	29.016	29.020	29.024	29.028	29.031 29.071	29.035	29.039	29.043	29.047 29.087	29.051
739	29.094	29.098	29. 102	29.106	29.110	29.114	29.118	29.122	29.126	29.130
740 741	29. I 34 29. I 73	29.138 29.177	29.142 29.181	29.146 29.185	29.150 29.189	29.153 29.193	29.157 29.197	29.161 29.201	29.165 29.205	29.169 29.209
742	29.213	29.216	29.220	29.224	29.228	29.193	29.197	29.240	29.244	29.248
743 744	29.252 29.291	29.256 29.295	29.260 29.299	29.264 29.303	29.268 29.307	29.272	29.276	29.279 29.319	29.283 29.323	29.287 29.327
745	29.331	29.335	29.339	29.342	29.346	29.350	29.354	29.358	29.362	29.366
	29.370	29.374	29.378 29.417	29.382	29.386 29.425	29.390 29.429	29.394 29.433	29.398	29.402 29.44I	29.405 29.445
748	29.449	29.453	29.457	29.461	29.465	29.468	29.472	29.476	29.480	29.484
	29.488	29.492	29.496	29.500	29.504	29.508	29.512	29.516	29.520	29.524
750	29.528	29.531	29.535	29.539	29.543	29.547	29.551	29.555	29.559	29.563

1 mm. = 0.03937 inch.

						,				
Milli- meters.	.0	1.	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
750	29.528	29.531	29.535	29.539	29.543	29.547	29.551	29.555	29.559	29.563
751	29.567	29.571	29.575	29.579	29.583	29.587	29.590	29.594	29.598	29.602
752	29.606 29.646	29.610 29.650	29.614	29.618	29.622	29.626	29.630	29.634	29.638	29.642 29.681
753 754	29.685	29.689	29.653	29.657 29.697	29.661 29.701	29.665 29.705	29.669 29.709	29.673 29.713	29.677 29.716	29.720
755	29.724	29.728	29.732	29.736	29.740	29.744	29.748	29.752	29.756	29.760
756	29.764	29.768	29.772 29.811	29.776	29.779	29.783	29.787	29.791	29.795 29.835	29.799
757	29.803	29.807	29.811	29.815	29.819	29.823	29.827	29.831	29.835	29.839
758 7 5 9	29.842 29.882	29.846 29.886	29.850 29.890	29.854 29.894	29.858 29.898	29.862 29.902	29.866	29.870 29.909	29.874	29.878 29.917
760	29.921	29.925	29.929	29.933	29.937	29.941	29.945	29.949	29.953	29.957
761	29.961	29.965	29.968	29.972	29.976	29.980	29.984	29.988	29.992	29.996
762	30.000	30.004	30.008	30.012	30.016	30.020	30.024	30.027	30.031	30.035
763	30.039	30.043	30.047	30.051	30.055	30.059	30.063	30.067	30.071	30.075
764	30.079	30.083	30.087	30.090	30.094	30.098	30, 102	30.106	30.110	30.114
765	30.118	30.122	30.126	30.130	30.134	30.138	30.142	30.146	30.150	30.153
766 767	30.157	30.161	30.165	30.169	30.173	30.177	30,181	30.185	30.189	30.193
768	30.197 30.236	30.201 30.240	30.205	30.209	30.213	30.216 30.256	30.220 30.260	30.224 30.264	30.228 30.268	30.232 30.272
769	30.276	30.279	30.283	30.240	30.252	30.250	30.299	30.303	30.307	30.311
770	30.315	30.319	30.323	30.327	30.331	30.335	30.339	30.342	30.346	30.350
771	30.354	30.358	30.362	30.366	30.370	30.374	30.378	30.382	30.386	30.390
772	30.394	30.398	30.402	30.405	30.409	30.413	30.417	30.421	30.425	30.429
773 774	30.433	30.437	30.441	30.445 30.484	30.449 30.488	30.453	30.457 30.496	30.461	30.465 30.504	30.468 30.508
775	30.512	30.516	30.520	30.524	30.528	30.531	30.535	30.539	30.543	30.547
776	30.551	30.555	30.559	30.563	30.567	30.571	30.575	30.579	30.583	30.587
777	30.590	30.594	30.598	30.602	30.606	30.610	30.614	30.618	30.622	30.626
778	30.630	30.634	30.638	30.642	30.646	30.650	30.653	30.657	30.661	30.665
779	30.669	30.673	30.677	30.681	30. 685	30.689	30.693	30.697	30.701	30.705
780 781	30.709	30.713	30.716	30,720	30.724	30.728	30.732	30.736	30.740	30.744
782	30.748 30.787	30.752 30.791	30.756 30.795	30.760 30.799	30.764 30.803	30.768 30.807	30.772 30.811	30.776 30.815	30.779 30.819	30.783
783	30.827	30.831	30.835	30.839	30.842	30.846	30.850	30.854	30.858	30.862
784	30.866	30.870	30.874	30.878	30.882	30.886	30.890	30.894	30.898	30.902
785	30.905	30.909	30.913	30.917	30.921	30.925	30.929	30.933	30.937	30.941
786	30.945	30.949	30.953	30.957	30.961	30.965	30.968	30.972	30.976	30.980
787 788	30.984	30.988	30.992	30.996	31.000	31.004	31.008	31.012	31.016	31.020
789	31.024 31.063	31.027 31.067	31.031	31.035 31.075	31.039 31.079	31.043 31.083	31.047	31.051	31.055	31.059
790	31.102	31,106	31.110	31.114	31.118	31.122	31.126	31.130	31.134	31.138
791	31.142	31.146	31.150	31.153	31.157	31.161	31.165	31.169	31.173	31.177
792	31.181	31.185	31.189	31.193	31.197	31.201	31.205	31.209	31.213	31.216
793	31,220	31.224	31.228	31.232	31.236	31.240	31.244	31.248	31.252	31.256
794	31.260	31.264	31.268	31.272	31.276	31.279	31.283	31.287	31.291	31.295
795	31.299	31.303	31.307	31.311	31.315	31.319	31.323	31.327	31.331	31.335
796	31.339	31.342	31.346	31.350	31.354	31.358	31,362	31.366	31.370	31.374
797 798	31.378	31.382	31.386	31.390	31.394	31.398	31.402	31.405	31.409	31.413
799	31.457	31.461	31.425	31.429	31.433	31.476	31.480	31.484	31.488	31.492
800	31.496	31.500	31.504	31.508	31.512	31.516	31.520	31.524	31.527	31.531
	- '/	J J - 1	3 3-7	33	30	J 1J=1			- · · ·	

1 mm. = 0.03937 inch.

Milli- meters.	.0	1.	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.						
800	31.496	31.500	31.504	31.508	31.512	31.516	31.520	31.524	31.527	31.531
801	31.535	31.539	31.543	31.547	31.551	31.555	31.559	31.563	31.567	31.571
802	31.575	31.579	31.583	31.587	31.590	31.594	31.598	31.602	31.606	31.610
803	31.614	31.618	31.622	31.626	31.630	31.634	31.638	31.642	31.646	31.650
804	31.653	31.657	31.661	31.665	31.669	31.673	31.677	31.681	31.685	31.689
805	31.693	31.697	31.701	31.705	31.709	31.713	31.716	31.720	31.724	31.728
806	31.732	31.736	31.740	31.744	31.748	31.752	31.756	31.760	31.764	31.768
807	31.772	31.776	31.779	31.783	31.787	31.791	31.795	31.799	31.803	31.807
808	31.811	31.815	31.819	31.823	31.827	31.831	31.835	31.839	31.842	31.846
809	31.850	31.854	31.858	31.862	31.866	31.870	31.874	31.878	31.882	31.886
810	31.890	31.894	31.898	31.902	31.905	31.909	31.913	31.917	31.921	31.925
811	31.929	31.933	31.937	31.941	31.945	31.949	31.953	31.957	31.961	31.965
812	31.968	31.972	31.976	31.980	31.984	31.988	31.992	31.996	32.000	32.004
813	32.008	32.012	32.016	32.020	32.024	32.027	32.031	32.035	32.039	32.043
814	32.047	32.051	32.055	32.059	32.063	32.067	32.071	32.075	32.079	32.083
815	32.087	32.090	32.094	32.098	32.102	32.106	32.110	32.114	32.118	32.122
816	32.126	32.130	32.134	32.138	32.142	32.146	32.150	32.153	32.157	32.161
817	32.165	32.169	32.173	32.177	32.181	32.185	32.189	32.193	32.197	32.201
818	32.205	32.209	32.213	32.216	32.220	32.224	32.228	32.232	32.236	32.240
819	32.244	32.248	32.252	32.256	32.260	32.264	32.268	32.272	32.276	32.279
820	32.283	32.287	32.291	32.295	32.299	32.303	32.307	32.311	32.315	32.319
821	32.323	32.327	32.331	32.335	32.339	32.342	32.346	32.350	32.354	32.358
822	32.362	32.366	32.370	32.374	32.378	32.382	32.386	32.390	32.394	32.398
823	32.402	32.405	32.409	32.413	32.417	32.421	32.425	32.429	32.433	32.437
824	32.441	32.445	32.449	32.453	32.457	32.461	32.465	32.468	32.472	32.476
825	32.480	32.484	32.488	32.492	32.496	32.500	32.504	32.508	32.512	32.516
826	32.520	32.521	32.527	32.531	32.535	32.539	32.543	32.547	32.551	32.555
827	32.559	32.563	32.567	32.571	32.575	32.579	32.583	32.587	32.590	32.594
828	32.598	32.602	32.606	32.610	32.614	32.618	32.622	32.626	32.630	32.634
829	32.638	32.642	32.646	32.650	32.653	32.657	32.661	32.665	32.669	32.673
830	32.677	32.681	32.685	32.689	32.693	32.697	32.701	32.705	32.709	32.713
831	32.716	32.720	32.724	32.729	32.732	32.736	32.740	32.744	32.748	32.752
832	32.756	32.760	32.764	32.768	32.772	32.776	32.779	32.783	32.787	32.791
833	32.795	32.799	32.803	32.807	32.811	32.815	32.819	32.823	32.827	32.831
834	32.835	32.839	32.842	32.846	32.850	32.854	32.858	32.862	32.866	32.870
835	32.874	32.878	32.882	32.886	32.890	32.894	32.898	32.902	32.905	32.909
836	32.913	32.917	32.921	32.925	32.929	32.933	32.937	32.941	32.945	32.949
837•	32.953	32.957	32.961	32.965	32.968	32.972	32.976	32.980	32.984	32.988
838	32.992	32.996	33.000	33.004	33.008	33.012	33.016	33.020	33.024	33.027
839	33.031	33.035	33.039	33.043	33.047	33.051	33.055	33.059	33.063	33.067
840	33.071	33.075	33.079	33.083	33.087	33.090	33.094	33.098	33.102	33.106
841	33.110	33.114	33.118	33.122	33.126	33.130	33.134	33.138	33.142	33.146
842	33.150	33.153	33.157	33.161	33.165	33.169	33.173	33.177	33.181	33.185
843	33.189	33.193	33.197	33.201	33.205	33.209	33.213	33.216	33.220	33.224
844	33.228	33.232	33.236	33.240	33.244	33.248	33.252	33.256	33.260	33.264
845	33.268	33.272	33.276	33.279	33.283	33.287	33.291	33.295	33.299	33.303
846	33.307	33.311	33.315	33.319	33.323	33.327	33.331	33.335	33.339	33.342
847	33.346	33.350	33.354	33.358	33.362	33.366	33.370	33.374	33.378	33.382
848	33.386	33.390	33.394	33.398	33.402	33.405	33.409	33.413	33.417	33.421
849	33.425	33.429	33.433	33.437	33.441	33.445	33.449	33.453	33.457	33.461
850	33.464	33.468	33-472	33.476	33.480	33.484	33.48 8	33.49 2	33.496	33.500

1 mm. = 0.03937 inch.

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
850	33.464	33.468	33.472	33.476	33.480	33.484	33.488	33.492	33.496	33.500
851	33.504	33.508	33.512	33.516	33.520	33.524	33.527	33.531	33.535	33.539
852	33.543	33.547	33.551	33.555	33.559	33.563	33.567	33.571	33.575	33.579
853	33.583	33.587	33.590	33.594	33.598	33.602	33.606	33.610	33.614	33.618
854	33.622	33.626	33.630	33.634	33.638	33.642	33.646	33.650	33.653	33.657
855	33.661	33.665	33.659	33.673	33.677	33.681	33.685	33.689	33.693	33.697
856	33.701	33.705	33.709	33.713	33.716	33.720	33.724	33.728	33.732	33.736
857	33.740	33.744	33.748	33.752	33.756	33.760	33.764	33.768	33.772	33.776
858	33.779	33.783	33.787	33.791	33.795	33.799	33.803	33.807	33.811	33.815
859	33.819	33.823	33.827	33.831	33.835	33.839	33.842	33.846	33.850	33.854
860	33.858	33.862	33.866	33.870	33.874	33.878	33.882	33.886	33.890	33.894
861	33.898	33.902	33.905	33.909	33.913	33.917	33.921	33.925	33.929	33.933
862	33.937	33.941	33.945	33.949	33.953	33.957	33.961	33.964	33.968	33.972
863	33.976	33.980	33.984	33.988	33.992	33.996	34.000	34.004	34.008	34.012
864	34.016	34.020	34.024	34.027	34.031	34.035	34.039	34.043	34.047	34.051
865	34.055	34.059	34.063	34.067	34.071	34.075	34.079	34.083	34.087	34.090
866	34.694	34.098	34.102	34.106	34.110	34.114	34.118	34.122	34.126	34.130
867	34.134	34.138	34.142	34.146	34.150	34.153	34.157	34.161	34.165	34.169
868	34.173	34.177	34.181	34.185	34.189	34.193	34.197	34.201	34.205	34.209
869	34.213	34.216	34.220	34.224	34.228	34.232	34.236	34.240	34.244	34.248
870	34.252	34.256	34.260	34.264	34.268	34.272	34.276	34.279	34.283	34.287
871	34.291	34.295	34.299	34.303	34.307	34.311	34.315	34.319	34.323	34.327
872	34.331	34.335	34.339	34.342	34.346	34.350	34.354	34.358	34.362	34.366
873	34.370	34.374	34.378	34.382	34.386	34.390	34.394	34.398	34.402	34.405
874	34.409	34.413	34.417	34.421	34.425	34.429	34.433	34.437	34.441	34.445
875	34.449	34.453	34·457	34.461	34.464	24.468	34.472	34.476	34.480	34.484
876	34.488	34.492	34·496	34.500	34.504	34.508	34.512	34.516	34.520	34.524
877	34.527	34.531	34·535	34.539	34.543	34.547	34.551	34.555	34.559	34.563
878	34.567	34.571	34·575	34.579	34.583	34.587	34.590	34.594	34.598	34.602
879	34.606	34.610	34·614	34.618	34.622	34.626	34.630	34.634	34.638	34.642
880	34.646	34.650	34.653	34.657	34.661	34.665	34.669	34.673	34.677	34.681
881	34.685	34.689	34.693	34.697	34.701	34.705	34.709	34.713	34.716	34.720
882	34.724	34.728	34.732	34.736	34.740	34.744	34.748	34.752	34.756	34.760
883	34.764	34.768	34.772	34.776	34.779	34.783	34.787	34.791	34.795	34.799
884	34.803	34.807	34.811	34.815	34.819	34.823	34.827	34.831	34.835	34.839
885	34.842	34.846	34.850	34.854	34.858	34.862	34.866	34.870	34.874	34.878
886	34.882	34.886	34.890	34.894	34.898	34.902	34.905	34.909	34.913	34.917
887	34.921	34.925	34.929	34.933	34.937	34.941	34.945	34.949	34.953	34.957
888	34.961	34.964	34.968	34.972	34.976	34.980	34.984	34.988	34.992	34.996
889	35.000	35.004	35.008	35.012	35.016	35.020	35.024	35.027	35.031	35.035
890	35.039	35.043	35.047	35.051	35.055	35.059	35.063	35.067	35.071	35.075
891	35.079	35.083	35.087	35.090	35.094	35.098	35.102	35.106	35.110	35.114
892	35.118	35.122	35.126	35.130	35.134	35.138	35.142	35.146	35.150	35.153
893	35.157	35.161	35.165	35.169	35.173	35.177	35.181	35.185	35.189	35.193
894	35.197	35.201	35.205	35.209	35.213	35.216	35.220	35.224	35.228	35.232
895	35.236	35.240	35.244	35.248	35.252	35.256	35.260	35.264	35.268	35.272
896	35.276	35.279	35.283	35.287	35.291	35.295	35.299	35.303	35.307	35.311
897	35.315	35.319	35.323	35.327	35.331	35.335	35.339	35.342	35.346	35.350
898	35.354	35.358	35.362	35.366	35.370	35.374	35.378	35.382	35.386	35.390
899	35.394	35.398	35.402	35.405	35.409	35.413	35.417	35.421	35.425	35.429
900	35-433	35-437	35.441	35-445	35.449	35.453	35-457	35.461	35.464	35.468

1 mm. = 0.03937 inch.

			·					1	1	1
Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
900	35.433	35.437	35.441	35.445	35.449	35.453	35.457	35.461	35.464	35.468
901	35.472	35.476	35.480	35.484	35.488	35.492	35.496	35.500	35.504	35.508
902	35.512	35.516	35.520	35.524	35.527	35.531	35.535	35.539	35.543	35.547
903	35.551	35.555	35.559	35.563	35.567	35.571	35.575	35.579	35.583	35.587
904	35.590	35.594	35.598	35.602	35.606	35.610	35.614	35.618	35.622	35.626
905	35.630	35.634	35.638	35.642	35.646	35.650	35.653	35.657	35.661	35.665
906	35.669	35.673	35.677	35.681	35.685	35.689	35.693	35.697	35.701	35.705
907	35.709	35.713	35.716	35.720	35.724	35.728	35.732	35.736	35.740	35.744
908	35.748	35.752	35.756	35.760	35.764	35.768	35.772	35.776	35.779	35.783
909	35.787	35.791	35.795	35.799	35.803	35.807	35.811	35.815	35.819	35.823
910	35.827	35.831	35.835	35.839	35.842	35.846	35.850	35.854	35.858	35.862
911	35.866	35.870	35.874	35.878	35.882	35.886	35.890	35.894	35.898	35.902
912	35.905	35.909	35.913	35.917	35.921	35.925	35.929	35.933	35.937	35.941
913	35.945	35.949	35.953	35.957	35.961	35.964	35.968	35.972	35.976	35.980
914	35.984	35.988	35.992	35.996	36.000	36.004	36.008	36.012	36.016	36.020
915	36.024	36.027	36.031	36.035	36.039	36.043	36.047	36.051	36.055	36.059
916	36.063	36.067	36.071	36.075	36.079	36.083	36.087	36.090	36.094	36.098
917	36.102	36.106	36.110	36.114	36.118	36.122	36.126	36.130	36.134	36.138
918	36.142	36.146	36.150	36.153	36.157	36.161	36.165	36.169	36.173	36.177
919	36.181	36.185	36.189	36.193	36.197	36.201	36.205	36.209	36.213	36.216
920	36.220	36.224	36.228	36.232	36.236	36.240	36.244	36.248	36.252	36.256
921	36.260	36.264	36.268	36.272	36.276	36.279	36.283	36.287	36.291	36.295
922	36.299	36.303	36.307	36.311	36.315	36.319	36.323	36.327	36.331	36.335
923	36.339	36.342	36.346	36.350	36.354	36.358	36.362	36.366	36.370	36.374
924	36.378	36.382	36.386	36.390	36.394	36.398	36.402	36.405	36.409	36.413
925	36.417	36.421	36.425	36.429	36.433	36.437	36.441	36.445	36.449	36.453
926	36.457	36.461	36.464	36.468	36.472	36.476	36.480	36.484	36.488	36.492
927	36.496	36.500	36.504	36.508	36.512	36.516	36.520	36.524	36.527	36.531
928	36.535	36.539	36.543	36.547	36.551	36.555	36.559	36.563	36.567	36.571
929	36.575	36.579	36.583	36.587	36.590	36.594	36.598	36.602	36.606	36.610
930	36.614	36.618	36.622	36.626	36.630	36.634	36.638	36.642	36.646	36.650
931	36.653	36.657	36.661	36.665	36.669	36.673	36.677	36.681	36.685	36.689
932	36.693	36.697	36.701	36.705	36.709	36.713	36.716	36.720	36.724	36.728
933	36.732	36.736	36.740	36.744	36.748	36.752	36.756	36.760	36.764	36.768
934	36.772	36.776	36.779	36.783	36.787	36.791	36.795	36.799	36.803	36.807
935	36.811	36.815	36.819	36.823	36.827	36.831	36.835	36.839	36.842	36.846
936	36.850	36.854	36.858	36.862	36.866	36.870	36.874	36.878	36.882	36.886
937	36.890	36.894	36.898	36.902	36.905	36.909	36.913	36.917	36.921	36.925
938	36.929	36.933	36.937	36.941	36.945	36.949	36.953	36.957	36.961	36.964
939	36.968	36.972	36.976	36.980	36.984	36.988	36.992	36.996	37.000	37.004
940	37.008	37.012	37.016	37.020	37.024	37.027	37.031	37.035	37.039	37.043
941	37.047	37.051	37.055	37.059	37.063	37.067	37.071	37.075	37.079	37.083
942	37.087	37.090	37.094	37.098	37.102	37.106	37.110	37.114	37.118	37.122
943	37.126	37.130	37.134	37.138	37.142	37.146	37.150	37.153	37.157	37.161
944	37.165	37.169	37.173	37.177	37.181	37.185	37.189	37.193	37.197	37.201
945	37.204	37.208	37.212	37.216	37.220	37.224	37.228	37.232	37.236	37.240
946	37.244	37.248	37.252	37.256	37.260	37.264	37.268	37.272	37.276	37.279
947	37.283	37.287	37.291	37.295	37.299	37.303	37.307	37.311	37.315	37.319
948	37.323	37.327	37.331	37.335	37.339	37.342	37.346	37.350	37.354	37.358
949	37.362	37.366	37.370	37.374	37.378	37.382	37.386	37.390	37.394	37.398
950	37.402	37-405	37.409	37.413	37.417	37.421	3 7.42 5	3 7.42 9	37-433	37.437

r mm. = 0.03937 inch.

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
950	37.402	37.405	37.409	37.413	37.417	37.421	37.425	37.429	37.433	37.437
951	37.441	37.445	37.449	37.453	37.457	37.461	37.464	37.468	37.472	37.476
952	37.480	37.484	37.488	37.492	37.496	37.500	37.504	37.508	37.512	37.516
953	37.520	37.524	37.527	37.531	37.535	37.539	37.543	37.547	37.551	37.555
954	37.559	37.563	37.567	37.571	37.575	37.579	37.583	37.587	37.590	37.594
955	37.598	37.602	37.606	37.610	37.614	37.618	37.622	37.626	37.630	37.634
956	37.638	37.642	37.646	37.650	37.653	37.657	37.661	37.665	37.669	37.673
957	37.677	37.681	37.685	37.689	37.693	37.697	37.701	37.705	37.709	37.713
958	37.716	37.720	37.724	37.728	37.732	37.736	37.740	37.744	37.748	37.752
959	37.756	37.760	37.764	37.768	37.772	37.776	37.779	37.783	37.787	37.791
960	37·795	37.799	37.803	37.807	37.811	37.815	37.819	37.823	37.827	37.831
961	37·835	37.839	37.842	37.846	37.850	37.854	37.858	37.862	37.866	37.870
962	37·874	37.878	37.882	37.886	37.890	37.894	37.898	37.901	37.905	37.909
963	37·9 ¹ 3	37.917	37.921	37.925	37.929	37.933	37.937	37.941	37.945	37.949
964	37·953	37.957	37.961	37.964	37.968	37.972	37.976	37.980	37.984	37.988
965	37.992	37.996	38.000	38.004	38.008	38.012	38.016	38.020	38.024	38.027
966	38.031	38.035	38.039	38.043	38.047	38.051	38.055	38.059	38.063	38.067
967	38.071	38.075	38.079	38.083	38.087	38.090	38.094	38.098	38.102	38.106
968	38.110	38.114	38.118	38.122	38.126	38.130	38.134	38.138	38.142	38.146
969	38.150	38.153	38.157	38.161	38.165	38.169	38.173	38.177	38.181	38.185
970	38.189	38.193	38.197	38.201	38.205	38.209	38.213	38.216	38.220	38.224
971	38.228	38.232	38.236	38.240	38.244	38.248	38.252	38.256	38.260	38.264
972	38.268	38.272	38.276	38.279	38.283	38.287	38.291	38.295	38.299	38.303
973	38.307	38.311	38.315	38.319	38.323	38.327	38.331	38.335	38.339	38.342
974	38.346	38.350	38.354	38.358	38.362	38.366	38.370	38.374	38.378	38.382
975	38.386	38.390	38.394	38.398	38.401	38.405	38.409	38.413	38.417	38.421
976	38.425	38.429	38.433	38.437	38.441	38.445	38.449	38.453	38.457	38.461
977	38.464	38.468	38.472	38.476	38.480	38.484	38.488	38.492	38.496	38.500
978	38.504	38.508	38.512	38.516	38.520	38.524	38.527	38.531	38.535	38.539
979	38.543	38.547	38.551	38.555	38.559	38.563	38.567	38.571	38.575	38.579
980	38.583	38.587	38.590	38.594	38.598	38.602	38.606	38.610	38.614	38.618
981	38.622	38.626	38.630	38.634	38.638	38.642	38.646	38.650	38.653	38.657
982	38.661	38.665	38.669	38.673	38.677	38.681	38.685	38.689	38.693	38.697
983	38.701	38.705	38.709	38.713	38.716	38.720	38.724	38.728	38.732	38.736
984	38.740	38.744	38.748	38.752	38.756	38.760	38.764	38.768	38.772	38.776
985	38.780	38.783	38.787	38.791	38.795	38.799	38.803	38.807	38.811	38.815
986	38.819	38.823	38.827	38.831	38.835	38.839	38.842	38.846	38.850	38.854
987	38.858	38.862	38.866	38.870	38.874	38.878	38.882	38.886	38.890	38.894
988	38.898	38.901	38.905	38.909	38.913	38.917	38.921	38.925	38.929	38.933
989	38.937	38.941	38.945	38.949	38.953	38.957	38.961	38.964	38.968	38.972
990	38.976	38.980	38.984	38.988	38.992	38.996	39.000	39.004	39.008	39.012
991	39.016	39.020	39.024	39.027	39.031	39.035	39.039	39.043	39.047	39.051
992	39.055	39.059	39.063	39.067	39.071	39.075	39.079	39.083	39.087	39.090
993	39.094	39.098	39.102	39.106	39.110	39.114	39.118	39.122	39.126	39.130
994	39.134	39.138	39.142	39.146	39.150	39.153	39.157	39.161	39.165	39.169
995 996 997 998 999	39.173 39.213 39.252 39.291 39.331	39.177 39.216 39.256 39.295 39.335	39.181 39.220 39.260 39.299 39.339	39.185 39.224 39.264 39.303 39.342	39.268 39.307	39.193 39.232 39.272 39.311 39.350	39.197 39.236 39.276 39.315 39.354	39.201 39.240 39.279 39.319 39.358	39.205 39.244 39.283 39.323 39.362	39.209 39.248 39.287 39.327 39.366
1000	39.370	39-374	39.378	39.382	39.386	39.390	39-394	39.398	39.401	39.405

TABLE 11.

BAROMETRIC INCHES (MERCURY) INTO MILLIBARS.

1 inch = 33.86395 mb.

···					_ 33.60,					
Inches	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mb.	mb.	mb.	mb.						
0.0	0.00	0.34	0.68	1.02	1.35	1.69	2.03	2.37	2.71	3.05
0.1	3.39	3.73	4.06	4.40	4.74	5 .0 8	5.42 8.80	5.76	6.10	3.05 6.43
0.2	6.77	7.11	7.45	7.79	8.13	8.47		9.14	9.48	9.82
0.3	10.16	10.50	10.84	11.18	11.51	11.85	12.19	12.53	12.87	13.21
0.4	13.55	13.88	14.22	14.56	14.90	15.24	15.58	15.92	16.25	16.59
0.5	16.93	17.27	17.61	17.95	18.29	18.63	18.96	19.30	19.64	19.98
0.6	20.32	20.66	21.00	21.33	21.67	22.01	22.35	22.69	23.03	23.37
0.7	23.70	24.04	24.38	24.72	25.06	25.40	25.74	26.08	26.41	26.75
0.8	27.00	27.43	27.77	28.11	28.45	28.78	29.12	29.46	29.80	30.14
0.9	30.48	30.82	31.15	31.49	31.83	32.17	32.51	32.85	33.19	33.53
1.0	33.86	34.20	34.54	34.88	35.22	35.56	35.90	36.23	36.57	36.91
1.1	37.25	37.59	37.93	38.27	38.60	38.94	39.28	39.62	39.96	40.30
1.2	40.64	40.98	41.31	41.65	41.99	42.33	42.67	. 43.01	43.35	43.68
1.3	44.02 47.41	44.36	44.70 48.00	45.04 48.43	45.38 48.76	45.72 49.10	46.05 49.44	46.39 49.78	46.73 50.12	47.07 50.46
1.4	47.41	47.73	40.09	40.43	40.70	49.10	49.44	49.70	30.12	30.40
1.5	50.80	51.13	51.47	51.81	52.15	52.49	52.83	53.17	53.51	53.84
1.6	54.18	54.52	54.86	55.20	55.54	55.88	56.21	56.55	56.89	57.23
1.7	57.57	57.91	58.25	58.58	58.92	59.26	59.60	59.94	60.28	60.62
1.8	60.96	61.20	61.63	61.97	62.31	62.65	62.99	63.33	63.66	64.00
1.9	64.34	64.68	65.02	65.36	65.70	66.03	66.37	66.71	67.05	67.39
2.0	67.73	68.07	68.41	68.74	69.08	69.42	69.76	70.10	70.44	70.78
2.1	71.11	71.45	71.79	72.13	72.47	72.81	73.15	73.48	73.82	74.16
2.2	74.50	74.84	75.18	75.52	75.86	76.19	76.53	76.87	77.21	77.55
2.3	77.89	78.23	78.56	78.90	79.24	79.58	79.92	80.26	80.60	80.93
2.4	81.27	81.61	81.95	82.29	82.63	82.97	83.31	83.64	83.98	84.32
25.0	846.6	846.9	847.3	847.6	848.0	848.3	848.6	849.0	849.3	849.6
25.1	850.0	850.3	850.7	851.0	851.3	851.7	852.0	852.4	852.7	853.0
25.2	853.4	853.7	854.0	854.4	854.7	855.1	855.4	855.7	856.1	856.4
25.3	856.8	857.1	857.4 860.8	857.8	858.1	858.5	858.8 862.2	859.1	859.5	859.8
25.4	860.1	860.5	000.0	861.2	861.5	861.8	002.2	862.5	862.9	863.2
25.5	863.5	863.9	864.2	864.5	864.9	865.2	865.6	865.9	866.2	866.6
25.6	866.9	867.3	867.6	867.9	868.3	868.6	868.9	869.3	869.6	870.0
25.7	870.3	870.7	871.0	871.3	871.7	872.0	872.3	872.7	873.0	873.4
25.8	873.7	874.0	874.4	874.7	875.0	875.4	875.7	876.1	876.4	876.7 880.1
25.9	877.1	877.4	877.8	878.1	878.4	878.8	879.1	879.4	879.8	300.1
26.0	880.5	880.8	881.1	881.5	881.8	882.2	882.5	882.8	883.2	883.5
26.1	883.8	884.2	884.5	884.9	885.2	885.5	885.9	886.2	886.6	886.9
26.2	887.2	887.6	887.9	888.3	888.6	888.9	889.3	889.6	889.9	890.3
26.3	890.6	891.0	891.3	891.6	892.0	892.3	892.7 806.0	893.0 896.4	893.3 896.7	893.7
26.4	894.0	894.3	894.7	895.0	895.4	895.7	390.0	090.4	390.7	897.1
26.5	897.4	897.7	898.1	898.4	898.7	899.1	899.4	899.8	900.1	900.4
26.6	900.8	901.1	901.5	901.8	902.1	902.5	902.8	903.2	903.5	903.8
26.7 26.8	904.2	904.5	904.8 908.2	905.2 908.6	905.5	905.9 909.2	906.2 909.6	906.5 909.9	906.9 910.3	907.2 910.6
26.0	907.0	911.3	911.6	912.0	912.3	909.2	913.0	913.3	913.6	914.0
	920.9									
27.0	914.3	914.7	915.0	915.3	915.7	916.0	916.4	916.7	917.0	917.4
27.1	917.7	918.1	918.4	918.7	919.1	919.4 922.8	919.7	920.1	92 0.4 923.8	920.8
27.2	921.1 924.5	921.4 924.8	921.8 925.2	922.1 925.5	922.5 925.8	922.0	923. 1 926.5	923.5 926.9	923.0	924.I 927.5
27.3 27.4	924.3	924.0	923.2	923.3	923.0	929.6	920.3	930.2	930.6	930.9
~/.4	9-1-9	920.2	9-0.0	3-0.9	,-,-	, , , , ,	2-2-2	,,,,,	70	70-19

BAROMETRIC INCHES (MERCURY) INTO MILLIBARS.

1 inch = 33.86395 mb.

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
27.5	931.3	931.6	931.9	932.3	932.6	933.0	933-3	933.6	934.0	934.3
27.6	934.6	935.0	935.3	935.7	936.0	936.3	936.7	937.0	937-4	937.7
27.7	938.0	938.4	938.7	939.0	939.4	939.7	940.1	940.4	940.7	941.1
27.8	941.4	941.8	942.1	942.4	942.8	943.1	943.4	943.8	944.1	944.5
27.9	944.8	945.1	945.5	945.8	946.2	946.5	946.8	947.2	947-5	947-9
28.0	948.2	948.5	948.9	949.2	949.5	949.9	950.2	950.6	950.9	951.2
28.1	951.6	951.9	952.3	952.6	952.9	953.3	953.6	953.9	954-3	954.6
28.2	955.0	955-3	955.6	956.0	956.3	956.7	957.0	957-3	957.7	958.0
28.3	958.3	958.7	959.0	959.4	959.7	960.0	960.4	960.7	961.1	961.4
28.4	961.7	962.1	962.4	962.8	963.1	963.4	963.8	964.1	964.4	964.8
28.5	965.1	965.5	965.8	966. 1	966.5	966.8	967.2	967.5	967.8	968.2
28.6	968.5	968.8	969.2	969.5	969.9	970.2	970.5	970.9	971.2	971.6
28.7	971.9	972.2	972.6	. 972.9	973.2	973.6	973.9	974.3	974.6	974.9
28.8	975.3	975.6	976.0	976.3	976.6	977.0	977.3	977.7	978.0	978.3
28.9	978.7	979.0	979-3	979.7	980.0	980.4	980.7	981.0	981.4	981.7
29.0	982.1	982.4	982.7	983.1	983.4	983.7	984.1	984.4	984.8	985.1
29.1	985.4	985.8	986.1	986.5	986.8	987.1	987.5	987.8	988.2	988.5
29.2	988.8	989.2	989.5	989.8	990.2	990.5	990.9	991.2	991.5	991.9
29.3	992.2	992.6	992.9	993.2	993.6	993.9	994.2	994.6	994.9	995.3
29.4	995.6	995.9	996.3	996.6	997.0	997.3	997.6	998.0	998.3	998.6
29.5	999.0	999.3	999.7	1000.0	1000.4	1000.7	1001.0	1001.4	1001.7	1002.0
29.6	1002.4	1002.7	1003.1	1003.4	1003.7	1004.1	1004.4	1004.7	1005.1	1005.4
29.7	1005.8	1006.1	1006.4	1006.8	1007.1	1007.5	1007.8	1008.1	1008.5	1008.8
29.8	100g.1	1009.5	1009.8	1010.2	1010.5	1010.8	1011.2	1011.5	1011.9	1012.2
29.9	1012.5	1012.9	1013.2	1013.5	1013.9	1014.2	1014.6	1014.9	1015.2	1015.6
30.0	1015.9	1016.3	1016.6	1016.9	1017.3	1017.6	1018.0	1018.3	1018.6	1019.0
30.1	1019.3	1019.6	1020.0	1020.3	1020.7	1021.0	1021.3	1021.7	1022.0	1022.4
30.2	1022.7	1023.0	1023.4	1023.7	1024.0	1024.4	1024.7	1025.1	1025.4	1025.7
30.3	1026.1	1026.4	1026.8	1027.1	1027.4	1027.8	1028.1	1028.4	1028.8	1029.1
30.4	1029.5	1029.8	1030.1	1030.5	1030.8	1031.2	1031.5	1031.8	1032.2	1032.5
30.5	1032.0	1033.2	1033.5	1033.9	1034.2	1034.5	1034.9	1035.2	1035.6	1035.9
30.6	1036.2	1036.6	1036.9	1037.3	1037.6	1037.9	1038.3	1038.6	1038.9	1039.3
30.7	1039.6	1040.0	1040.3	1040.6	1041.0	1041.3	1041.7	1042.0	1042.3	1042.7
30.8	1043.0	1043.3	1043.7	1044.0	1044.4	1044.7	1045.0	1045.4	1045.7	1046.1
30.9	1046.4	1046.7	1047.1	1047.4	1047.8	1048.1	1048.4	1048.8	1049.1	1049.5
31.0	1049.8	1050.1	1050.5	1050.8	1051.1	1051.5	1051.8	1052.2	1052.5	1052.8
31.1	1053.2	1053.5	1053.8	1054.2	1054.5	1054.9	1055.2	1055.5	1055.9	1056.2
31.2	1056.6	1056.9	1057.2	1057.6	1057.9	1058.2	1058.6	1058.9	1059.3	1059.6
31.3	1059.9	1060.3	1060.6	1061.0	1061.3	1061.6	1062.0	1062.3	1062.7	1063.0
31.4	1063.3	1063.7	1064.0	1064.3	1064.7	1065.0	1065.4	1065.7	1066.0	1066.4
31.5	1066.7	1067.1	1067.4	1067.7	1068.1	1068.4	1068.7	1069.1	1069.4	1069.8
31.6	1070.1	1070.4	1070.8	1071.1	1071.5	1071.8	1072.1	1072.5	1072.8	1073.1
31.7	1073.5	1073.8	1074.2	1074.5	1074.8	1075.2	1075.5	1075.9	1076.2	1076.5
31.8	1076.9	1077.2	1077.6	1077.9	1078.2	1078.6	1078.9	1079.2	1079.6	1079.9
31.9	1080.3	1080.6	1080.9	1081.3	1081.6	1082.0	1082.3	1082.6	1083.0	1083.3
										<u> </u>

Table 12.

BAROMETRIC MILLIMETERS (MERCURY) INTO MILLIBARS.

1 mm. = 1.33322387 mb.

0	Milli- meters.	o	1	2	3	4	5	6	7	8	9
10		mb.									
100	0	0	1.3	2.7	4.0	5.3	6.7	8.0	9.3	10.7	12.0
30				16.0	17.3		20.0	21.3		24.0	25.3
40 53.3 54.7 56.0 57.3 58.7 60.0 61.3 62.7 64.0 65.3 50 66.7 68.0 69.3 70.7 72.0 73.3 74.7 76.0 77.3 78.7 60 80.0 81.3 82.7 84.0 85.3 86.7 88.0 89.3 90.7 90.0 70 93.3 94.7 96.0 97.3 98.7 100.0 101.3 102.7 104.0 105.3 80 106.7 108.0 109.3 110.7 112.0 113.3 114.7 116.0 117.3 118.7 90 120.0 121.3 122.7 124.0 125.3 126.7 128.0 129.3 130.7 132.0 100 133.3 134.7 136.0 137.3 138.7 140.0 141.3 142.7 144.0 145.3 120 160.0 161.3 162.7 164.0 165.3 166.7 168.0 169.3 170.7 172.0 130 173.3 174.7 176.0 177.3 178.7 180.0 181.3 182.7 184.0 185.3 140 186.7 188.0 189.3 190.7 192.0 193.3 194.7 196.0 197.3 198.7 150 200.0 201.3 202.7 204.0 205.3 206.6 208.0 209.3 210.6 213.3 214.6 216.0 217.3 218.6 220.0 221.3 222.6 224.0 225.3 230.6 233.0 233.3 234.6 236.0 237.3 238.6 190 253.3 254.6 256.0 257.3 258.6 260.0 261.3 262.6 264.0 265.3 260.0 261.3 262.6 264.0 265.3 260.0 261.3 262.6 264.0 265.3 260.0 261.3 262.6 264.0 265.3 260.0 261.3 322.0 260.0 261.3 322.0 260.0 261.3 322.0 260.0 260.0 261.3 322.0 260.0 260.0 261.3 322.0 260.0 2						_			1 -		38.7
50 66.7 68.0 69.3 70.7 72.0 73.3 74.7 76.0 77.3 78.7 60 80.0 81.3 82.7 84.0 85.3 86.7 88.0 89.3 90.7 92.0 70 93.3 94.7 96.0 97.3 98.7 100.0 101.3 102.7 104.0 105:3 80 106.7 108.0 109.3 110.7 112.0 113.3 114.7 116.0 117.3 118.7 129.3 130.7 132.0 100 133.3 134.7 148.0 149.3 150.7 152.0 153.3 154.7 156.0 157.3 158.7 140.0 141.3 142.7 144.0 145.3 142.7 144.0 145.3 150.7 152.0 153.3 154.7 156.0 157.3 158.7 156.0 157.3 158.7 156.0 157.3 158.7 156.0 160.3 167.7 178.7 180.0 181.3 182.7 <th></th> <td></td>											
60 80.0 81.3 82.7 84.0 85.3 86.7 88.0 89.3 90.7 92.6 70 93.3 94.7 96.0 97.3 98.7 100.0 101.3 102.7 104.0 105.3 80 106.7 108.0 109.3 110.7 112.0 113.3 114.7 116.0 117.3 118.7 90 120.0 121.3 122.7 124.0 125.3 126.7 128.0 129.3 130.7 132.0 100 133.3 134.7 136.0 137.3 150.7 152.0 153.3 154.7 156.0 157.3 158.7 120 160.0 161.3 162.7 164.0 165.3 166.7 168.0 169.3 170.7 172.0 130 173.3 174.7 176.0 177.3 178.7 180.0 187.3 182.7 184.0 185.3 190.7 192.0 193.3 194.7 196.0 197.3 198.7	40	53.3	54.7	50.0	57.3	50.7	00.0	01.3	02.7	04.0	05.3
60 80.0 81.3 82.7 84.0 85.3 86.7 88.0 89.3 90.7 92.6 70 93.3 94.7 96.0 97.3 98.7 100.0 101.3 102.7 104.0 105.3 80 106.7 108.0 109.3 110.7 112.0 113.3 114.7 116.0 117.3 118.7 90 120.0 121.3 122.7 124.0 125.3 126.7 128.0 129.3 130.7 132.0 100 146.7 148.0 149.3 150.7 152.0 153.3 154.7 156.0 157.3 158.7 120 160.0 161.3 162.7 164.0 165.3 160.7 168.0 169.3 170.7 172.0 130 173.3 174.7 176.0 177.3 178.7 180.0 187.3 182.7 184.0 185.3 140.7 186.0 189.3 190.7 192.0 193.3 194.7 196.0	50	66.7	68.0	60.3	70.7	72.0	73.3	74.7	76.0	77.3	78.7
80 106,7 108,0 109,3 110,7 112.0 113,3 114,7 116.0 117,3 118,7 90 120.0 121,3 122,7 124.0 125,3 126,7 128.0 129,3 130,7 132.0 100 133,3 134,7 136.0 137,3 138,7 140.0 141,3 142,7 144.0 145,3 120 160.0 161,3 162,7 164.0 165,3 166,7 168.0 169,3 170,7 172.0 130 173,3 174,7 176.0 177,3 178,7 180.0 181,3 182,7 184.0 185,3 140 186,7 188.0 189,3 190.7 192.0 193,3 194.7 196.0 197,3 198.7 150 200.0 201,3 202.7 204.0 205,3 206.6 208.0 293,3 221.6 224.0 225.3 286.0 228.0 229,3 230.6 232.0 221.3	60		81.3				86.7		89.3		92.0
100				96.0	97.3	98.7	100.0	101.3			105:3
100		,									1 1
110	90	120.0	121.3	122.7	124.0	125.3	120.7	128.0	129.3	130.7	132.0
110	100	133.3	134.7	136.0	137.3	138.7	140.0	141.3	142.7	144.0	145.3
120	1			149.3			153.3		156.0	157.3	158.7
140			161.3		164.0		166.7				172.0
150											185.3
160 213.3 214.6 216.0 217.3 218.6 220.0 221.3 222.6 224.0 225.3 170 226.6 228.0 229.3 230.6 232.0 233.3 234.6 236.0 237.3 238.6 180 240.0 241.3 242.6 244.0 245.3 246.6 248.0 249.3 250.6 252.0 190 253.3 254.6 256.0 257.3 258.6 260.0 261.3 262.6 264.0 265.3 200 266.6 268.0 269.3 270.6 272.0 273.3 274.6 276.0 277.3 278.6 210 280.0 281.3 282.6 284.0 285.3 286.6 288.0 289.3 290.6 292.0 220 293.3 294.6 296.0 297.3 298.6 300.0 301.3 302.6 304.0 305.3 230 333.3 334.6 336.0 337.3 338.0 <	140	180.7	188.0	189.3	190.7	192.0	193.3	194.7	190.0	197.3	198.7
160 213.3 214.6 216.0 217.3 218.6 220.0 221.3 222.0 224.0 225.3 170 226.6 228.0 229.3 230.6 232.0 233.3 234.6 236.0 237.3 238.6 180 240.0 241.3 242.6 244.0 245.3 246.6 248.0 249.3 250.6 252.0 190 253.3 254.6 256.0 257.3 258.6 260.0 261.3 262.6 264.0 265.3 200 266.6 268.0 269.3 270.6 272.0 273.3 274.6 276.0 277.3 278.6 210 280.0 281.3 282.6 284.0 285.3 286.6 288.0 289.3 290.6 292.0 230 306.6 308.0 309.3 310.6 312.0 313.3 314.6 316.0 317.3 318.6 240 320.0 321.3 322.6 324.0 325.3 <	150	200.0	201.3	202.7	204.0	205.3	206.6	208.0	200.3	210.6	212.0
170	160	213.3					220.0				
190 253.3 254.6 256.0 257.3 258.6 260.0 261.3 262.6 264.0 265.3 200 266.6 268.0 269.3 270.6 272.0 273.3 274.6 276.0 277.3 278.6 210 280.0 281.3 282.6 284.0 285.3 286.6 288.0 289.3 290.6 292.0 220 293.3 294.6 296.0 297.3 298.6 380.0 301.3 302.6 304.0 305.3 230 306.6 308.0 309.3 310.6 312.0 313.3 314.6 316.0 317.3 318.6 240 320.0 321.3 322.6 324.0 325.3 326.6 328.0 329.3 330.6 332.0 250 333.3 334.6 336.0 337.3 338.6 340.0 341.3 342.6 344.0 345.3 260 346.6 348.0 349.3 350.6 352.0 <						232.0			236.0	237.3	238.6
200 266.6 268.0 269.3 270.6 272.0 273.3 274.6 276.0 277.3 278.6 210 280.0 281.3 282.6 284.0 285.3 286.6 288.0 289.3 290.6 292.0 220 293.3 294.6 296.0 297.3 298.6 300.3 301.3 302.6 304.0 305.3 230 306.6 308.0 309.3 310.6 312.0 313.3 314.6 316.0 317.3 318.6 240 320.0 321.3 322.6 324.0 325.3 326.6 328.0 329.3 330.6 332.0 250 333.3 334.6 336.0 337.3 338.6 340.0 341.3 342.6 344.0 345.3 260 346.6 348.0 349.3 350.6 352.0 353.3 354.6 356.0 357.3 358.6 270 360.0 361.3 362.6 364.0 365.3 <										250.6	252.0
210	190	253.3	254.6	256.0	257.3	258.6	200.0	201.3	202.6	204.0	265.3
210	200	266.6	268.0	260.3	270.6	272:0	273.3	274.6	276.0	277.3	278.6
220 293.3 294.6 296.0 297.3 298.6 300.0 301.3 302.6 304.0 305.3 230 306.6 308.0 309.3 310.6 312.0 313.3 314.6 316.0 317.3 318.6 240 320.0 321.3 322.6 324.0 325.3 326.6 328.0 329.3 330.6 317.3 318.6 250 333.3 334.6 336.0 337.3 350.0 353.3 354.6 356.0 357.3 358.6 270 360.0 361.3 362.6 364.0 365.3 366.6 368.0 359.3 370.6 372.0 280 373.3 374.6 376.0 377.3 378.6 380.0 381.3 382.6 384.0 385.3 290 386.6 388.0 389.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 300 400.0 401.3 402.6 404.0 <											202.0
240 320.0 321.3 322.6 324.0 325.3 326.6 328.0 329.3 330.6 332.0 250 333.3 334.6 336.0 337.3 338.6 340.0 341.3 342.6 344.0 345.3 260 346.6 348.0 340.3 350.6 352.0 353.3 354.6 356.0 357.3 358.6 270 360.0 361.3 362.6 364.0 365.3 366.6 368.0 369.3 370.6 372.0 280 373.3 374.6 376.0 377.3 378.6 380.0 381.3 382.6 384.0 385.3 290 386.6 388.0 389.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 300 400.0 401.3 402.6 404.0 405.3 406.6 408.0 409.3 410.6 412.0 310 413.3 414.6 416.0 417.3 418.6 <	220	293.3		296.0	297.3		300.0	301.3		304.0	305.3
250 333.3 334.6 336.0 337.3 338.6 340.0 341.3 342.6 344.0 345.3 350.6 350.0 357.3 358.6 360.0 361.3 362.6 364.0 365.3 366.6 368.0 369.3 370.6 372.0 386.6 388.0 389.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 380.0 392.0 393.3 394.6 396.0 397.3 398.6 380.0 392.0 393.3 394.6 396.0 397.3 398.6 380.0 381.3 382.6 384.0 385.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 380.0 390.6 392.0 393.3 394.6 396.0 397.3 398.6 390.0 39			308.0								318.6
260 346.6 348.0 349.3 350.6 352.0 353.3 354.6 356.0 357.3 358.6 270 360.0 361.3 362.6 364.0 365.3 366.6 368.0 369.3 370.6 372.0 380.3 382.6 388.0 389.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 390.0 490.0 420.	240	320.0	321.3	322.6	324.0	325.3	320.6	328.0	329.3	330.6	332.0
260 346.6 348.0 349.3 350.6 352.0 353.3 354.6 356.0 357.3 358.6 270 360.0 361.3 362.6 364.0 365.3 366.6 368.0 369.3 370.6 372.0 380.3 382.6 388.0 389.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 390.0 490.0 420.	250	222.2	334.6	336.0	337.3	338.6	340.0	341.3	342.6	344.0	345.3
270 360.0 361.3 362.6 364.0 365.3 366.6 368.0 369.3 370.6 372.0 280 373.3 374.6 376.0 377.3 378.6 380.0 381.3 382.6 384.0 385.3 290 386.6 388.0 389.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 300 400.0 401.3 402.6 404.0 405.3 406.6 408.0 409.3 410.6 412.0 310 413.3 414.6 446.0 417.3 418.6 420.0 421.3 422.6 424.0 425.3 320 426.6 428.0 429.3 430.6 432.0 433.3 434.6 446.0 447.0 445.3 340 453.3 454.6 444.0 445.3 446.6 448.0 449.3 450.6 450.0 350 466.6 468.0 469.3 470.6 472.0 473.3 474.6 476.0 477.3 478.6 360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 490.0 370 493.3 494.6						352.0	353.3			•	358.6
280 373.3 374.6 376.0 377.3 378.6 380.0 381.3 382.6 384.0 385.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 380.0 386.6 388.0 389.3 390.6 392.0 393.3 394.6 396.0 397.3 398.6 390.6 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 397.3 398.6 390.0 493.3 410.6 412.0 425.3 420.0 421.3 422.6 424.0 425.3 320 426.6 428.0 429.3 430.6 432.0 433.3 434.6 436.0 437.3 438.6 340.0 453.3 454.6 456.0 457.3 458.6 460.0 461.3 462.6 464.0 465.3 458.0 460.0 461.3 462.6 464.0 465.3 350 466.6 468.0 469.3 470.6 472.0 473.3 474.6 476.0 477.3 478.6 360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 492.0 370 493.3 494.6 496.0 497.3 498.6 500.0 501.3 502.6 504.0 505.3 380 506.6 508.0 509.3 510.6 512.0 513.3 514.6 516.0 517.3 518.6					364.0	365.3	366.6	368.0			372.0
300 400.0 401.3 402.6 404.0 405.3 406.6 408.0 409.3 410.6 412.0 310 413.3 414.6 416.0 417.3 418.6 420.0 421.3 422.6 424.0 425.3 320 426.6 428.0 429.3 430.6 432.0 433.3 434.6 436.0 437.3 438.6 340 453.3 454.6 456.0 457.3 458.6 460.0 461.3 462.6 464.0 465.3 350 466.6 468.0 469.3 470.6 472.0 473.3 474.6 476.0 477.3 478.6 360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 492.0 370 493.3 494.6 496.0 497.3 498.6 500.0 501.3 502.6 504.0 505.3 380 506.6 508.0 509.3 510.6 512.0 513.3 514.6 516.0 517.3 518.6						378.6					385.3
310 413.3 414.6 416.0 417.3 418.6 420.0 421.3 422.6 424.0 425.3 320 426.6 428.0 429.3 430.6 432.0 433.3 434.6 436.0 437.3 438.6 330 440.0 441.3 442.6 444.0 445.3 446.6 448.0 449.3 450.6 452.0 350 466.6 468.0 469.3 470.6 472.0 473.3 474.6 476.0 477.3 478.6 360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 492.0 370 493.3 494.6 496.0 497.3 498.6 500.0 501.3 502.6 504.0 505.3 380 506.6 508.0 509.3 510.6 512.0 513.3 514.6 516.0 517.3 518.6	290	386.6	388.0	389.3	390.0	392.0	393-3	394.6	396.0	397.3	398.6
310 413.3 414.6 416.0 417.3 418.6 420.0 421.3 422.6 424.0 425.3 320 426.6 428.0 429.3 430.6 432.0 433.3 434.6 436.0 437.3 438.6 330 440.0 441.3 442.6 444.0 445.3 446.6 448.0 449.3 450.6 452.0 350 466.6 468.0 469.3 470.6 472.0 473.3 474.6 476.0 477.3 478.6 360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 492.0 370 493.3 494.6 496.0 497.3 498.6 500.0 501.3 502.6 504.0 505.3 380 506.6 508.0 509.3 510.6 512.0 513.3 514.6 516.0 517.3 518.6	300	400.0	401.3	402.6	404.0	405.3	406.6	408.0	400.3	410.6	412.0
320							'				425.3
330			428.0			432.0			436.0	437-3	438.6
350 466.6 468.0 469.3 470.6 472.0 473.3 474.6 476.0 477.3 478.6 360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 492.0 370 493.3 494.6 496.0 497.3 498.6 500.0 501.3 502.6 504.0 505.3 380 506.6 508.0 509.3 510.6 512.0 513.3 514.6 516.0 517.3 518.6	330										452.0
360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 492.0 370 493.3 494.6 496.0 497.3 498.6 500.0 501.3 502.6 504.0 505.3 380 506.6 508.0 509.3 510.6 512.0 513.3 514.6 516.0 517.3 518.6	340	453-3	454.0	450.0	457-3	458.0	400.0	401.3	402.0	404.0	405.3
360 480.0 481.3 482.6 484.0 485.3 486.6 488.0 489.3 490.6 492.0 370 493.3 494.6 496.0 497.3 498.6 500.0 501.3 502.6 504.0 505.3 380 506.6 508.0 509.3 510.6 512.0 513.3 514.6 516.0 517.3 518.6	350	466.6	468.0	469.3	470.6	472.0	473-3	474.6	476.0	477.3	478.6
370				482.6		485.3					492.0
	370						•				505.3
# 200 #20.0 521.3 522.0 524.0 525.3 520.0 528.0 520.2 520.6 522.0			- 1			-			• .		518.6
1 340 3-10 3-10 3-10 3-10 3-10 3-10 3-10 3-1	390	520.0	521.3	522.0	524.0	525.3	520.0	528.0	529-3	530.6	532.0
400 533.3 534.6 536.0 537.3 538.6 540.0 541.3 542.6 544.0 545.3	400	533.3	534.6	536.0	537.3	538.6	540.0	541.3	542.6	544.0	545-3
410 546.6 548.0 549.3 550.6 552.0 553.3 554.6 556.0 557.3 558.6			548.0	549.3			553-3	554.6			558.6
420 560.0 561.3 562.6 564.0 565.3 566.6 568.0 569.3 570.6 572.0				562.6		565.3	566.6	568.o	569.3		572.0
											585.3
440 586.6 588.0 589.3 590.6 592.0 593.3 594.6 596.0 597.3 598.6	440	586.6	588.0	589.3	590.0	592.0	593.3	594.6	596.0	597.3	598.6

TABLE 12.
BAROMETRIC MILLIMETERS (MERCURY) INTO MILLIBARS.

l mm. = 1.33322387 mb.

		,								
Milli- meters,	0	1	2	3	4	5	6	7	8	9
450 460 470 480 490	mb. 600.0 613.3 626.6 639.9 653.3	mb. 601.3 614.6 627.9 641.3 654.6	mb. 602.6 615.9 629.3 642.6 655.9	mb. 604.0 617.3, 630.6 643.9 657.3	mb. 605.3 618.6 631.9 645.3 658.6	mb. 606.6 619.9 633.3 646.6 659.9	mb. 608.0 621.3 634.6 647.9 661.3	mb. 609.3 622.6 635.9 649.3 662.6	mb. 610.6 623.9 637.3 650.6 663.9	mb. 611.9 625.3 638.6 651.9 665.3
500	666.6	667.9	669.3	670.6	671.9	673.3	674.6	675.9	677.3	678.6
510	679.9	681.3	682.6	683.9	685.3	686.6	687.9	689.3	690.6	691.9
520	693.3	694.6	695.9	697.3	698.6	699.9	701.3	702.6	703.9	705.3
530	706.6	707.9	709.3	710.6	711.9	713.3	714.6	715.9	717.3	718.6
540	719.9	721.3	722.6	723.9	725.3	726.6	727.9	729.3	730.6	731.9
550	733·3	734.6	735.9	737.3	738.6	739.9	741.3	742.6	743.9	745.3
560	746.6	747.9	749.3	750.6	751.9	753.3	754.6	755.9	757.3	758.6
570	759·9	761.3	762.6	763.9	765.3	766.6	767.9	769.3	770.6	771.9
580	773·3	774.6	775.9	777.3	778.6	779.9	781.3	782.6	783.9	785.3
590	786.6	787.9	789.3	790.6	791.9	793.3	794.6	795.9	797.3	798.6
600	799.9	801.3	802.6	803.9	805.3	806.6	807.9	809.3	810.6	811.9
610	813.3	814.6	815.9	817.3	818.6	819.9	821.3	822.6	823.9	825.3
620	826.6	827.9	829.3	830.6	831.9	833.3	834.6	835.9	837.3	838.6
630	839.9	841.3	842.6	843.9	845.3	846.6	847.9	849.3	850.6	851.9
640	853.3	854.6	855.9	857.3	858.6	859.9	861.3	862.6	863.9	865.3
650	866.6	867.9	869.3	870.6	871.9	873.3	874.6	875.9	877.3	878.6
660	879.9	881.3	882.6	883.9	885.3	886.6	887.9	889.3	890.6	891.9
670	893.3	894.6	895.9	897.3	898.6	899.9	901.3	902.6	903.9	905.3
680	906.6	907.9	909.3	910.6	911.9	913.3	914.6	915.9	917.3	918.6
690	919.9	921.3	922.6	923.9	925.3	926.6	927.9	929.3	930.6	931.9
700	933.3	934.6	935.9	937·3	938.6	939.9	941.3	942.6	943.9	945·3
710	946.6	947.9	949.3	950.6	951.9	953.3	954.6	955.9	957.3	958.6
720	959.9	961.3	962.6	963.9	965.3	966.6	967.9	969.3	970.6	971.9
730	973.3	974.6	975.9	977·3	978.6	979.9	981.3	982.6	983.9	985·3
740	986.6	987.9	989.3	990.6	991.9	993.3	994.6	995.9	997.3	998.6
750	999-9	1001.3	1002.6	1003.9	1005.3	1006.6	1007.9	1009.3	1010.6	1011.9
760	1013.3	1014.6	1015.9	1017.2	1018.6	1019.9	1021.2	1022.6	1023.9	1025.2
770	1026.6	1027.9	1029.2	1030.6	1031.9	1033.2	1034.6	1035.9	1037.2	1038.6
780	1039.9	1041.2	1042.6	1043.9	1045.2	1046.6	1047.9	1049.2	1050.6	1051.9
790	1053.2	1054.6	1055.9	1057.2	1058.6	1059.9	1061.2	1062.6	1063.9	1065.2

FEET INTO METERS.

I foot = 0.3048006 meter.

Feet,	0	1	2	3	4	5	6	7	8	9
	<u> </u>	-			<u> </u>					
0	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	0.000	0.305	0.610	0.914	1.219	1.524	1.829	2.134	2.438	2.743
10	3.048	3.353	3.658	3.962	4.267	4.572	4.877	5.182	5.486	5.791
20	6.096	6.401	6.706	7.010	7.315	7.620	7.925	8.230	8.534	8.839
30	9.144	9.449	9.754	10.058	10.363	10.668	10.973	11.278	11.582	11.887
40	12.192	12.497	12.802	13.106	13.411	13.716	14.021	14.326	14.630	14.935
50	15.240	15.545	15.850	16.154	16.459	16.764	17.069	17.374	17.678	17.983
60	18.288	18.593	18.898	19.202	19.507	19.812	20.117	20.422	20.726	21.031
70	21.336	21.641	21.946	22.250	22.555	22.860	23.165	23.470	23.774	24.079
80	24.384	24.689	24.994	25.298	25.603	25.908	26.213	26.518	26.822	27.127
90	27.432	27.737	28.042	28.346	28.651	28.956	29.261	29.566	29.870	30.175
	0	10	20	-30	40	50	60	70	80	90
100	30.48	33·53	36.58	39.62	42.67	45.72	48.77	51.82	54.86	57.91
200	60.96	64.01	67.06	70.10	73.15	76.20	79.25	82.30	85.34	88.39
300	91.44	94·49	97.54	100.58	103.63	106.68	109.73	112.78	115.82	118.87
400	121.92	124·97	128.02	131.06	134.11	137.16	140.21	143.26	146.30	149.35
500	152.40	155.45	158.50	161.54	164.59	167.64	170.69	173.74	176.78	179.83
600	182.88	185.93	188.98	192.02	195.07	198.12	201.17	204.22	207.26	210.31
700	213.36	216.41	219.46	222.50	225.55	228.60	231.65	234.70	237.74	240.79
800	243.84	246.89	249.94	252.98	256.03	259.08	262.13	265.18	268.22	271.27
900	274-32	277.37	280.42	283.46	286.51	289.56	292.61	295.66	298.70	301.75
1000	304.80	307.85	310.90	313.94	316.99	320.04	323.09	326.14	329.18	332.23
1100	335.28	338.33	341.38	344.42	347.47	350.52	353.57	356.62	359.67	362.71
1200	365.76	368.81	371.86	374.90	377.95	381.00	384.05	387.10	390.14	393.19
1300	396.24	399.29	402.34	405.38	408.43	411.48	414.53	417.58	420.62	423.67
1400	426.72	429.77	432.82	435.86	438.91	441.96	445.01	448.06	451.10	454.15
1500	457.20	460.25	463.30	466.34	469.39	472.44	475.49	478.54	481.58	484.63
1600	487.68	490.73	493.78	496.82	499.87	502.92	505.97	509.02	512.07	515.11
1700	518.16	521.21	524.26	527.31	530.35	533.40	536.45	539.50	542.55	545.59
1800	548.64	551.69	554.74	557.79	560.83	563.88	566.93	569.98	573.03	576.07
1900	579.12	582.17	585.22	588.27	591.31	594.36	597.41	600.46	603.51	606.55
2000	609.60	612.65	615.70	618.75	621.79	624.84	627.89	630.94	633.99	637.03
2100	640.08	643.13	646.18	649.23	652.27	655.32	658.37	661.42	664.47	667.51
2200	670.56	673.61	676.66	679.71	682.75	685.80	688.85	691.90	694.95	697.99
2300	701.04	704.09	707.14	710.19	713.23	716.28	719.33	722.38	725.43	728.47
2400	731.52	734.57	737.62	740.67	743.71	746.76	749.81	752.86	755.91	758.95
2500	762.00	765.05	768.10	771.15	774.19	777.24	780.29	783.34	786.39	789.43
2600	792.48	795.53	798.58	801.63	804.67	807.72	810.77	813.82	816.87	819.91
2700	822.96	826.01	829.06	832.11	835.15	838.20	841.25	844.30	847.35	850.39
2800	853.44	856.49	859.54	862.59	865.63	868.68	871.73	874.78	877.83	880.87
2900	883.92	886.97	890.02	893.07	896.11	899.16	902.21	905.26	908.31	911.35
3000 3100 3200 3300 3400	1036.32	1008.89	1011.94 104 2. 42	954.03 984.51 1014.99 1045.47	1018.03 1048.51	990.60 1021.08 1051.56	1024.13	1027.18	1030.23 1060.71	1063.75
3700 3800	1097.28 1127.76 1158.24	1100.33 1130.81 1161.29	1102.38 1133.86 1164.34	1106.43 1136.91 1157.39	1109.47 1139.95 1170.43	1112.52 1143.00 1173.48	1115.57 1146.05 1176.53	1118.62 1149.10 1179.58	1091.19 1121.67 1152.15 1182.63 1213.11	1124.71 1155.19 1185.67
4000	1219.20	1222.25	1225.30	1228.35	1231.39	1234.44	1237.49	1240.54	1243.59	1246.63

FEET INTO METERS.

I foot == 0.3048006 meter.

Feet.	0	10	20	30	40	50	60	70	80	90
	m.	m.	m.	m,	m.	m.	m.	m.	m.	m.
4000 4100 4200 4300 4400	1219.2 1249.7 1280.2 1310.6 1341.1	1222.3 1252.7 1283.2 1313.7 1344.2	1225.3 1255.8 1286.3 1316.7 1347.2	1228.3 1258.8 1289.3 1319.8 1350.3	1231.4 1261.9 1292.4 1322.8	1234.4 1264.9 1295.4 1325.9 1356.4	1237.5 1268.0 1298.5 1328.9 1359.4	1240.5 1271.0 1301.5 1332.0 1362.5	1243.6 1274.1 1304.5 1335.0 1365.5	1246.6 1277.1 1307.6 1338.1 1368.6
4500	1371.6	1374.7	1377.7	1380.7	1383.8	1386.8	1389.9	1392.9		1399.0
4600	1402.1	1405.1	1408.2	1411.2	1414.3	1417.3	1420.4	1423.4		1429.5
4700	1432.6	1435.6	1438.7	1441.7	1444.8	1447.8	1450.9	1453.9		1460.0
4800	1463.0	1466.1	1469.1	1472.2	1475.2	1478.3	1481.3	1484.4		1490.5
4900	1493.5	1496.6	1499.6	1502.7	1505.7	1508.8	1511.8	1514.9		1521.0
5000	1524.0	1527.1	1530.1	1533.1	1536.2	1539.2	1542.3	1545.3	1548.4	1551.4
5100	1554.5	1557.5	1560.6	1563.6	1566.7	1569.7	1572.8	1575.8	1578.9	1581.9
5200	1585.0	1588.0	1591.1	1594.1	1597.2	1600.2	1603.3	1606.3	1609.3	1612.4
5300	1615.4	1618.5	1621.5	1624.6	1627.6	1630.7	1633.7	1636.8	1639.8	1642.9
5400	1645.9	1649.0	1652.0	1655.1	1658.1	1661.2	1664.2	1667.3	1670.3	1673.4
5500	1676.4	1679.5	1682.5	1685.5	1688.6	1691.6	1694.7	1697.7	1700.8	1703.8
5600	1706.9	1709.9	1713.0	1716.0	1719.1	1722.1	1725.2	1728.2	1731.3	1734.3
5700	1737.4	1740.4	1743.5	1746.5	1749.6	1752.6	1755.7	1758.7	1761.7	1764.8
5800	1767.8	1770.9	1773.9	1777.0	1780.0	1783.1	1786.1	1789.2	1792.2	1795.3
5900	1798.3	1801.4	1804.4	1807.5	1810.5	1813.6	1816.6	1819.7	18 2 2.7	1825.8
6000	1828.8	1831.9	1834.9	1837.9	1841.0	1844.0	1847.1	1850.1	1853.2	1856.2
6100	1859.3	1862.3	1865.4	1868.4	1871.5	1874.5	1877.6	1880.6	1883.7	1886.7
6200	1889.8	1892.8	1895.9	1898.9	1902.0	1905.0	1908.1	1911.1	1914.1	1917.2
6300	1920.2	1923.3	1926.3	1929.4	1932.4	1935.5	1938.5	1941.6	1944.6	1947.7
6400	1950.7	1953.8	1956.8	1959.9	1962.9	1966.0	1969.0	1972.1	1975.1	1978.2
6500	1981.2	1984.3	1987.3	1990.3	1993.4	1996.4	1999.5	2002.5	2005.6	2008.6
6600	2011.7	2014.7	2017.8	2020.8	2023.9	2026.9	2030.0	2033.0	2036.1	2039.1
6700	2042.2	2045.2	2048.3	2051.3	2054.4	2057.4	2060.5	2063.5	2066.5	2069.6
6800	2072.6	2075.7	2078.7	2081.8	2084.8	2087.9	2090.9	2094.0	2097.0	2100.1
6900	2103.1	2106.2	2109.2	2112.3	2115.3	2118.4	2121.4	2124.5	2127.5	2130.6
7000	2133.6	2136.7	2139.7	2142.7	2145.8	2148.8	2151.9	2154.9	2158.0	2161.0
7100	2164.1	2167.1	2170.2	2173.2	2176.3	2179.3	2182.4	2185.4	2188.5	2191.5
7200	2194.6	2197.6	2200.7	2203.7	2206.8	2209.8	2212.9	2215.9	2218.9	2222.0
7300	2225.0	2228.1	2231.1	2234.2	2237.2	2240.3	2243.3	2246.4	2249.4	2252.5
7400	2255.5	2258.6	2261.6	2264.7	2267.7	2270.8	2273.8	2276.9	2279.9	2283.0
7500	2286.0	2289.1	2292.1	2295.1	2298.2	2301.2	2304.3	2307.3	2310.4	2313.4
7600	2316.5	2319.5	2322.6	2325.6	2328.7	2331.7	2334.8	2337.8	2340.9	2343.9
7700	2347.0	2350.0	2353.1	2356.1	2359.2	2362.2	2365.3	2368.3	2371.3	2374.4
7800	2377.4	2380.5	2383.5	2386.6	2389.6	2392.7	2395.7	2398.8	2401.8	2404.9
7900	2407.9	2411.0	2414.0	2417.1	2420.1	2423.2	2426.2	2429.3	2432.3	2435.4
8000	2438.4	2441.5	2444.5	2447.5	2450.6	2453.6	2456.7	2459.7	2462.8	2465.8
8100	2468.9	2471.9	2475.0	2478.0	2481.1	2484.1	2487.2	2490.2	2493.3	2496.3
8200	2499.4	2502.4	2505.5	2508.5	2511.6	2514.6	2517.7	2520.7	2523.7	2526.8
8300	2529.8	2532.9	2535.9	2539.0	2542.0	2545.1	2548.1	2551.2	2554.2	2557.3
8400	2560.3	2563.4	2566.4	2569.5	2572.5	2575.6	2578.6	2581.7	2584.7	2587.8
8500	2590.8	2593.9	2596.9	2599.9	2603.0	2606.0	2609.1	2612.1	2615.2	2618.2
8600	2621.3	2624.3	2627.4	2630.4	2633.5	2636.5	2639.6	2642.6	2645.7	2648.7
8700	2651.8	2654.8	2657.9	2660.9	2664.0	2667.0	2670.1	2673.1	2676.1	2679.2
8800	2682.2	2685.3	2688.3	2691.4	2694.4	2697.5	2700.5	2703.6	2706.6	2709.7
8900	2712.7	2715.8	2718.8	2721.9	2724.9	2728.0	2731.0	2734.1	2737.1	2740.2
9000	2743.2	2746.3	2749.3	2752.3	2755.4	2758.4	2761.5	2764.5	2767.6	2770.6

METERS INTO FEET.

1 meter = 39.3700 inches = 3.280833 feet.

Meters.	0	1	2	3	4	5	6	7	8	9
	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
0	0.00		6.56		13.12		_			
10 2 0	32.81 65.62		39·37 72.18	42.65 75.46	45.93 78.74				59.05 91.86	
30	98.42	101.71	104.99		111.55		118.11			127.95
40	131.23	134.51	137.79	141.08	144.36	147.64	150.92	154.20	157.48	160.76
50	164.04	,	170.60				183.73	187.01		193.57
60 70	196.85 229.66	200.13	203.41		209.97		216.53	219.82		1
80	262.47	265.75	269.03		275.59		249.34		255.90 288.71	259.19 291.99
90	295.27		301.84		308.40			318.24		324.80
100	328.08	331.36	334.64	337.93	341.21	344.49	347-77	351.05	354-33	357.61
110	360.89	364.17	367.45	370.73	374.01	377.30	380.58	383.86	387.14	390.42
120 130	393.70 426.51	396.98 429.79	433.07	436.35	406.82 439.63	410.10 442.91	413.38 446.19	416.67		423.23
140	459.32	462.60	465.88	469.16	472.44	475.72	479.00	449.47 482.28	452.75 485.56	456.04 488.84
150	492.12	495.41	498.69	501.97	505.25	508.53	511.81	515.09	518.37	521.65
160	524.93	528.21	531.49		538.06	541.34	544.62			554.46
170 180	557·74 590.55	593.83	564.30 597.11	567.58	570.86 603.67		577.43 610.23	580.71 613.52	583.99 616.80	587.27 620.08
190	623.36		629.92		636.48		643.04	646.32	649.60	652.89
200	656.17	659.45	662.73	666.01	669.29	672.57	675.85	679.13	682.41	685.69
210 220	688.97 721.78	692.26 725.06	695.54 728.34		702.10		708.66	711.94		718.50
2 30	754.59	757.87	761.15	764.43	734.91 767.71	738.19	741.47 774.28	744.75	748.03	751.31 784.12
240	787.40	790.68	793.96	797.24	800.52	803.80	807.08	810.37	813.65	816.93
250	820.21	823.49	826.77	830.05	833.33	836.61		843.17	846.45	849.74
260 270	853.02 885.82	856.30 889.11	859.58 892.39	862.86	866.14 898.95	902.23	872.70 905.51	875.98 908.79		882.54
280	918.63	921.91	925.19	928.48	931.76	935.04	938.32	941.60	912.07	915.35 948.16
290	951.44	954.72	958.00	961.28	964.56	967.85	971.13	974.41		980.97
300	984.25	987.53	990.81	994.09	997.37	1000.65	1003.93	1007.22	1010.50	1013.78
310 320	1017.00	1020.34	1023.02	1020.90	1030,10	1033.40	1030.74	1040.02	1043.30	1046.59
330	1082.67	1085.96	1089.24	1092.52	1095.80	10000.08	1102.36	1105.64	1100.02	TTT2.20
	1115.48	1118.76	1122.04	1125.33	1128.61	1131.89	1135.17	1138.45	1141.73	1145.01
350 360	1148.29	1151.57	1154.85	1158.13	1161.41	1164.70	1167.98	1171.26	1174.54	1177.82
370	1213.91	1217.19	1220.47	1223.75	1227.03	1230.31	1233.50	1236.87	1207.35	12/13.//
380	1246.72	1250.00	1253.28	1256.56	1259.84	1263.12	1266.40	1260.68	1272.06	1276.24
390	1279.52	1282.81	1286.09	1289.37	1292.65	1295.93	1299.21	1302.49	1305.77	1309.05
400	1312.33	1315.61	1318.89	1322.18	1325.46	1328.74	1332.02	1335.30	1338.58	1341.86
410 420	1377-05	1381.22	1384.51	1387.70	1350,20	1301.55	1304.83	1308.11	1371.39	1374.67
4.30	1410.76	1414.04	1417.32	1420.60	1423.881	1427.16	1430.44	1/133.72	1/27 00	T440 20
440	1443.57	1446.85	1450.13	1453.41	1456.69	1459.97	1463.25	1466.53	1469.81	1473.09
450	1476.37	1479.66	1482.94	1486.22	1489.50	1492.78	1496.06	1499.34	1502.62	1505.90
460 470	1509.18	1545.27	1548.55	1519.03	1522.31	1525.59	1528.87	1532.15	1535.43 1568.24	1538.71
480	1574.80	1578.081	1581.361	1584.64	I 587.02 l	1501.20	1504.48	T507.77	Ιτόρτ σε Ι	1604 22 H
490	1607.61	1610.89	1614.17	1617.45	1620.73	1624.01	1627.29	1630.57	1633.85	1637.14
50 0	1640.42	1643.70	1646.98	1650.26	1653.54	1656.82	1660.10	1663.38	1666.66	1669.94
' <u> </u>										

METERS INTO FEET.

1 meter = 39.3700 inches = 3.280833 feet.

Meters.	0	10	20	30	40	50	60	70	80	90
	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
500	1640.4	1673.2	1706.0	1738.8	1771.6	1804.5	1837.3	1870.1	1902.9	1935.7
600 700	1968.5 2296.6	2001.3	2034.I 2362.2	2066.9	2099.7 2427.8	2132.5 2460.6	2165.3	2198.2 2526.2	2231.0 2559.0	2263.8
800	2624.7	2657.5	2690.3	2723.I	2755.9	2788.7	2821.5	2854.3	2887.1	2919.9
900	2952.7	2985.6	3018.4	3051.2	3084.0	3116.8	3149.6	3182.4	3215.2	3248.0
1000	3280.8	3313.6	3346.4	3379-3	3412.1	3444.9	3477-7	3510.5	3543-3	3576.1
1100	3608.9	3641.7	3674.5	3707.3	3740.1	3773.0	3805.8	3838.6	3871.4	3904.2
1200 1300	3937.0 4265.1	3969.8 4297.9	4002.6	4035.4	4068.2 4396.3		4133.8	4166.7	4199.5	4232.3 4560.4
1400	4593.2	4626.0	4330.7 4658.8	4691.6	4724.4	4757.2	4461.9 47 90. 0	4494.7 4822.8	4527.5 4855.6	4888.4
1500	4921.2	4954.1	4986.9	5019.7	5052.5	5085.3	5118.1	5150.9	5183.7	5216.5
1600	5249.3	5282.1	5314.9	5347.8	5380.6	5413.4	5446.2	5479.0	5511.8	5544.6
17c o 18co	5577.4	5610.2	5643.0	5675.8	5708.6	5741.5	5774.3 6102.3	5807.1	5839.9 6168.0	5872.7 6200.8
1900	5905.5 6233.6	5938.3 6266.4	5971.1 6299.2	6332.0	6036.7 6364.8	6069.5 6397.6	6430.4	6135.2	6496.0	6528.9
2000	6561.7	6594.5	6627.3	6660.1	6692.9	6725.7	6758.5	6791.3	6824.1	6856.9
2100	6889.7	6922.6	6955.4	6988.2	7021.0	7053.8	7086.6	7119.4	7152.2	7185.0
2200	7217.8	7250.6	7283.4	7316.3	7349.1	7381.9	7414.7	7447-5	7480.3	7513.1
2300 2400	7545.9 7874.0	7578.7	7611.5 7939.6	7644.3 79 72. 4	7677.1 8005.2	7710.0 8038.0	7742.8 8070.8	7775.6 8103.7	7808.4 8136.5	7841.2 8169.3
2500	8202.1					1				1 1
2600	8530.2	8234.9 8563.0	8267.7 8595.8	8300.5 8628.6	8333.3 8661.4	8366.1	8398.9 8727.0	8431.7 8759.8	8464.5 8792.6	8497.4 8825.4
2700	8858.2	8891.1	8923.9	8956.7	8989.5	9022.3	9055.1	9087.9	9120.7	9153.5
2800	9186.3	9219.1	9251.9	9284.8	9317.6	9350.4	9383.2	9416.0	9448.8	9481.6
2900	9514.4	9547.2	9580.ó	9612.8	9645.6		9711.3	9744.1	9776.9	
3000	9842.5	9875.3	9908.1	9940.9	9973.7	10006.5	10039.3		10105.0	
3100	10170.6	10203.4		10269.0						
3200 3300	10826.7	10531.5	10564.3	10597.1	10029.9	10002.7	110095.5		10761.1	
3400		11187.6		11253.3	11286.1	11318.9	11351.7	11384.5		11450.1
3500	11482.9	11515.7	11548.5	11581.3	11614.1	11647.0	11679.8	11712.6	11745.4	11778.2
3600		11843.8	11876.6	11909.4	11942.2	11975.0	12007.8	12040.7	12073.5	12106.3
3700		12171.9		12237.5	12270.3	12303.1	12335.9	12368.7	12401.5	12434.4
3800	12467.2						12664.0			12762.4
3900		12828.1				'				13090.5
4000		13156.1							13385.8	
4100 4200	13451.4 13779.5	13484.2		13549.8				14009.2	13713.9	
4300	14107.6			14206.0	14238.8	14271.6	14304.4	14337.2		14402.9
4400		14468.5			14566.9		14632.5	14665.3		14730.9
4500		14796.6						14993.4		15059.0
4600		15124.6		15190.3				15321.5	15354-3	15387.1
4700 4800	15419.9	15452.7 15780.8	15485.5	15518.3	15551.1	15584.0	15944.8	15049.6	15682.4	
4900	16076.1	16108.9	16141.7					16305.7	16010.5 16338.5	16043.3 16371.4
5000	16404.2	16437.0	1 6 469.8	16502.6	16535.4	16568.2	16601.0	16633.8	16666.6	16699.4
Ten Fee	ths of a me	ster.		0,2 0,3 0,656 0,9	3 0.4 984 1.31	0.5 2 1.640	o.6 1.968	•	. 8 0. 9	

MILES INTO KILOMETERS.

1 mile = 1.609347 kilometers.

				· · · · · · · · · · · · · · · · · · ·						
Miles.	0	- 1	2	3	4	5	6	7	8	9
0	km.	km.	km.	km.	km.	km. 8	km. IO	km.	km. 13	km. 14
10 20	16 32	18 34	19 35	2I 37	23 39	24 40	26 42	27 43 60	29 45	31 47
30	48	50	51	53	55	56	58	60	61	63
40	64	66	68	69	71	72	74	76	77	79
50	80	82	84	85	87	89	90	92	93	95
60	97	98	100	101	103	105	106	108	109	111
70 80	113 129	114	116 132	117	119	121	122	124 140	126 142	127 143
90	145	130 146	148	134 150	135 151	137 153	154	156	158	159
110	161	163	164	166	167	169	171	172	174	175
	177	179	180	182	183	185	187	188	190	192
120	193	195	196	198	200	20I	203	204	206	208
130	209	211	212	214	216	217	219	220	222	224
140	225	227	229	230	232	233	235	237	238	240
150 160	24I 257	243 259	245 261	246 262	248 264	249 266	251 267	253 269	254 270	256 272 288
170	274	275	277	278	280	282	283	285	286	304
180	290	291	293	295	296	298	299	301	303	
190 200	306 322	307 323	309 325	311 3 2 7	312 328	314 330	315	317	319 335	320 336
210	338	340	341	343	344	346	348	349	351	352
220	354	356	357	359	360	362	364	365	367	369
230	370	372	373	375	377	378	380	381	383	385
240	386	388	389	391	393	394	396	398	399	401
250	402	404	406	407	409	410	412	414	415	417
260	418	420	422	423	425	426	428	430	431	433
270	435	436	438	439	441	443	444	446	447	449
280	451	452	454	455	457	459	460	462	463	465
290	467	468	470	472	473	475	476	478	480	481
300	483	484	486	488	489	491	492	494	496	497
310	499	501	502	504	505	507	509	510	512	513
320	515	517	518	520	521	523	525	526	528	529
	531	533	534	536	538	539	541	542	544	546
330 340	547	549	550	552	554	555	557	558	560	562
350	563	565	566	568	570	571	573	575	576	578
360	579	581	583	584	586	587	589	591	592	594
370	595	597	599	600	602	604	605	607	608	610
380	612	613	615	616	618	620	621	623	624	626
390	628	629	631	632	634	636	637	639	641	642
400	644	645	647	649	650	652	653	655	657	658
410	660	661	663	665	666	668	669	671	673	674
	676	678	679	681	682	684	686	687	689	690
420 430	692 708	694 710	695 711	697 713	698	700 716	702 718	703	705 721	706 723
440 450	724	726	727	713	715 731	732	734	719 735	737	739
460	740	742	744	745	747	748	750	752	753	755
470	756	758	760	761	763	764	766	768	769	771
480	772	774	776	778	779	781	782	784	78 5	787
490	789	790	792	793	795	797	798	800	80 1	803
500	805	806 822	808	809 826	811 827	813	814	816 832	818 834	819 835
510 520	821 837	838	824 840	842	843	829 845 861	830 847 862	848	850 866	851 867
530 540	853 869	855 871	856 872	858 874	859 875	877	863 879	864 880	882	884
550	885	887	888	890	892	893	895	896	898	900

MILES INTO KILOMETERS.

Miles.	0	1	2	3	4	5	-	;	7	8	9
550 560 570 580 590	km. 885 901 917 933 950	km. 887 903 919 935 951	km. 888 904 921 937 953	km. 890 906 922 938 954	km. 892 908 924 940 956		8 9 9 5 9 9 1 9 9 1 9 1 9 1 9 1	m. 95 11 27 43	km. 896 912 929 945 961	km. 898 914 930 946 962	km. 900 916 932 948 964
600 610 620 630 640	966 982 998 1014 1030	967 983 999 1015 1032	969 985 1001 1017 1033	970 987 1003 1019 1035	972 988 1004 1020 1036	1006	9 5 10 2 10	24	977 993 1009 1025 1041	978 995 1011 1027 1043	980 996 1012 1028 1044
650 660 670 680 690	1046 1062 1078 1094	1048 1064 1080 1096 1112	1049 1065 1081 1098	1051 1067 1083 1099	1053 1069 1085 1101 1117	1086	0 10 5 10 2 11	72 88 04	1057 1073 1090 1106 1122	1059 1075 1091 1107 1123	1061 1077 1093 1109 1125
700 710 720 730 740	1127 1143 1159 1175 1191	1128 1144 1160 1176 1193	1130 1146 1162 1178 1194	1131 1147 1164 1180 1196	1133 1149 1165 1181 1197	115 116 118	1 11 7 11 3 11	52 68 84	1138 1154 1170 1186 1202	1139 1156 1172 1188 1204	1141 1157 1173 1189 1205
750 760 770 780 790	1207 1223 1239 1255 1271	1209 1225 1241 1257 1273	1210 1226 1242 1259 1275	1212 1228 1244 1260 1276	1213 1230 1246 1262 1278	123 124 126	1 12 7 12 3 12	33 49 65	1218 1234 1250 1267 1283	1220 1236 1252 1268 1284	1221 1238 1254 1270 1286
800 810 820 830 840	1287 1304 1320 1336 1352	1289 1305 1321 1337 1353	1291 1307 1323 1339	1292 1308 1324 1341 1357	1294 1310 1326 13 42 1358	131: 132: 134:	2 13 8 13 4 13		1299 1315 1331 1347 1363	1300 1316 1333 1349 1365	1302 1318 1334 1350 1366
850 860 870 880 - 890	1368 1384 1400 1416 1432	1370 1386 1402 1418 1434	1371 1387 1403 1419 1436	1373 1389 1405 1421 1437	1374 1390 1407 1423 1439	139: 140 142	2 13 8 14 4 14	78 94 10 26 42	1379 1395 1411 1427 1444	1381 1397 1413 1429 1445	1382 1399 1415 1431 1447
900 910 920 930 940	1448 1464 1481 1497 1513	1450 1466 1482 1498 1514	1452 1468 1484 1500 1516	1453 1469 1485 1502 1518	1455 1471 1487 1503 1519	147 148 150	3 14 9 14 5 15	58 74 90 06 22	1460 1476 1492 1508 1524	1461 1477 1493 1510 1576	1463 1479 1495 1511 1527
950 960 970 980 990	1529 1545 1561 1577 1593	1530 1547 1563 1579 1595	1532 1548 1564 1580 1596	1534 1550 1566 1582 1598	1535 1551 1567 1584 1600	155 156 158 160	3 15 9 15 5 15 1 16	39 55 71 87 03	1540 1556 1572 1588 1605	1542 1558 1574 1590 1606	1543 1559 1576 1592 1608
1000	Miles 1000 2000 3000 4000 5000	1609 3219 4828 6437	Mil 600 700 800 900 1000	00 96 00 112 00 128	556 265 375 484	Miles. 11000 12000 13000 14000	km. 17703 19312 20922 22531 24140		Miles. 16000 17000 18000 19000 20000	km. 25750 27359 28968 30578 32187	1624

KILOMETERS INTO MILES.

1 kilometer = 0.621370 mile.

Kilo- meters.	0	1	2	3	. 4	5	6	7	8	9
	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.
0 10	0.0 6.2	o.6 6.8	1.2 7.5	1.9 8.1	2.5 8.7	3.1 9.3	3.7 9.9	4.3	5.0 11.2	5.6 11.8
20	12.4	13.0	13.7	14.3	14.9	15.5	16.2	16.8	17.4	18.o
30 40	18.6 24.9	19.3 25.5	19.9 26.1	20.5 26.7	21.1 27.3	21.7 28.0	22.4 28.6	23.0 29.2	23.6 29.8	24.2 30.4
50	31.1	31.7	32.3	32.9	33.6	34.2	34.8	35.4	36.0	36.7
60	37.3	37.9	38.5	39.1	39.8	40.4	41.0	41.6	42.3	42.9
70 80	43·5 49·7	44.1 50.3	44.7 51.0	45.4 51.6	46.0 52.2	46.6 52.8	47.2 53.4	47.8 54.1	48.5 54.7	49.1
90	55.9	56.5	57.2	57.8	58.4	59.0	59.7	60.3	60.9	55·3 61.5
100	62.1	62.8	63.4	64.0	64.6	65.2	65.9	66.5	67.1	67.7
110 120	68.4 74.6	69.0 75.2	69.6 75.8	70.2 76.4	70.8 77.0	71.5	72.1 78.3	72.7 78.9	73.3	73·9 80.2
130	80.8	81.4	82.0	82.6	83.3	77.7 83.9	84.5	85.1	79·5 85·7	86.4
140	87.0	87.6	88.2	88.9	89.5	90.1	90.7	91.3	92.0	92.6
150 160	93.2	93.8	94.4	95.1	95.7 101.9	96.3	96.9	97.6	98.2	98.8
170	99.4 105.6	100.0 106.3	100.7 106.9	101.3 107.5	108.1	102.5	103.1	103.8 110.0	104.4 110.6	105.0 111.2
180	111.8	112.5	113.1	113.7	114.3	115.0	115.6	116.2	116.8	117.4
190	118.1	118.7	119.3	119.9	120.5	121.2	121.8	122.4	123.0	123.7
200 210	124.3	124.9 131.1	125.5 131.7	126.1 132.4	126.8 133.0	127.4 133.6	128.0 134.2	128.6 134.8	129.2 135.5	129.9 136.1
220	136.7	137.3	137.9	138.6	139.2	139.8	140.4	141.1	141.7	142.3
230 240	142.9	143.5 149.8	144.2 150.4	144.8 151.0	145.4 151.6	146.0 152.2	146.6 152.9	147.3	147.9	148.5
250	155.3	156.0	156.6	157.2	157.8	158.4	159.1	153.5 159.7	154.1 160.3	154.7 160.9
260	161.6	162.2	162.8	163.4	164.0	164.7	165.3	165.9	166.5	167.1
270 280	167.8	168.4	169.0	169.6	170.3	170.9	171.5	172.1	172.7	173.4
290	174.0 180.2	174.6 180.8	175.2 181.4	175.8 182.1	176.5 182.7	177.1 183.3	177.7	178.3 184.5	179.0 185.2	179.6 185.8
300	186.4	187.0	187.7	188.3	188.9	189.5	190.1	190.8	191.4	192.0
310	192.6	193.2	193.9	194.5	195.1	195.7	196.4	197.0	197.6	198.2
320 330	198.8 205.1	199.5 205.7	200.I 206.3	200.7 206.9	201.3 207.5	201.9	202.6 208.8	203.2 209.4	203.8 210.0	204.4 210.6
340	211.3	211.9	212.5	213.1	213.8	214.4	215.0	215.6	216.2	216.9
350	217.5	218.1	218.7	219.3	220.0	220.6	221.2	221.8	222.5	223.1
360 370	223.7 229.9	224.3 230.5	224.9 231.1	225.6 231.8	226.2 232.4	226.8 233.0	227.4 233.6	228.0 234.3	228.7 234.9	229.3 235.5
38o	236.1	236.7	237.4	238.0	238.6	239.2	239.8	240.5	241.1	241.7
390	242.3	243.0	243.6	244.2	244.8	245.4	246.1	246.7	247.3	247.9
400 410	248.5 254.8	249.2 255.4	249.8 256.0	250.4 256.6	251.0 257.2	251.7 257.9	252.3 258.5	252.9 259.1	253.5 259.7	254.1 260.4
420	261.0	261.6	262.2	262.8	263.5	264.1	264.7	265.3	265.9	266.6
430 440	267.2 273.4	267.8 274.0	268.4 274.6	269.1	269.7	270.3 276.5	270.9	271.5	272.2	272.8
450	279.6	280.2	280.9	275.3 281.5	275.9 282.1	282.7	277.I 283.3	277.8 284.0	278.4 284.6	279.0 285.2
460	285.8	286.5	287.I	287.7	288.3	288.9	289.6	290.2	290.8	285.2
470	292.0	292.7 298.9	293.3	293.9	294.5	295.2	295.8	296.4	297.0	297.6
480 490	298.3 304.5	305.1	299.5 305.7	300. I 306. 3	300.7 307.0	301.4 307.6	302.0 308.2	302.6 308.8	303.2	303.8 310.1
500	310.7	311.3	311.9	312.5	313.2	313.8	314.4	315.0	315.7	316.3
510	316.9	317.5	318.1	318.8	319.4	320.0	320.6	321.2	321.9	322.5
520 530	323. I 329. 3	323.7 329.9	324.4 330.6	325.0	325.6 331.8	326.2 332.4	326.8 333.1	327.5 333.7	328.1 334.3	328.7 334.9
540	335.5	336.2	336.8	337.4	338.0	338.6	339.3	339.9	340.5	341.1

KILOMETERS INTO MILES.

Kilo- meters.	0	1	2	3	4	5	6	7	8	9
550 560 570 580	Miles. 341.8 348.0 354.2 360.4	Miles. 342.4 348.6 354.8 361.0	Miles. 343.0 349.2 355.4 361.6	Miles. 343.6 349.8 356.0 362.3	Miles. 344.2 350.5 356.7 362.9	Miles. 344.9 351.1 357.3 363.5	Miles. 345.5 351.7 357.9 364.1	Miles. 346.1 352.3 358.5 364.7	Mile 346.7 352.9 359.2 365.4	Miles. 347·3 353.6 359.8 366.0
590	366.6	367.2	367.9	368.5	369. 1	369.7	370.3	371.0	371.6	372.2
600	372.8	373.4	374.1	374.7	375.3	375.9	376.6	377.2	377.8	378.4
610	379.0	379.7	380.3	380.9	381.5	382.1	382.8	383.4	384.0	384.6
620	385.2	385.9	386.5	387.1	387.7	388.4	389.0	389.6	390.2	390.8
630	391.5	392.1	392.7	393.3	393.9	394.6	395.2	395.8	396.4	397.1
640	397.7	398.3	398.9	399.5	400.2	400.8	401.4	402.0	402.6	403.3
650	403.9	404.5	405.1	405.8	406.4	407.0	407.6	408.2	408.9	409.5
660	410.1	410.7	411.3	412.0	412.6	413.2	413.8	414.5	415.1	415.7
670	416.3	416.9	417.6	418.2	418.8	419.4	420.0	420.7	421.3	421.9
680	422.5	423.2	423.8	424.4	425.0	425.6	426.3	426.9	427.5	428.1
690	428.7	429.4	430.0	430.6	431.2	431.9	432.5	433.1	433.7	434.3
700	435.0	435.6	436.2	436.8	437.4	438.1	438.7	439·3	439.9	440.6
710	441.2	441.8	442.4	443.0	443.7	444.3	444.9	445·5	446.1	446.8
720	447.4	448.0	448.6	449.3	449.9	450.5	451.1	451·7	452.4	453.0
730	453.6	454.2	454.8	455.5	456.1	456.7	457.3	457·9	458.6	459.2
740	459.8	460.4	461.1	461.7	462.3	462.9	463.5	464·2	464.8	465.4
750	466.0	466.6	467.3	467.9	468.5	469.1	469.8	470.4	471.0	471.6
760	472.2	472.9	473.5	474.1	474.7	475.3	476.0	476.6	477.2	477.8
770	478.5	479.1	479.7	480.3	480.9	481.6	482.2	482.8	483.4	484.0
780	484.7	485.3	485.9	486.5	487.2	487.8	488.4	489.0	489.6	490.3
790	490.9	491.5	492.1	492.7	493.4	494.0	494.6	495.2	495.9	496.5
800	497.1	497.7	498.3	499.0	499.6	500.2	500.8	501.4	502.1	502.7
810	503.3	503.9	504.6	505.2	505.8	506.4	507.0	507.7	508.3	508.9
820	509.5	510.1	510.8	511.4	512.0	512.6	513.3	513.9	514.5	515.1
830	515.7	516.4	517.0	517.6	518.2	518.8	519.5	520.1	520.7	521.3
840	522.0	522.6	523.2	523.8	524.4	525.1	525.7	526.3	526.9	527.5
850	528.2	528.8	529.4	530.0	530.6	531.3	531.9	532.5	533.1	533.8
860	534.4	535.0	535.6	536.2	536.9	537.5	538.1	538.7	539.3	540.0
870	540.6	541.2	541.8	542.5	543.1	543.7	544.3	544.9	545.6	546.2
880	546.8	547.4	548.0	548.7	549.3	549.9	550.5	551.2	551.8	552.4
890	553.0	553.6	554.3	554.9	555.5	556.1	556.7	557.4	558.0	558.6
900	559.2	559.9	560.5	561.1	561.7	562.3	563.0	563.6	564.2	564.8
910	565.4	566.1	566.7	567.3	567.9	568.6	569.2	569.8	570.4	571.0
920	571.7	572.3	572.9	573.5	574.1	574.8	575.4	576.0	576.6	577.3
930	577.9	578.5	579.1	579.7	580.4	581.0	581.6	582.2	582.8	583.5
940	584.1	584.7	585.3	586.0	586.6	587.2	587.8	588.4	589.1	589.7
950 960 970 980 990	590.3 596.5 602.7 608.9 615.2	590.9 597.1 603.4 609.6 615.8 622.0	591.5 597.8 604.0 610.2 616.4 622.6	592.2 598.4 604.6 610.8 617.0	592.8 599.0 605.2 611.4 617.6	593.4 599.6 605.8 612.0 618.3	594.0 600.2 606.5 612.7 618.9	594.7 600.9 607.1 613.3 619.5	595.3 601.5 607.7 613.9 620.1	595.9 602.1 608.3 614.5 620.7
1000	km. 1000 2000 3000 4000 5000	Miles 621. 1242. 1864.	km 4 600 7 700 1 800 5 900	372 00 434 00 497 00 559	8.2 11 9.6 12 1.0 13 2.3 14	000 6 000 7 000 8 000 8	625.1 Ailes. 835.1 456.4 077.8 699.2 320.5	km. 16000 17000 18000 19000 20000	Miles. 9941.9 10563.3 11184.7 11806.0 12427.4	627.0

INTERCONVERSION OF NAUTICAL AND STATUTE MILES.

1 nautical mile* = 6080.20 feet.

Nautical Miles.	Statute Miles.	Statute Miles.	Nautical Miles.
1	1.1516	1	0,8684
2	2.3031	2	1,7368
3	3.4547	3	2,6052
4	4.6062	4	3,4736
5 6 7 8	5.7578	5	4.3420
	6.9093	6	5.2104
	8.0609	7	6.0787
	9.2124	8	6. 9471
	10.3640	9	7.8155

^{*} As defined by the United States Coast Survey.

TABLE 18.

CONTINENTAL MEASURES OF LENGTH WITH THEIR METRIC AND ENGLISH EQUIVALENTS.

The asterisk (*) indicates that the measure is obsolete or seldom used.

Measure.	Metric Equivalent.	English Equivalent.
El (Netherlands) Fathom, Swedish = 6 feet Foot, Austrian* old French* Russian Rheinlandisch or Rhenish (Prussia*, Denmark, Norway*). Swedish* Spanish* = ½ vara *Klafter, Wiener (Vienna) *Line, old French = ½ foot Mile, Austrian post* = 24000 feet Germau sea Swedish = 36000 feet Norwegian = 36000 feet Norwegian = 36000 feet Netherlands (mijl) Prussian (law of 1868) Danish Palm, Netherlands *Rode, Danish *Ruthe, Prussian, Norwegian Sagene (Russian) *Toise, old French = 6 feet *Vara. Spauish	I meter. 1.7814 " 0.31608 " 0.32484 " 0.30480 " 0.2786 " 1.89648 " 0.22558 cm. 7.58594 km. 1.852 " 10.69 " 11.2986 " 17.500 " 7.5324 " 0.1 meter. 3.7662 " 3.7662 " 2.1336 " 1.9490 " 0.8359 "	3.2808 feet. 5.8445 " 1.0370 " 1.0657 " 1 " 1.0297 " 0.9741 " 0.9140 " 6.2221 " 0.0888 inch. 4.714 statute miles. 1.1508 " " 6.642 " " 7.02 " " 4.660 " " 4.660 " " 4.6804 " " 0.3281 feet. 12.356 " 7 " 6.3943 " 2.7424 "
Mexican	o.838o '' 1.0668 km.	2.7493 '' 3.500 ''

CONVERSION OF MEASURES OF TIME AND ANGLE.

Arc into time				Table 19
Time into arc				TABLE 20
Days into decimals of a year and angle				TABLE 21
Hours, minutes and seconds into decimals of a day				TABLE 22
Decimals of a day into hours, minutes and seconds				TABLE 23
Minutes and seconds into decimals of an hour .				TABLE 24
Local mean time at apparent noon				TABLE 25
Sidereal time into mean solar time				TABLE 26
Mean solar time into sidereal time	•	•		Table 27

ARC INTO TIME.

56 3 44 116 7 44 176 11 44 236 15 44 296 19 44 356 23 44 56 3 44 56 3 733 57 3 48 117 7 48 177 11 48 237 15 48 297 19 48 357 23 48 57 3 48 57 3 800 58 3 52 118 7 52 178 11 52 238 15 52 298 19 52 358 23 52 58 3 52 58 3 867				- 1		- 				1	- 1	_	= 1	ı	_	ì	Ī			
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40 240 100 640 160 1040 220 1440 280 1840 340 2240 40 240 40 2.667 41 244 101 644 161 1044 221 1444 281 1844 341 2244 41 244 41 2.733 42 248 102 648 162 1048 222 1448 282 1848 342 2248 42 248 42 2.800 43 252 103 652 163 1052 223 1452 283 1852 343 2225 243 2.52 43 2.867 44 256 104 656 164 1056 224 1456 284 1856 344 2256 44 256 44 2.933 45 3 0 105 7 0 165 11 0 225 15 0 285 19 0 345 23 0 45 3 0 45 3.000 46 3 4 106 7 4 166 11 4 226 15 4 286 19 4 346 23 4 46 3 4 46 3.057 47 3 8 107 7 8 167 11 8 227 15 8 287 19 8 347 23 8 47 3 8 312 108 7 12 168 11 12 228 15 12 288 19 12 348 23 12 48 3 12 48 3 12 48 3 12 48 3 12 38 47 3 36 49 3 16 49 3 16 49 3 16 49 3 16 49 3 16 50 3 20 110 7 7 7 7 7 7 7 7 7	T -	1 -		-		2 158 5 150					278	18						1 -		
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TIME INTO ARC.

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Time.	Arc.	Time.	Arc.	Time.	. Arc.	1	Time.	Arc.	Time.	Arc.	ime.	Arc.
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10 11 12 13 14	2 30 2 45 3 0 3 15 3 30	30 31 32 33 34	7 30 7 45 8 0 8 15 8 30	50 51 52 53 54	12 4 13 13 1	o 5 0 5 0	10 11 12 13 14	2 30 2 45 3 0 3 15 3 30	30 31 32 33 34	7 30 7 45 8 0 8 15 8 30	50 51 52 53 54	12 30 12 45 13 0 13 15 13 30
15 16 17 18 19	3 45 4 0 4 15 4 30 4 45	35 36 37 38 39	8 45 9 0 9 15 9 30 9 45	55 56 57 58 59	14 14 1 14 3	5 5 5 5	15 16 17 18 19	3 45 4 0 4 15 4 30 4 45	35 36 37 38 39	8 45 9 0 9 15 9 30 9 45	55 56 57 58 59	13 45 14 0 14 15 14 30 14 45
20	5 0	40	10 0	60	15	0	20	5 0	40	10 0	60	15 0
		Н	undred	hs o	f a S	ecc	ond	of Tim	e into	Arc.		
Hundre of a S ond of T	ec	00	.01	02	.03	٠.	04	.05	.06	.07	.08	.09
.1	0.00 0.00 0.15 0.30 0.45 .10 1.50 1.65 1.80 1.95 .20 3.00 3.15 3.30 3.45 .30 4.50 4.65 4.80 4.95 .40 6.00 6.15 6.30 6.45						.60 .10 .60 .10	0.75 2.25 3.75 5.25 6.75	0.90 2.40 3.90 5.40 6.90	1.05 2.55 4.05 5.55 7.05	1.20 2.70 4.20 5.70 7.20	1.35 2.85 4.35 5.85 7.35
.6 .7 .8	0.50 7.50 7.65 7.80 7.95 .60 9.00 9.15 9.30 9.45 .70 10.50 10.65 10.80 10.95 .80 12.00 12.15 12.30 12.45 .90 13.50 13.65 13.80 13.95					9 11 12	6.10 6.60 6.10 6.60	8.25 9.75 11.25 12.75 14.25	8.40 9.90 11.40 12.90 14.40	8.55 10.05 11.55 13.05 14.55	8.70 10.20 11.70 13.20 14.70	8.85 10.35 11.85 13.35 14.85

Day	• 1		Day of	Month.	Day	Decima!		Day of	Month.
of Year.	of a Year.	Angle.	Common Year.	Bissexfile Year.	of Year.	of a Year,	Angle.	Common Year.	Bissextile Year.
1 2 3 4	0.00000 .00274 .00548 .00821	o° o′ o 59 i 58 2 57	Jan. 1 2 3 4	Jan. 1 2 3 4	51 52 53 54	0.13689 .13963 .14237 .14511	49° 17′ 50 16 51 15 52 14	Feb. 20 21 22 23	Feb. 20 21 22 23
5 6 7 8 9	0.01095 .01369 .01643 .01916 .02190	3 57 4 56 5 55 6 54 7 53	5 7 8 9	5 6 7 8 9	55 56 57 58 59	0.14784 .15058 .15332 .15606 .15880	53 13 54 13 55 12 56 11 57 10	24 25 26 27 28	24 25 26 27 28
10 11 12 13 14	0.02464 .02738 .03011 .03285	8 52 9 51 10 51 11 50 12 49	10 11 12 13 14	10 11 12 13 14	60 61 62 63 64	0.16153 .16427 .16701 .16975 .17248	58 9 59 8 60 7 61 7 62 6	Mar. 1 2 3 4 5	Mar. 1 2 3 4
15 16 17 18	0.03833 .04107 .04381 .04654 .04928	13 48 14 47 15 46 16 45 17 44	15 16 17 18	15 16 17 18	65 66 67 68 69	0.17522 .17796 .18070 .18344 .18617	63 5 64 4 65 3 66 2 67 1	6 7 8 9	5 6 7 8
20 21 22 23 24	0.05202 .05476 .05749 .06023 .06297	18 44 19 43 20 42 21 41 22 40	20 21 22 23 24	20 21 22 23 24	70 71 72 73 74	0.18891 .19165 .19439 .19713 .19986	68 0 69 0 69 59 70 58 71 57	11 12 13 14 15	10 11 12 13 14
25 26 27 28 29	0.06571 .06845 .07118 .07392 .07666	23 39 24 38 25 38 26 37 27 36	25 26 27 28 29	25 26 27 28 29	75 76 77 78 79	0.20260 .20534 .20808 .21081	72 56 73 55 74 54 75 54 76 53	16 17 18 19 20	15 16 17 18
30 31 32 33 34	0.07940 .08214 .08487 .08761 .09035	28 35 29 34 30 33 31 32 32 32	30 31 Feb. 1 2 3	30 31 Feb. 1 2 3	80 81 82 83 84	0.21629 .21903 .22177 .22450 .22724	77 52 78 51 79 50 80 49 81 48	21 22 23 24 25	20 21 22 23 24
35 36 37 38 39	0.09309 .09582 .09856 .10130 .10404	33 31 34 30 35 29 36 28 37 27	4 5 6 7 8	4 5 6 7 8	85 86 87 88 89	0.22998 .23272 .23546 .23819 .24093	82 48 83 47 84 46 85 45 86 44	26 27 28 29 30	25 26 27 28 29
40 41 42 43 44	0.10678 .10951 .11225 .11499 .11773	38 26 39 26 40 25 41 24 42 23	9 10 11 12 13	9 10 11 12 13	90 91 92 93 94	0.24367 .24641 .24914 .25188 .25462	87 43 88 42 89 42 90 41 91 40	Apr. 1 2 3 4	30 31 Apr. 1 2
45 46 47 48 49	0.12047 .12320 .12594 .12868 .13142	43 22 44 21 45 20 46 19 47 19	14 15 16 17 18	14 15 16 17 18	95 96 97 98 99	0.25736 .26010 .26283 .26557 .26831	92 39 93 38 94 37 95 36 96 35	5 6 7 8 9	4 5 6 7 8
50	0.13415	48 18	19	19	100	0.27.105	97 35	10	9

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101 102 103 104	0.27379 .27652 .27926 .28200	98°34′ 99 33 100 32 101 31	Apr. 11 12 13 14	Apr. 10 11 12 13	151 152 153 154	0.41068 .41342 .41615 .41889	147° 51′ 148 50 149 49 150 48	May 31 June 1 2 3	May 30 31 June 1
105 106 107 108 109	0.28474 .28747 .29021 .29295 .29569	102 30 103 29 104 29 105 28 106 27	15 16 17 18 19	14 15 16 17 18	155 156 157 158 159	0.42163 .42437 .42710 .42984 .43258	151 47 152 46 153 45 154 45 155 44	4 5 6 7 8	3 4 5 6 7
110 111 112 113 114	0.29843 .30116 .30390 .30664 .30938	107 26 108 25 109 24 110 23 111 23	20 21 22 23 24	19 20 21 22 23	160 161 162 163 164	0.43532 .43806 .44079 .44353 .44627	156 43 157 42 158 41 159 40 160 39	9 10 11 12 13	8 9 10 11 12
115 116 117 118 119	0.31211 .31485 .31759 .32033 .32307	112 22 113 21 114 20 115 19 116 18	25 26 27 28 29	24 . 25 . 26 27 28	165 166 167 168 169	0.44901 •45175 •45448 •45722 •45996	161 39 162 38 163 37 164 36 165 35	14 15 16 17 18	13 14 15 16 17
120 121 122 123 124	0.32580 .32854 .33128 .33402 .33676	117 17 118 17 119 16 120 15 121 14	May 1 2 3 4	29 30 May I 2	170 171 172 173 174	0.46270 .46543 .46817 .47091 .47365	166 34 167 33 168 33 169 32 170 31	19 20 21 22 23	18 19 20 21 22
125 126 127 128 129	0.33949 .34223 .34497 34771 .35044	122 13 123 12 124 11 125 10 126 10	5 6 7 8 9	4 5 6 7 8	175 176 177 178 179	0.47639 .47912 .48186 .48460 .48734	171 30 172 29 173 28 174 27 175 26	24 25 26 27 28	23 24 25 26 27
130 131 132 133 134	0.35318 ·35592 ·35866 ·36140 ·36413	127 9 128 8 129 7 130 6 131 5	10 11 12 13 14	9 10 11 12 13	180 181 182 183 184	0.49008 .49281 .49555 .49829 .50103	176 26 177 25 178 24 179 23 180 22	29 30 July 1 2 3	28 29 30 July 1
135 136 137 138 139	0.36687 .36961 .37235 .37509 .37782	132 4 133 4 134 3 135 2 136 1	15 16 17 18 19	14 15 16 17 18	185 186 187 188 189	0.50376 .50650 .50924 .51198 .51472	181 21 182 20 183 20 184 19 185 18	4 56 78	3 4 5 6 7
140 141 142 143 144	0.38056 .38330 .38604 .38877 .39151	137 0 137 59 138 58 139 58 140 57	20 21 22 23 24	19 20 21 22 23	190 191 192 193 194	0.51745 .52019 .52293 .52567 .52841	186 17 187 16 188 15 189 14 190 14	9 10 11 12 13	8 9 10 11 12
145 146 147 148 149	0.39425 .39699 .39973 .40246 .40520	141 56 142 55 143 54 144 53 145 52	25 26 27 28 29	24 25 26 27 28	195 196 197 198 199	0.53114 ·53388 ·53662 ·53936 ·54209	191 13 192 12 193 11 194 10 195 9	14 15 16 17 18	13 14 15 16
150	0.40794	146 51	30	29	200	0.54483	196 8	19	18

		*				1		1	
Day of	Decimal	Anala	Day of	Month.	Day	Decimal		Day of	Month,
Year	of a Year.	Angle.	Common Year.	Bissextile Year.	of \\ear.	of a Year.	Angle.	Common Year.	Bis sextile Year.
201	0.54757	197° 8′	July 20	July 19	251	o.68446	246° 24′	Sept. 8	Sept. 7
202	.55031	198 7	21	20	252	.68720	247 24	9	8
203	.55305	199 6	22	21	253	.68994	248 23	10	9
204	.55578	200 5	23	22	254	.69268	249 22	11	10
205	0.55852	20I 4	24	23	255	0.69541	250 21	12	11
206	.56126	202 3	25	24	256	.69815	251 20	13	12
207	.56400	203 2	26	25	257	.70089	252 19	14	13
208	.56674	204 I	27	26	258	.70363	253 18	15	14
209	.56947	205 I	28	27	259	.70637	254 17	16	15
210	0.57221	206 0	29	28	260	0.70910	255 17	17	16
211	·57495	206 59	30	29	261	.71184	256 16	18	17
212	·57769	207 58	31	30	262	.71458	257 15	19	18
213	·58042	208 57	Aug. 1	31	263	.71732	258 14	20	19
214	·58316	209 56	2	Aug. 1	264	.72005	259 13	21	20
215	0.58590	210 55	3	2	265	0.72279	260 12	22	21
216	.58864	211 55	4	3	266	.72553	261 11	23	22
217	.59138	212 54	5	4	267	.72827	262 11	24	23
218	.59411	213 53	6	5	268	.73101	263 10	25	24
219	.59685	214 52	7	6	269	.73374	264 9	26	25
220	0.59959	215 51	8	7	270	0.73648	265 8	27	26
221	.60233	216 50	9	8	271	.73922	266 7	28	27
222	.60507	217 49	10	9	272	.74196	267 6	29	28
223	.60780	218 49	11	10	273	.74470	268 5	30	29
224	.61054	219 48	12	11	274	.74743	269 5	Oct. I	30
225	0.61328	220 47	13	12	275	0. 7 5017	270 4	2	Oct. 1
226	.61602	221 46	14	13	276	.75291	271 3	3	2
227	.61875	222 45	15	14	277	.75565	272 2	4	3
228	.62149	223 44	16	15	278	.75838	273 1	5	4
229	.62423	224 43	17	16	279	.76112	274 0	6	5
230 231 232 233 234	0.62697 .62971 .63244 .63518 .63792	225 43 226 42 227 41 228 40 229 39	18 19 20 21 22	17 18 19 20 21	280 281 282 283 284	0.76386 .76660 .76934 .77207 .77481	274 59 275 59 276 58 277 57 278 56	7 8 9 10	6 7 8 9
235	0.64066	230 38	23	22	285	0.77755	279 55	12	11
236	.64339	231 37	24	23	286	.78029	280 54	13	12
237	.64613	232 36	25	24	287	.78303	281 53	14	13
238	.64887	233 36	26	25	288	.78576	282 52	15	14
239	.65161	234 35	27	26	289	.78850	283 52	16	15
240	0.65435		28	27	290	0.79124	284 51	17	16
241	.65708		29	28	291	.79398	285 50	18	17
242	.65982		30	29	292	.79671	286 49	19	18
243	.66256		31	30	293	.79945	287 48	20	19
244	.66530		Sept. 1	31	294	.80219	288 47	21	20
245	o.66804	240 30	2	Sept. 1	295	0.80493	289 46	22	21
246	.67077	241 29	3	2	296	.80767	290 46	23	22
247	.67351	242 28	4	3	297	.81040	291 45	24	2 3
248	.67625	243 27	5	4	298	.81314	292 44	25	24
249	.67899	244 26	6	5	299	.81588	293 43	26	25
250	0.68172	245 25	7	6	300	0.81862	294 42	27	26

Day	Decimal		Day of	Month.	Day	Decimal			Day of	Month.
of Year.	of a Year.	Angle.	Common Year	Bissextile Year.	Yenr.	of a Year.	Angl		Common Year.	Bissextile Year.
301 302 303 304	0.82136 .82409 .82683 .82957	295°41′ 296 40 297 40 298 39	Oct. 28 29 30 31	Oct. 27 28 29 30	351 352 353 354	0.95825 .96099 .96372 .96646	346	57	Dec. 17 18 19 20	Dec. 16 17 18 19
305 306 307 308 309	0.83231 .83504 .83778 .84052 .84326	299 38 300 37 301 36 302 35 303 34	Nov. 1 2 3 4 5	Nov. 1 2 3 4	355 356 357 358 359	0.96920 ,97194 .97467 .97741 .98015	348 349 350 351 352	54 53 52	21 22 23 24 25	20 21 22 23 24
310 311 312 313 314	0.84600 .84873 .85147 .85421 .85695	304 34 305 33 306 32 307 31 308 30	6 7 8 9 10	5 6 7 8 9	360 361 362 363 364	0.98289 .98563 .98836 .99110 .99384	353 354 355 356 357	50 49 48	26 27 28 29 30	25 26 27 28 29
315 316 317	0.85969 .86242 .86516	309 29 310 28 311 27	11 12 13	IO 11 12	365 366	0.99658 .99932	358 359		31	30 31
318 319	.86790 .87064	312 27 313 26	14	13	Con	version for	Hours.	Conv	ersion for	Minutes.
320 321 322 323	0.87337 .87611 .87885 .88159	314 25 315 24 316 23 317 22	. 16 17 18 19	15 16 17 18	Hrs.	Dec. of Year.	Angle.	Min.	Dec. of Year.	Angie.
324 325	.88433 o.88706	318 21 319 21	20 21	19 20	2	0.00011	2.5 4.9	1 2	0.00000	80.
326 327 328	.88980 .89254 .89528	320 20 321 19 322 18	22 23 24	21 22 23	3 4	34 46	7·4 9·9	3 4]]	4 - 1
329 330	.89802	323 17	25 26	24	5	0.00057 68 80	12.3 14.8 17.2	5 6	0,0000	.25
331 332	0.90075 90349 90623	324 16 325 15 326 15	27 28	25 26 27	7 8 9	91	19.7	7 8 9	2	.33
333 334	.90897 .91170	327 14 328 13	29 30	28 29	11	0.00114	24.6 27.1	10 20	o.00002	1 11
335 336	0.91444 .91718	329 12 330 11	Dec. 1	Dec. 1	12 13	137 148	29.6 32.0	30 40	8	1.23
337 338 339	.91992 .92266 .92539	331 10 332 9 333 9	3 4 5	2 3 4	14 15	160 0.00171	34·5 37·0	50 60	0.00011	
340	0.92813	334 8	6	5	16 17	183	39.4 41.9		0.00011	2.40
34I 342	.93087 .93361	335 7 336 6	7 8	6 7 8	18 19	205 217	44.4 46.8			
343 344	.93634 .93 9 08	337 5 338 4	9 10	9	20	0.00228	49-3			
345 346	0.94182 .94456	339 3 340 2	11 12	11 10	2I 22	240 251 262	51.7 54.2			
347 348	.94730 .95003	34I 2 342 I	13 14	12	23 24	202 274	56.7 59.1			
349 350	.95277 0.95551	343 ° 343 59	15	14						

TABLE 22.
HOURS, MINUTES AND SECONDS INTO DECIMALS OF A DAY.

Hours,	Day.	Min.	Day.	Min.	Day.	Sec.	Day.	Sec.	Day.
1 2 3 4	0.041 667 .083 333 .125 000 .166 667	1 2 3 4	0.000 694 .001 389 .002 083 .002 778	31 32 33 34	0.021 528 .022 222 .022 917 .023 611	1 2 3 4	0.000 012 .000 023 .000 035 .000 046	31 32 33 34	0.000 359 .000 370 .000 382 .000 394
5 6 7 8 9	0.208 333 .250 000 .291 667 .333 333 .375 000	5 6 7 8 9	0.003 472 .004 167 .004 861 .005 556 .006 250	35 36 37 38 39	0.024 305 .025 000 .025 694 .026 389 .027 083	5 6 7 8 9	0.000 058 .000 069 .000 081 .000 093 .000 104	35 36 37 38 39	0.000 405 .000 417 .000 428 .000 440
10 11 12 13 14 15 16 17 18	0.416 667 .458 333 .500 000 .541 667 .583 333 0.625 000 .666 667 .708 333 .750 000	10 11 12 13 14 15 16 17 18	0.006 944 .007 639 .008 333 .009 028 .009 722 0.010 417 .011 111 .011 806 .012 500	40 41 42 43 44 45 46 47 48	0.027 778 .028 472 .029 167 .029 861 .030 556 0.031 250 .031 944 .032 639 .033 333	10 11 12 13 14 15 16 17 18	0.000 I16 .000 I27 .000 I39 .000 I50 .000 I62 0.000 I74 .000 I85 .000 I97 .000 208	40 41 42 43 44 45 46 47 48	0.000 463 .000 475 .000 486 .000 498 .000 509 0.000 521 .000 532 .000 544 .000 556
19 20 21 22 23 24	.791 667 0.833 333 .875 000 .916 667 .958 333 1.000 000	20 21 22 23 24	.013 194 0.013 889 .014 583 .015 278 .015 972 .016 667	49 50 51 52 53 54	.034 028 0.034 722 .035 417 .036 111 .036 806 .037 500	20 21 22 23 24	.000 220 0.000 23I .000 243 .000 255 .000 266 .000 278	49 50 51 52 53 54	.000 567 0.000 579 .000 590 .000 602 .000 613 .000 625
		25 26 27 28 29 30	0.017 361 .018 056 .018 750 .019 444 .020 139 0.020 833	55 56 57 58 59 60	0.038 194 .038 889 .039 583 .040 278 .040 972 0.041 667	25 26 27 28 29 30	0.000 289 .000 301 .000 313 .000 324 .000 336	55 56 57 58 59 60	0.000 637 .000 648 .000 660 .000 671 .000 683

TABLE 23.

DECIMALS OF A DAY INTO HOURS, MINUTES AND SECONDS.

Hundre	dths of a	a Da	ıy.	Ten Thousa	ndths of a Day.	Millionths of a Day.			
d.	h.	m.	s.	d.	min. sec.	d.	sec.		
0.01		14	24	0.0001	8.64	0.000001	0.09		
.02		28	48	2	17.28	2	0.17		
.03		43	12	3	25.92	3	0.26		
.04		57	36	4	34.56	4	0.35		
0.05	1	12	0	0.0005	43.20	0.000005	0.43		
.06	1	26	24	6	51.84	6	0.52		
.07	1	40	48	7 8	I 0.48	7	0.60		
.08	1	55	12	8	1 9.12	8	0.69		
.09	2	9	36	9	1 17.76	9	0.78		
0.10	2	24	0	0.0010	· I 26.40	0.000010	0.86		
.20	4	48	0	20	2 52.80	20	1.73		
.30	7	12	0	30	4 19.20	30	2.59		
.40	9	36	0	40	5 45.60	40	3.46		
0.50	12	0	О	0.0050	7 12.00	0.000050	4.32		
.60	14	24	0	60	8 38.40	60	5.18		
.70	16	48	О	70	10 4.80	70	6.05		
.80	19	12	0	80	11 31.20	8o	6.91		
.90	21	36	0	90	12 57.60	90	7.78		
	1			(1)	·	Y]		

TABLE 24.
MINUTES AND SECONDS INTO DECIMALS OF AN HOUR.

Min.	Decimals of an hour.	Min.	Decimals of an hour.	Sec.	Decimals of an hour.	Sec.	Decimals of an hour.
1	0.016 667	31	0.516 667	1	0.000 278	31	0.008 611
2	.033 333	32	·533 333	2	.000 556	32	.008 889
3	.050 000	33	·550 000	3	.000 833	33	.009 167
4	.066 667	34	·566 667	4	.001 111	34	.009 444
5 6 7 8 9	0.083 333 .100 000 .116 667 .133 333 .150 000	35 36 37 38 39	0.583 333 .600 000 .616 667 .633 333 .650 000	5 6 7 8 9	0.001 389 .001 667 .001 944 .002 222	35 36 37 38 39	0.009 722 .010 000 .010 278 .010 556 .010 833
10	0.166 667	40	o.666 667	10	0.002 778	40	0.011 111
11	.183 333	41	.683 333	11	.003 056	41	.011 389
12	.200 000	42	.700 000	12	.003 333	42	.011 667
13	.216 667	43	.716 667	13	.003 611	43	.011 944
14	.233 333	44	.733 333	14	.003 889	44	.012 222
15 16 17 18	0.250 000 .266 667 .283 333 .300 000 .316 667	45 46 47 48 49	0.750 000 .766 667 .783 333 .800 000 .816 667	15 16 17 18 19	0.004 167 .004 444 .004 722 .005 000 .005 278	45 46 47 48 49	0.012 500 .012 778 .013 056 .013 333 .013 611
20	0.333 333	50	o.833 333	20	0.005 556	50	0.013 889
21	.350 000	51	.850 000	21	.005 833	51	.014 167
22	.366 667	52	.866 667	22	.006 111	52	.014 444
23	.383 333	53	.883 333	23	.006 389	53	.014 722
24	.400 000	54	.900 000	24	.006 667	54	.015 000
25	0.416 667	55	0.916 667	25	0,006 944	55	0.015 278
26	·433 333	56	•933 333	26	.007 222	56	.015 556
27	·450 000	57	•950 000	27	.007 500	57	.015 833
28	·466 667	58	•966 667	28	.007 778	58	.016 111
29	·483 333	59	•983 333	29	.008 056	59	.016 389
30	0.500 000	60	1.000 000	30	0.008 333	60	0.016 667

TABLE 25.
LOCAL MEAN TIME AT APPARENT NOON.

Day of Month.	JAN.	FEB.	MAR.	APR.	MAY.	JUNE.
1 8 16 24	h. m. 12 4 12 7 12 10 12 12	h. m. 12 14 12 14 12 14 12 13	h. m. 12 12 12 11 12 9 12 6	h. m. 12 4 12 2 12 0 11 58	h. m. 11 57 11 56 11 56 11 57	h. m. 11 58 11 59 12 0 12 2
	JULY.	AUG.	SEPT.	oct.	Nov.	DIC.
1 8 16 24	h. m. 12 4 12 5 12 6 12 6	h. m. 12 6 12 5 12 4 12 2	h. m. 12 0 11 58 11 55 11 52	h. m. 11 50 11 48 11 46 11 44	h. m. 11 44 11 44 11 45 11 47	h. m. 11 49 11 52 11 56 12 0

TABLE 27.

SIDEREAL TIME INTO MEAN SOLAR TIME.

The tabular values are to be *subtracted* from a sidereal time interval.

MEAN SOLAR TIME INTO SIDEREAL TIME.

The tabular values are to be added to a mean solar time interval.

Ĥrs.	Reduction to Mean Time.	Min.	Reduc- tion to Mean Time.	Min.	Reduc- tion to Mean Time.	Hrs.	Reduction to Sidereal Time.	Min.	Reduc- tion to Sidereal Time.	Min.	Reduc- tion to Sidereal Time.
h. 2 3 4	m. s. o 9.83 o 19.66 o 29.49 o 39.32	m. ! 2 3 4	s. o.16 o.33 o.49 o.66	m. 31 32 33 34	s. 5.08 5.24 5.41 5.57	h. 1 2 3 4	m. s. o 9.86 o 19.71 o 29.57 o 39.43	m. 1 2 3 4	o. 16 o. 33 o. 49 o. 66	m. 31 32 33 34	s. 5.09 5.26 5.42 5.59
5 6 7 8 9	0 49.15 0 58.98 1 8.81 1 18.64 1 28.47	5 6 7 8 9	0.82 0.98 1.15 1.31 1.47	35 36 37 38 39	5·73 5·90 6.06 6.23 6.39	5 6 7 8 9	0 49.28 0 59.14 1 9.00 1 18.85 1 28.71	5 6 7 8 9	0.82 0.99 1.15 1.31 1.48	35 36 37 38 39	5.75 5.91 6.08 6.24 6.41
10 11 12 13 14	1 38.30 1 48.13 1 57.95 2 7.78 2 17.61	10 11 12 13 14	1.64 1.80 1.97 2.13 2.29	40 41 42 43 44	6.55 6.72 6.88 7.04 7.21	10 11 12 13 14	1 38.56 1 48.42 1 58.28 2 8.13 2 17.99	10 11 12 13 14	1.64 1.81 1.97 2.14 2.30	40 41 42 43 44	6.57 6.74 6.90 7.06 7.23
15 16 17 18	2 27.44 2 37.27 2 47.10 2 56.93 3 6.76	15 16 17 18 19	2.46 2.62 2.79 2.95 3.11	45 46 47 48 49	7·37 7·54 7·70 7.86 8.03	15 16 17 18	2 27.85 2 37.70 2 47.56 2 57.42 3 7.27	15 16 17 18 19	2.46 2.63 2.79 2.96 3.12	45 46 47 48 49	7.39 7.56 7.72 7.89 8.05
20 21 22 23 24	3 16.59 3 26.42 3 36.25 3 46.08 3 55.91	20 21 22 23 24	3.28 3.44 3.60 3.77 3.93	50 51 52 53 54	8.19 8.36 8.52 8.68 8.85	20 21 22 23 24	3 17.13 3 26.99 3 36.84 3 46.70 3 56.56	20 21 22 23 24	3.29 3.45 3.61 3.78 3.94	50 51 52 53 54	8.21 8.38 8.54 8.71 8.87
		25 26 27 28 29	4.10 4.26 4.42 4.59 4.75	55 56 57 58 59	9.01 9.17 9.34 9.50 9.67			25 26 27 28 29	4.11 4.27 4.44 4.60 4.76	55 56 57 58 59	9.04 9.20 9.36 9.53 9.69
		30	4.91	60	9.83			30	4-93	60	9.86

Reduction for Seconds-sidereal or mean solar.

The tabular values are to be $\left\{ \begin{array}{l} \textit{subtracted} \\ \textit{added} \end{array} \right.$ from a sidereal $\left. \right\}$ time interval.

Sidereal or Mean Time.	0	1	2	3	4	5	6	7	8	9
s.	ъ.	ъ.	b.	s.	s. ·	ъ.	s.	s.	s.	s.
0	0.00	0.00	0.01	0.01	0,01	10.0	0.02	0.02	0.02	0.02
IO	.03	.03	.03	.04	.04	.04	.04	.05	.05	.05 .08
20	.05	.06	.06	.06	.07	.07	.07	.07	. 0 8	.08
30	.o8	.08	.09	.09	.09	.10	.10	.IO	.IO	.11
40	.11	.11	.11	.12	.12	.12	.13	.13	.13	.13
50	0.14	0.14	0.14	0.15	0.15	0.15	0.15	0.16	0.16	0.16

^{*} Subtract 0.14 from a sidereal time interval.

CONVERSION OF MEASURES OF WEIGHT.

Conversion of avoirdupois pound	s a	nd	ou	nce	s ii	ıto	kil	logi	ran	ıs	TABLE 28
Conversion of kilograms into avo	ird	up	ois	poi	unc	ls a	ınd	ou	nce	es	Table 29
Conversion of grains into grams											TABLE 30
Conversion of grams into grains											TABLE 31

TABLE 28.

AVOIRDUPOIS POUNDS AND OUNCES INTO KILOGRAMS.

1 avoirdupois pound = 0.4535924 kilogram. 1 avoirdupois ounce = 0.0283495 kilogram.

Pounds.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	kg.	kg.	kg.	kg.	kg.	kg.	kg.	kg.	kg.	kg.
o	0,0000	0.0454	0.0907	0.1361	0.1814	0.2268	0.2722	0.3175	0.3629	0.4082
1	0.4536	0.4990	0.5443	0.5897	0.1314	0.6804	0.7257	0.7711	0.8165	0.8618
2	0.9072	0.9525	0.9979	1.0433	1.0886	1.1340	1.1793	1.2247	1.2701	1.3154
3	1.3608	1.4061	1.4515	1.4969	1.5422	1.5876	1.6329	1.6783	1.7237	1.7690
4	1.8144	1.8597	1.9051	1.9504	1.9958	2.0412	2.0865	2.1319	2.1772	2.2226
, ,		-1.0097	~-5-0-	219004	1.9930	2.0412	2.000	20.23.9		_,
5	2.2680	2.3133	2.3587	2.4040	2.4494	2.4948	2.5401	2.5855	2.6308	2.6762
6	2.7216	2.7669	2.8123	2.8576	2.9030	2.9484	2.9937	3.0391	3.0844	3.1298
7	3.1751	3.2205	3.2659	3.3112	3.3566	3.4019	3.4473	3.4927	3.5380	3.5834
8	3.6287	3.6741	3.7195	3.7648	3.8102	3.8555	3.9009	3.9463	3.9916	4.0370
9	4.0823	4.1277	4.1731	4.2184	4.2638	4.3091	4.3545	4.3998	4.4452	4.4906
				1		1	<u> </u>	<u> </u>	1	1
Ounces.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	kg.	kg.	kg.	kg.	kg.	kg.	kg.	kg.	kg.	kg.
0	0.0000	0.0028	0.0057	0.0085	0.0113	0.0142	0.0170	0,0198	0.0227	0.0255
1	.0283	.0312	.0340	.0369	.0397	.0425	.0454	.0482	.0510	.0539
2	.0567	.0595	.0624	.0652	.0680	.0709	.0737	.0765	.0794	.0822
3	.0850	.0879	.0907	.0936	.0964	.0992	.1021	.1049	.1077	.1106
4	.1134	.1162	.1191	.1219	.1247	.1276.	.1304	.1332	.1361	.1389
5	0.1417	0.1446	o. 1474	0.1503	0.1531	0.1559	0.1588	0.1616	0.1644	0.1673
6	.1701	.1729	.1758	.1786	.1814	.1843	.1871	.1899	.1928	.1956
7	.1984	.2013	.2041	.2070	.2098	.2126	.2155	.2183	.2211	.2240
8	.2268	.2296	.2325	.2353	.2381	.2410	.2438	.2466	.2495	.2523
9	.2551	.2580	.2608	.2637	.2665	.2 693	.2722	.2750	.2778	.2807
10	0.2835	0.2863	0.2892	0.2920	0.2948	0.2977	0.3005	0.3033	0.3062	0.3090
11	.3118	.3147	.3175	.3203	.3232	.3260	.3289	.3317	·3345	-3374
12	.3402	.3430	•3459	.3487	-3515	•3544	.3572	.3600	.3629	.3657
13	.3685	.3714	.3742	.3770	•3799	.3827	.3856	.3884	.3912	.3941
14	.3969	.3997	.4026	.4054	.4082	.4111	.4139	.4167	.4196	.4224
15	.4252	.4281	.4309	•4337	.4366	•4394	·4423	-4451	•4479	.4508

TABLE 29.

KILOGRAMS INTO AVOIRDUPOIS POUNDS AND OUNCES.

1 kilogram = 2.204622 avoirdupois pounds.

Kilograms.	0.0	0.1	0.2	0.3	3	0.4	0.5	0.6	0.7	0.8	0.9
	Av. lbs.	Av. lbs.	Av. lbs.	Av. 1	bs.	Av. lbs.	Av. 1bs	. Av. lbs.	Av. 1bs.	Av. lbs.	Av. 1bs.
0	0.000	0.220	0.441	0.6	61	0.882	1.102	1.323	1.543	1.764	1.984
I	2.205	2.425	2.646	2.8	66	3.086	3.307	3.527	3.748	3.968	4.189
2	4.409	4.630	4.850	5.0	71	5.291	5.512	5.732	5.952	6.173	6.393
3	6.614	6.834	7.055	7.2	75	7.496	7.716	7.937	8.157	8.378	8.598
4	8.818	9.039	9.259	9.4	.8o	9.700	9.921	10.141	10.362	10.582	10.803
5	11.023	11.244	11.464	11.6	84	11.905	12.125	12.346	12,566	12.787	13.007
6	13.228	13.448	13.669	13.8	٠,	14.110	14.330	١ .	14.771	14.991	15.212
7	15.432	15.653	15.873	16.0	- 1	16.314	16.535	1	16.976	17.196	17.417
8	17.637	17.857	18.078	18.2	98	18.519	18.739		19.180	19.401	19.621
9	19.842	20.062	20.283	20.5	- 1	20.723	20.944		21.385	21.605	21.826
		Tenths of a	Kilogram	into Ou	nces.		i	Hundre nto Decimals	dths of a K of a Poun	llogram d and Ounc	es.
	kg.	Oz.	1	g.		Oz.	kg.	Av. 1bs.	Oz. k	g. Av. 1b	s. Oz.
	0.1	3.527	·	0.6		.1644	10.0	0,022 == 0		, ,	= 2.12
	.2	7.054		.7		1.6918	.02	.044 = 0			= 2.47
	•3	10.582		.8		3.2192	.03	.066 = 1			= .2.82
	.4 .5	14.109		.0	-	1.7466 5.2740	.04 .05	.088 = 1		- 1	3 = 3.17 0 = 3.53
	.5	17.537				J. 2/40	.53			.220	3.33

TABLE 30.

CRAINS INTO CRAMS.

I grain = 0.06479892 gram.

Grains.	0	ı	2	:	3	4	5	6	7	8	9
	grams.	grams.	gram	s. gra	ms.	grams.	grams.	grams.	grams.	grams.	grams.
0	0,0000	0.0648	0.129	6 0.1	944	0.2592	0.3240	0.3888	0.4536	0.5184	0.5832
10	0.6480	0.7128	0.777	6 0.8	424	0.9072	0.9720	1.0368	1.1016	1.1664	1.2312
20	1.2960	1.3608	1.425		904	1.5552	1.6200	1.6848	1.7496	1.8144	1.8792
30	1.9440	2.0088	2.073	6 2.1	384	2.2032	2 .2 680	2.3328	2.3976	2.4624	2.5272
40	2.5920	2.6568	2.721	6 2.7	864	2.8512	2. 9160	2.9808	3.0455	3.1103	3.1751
50	3.2399	3.3047	3.369	3.4	343	3.4991	3.5639	3.6287	3.6935	3.7583	3.8231
60	3.8879	3.9527	4.017	′5 4.c	823	4.1471	4.2119	4.2767	4.3415	4.4063	4.4711
70	4.5359	4.6007	4.665	5 4.7	303	4.7951	4.8599	4.9247	4.9895	5.0543	5.1191
80	5.1839	5.2487	5.313	5 5.3	783	5.4431	5.5079	5.5727	5.6375	5.7023	5.7671
90	5.8319	5.8967	5.961	5 6.0	263	6.0911	6.1559	6.2207	6.285	6.3503	6.4151
		Ten	ths of a	Grain.	-	<u>.</u>		Hundr	edths of	a Grain.	
	Grain.	gram	. '	Grain.		grain.	Grain.	gran	n. (Grain.	gram,
	0.1	0.006	' 1	0.6		0.0389	0,01	0.000		0.06	0.0039
	.2	.0130		.7		.0454	.02	.001	- 1	.07	.0045
	•3	.019		.8		.0518	.03 .04	.001	- 1	.08	.0052
	.4 .5	.0259	•	.9 1.0	ļ	.0503 .0648	.05	.003		.10	.0055

GRAMS INTO CRAINS.

1 gram = 15.432356 grains.

Grams.	.0		.2	.3	.4	.5	.6	.7	.8	.9
0 1 · · · 2 3 · 4 5 · 6 7 · 8	Grains. 0.00 15.43 30.86 46.30 61.73 77.16 92.59 108.03 123.46 138.89	Grains. 1.54 16.98 32.41 47.84 63.27 78.71 94.14 109.57 125.00 140.43	Grains. 3.09 18.52 33.95 49.38 64.82 80.25 95.68 111.11 126.55 141.98	Grains 4.6 20.00 35.44 50.9 66.3 81.79 97.22 112.66 128.00	6.17 21.61 37.04 52.47 67.90 83.33 98.77 114.20	23.15	Grains. 9.26 24.69 40.12 55.56 70.99 86.42 101.85 117.29 132.72 148.15	Grains. 10.80 26.24 41.67 57.10 72.53 87.96 103.40 118.83 134.26 149.69	Grains. 12.35 27.78 43.21 58.64 74.08 89.51 104.94 120.37 135.80 151.24	Grains. 13.89 29.32 44.75 60.19 75.62 91.05 106.48 121.92 137.35 152.78
	0	ł	2	3	4	5	6	7	8	9
0 10 20 30 40 50 60 70 80 90	1234.59	Grains. 15.43 169.76 324.08 478.40 632.73 787.05 941.37 1095.70 1250.02 1404.34	1265.45		61.73 216.05 4 370.38 7 524.70 679.02 1 833.35 4 987.67	694.46 848.78 1003.10 1157.43 1311.75	1172.86 1327.18	1188.29 1342.61	740.75 895.08 1049.40 1203.72 1358.05	Grains. 138.89 293.21 447.54 601.86 756.19 910.51 1064.83 1219.16 1373.48 1527.80
	gram. 0.01 .02 .03 .04 .05	Grain 0.154 .309 .463 .617 .772	0.0	,	Grain. 0.926 1.080 1.235 1.389 1.543	gram. 0.001 .002 .003 .004 .005	Grain •.015 .031 .046 .062 .077	0.	ram. .006 .007 .008 .009 .010	Grain. 0.093 .108 .123 .139 .154

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SYNOPTIC CONVERSION OF VELOCITIES.

Miles per hour into meters per second, feet per second and kilometers per hour.

T								24.1		F .	Wil
Miles	Meters	Feet	Kilome-	Miles	Meters	Feet	Kilome-	Miles	Meters	Feet	Kilome-
per	per	per	ters per	per	per	per	ters per	per	per	per	ters per
hour.	second.	second,	hour.	hour.	second.	second,	hour,	hour.	second.	second.	hour.
0.0 0.5 1.0 1.5 2.0 2.5	0.0 0.2 0.4 0.7 0.9 1.1	0.0 0.7 1.5 2.2 2.9 3.7	0.0 0.8 1.6 2.4 3.2 4.0	26.0 26.5 27.0 27.5 28.0 28.5	11.6 11.8 12.1 12.3 12.5 12.7	38.1 38.9 39.6 40.3 41.1 41.8	41.8 42.6 43.5 44.3 45.1 45.9	52.0 52.5 53.0 53.5 54.0 54.5	23.2 23.5 23.7 23.9 24.1 24.4	76.3 77.0 77.7 78.5 79.2 79.9	83.7 84.5 85.3 86.1 86.9
3.0	1.3	4.4	4.8	29.0	13.0	42.5	46.7	55.0	24.6	80.7	88.5
3.5	1.6	5.1	5.6	29.5	13.2	43.3	47.5	55.5	24.8	81.4	89.3
4.0	1.8	5.9	6.4	30.0	13.4	44.0	48.3	56.0	25.0	82.1	90.1
4.5	2.0	6.6	7.2	30.5	13.6	44.7	49.1	56.5	25.3	82.9	90.9
5.0	2.2	7.3	8.0	31.0	13.9	45.5	49.9	57.0	25.5	83.6	91.7
5.5	2.5	8.1	8.9	31.5	14.1	46.2	50.7	57.5	25.7	84.3	92.5
6.0	2.7	8.8	9.7	32.0	14.3	46.9	51.5	58.0	25.9	85.1	93.3
6.5	2.9	9.5	10.5	32.5	14.5	47.7	52.3	58.5	26.2	85.8	94.1
7.0	3.1	10.3	11.3	33.0	14.8	48.4	53.1	59.0	26.4	86.5	95.0
7.5	3.4	11.0	12.1	33.5	15.0	49.1	53.9	59.5	26.6	87.3	95.8
8.0	3.6	11.7	12.9	34.0	15.2	49.9	54.7	60.0	26.8	88.0	96.6
8.5	3.8	12.5	13.7	34.5	15.4	50.6	55.5	60.5	27.0	88.7	97.4
9.0 9.5 10.0 10.5 11.0	4.0 4.2 4.5 4.7 4.9 5.1	13.2 13.9 14.7 15.4 16.1 16.9	14.5 15.3 16.1 16.9 17.7 18.5	35.0 35.5 36.0 36.5 37.0 37.5	15.6 15.9 16.1 16.3 16.5 16.8	51.3 52.1 52.8 53.5 54.3 55.0	56.3 57.1 57.9 58.7 59.5 60.4	61.0 61.5 62.0 62.5 63.0 63.5	27.3 27.5 27.7 27.9 28.2 28.4	89.5 90.2 90.9 91.7 92.4 93.1	98.2 99.0 99.8 100.6 101.4 102.2
12.0	5.4	17.6	19.3	38.0	17.0	55.7	61.2	64.0	28.6	93.9	103.0
12.5	5.6	18.3	20.1	38.5	17.2	56.5	62.0	64.5	28.8	94.6	103.8
13.0	5.8	19.1	20.9	39.0	17.4	57.2	62.8	65.0	29.1	95.3	104.6
13.5	6.0	19.8	21.7	39.5	17.7	57.9	63.6	65.5	29.3	96.1	105.4
14.0	6.3	20.5	22.5	40.0	17.9	58.7	64.4	66.0	29.5	96.8	106.2
14.5	6.5	21.3	23.3	40.5	18.1	59.4	65.2	66.5	29.7	97.5	107.0
15.0 15.5 16.0 16.5 17.0	6.7 6.9 7.2 7.4 7.6 7.8	22.0 22.7 23.5 24.2 24.9 25.7	24.1 24.9 25.7 26.6 27.4 28.2	41.0 41.5 42.0 42.5 43.0 43.5	18.3 18.6 18.8 19.0 19.2	60.1 60.9 61.6 62.3 63.1 63.8	66.0 66.8 67.6 68.4 69.2 70.0	67.0 67.5 68.0 68.5 69.0 69.5	30.0 30.2 30.4 30.6 30.8 31.1	98.3 99.0 99.7 100.5 101.2 101.9	107.8 108.6 109.4 110.2 111.0 111.8
18.0	8.0	26.4	29.0	44.0	19.7	64.5	70.8	70.0	31.3	102.7	112.7
18.5	8.3	27.1	29.8	44.5	19.9	65.3	71.6	70.5	31.5	103.4	113.5
19.0	8.5	27.9	30.6	45.0	20.1	66.0	72.4	71.0	31.7	104.1	114.3
19.5	8.7	28.6	31.4	45.5	20.3	66.7	73.2	71.5	32.0	104.9	115.1
20.0	8.9	29.3	32.2	46.0	20.6	67.5	74.0	72.0	32.2	105.6	115.9
20.5	9.2	30.1	33.0	46.5	20.8	68.2	74.8	72.5	32.4	106.3	116.7
21.0	9.4	30.8	33.8	47.0	21.0	68.9	75.6°	73.0	32.6	107.1	117.5
21.5	9.6	31.5	34.6	47.5	21.2	69.7	76.4	73.5	32.9	107.8	118.3
22.0	9.8	32.3	35.4	48.0	21.5	70.4	77.2	74.0	33.1	108.5	119.1
22.5	10.1	33.0	36.2	48.5	21.7	71.1	78.1	74.5	33.3	109.3	119.9
23.0	10.3	33.7	37.0	49.0	21.9	71.9	78.9	75.0	33.5	110.0	120.7
23.5	10.5	34.5	37.8	49.5	22.1	72.6	79.7	75.5	33.8	110.7	121.5
24.0	10.7	35.2	38.6	50.0	22.4	73.3	80.5	76.0	34.0	111.5	122.3
24.5	11.0	35.9	39.4	50.5	22.6	74.1	81.3	76.5	34.2	112.2	123.1
25.0	11.2	36.7	40.2	51.0	22.8	74.8	82.1	77.0	34.4	112.9	123.9
25.5	11.4	37.4	41.0	51.5	23.0	75.5	82.9	77.5	34.6	113.7	124.7
26.0	11.6	38.1	41.8	52.0	23.2	76.3	83.7	78.0	34.9	114.4	125.5

MILES PER HOUR INTO FEET PER SECOND.

I mile per hour $=\frac{44}{30}$ feet per second.

Miles per hour.	0	ı	2	3	4	5	6	7	8	9
o	Feet per sec. 0.0	Feet per sec.	Feet per sec. 2.9	Feet per sec.	Feet per sec 5.9	Feet per sec. 7.3	Feet per sec. 8.8	Feet per sec. 10.3	Feet per sec. II.7	Feet per sec. 13.2
10 20	14.7 29.3	16.1 30.8	17.6 32.3	19.1	20.5	22.0 36.7	23.5 38.1	24.9 39.6	26.4 41.1	27.9
30 40	44.0 58.7	45.5 60.1	46.9 61.6	33.7 48.4 63.1	35.2 49.9 64.5	51.3 66.0	52.8 67.5	54·3 68.9	55·7 70.4	42.5 57.2 71.9
50 60 70 80 90	73.3 88.0 102.7 117.3 132.0	74.8 89.5 104.1 118.8 133.5	76.3 90.9 105.6 120.3 134.9	77.7 92.4 107.1 121.7 136.4	79.2 93.9 108.5 123.2 137.9	80.7 95.3 110.0 124.7 139.3	82.1 96.8 111.5 126.1 140.8	83.6 98.3 112.9 127.6 142.3	85.1 99.7 114.4 129.1 143.7	86.5 101.2 115.9 130.5 145.2
100 110 120 130 140	146.7 161.3 176.0 190.7 205.3	148.1 162.8 177.5 192.1 206.8	149.6 164.3 178.9 193.6 208.3	151.1 165.7 180.4 195.1 209.7	152.5 167.2 181.9 196.5 211.2	154.0 168.7 183.3 198.0 212.7	155.5 170.1 184.8 199.5 214.1	156.9 171.6 186.3 200.9 215.6	158.4 173.1 187.7 202.4 217.1	159.9 174.5 189.2 203.9 218.5

TABLE 34.

FEET PER SECOND INTO MILES PER HOUR.

r foot per second = $\frac{30}{44}$ miles per hour.

Feet per sec.	0	1	2	3	4	5	6	7	8	9
0 IO 20	Miles per hr. 0.0 6.8 13.6	Miles per hr. 0.7 7.5 14.3	Miles per hr. I.4 8.2 I5.0	Miles per hr. 2.0 8.9 15.7	Miles per hr. 2.7 9.5 16.4	Miles per hr. 3.4 IO.2 I7.0	Miles per hr. 4.1 10.9 17.7	Miles per hr. 4.8 11.6 18.4	Miles per hr. 5.5 12.3 19.1	Miles per hr. 6.1 13.0
30	20.5	21.1	21.8	22.5	23.2	23.9	24.5	25.2	25.9	26.6
40	27.3	28.0	28.6	29.3	30.0	30.7	31.4	32.0	32.7	33.4
50	34.1	34.8	35.5	36.1	36.8	37.5	38.2	38.9	39.5	40.2
60 70 80 90	40.9 47.7 54.5 61.4	41.6 48.4 55.2 62.0	42.3 49.1 55.9 62.7	43.0 49.8 56.6 63.4	43.6 50.5 57.3 64.1	51.1 58.0 64.8	45.0 51.8 58.6 65.5	45.7 52.5 59.3 66.1	53.2 60.0 66.8	47.0 53.9 60.7 67.5
100	68.2	68.9	69.5	70.2	70.9	71.6	72.3	73.0	73.6	74.3
110	75.0	75.7	76.4	77.0	77.7	78.4	79.1	79.8	80.5	81.1
120	81.8	82.5	83.2	83.9	84.5	85.2	85.9	86.6	87.3	88.0
130	88.6	89.3	90.0	90.7	91.4	92.0	92.7	93.4	94.1	94.8
140	95.5	96.1	96.8	97.5	98.2	98.9	99.5	100.2	100.9	101.6
150	102.3	103.0	103.6	104.3	105.0	105.7	106.4	107.0	107.7	108.4
160	109.1	109.8	110.5	111.1	111.8	112.5	113.2	113.9	114.5	115.2
170	115.9	116.6	117.3	118.0	118.6	119.3	120.0	120.7	121.4	120.0
180	122.7	123.4	124.1	124.8	125.5	126.1	126.8	127.5	128.2	128.9
190	129.5	130.2	130.9	131.6	132.3	133.0	133.6	134.3	135.0	135.7

METERS PER SECOND INTO MILES PER HOUR.

1 meter per second = 2.236932 miles per hour.

Meters per										
second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	Miles	Miles	Miles	Miles	Miles	Miles	Miles	Miles	Miles	Miles
	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.
0	0.0	0.2	0.4	0.7	0.9	1.1	1.3	1.6	1.8	2.0
1	2.2	2.5	2.7	2.9	3.1	3.4	3.6	3.8	4.0	4.3
2	4.5	4.7	4.9	5.1	5.4	5.6	5.8	6.0	6.3	6.5
3	6.7	6.9	7.2	7.4	7.6	7.8	8.1	8.3	8.5	8.7
4	8.9	9.2	9.4	9.6	9.8	10.1	10.3	10.5	10.7	II.0
5	11.2	11.4	11.6	11.9	12.1	12.3	12.5	12.8	13.0	13.2
6	13.4	13.6	13.9	14.1	14.3	14.5	14.8	15.0	15.2	15.4
7	15.7	15.9	16.1	16.3	16.6	16.8	17.0	17.2	17.4	17.7
8	17.9	18.1	18.3	18.6	18.8	19.0	19.2	19.5	19.7	19.9
9	20.1	20.4	20.6	20.8	21.0	21.3	21.5	21.7	21.9	22.1
10	22.4	22.6	22.8	23.0	23.3	23.5	23.7	23.9	24.2	24.4
11	24.6	24.8	25.1	25.3	25.5	25.7	25.9	26.2	26.4	26.6
12	26.8	27.1	27.3	27.5	27.7	28.0	28.2	28.4	28.6	28.9
13	29.1	29.3	29.5	29.8	30.0	30.2	30.4	30.6	30.9	31.1
14	31.3	3 ¹ .5	31.8	32.0	32.2	32.4	32.7	32.9	33.1	33.3
15	33.6	33.8	34.0	34.2	34.4	34·7	34.9	35.1	35·3	35.6
16	35.8	36.0	36.2	36.5	36.7	36.9	37.1	37.4	37.6	37.8
17	38.0	38.3	38.5	38.7	38.9	39·1	39.4	39.6	39.8	40.0
18	40.3	40.5	40.7	40.9	41.2	41·4	41.6	41.8	42.1	42.3
19	42.5	42.7	43.0	43.2	43.4	43.6	43.8	44.1	44·3	44.5
20	44.7	45.0	45.2	45.4	45.6	45.9	46.1	46.3	46.5	46.8
21	47.0	47.2	47.4	47.6	47.9	48.1	48.3	48.5	48.8	49.0
22	49.2	49.4	49.7	49.9	50.1	50.3	50.6	50.8	51.0	51.2
23	51.5	51.7	51.9	52.1	52.3	52.6	52.8	53.0	53.2	53.5
24	53.7	53.9	54.1	54.4	54.6	54.8	55.0	55.3	55.5	55.7
25	55.9	56.1	56.4	56.6	56.8	57.0	57·3	57·5	57.7	57.9
26	58.2	58.4	58.6	58.8	59.1	59.3	59·5	59·7	60.0	60.2
27	60.4	60.6	60.8	61.1	61.3	61.5	61·7	62.0	62.2	62.4
28	62.6	62.9	63.1	63.3	63.5	63.8	64.0	64.2	64.4	64.6
29	64.9	65.1	65.3	65.5	65.8	66.0	66.2	66.4	66.7	66.9
30	67.1	67.3	67.6	67.8	68.0	68.2	68.5	68.7	68.9	69.1
31	69.3	69.6	69.8	70.0	70.2	70.5	70.7	70.9	71.1	71.4
32	71.6	71.8	72.0	72.3	72.5	72.7	72.9	73.1	73.4	73.6
33	73.8	74.0	74.3	74.5	74.7	74.9	75.2	75.4	75.6	75.8
34	76.1	76.3	76.5	76.7	77.0	77.2	77.4	77.6	77.8	78.1
35	78.3	78.5	78.7	79.0	79.2	79.4	79.6	79.9	80.1	80.3
36	80.5	80.8	S1.0	81.2	81.4	81.6	81.9	82.1	82.3	82.5
37	82.8	83.0	83.2	83.4	83.7	84.0	84.1	84.3	84.6	84.8
38	85.0	85.2	85.5	85.7	85.9	86.1	86.3	86.6	86.8	87.0
39	87.2	87.5	87.7	87.9	88.1	88.4	88.6	88.8	89.0	89.3
40	89.5	89.7	89.9	90.2	90.4	90.6	90.8	91.0	91.3	91.5
41	91.7	91.9	92.2	92.4	92.6	92.8	93.1	93.3	93.5	93.7
42	94.0	94.2	94.4	94.6	94.8	95.1	95.3	95.5	95.7	96.0
43	96.2	96.4	96.6	96.9	97.1	97.3	97.5	97.8	98.0	98.2
44	98.4	98.7	98.9	99.1	99.3	99.5	99.8	100.0	100.2	100.4

METERS PER SECOND INTO MILES PER HOUR.

Meters per second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	Miles per hr.	Miles per hr.	Miles per hr.	Miles per nr.	Miles per hr.					
45	100.7	100.9	101.1	101.3	101.6	101.8	102.0	102.2	102.5	102.7
46	102.9	103.Í	103.3	103.6	103.8	104.0	104.2	104.5	104.7	104.9
47	105.1	105.4	105.6	105.8	106.0	106.3	106.5	106.7	106.9	107.2
48	107.4	107.6	107.8	108.0	108.3	108.5	108.7	108.9	109.2	109.4
49	109.6	109.8	110.1	110.3	110.5	110.7	111.0	111.2	111.4	11Í.6
50	111.8	112.1	112.3	112.5	112.7	113.0	113.2	113.4	113.6	113.9
51	114.1	114.3	114.5	114.8	115.0	115.2	115.4	115.7	115.9	116.1
52	116.3	116.6	116.8	117.0	117.2	117.4	117.7	117.9	118.1	118.3
53	118.6	118.8	119.0	119.2	119.5	119.7	119.9	120.1	120.4	120.6
54	120.8	121.0	121.3	121.5	121.7	121.9	122.1	122.4	122.6	122.8
55	123.0	123.3	123.5	123.7	123.9	124.2	124.4	124.6	124.8	125.1
56	125.3	125.5	125.7	126.0	126.2	126.4	126.6	126.8	127.1	127.3
57	127.5	127.8	128.0	128.2	128.4	128.6	128.9	129.1	129.3	129.5
57 58	129.7	130.0	130.2	130.4	130.7	130.9	131.1	131.3	131.6	131.8
59	132.0	132.2	132.5	132.7	132.9	133.1	133.3	133.6	133.8	134.0

TABLE 36.

MILES PER HOUR INTO METERS PER SECOND.

I mile per hour = 0.4470409 meters per second.

Miles per hour.	0	1	2	3	4	5	6	7	8	9
	meters per sec.									
0	0.00	0.45	0.89	1.34	1.79	2.24	2.68	3.13	3.58	4.02
IO	4.47	4.92	5.36	5.81	6.26	6.71	7.15	7.60	8.05	8.49
20	8.94	9.39	9.83	10.28	10.73	11.18	11.62	12.07	12.52	12.96
30	13.41	13.86	14.31	14.75	15.20	15.65	16.09	16.54	16.99	17.43
40	17.88	18.33	18.78	19.22	19.67	20.12	20.56	21.01	21.46	21.90
50 60	22.35 26.82	22.80	23.25	23.69 28.16	24.14 28.61	24.59	25.03	25.48	25.93	26.37
70	31.29	27.27 31.74	27.72 32.19	32.63	33.08	29.06	29.50 33.98	29.95	30.40	30.85
80	35.76	36.21	36.66	37.10	37.55	33.53 38.00	38.44	34.42 38.89	34.87	35.32
90	40.23	40.68	41.13	41.57	42.02	42.47	42.92	43.36	39·34 43.81	39·79 44.26
100	44.70	45.15	45.60	46.04	46.49	46.94	47-39	47.83	48.28	48.73
110	49.17	49.62	50.07	50.51	50.96	51.41	51.86	52.30	52.75	53.20
120	53.64	54.09	54.54	54.98	55.43	55.88	56.33	56.77	57.22	57.67
130	58.12	58.56	59.01	59.46	59.90	60.35	60.80	6r.24 .	61.69	62.14
140	62.59	63.03	63.48	63.93	64.37	64.82	65.27	65.72	66.16	66.61

SMITHSONIAN TABLES.

METERS PER SECOND INTO KILOMETERS PER HOUR.

I meter per second = 3.6 kilometers per hour.

Meters per second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	km.									
	per hr.									
0	0.0	0.4	0.7	1.1	1.4	1.8	2.2	2.5	2.9	3.2
1	3.6	4.0	4.3	4.7	5.0	5.4	5.8	6.1	6.5	6.8
2	7.2	7.6	7.9	8.3	8.6	9.0	9.4	9.7	10.1	10.4
3	10.8	11.2	11.5	11.9	12.2	12.6	13.0	13.3	13.7	14.0
4	14.4	14.8	15.1	15.5	15.8	16.2	16.6	16.9	17.3	17.6
5	18.0	18.4	18.7	19.1	19.4	19.8	20.2	20.5	20.9	21.2
6	21.6	22.0	22.3	22.7	23.0	23.4	23.8	24.1	24.5	24.8
7	25.2	25.6	25.9	26.3	26.6	27.0	27.4	27.7	28.1	28.4
8	28.8	29.2	29.5	29.9	30.2	30.6	31.0	31.3	31.7	32.0
9	32.4	32.8	33.1	33.5	33.8	34.2	34.6	34.9	35.3	35.6
10	36.0	36.4	36.7	37.1	37.4	37.8	38.2	38.5	38.9	39.2
11	39.6	40.0	40.3	40.7	41.0	41.4	41.8	42.1	42.5	42.8
12	43.2	43.6	43.9	44.3	44.6	45.0	45.4	45.7	46.1	46.4
13	46.8	47.2	47.5	47.9	48.2	48.6	49.0	49.3	49.7	50.0
14	50.4	50.8	51.1	51.5	51.8	52.2	52.6	52.9	53.3	53.6
15	54.0	54.4	54.7	55.1	55.4	55.8	56.2	56.5	56.9	57.2
16	57.6	58.0	58.3	58.7	59.0	59.4	59.8	60.1	60.5	60.8
17	61.2	61.6	61.9	62.3	62.6	63.0	63.4	63.7	64.1	64.4
18	64.8	65.2	65.5	65.9	66.2	66.6	67.0	67.3	67.7	68.0
19	68.4	68.8	69.1	69.5	69.8	70.2	70.6	70.9	71.3	71.6
20	72.0	72.4	72.7	73.1	73.4	73.8	74.2	74.5	74.9	75.2
21	75.6	76.0	76.3	76.7	77.0	77.4	77.8	78.1	78.5	78.8
22	79.2	79.6	79.9	80.3	80.6	81.0	81.4	81.7	82.1	82.4
23	82.8	83.2	83.5	83.9	84.2	84.6	85.0	85.3	85.7	86.0
24	86.4	86.8	87.1	87.5	87.8	88.2	88.6	88.9	89.3	89.6
25	90.0	90.4	90.7	91.1	91.4	91.8	92.2	92.5	92.9	93.2
26	93.6	94.0	94.3	94.7	95.0	95.4	95.8	96.1	96.5	96.8
27	97.2	97.6	97.9	98.3	98.6	99.0	99.4	99.7	100.1	100.4
28	100.8	101.2	101.5	101.9	102.2	102.6	103.0	103.3	103.7	104.0
29	104.4	104.8	105.1	105.5	105.8	106.2	106.6	106.9	107.3	107.6
30	108.0	108.4	108.7	109.1	109.4	109.8	110.2	110.5	110.9	111.2
31	111.6	112.0	112.3	112.7	113.0	113.4	113.8	114.1	114.5	114.8
32	115.2	115.6	115.9	116.3	116.6	117.0	117.4	117.7	118.1	118.4
33	118.8	119.2	119.5	119.9	120.2	120.6	121.0	121.3	.121.7	122.0
34	122.4	122.8	123.1	123.5	123.8	124.2	124.6	124.9	125.3	125.6
35	126.0	126.4	126.7	127.1	127.1	127.8	128.2	128.5	128.9	129.2
36	129.6	130.0	130.3	130.7	131.0	131.4	131.8	132.1	132.5	132.8
37	133.2	133.6	133.9	134.3	134.6	135.0	135.4	135.7	136.1	136.4
38	136.8	137.2	137.5	137.9	138.2	138.6	139.0	139.3	139.7	140.0
39	140.4	140.8	141.1	141.5	141.8	142.2	142.6	142.9	143.3	143.6
40	144.0	144.4	144.7	145.1	145.4	145.8	146.2	146.5	146.9	147.2
41	147.6	148.0	148.3	148.7	149.0	149.4	149.8	150.1	150.5	150.8
42	151.2	151.6	151.9	152.3	152.6	153.0	153.4	153.7	154.1	154.4
43	154.8	155.2	155.5	155.9	156.2	156.6	157.0	157.3	157.7	158.0
44	158.4	158.8	159.1	159.5	159.8	160.2	160.6	160.9	161.3	161.6

METERS PER SECOND INTO KILOMETERS PER HOUR.

Meters per second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	km. per hr.	km. per hr.	km. per hr.	km.	km. per hr.	km, per hr.	km. per hr.	km. per hr.	km.	km. per hr.
45	162.0	162.4	162.7	163.1	163.4	163.8	164.2	164.5	164.9	165.2
46	165.6	166.0	166.3	166.7	167.0	167.4	167.8	168.1	168.5	168.8
47	169.2	169.6	169.9	170.3	170.6	171.0	171.4	171.7	172.1	172.4
48	172.8	173.2	173.5	173.9	174.2	174.6	175.0	175.3	175.7	176.0
49	176.4	176.8	177.1	177.5	177.8	178.2	178.6	178.9	179.3	179.6
50	180.0	180.4	180.7	181.1	181.4	181.8	182.2	182.5	182.9	183.2
51	183.6	184.0	184.3	184.7	185.0	185.4	185.8	186.1	186.5	186.8
52	187.2	187.6	187.9	188.3	188.6	189.0	189.4	189.7	190.1	190.4
53	190.8	191.2	191.5	191.9	192.2	192.6	193.0	193.3	193.7	194.0
54	194.4	194.8	195.1	195.5	195.8	196.2	196.6	196.9	197.3	197.6
55	198.0	198.4	198.7	199.1	199.4	199.8	200.2	200.5	200,9	201.2
56	201.6	202.0	202.3	202.7	203.0	203.4	203.8	·204.I	204.5	204.8
57	205.2	205.6	205.9	206.3	206.6	207.0	207.4	207.7	208.1	208.4
58	208.8	209.2	209.5	209.9	210,2	210,6	211.0	211.3	211.7	212.0
59	212.4	212.8	213.1	213.5	213.8	214.2	214.6	214.9	215.3	215.6
l										

TABLE 38.

KILOMETERS PER HOUR INTO METERS PER SECOND.

1 kilometer per hour $=\frac{10}{36}$ meters per second.

Kilometers per hour.	0	1	2	3	4	5	6	7	8	9
	meters per sec.	meters	meters per sec.							
0	0,00	0.28	0.56	0.83	1.11	1.39	1.67	1.94	2.22	2.50
10	2.78	3.06	3.33	3.61	3.89	4.17	4.44	4.72	5.00	5.28
20	5.56	5.83	6.11	6.39	6.67	6.94	7.22	7.50	7.78	8.06
30	8.33	8.61	8.89	9.17	9.44	9.72	10.00	10.28	10.56	10.83
40	11.11	11.39	11.67	11.94	12.22	12.50	12.78	13.06	13.33	13.61
50	13.89	14.17	14.44	14.72	15.00	15.28	15.56	15.83	16.11	16.39
60	16.67	16.94	17.22	17.50	17.78	18.06	18.33	18.61	18.89	19.17
70	19.44	19.72	20.00	20.28	20.56	20.83	21.11	21.39	21.67	21.94
80	22.22	22.50	22.78	23.06	23.33 26.11	23.61 26.39	23.89 26.67	24.17 26.94	24.44	24.72 27.50
90	25.00	25.28	25.56	25.83	20.11	20.39	20.07	20.94	2/.22	27.50
100	27.78	28.06	28.33	28.61	28.89	29.17	29.44	29.72	30.00	30.28
110	30.56	30.83	31.11	31.39	31.67	31.94	32.22	32.50	32.78	33.06
120	33.33	33.61	33.89	34.17	34.44	34.72	35.00	35.28	35.56	35.83
130	36.11	36.39	36.67	36.94	37.22	37.50	37.78	38.06	38.33	38.61
140	38.89	39.17	39.44	39.72	40.00	40.28	40.56	40.83	41.11	41.39
150	41.67	41.94	42.22	42.50	42.78	43.06	43.33	43.61	43.89	44.17
160	44.44	44.72	45.00	45.28	45.56	45.83	46.11	46.39	46.67	46.94
170	47.22	47.50	47.78	48.06	48.33	48.61	48.89	49.17	49-44	49.72
180	50.00	50.28	50.56	50.83	51.11	51.39	51.67	51.94	52.22	52.50
190	.52.78	53.06	53.33	53.61	53.89	54.17	54-44	54.72	55.00	55.28

TABLE 39.

SCALE OF VELOCITY EQUIVALENTS OF THE SO-CALLED BEAUFORT SCALE OF WIND.

			F WIND.	1	
Beaufort Number.	Explanatory titles.	Mode of estimating aboard salling vessels.	Specification for use on land.	Meters per second	Miles per hour.
٥	Calm		Calm, smoke	Less than 0.3	Less than 1
1	Light air		rises vertically. Direction of wind shown by smoke drift,	0.3-1.5	1-3
2	Slight breeze	Sufficient wind for working ship	but not by wind vanes. Wind felt on face; leaves rustle; ordi- nary vane	1.6-3.3	4-7
3	Gentle breeze		moved by wind. Leaves and small twigs in constant mo- tion; wind ex-	3.4-5.4	8–12
4	Moderate breeze	Forces most advantageous for sailing with lead-	tends light flag. Raises dust and loose paper; small branches are	5.5-7.9	13-18
5	Fresh breeze	ing wind and all sail drawing	moved. Small trees in leaf begin to sway; crested wavelets form	8.0-10.7	19-24
6	Strong breeze	Reduction of sail necessary with leading wind	waters form on inland waters. Large branches in motion; whistling heard in telegraph wires; umbrel- las used with	10.8–13.8	25-31
7	High wind		difficulty. Whole trees in motion; inconvenience felt when walking	r3.9–17.1	32–38
8	Gale }	Considerable re- duction of sail necessary even with wind	against wind. Breaks twigs off trees; gener- ally impedes progress.	17.2–20.7	39-46
9	Strong gale	quartering	Slight structural damage occurs (chimney pots and slate renoved).	20.8–24.4	47-54
10	Whole gale	Close reefed sail running, or hove to under storm	Seldom experi- enced inland; trees uprooted; considerable structural	24.5–28.4	55-63
11	Storm	sail	damage occurs. Very rarely experienced, accompanied by widespread damage.	28.5-33.5	64-75
12	Hurricane	No sail can stand even when running	J	33.6 or above	Above 75

$$\tan \alpha = \frac{E - W + (NE + SE - NW - SW)\cos 45^{\circ}}{N - S + (NE + NW - SE - SW)\cos 45^{\circ}}$$

Multiples of cos 45°.

Number.	0	ı	2	3	4	5	6	7	8	9
0 10 20 30 40	0.0 7.1 14.1 21.2 28.3	0.7 7.8 14.8 21.9 29.0	1.4 8.5 15.6 22.6 29.7	2.I 9.2 16.3 23.3	2.8 9.9 17.0 24.0 31.1	3.5 10.6 17.7 24.7 31.8	4.2 11.3 18.4 25.5	4.9 12.0 19.1 26.2	5.7 12.7 19.8 26.9	6.4 13.4 20.5 27.6
50 60 70 80 90	35·4 42·4 49·5 56.6 63.6	36.1 43.1 50.2 57.3 64.3	36.8 43.8 50.9 58.0 65.1	30.4 37.5 44.5 51.6 58.7 65.8	38.2 45.3 52.3 59.4 66.5	38.9 46.6 53.0 60.1 67.2	32.5 39.6 46.7 53.7 60.8 67.9	33.2 40.3 47.4 54.4 61.5 68.6	33.9 41.0 48.1 55.2 62.2 69.3	34.6 41.7 48.8 55.9 62.9 70.0
100 110 120 130 140	70.7 77.8 84.9 91.9	71.4 78.5 85.6 92.6 99.7	72.1 79.2 86.3 93.3 100.4	72.8 79.9 87.0 94.0	73.5 80.6 87.7 94.8	74.2 81.3 88.4 95.5 102.5	75.0 82.0 89.1 96.2 103.2	75.7 82.7 89.8 96.9	76.4 83.4 90.5 97.6	77.1 84.1 91.2 98.3 105.4
150 160 170 180 190	106.1 113.1 120.2 127.3 134.4	106.8 113.8 120.9 128.0 135.1	107.5 114.6 121.6 128.7 135.8	108.2 115.3 122.3 129.4 136.5	108.9 116.0 123.0 130.1 137.2	109.6 116.7 123.7 130.8 137.9	110.3 117.4 124.5 131.5 138.6	111.0 118.1 125.2 132.2 139.3	111.7 115.8 125.9 132.9 140.0	112.4 119.5 126.6 133.6 140.7
200	141.4	142.1	142.8	143.5	144.2	145.0	145.7	146.4	147.1	147.8

Form for Computing the Numerator and Denominator.

Directions.	E	W	N	S	NE	SW	SE	NW		
Observed values.	7	12	6	26	13	45	2	24		
	E -	·W	N-	- S	NE -	-SW	SE -			
	[-	5]	[-	< <i>cos</i> 45°						
Numerator(n).	[-	5]	+ $\begin{bmatrix} -22.6 \end{bmatrix} + \begin{bmatrix} -15.6 \end{bmatrix} = \begin{bmatrix} -43.2 \end{bmatrix}$							
Denominator (d) .			$\begin{bmatrix} -20 \end{bmatrix} + \begin{bmatrix} -22.6 \end{bmatrix} - \begin{bmatrix} -15.6 \end{bmatrix} = \begin{bmatrix} -29.6 \end{bmatrix}$							

a is the angle between the mean wind direction and the meridian.

The signs of the numerator (n) and denominator (d) determine the quadrant in which a lies.

When n and d are positive, u lies between N and E: $\frac{+}{+} = NE$

When n is positive and d negative, a lies between S and E: $\frac{+}{-} = SE$.

When n and d are negative, a lies between S and W: $\frac{-}{-} = SW$.

When n is negative and d positive, a lies between N and W: $\frac{-}{+} = NW$.

Values of the mean direction (a) or its complement $(90^{\circ}-a)$.

 $\alpha = tan^{-1} n/d$

n			-	·		DEN	омі	NAT	OR C	R N	JMEI	RATO	R (d	OR	n).				-
d.	10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	90	95	100
1 2 3 4	6° 11 17 22	4° 8 11	3° 6 9	2° 5 7 9	2° 4 6 8	2°, 3 5	1° 3 4 6	1° 3 4 5	1° 2 3 5	1° 2 3 4	1° 2 3 4	1° 2 3 4	1° 2 2 3	I 3 2 2 3	I° 1 2 3	I ° 1 2 3	1° 1 2 3	I° 1 2 2	I° I 2 2
5 6 .7 8 9	27 31 35 39 42	18 22 25 28 31	14 17 19 22 24	11 13 16 18 20	9 11 13 15	8 10 11 13 14	7 9 10 11	6 8 9 10	6 7 8 9	56 78 9	5 6 7 8 9	4 5 6 7 8	4 5 6 7 7	4 5 5 7	4 4 5 6 6	3 4 5 5 6	3 4 4 5 6	3 4 4 5 5	3 4 5 5
10 11 12 13 14	45	34 36 39 41 43	27 29 31 33 35	22 24 26 27 29	18 20 22 23 25	16 17 19 20 22	14 15 17 18 19	13 14 15 16 17	11 12 13 15 16	10 11 12 13 14	9 10 11 12 13	9 10 10 11 12	9 10 11	8 9 10 11	7 8 9 9	7 7 8 9	6 7 8 8 9	6 7 7 8 8	6 6 7 7 8
15 16 17 18 19		45	37 39 40 42 44	31 33 34 36 37	27 28 30 31 32	23 25 26 27 28	21 22 23 24 25	18 20 21 22 23	17 18 19 20 21	15 16 17 18	14 15 16 17 18	13 14 15 15	12 13 14 14 15	11 12 13 13 14	11 12 13 13	10 11 11 12 13	9 10 11 11	9 10 11	9 10 10
20 21 22 23 24			45	39 40 41 43 44	34 35 36 37 39	30 31 32 33 34	27 28 29 30 31	24 25 26 27 28	22 23 24 25 26	20 21 22 23 24	18 19 20 21 22	17 18 19 19	16 17 17 18	15 16 16 17 18	14 15 15 16	13 14 15 15	13 13 14 14 15	12 12 13 14 14	11 12 12 13 13
25 26 27 28 29				45	40 41 42 43 44	36 37 38 39 40	32 33 34 35 36	29 30 31 32 33	27 27 28 29 30	24 25 26 27 28	23 23 24 25 26	2I 22 22 23 24	20 20 21 22 23	18 19 20 20 21	17 18 19 19	16 17 18 18	16 16 17 17 18	15 15 16 16	14 15 15 16 16
30 31 32 33 34					45	41 42 42 43 44	37 38 39 40 40	34 35 35 36 37	31 32 33 33 34	29 29 30 31 .32	27 27 28 29 30	25 25 26 27 28	23 24 25 25 26	22 22 23 24 24	2I 2I 22 22 23	19 20 21 21 22	18 19 20 20 21	18 18 19 19	17 17 18 18 18
35 36 37 38 39						45	41 42 43 44 44	38 39 39 40 41	35 36 37 37 38	32 33 34 35 35	30 31 32 32 33	28 29 30 30 31	27 27 28 28 29	25 26 26 27 27	24 24 25 25 26	22 23 24 24 25	21 22 22 23 23	20 21 21 22 22	19 20 20 21 21
40 41 42 43 44							45	42 42 43 44 44	39 39 40 41 41	36 37 37 38 39	34 34 35 36 36	32 32 33 33 34	30 30 31 32 32	28 29 29 30 30	27 27 28 28 28	25 26 26 27 27	24 24 25 26 26	23 23 24 24 25	22 22 23 23 24
45 46 47 48 49								45	42 43 43 44 44	39 40 41 41 42	37 37 38 39 39	35 35 36 36 37	33 33 34 34 35	31 32 32 33 33	29 30 30 31 31	28 28 29 29 30	27 27 28 28 29	25 26 26 27 27	24 25 25 26 26
50									45	42	40	38	36	34	32	30	29	28	27

n or d.			DEN	MINATO	OR OR 1	NUMERA	TOR (d	or n).		
	105	110	115	120	125	130	135	140	145	150
1 2 3 4	1 ^o I 2 2	1° I 2 2	0° I I 2	0° I I 2	0° I I 2	0° I I 2	0° I I 2	0° I I 2	0° I I 2	0° I I 2
5 6 7 8 9	3 3 4 4 4	3 3 4 4 4	3 3 4 4	3 3 4 4	2 3 3 4 4	3 3 4 4	2 3 3 3 4	2 2 3 3 4	2 2 3 3 4	2 2 3 3 3
10 11 12 13 14	5 6 7 7 8	5 6 6 7 7	5 5 6 6 7	5 5 6 6 7	5 5 5 6 6	4 5 5 6 6	4 5 5 6 6	4 4 5 5 6	4 4 5 5 6	4 4 5 5 5
15 16 17 18 19	8 9 10 10	8 8 9 9	7 8 8 9 9	7 8 8 9 9	7 7 8 8 9	7 7 7 8 8	6 7 7 8 8	6 7 7 7 8	6 6 7 7 7	6 6 6 7 7
20 21 22 23 24	11 11 12 12 13	10 11 11 12 12	10 10 11 11 12	9 10 10 11	9 10 10 11	9 9 10 10	8 9 9 10	8 9 9 9	8 8 9 9	8 8 8 9
25 26 27 28 29	13 14 14 15 15	13 13 14 14 15	12 13 . 13 14 14	12 12 13 13	11 12 12 13 13	11 11 12 12 13	10 11 11 12 12	10 11 11 11 12	II II IO IO	9 10 11 11
30 31 32 33 34	16 16 17 17 18	15 16 16 17 17	15 15 16 16 16	14 14 15 15 16	13 14 14 15 15	13 13 14 14 15	13 13 14 14	12 12 13 13	12 12 12 13	11 12 12 12 13
35 36 37 38 39	18 19 19 20 20	18 18 19 19	17 17 18 18 19	16 17 17 18 18	16 16 16 17 17	15 15 16 16 17	15 15 15 16 16	14 14 15 15	14 14 14 15	13 13 14 14
40 41 42 43 44	2I 2I 22 22 23	20 20 21 21 22	19 20 20 21 21	18 19 19 20 20	18 19 19	17 18 18 18	17 17 17 18 18	16 16 17 17 17	15 16 16 17 17	15 16 16 16
45 46 47 48 49	23 24 24 25 25	22 23 23 24 24	21 22 22 23 23	2I 2I 2I 22 22	20 20 21 21 21	19 19 20 20 21	18 19 19 20 20	18 18 19 19	17 18 18 18	17 17 17 18 18
50	25	24	• 23	23	22	21	20	20	19	18

TABLE 41.

			DENO:	MINATO	R OR N	UMERAI	ror (d	OR n).		
n or d.	155	160	165	170	175	180	185	190	195	200
1 2 3 4	0°	0°	I I O°	0°	0°	0°	o° I	r r o°	0° : 1 1 1	I I I
5 6 78 9	2 2 3 3 3	2 2 3 3	2 2 2 3 3	2 2 2 3 3	2 2 2 3 3	2 2 2 3 3	2 2 2 2 3	2 2 2 3	1 2 2 2 3	1 2 2 2 3
10 11 12 13 14	4 4 4 5	4 4 5 5	3 4 4 5 5	3 4 4 4 5	3 4 4 4 5	3 3 4 4 4	3 3 4 4 4	3 3 4 4 4	3 3 4 4 4	3 3 4 4
15 16 17 18 19	6 6 7 7	5 6 6 7 7	5 6 6 7	5 5 6 6	5 5 6 6	5 5 6 6	5 5 6 6	5 5 5 6 6	4 5 5 5 6	4 5 5 5
20 21 22 23 24	7 8 8 8	7 7 8 8 9	7 7 8 8 8	7 7 7 8 8	7 7 7 7 8	6 7 7 7 8	6 7 7 7	6 6 7 7 7	6 6 7 7	6 6 7 7
25 26 27 28 29	10 10 10 10	9 9 10 10	9 9 10 10	8 9 9 9	8 9 9	8 9 9	8 8 9 9	7 8 8 8	7 8 8 8	7 7 8 8 8
30 31 32 33 34	11 11 12 12 12	11 11 11 12 12	10 11 11 11 12	11 11 10 10	11 10 10 10	9 10 10 11	9 10 10 10	9 10 10	9 9 9 10 10	9 9 9 9
35 36 37 38 39	13 13 13 14 14	12 13 13 13	12 12 13 13	12 12 12 13 13	11 12 12 12 13	11 11 12 12 12	11 11 11 12 12	10 11 11 11	11 11 10	10 10 11 11
40 41 42 43 44	14 15 15 16 16	14 14 15 15	14 14 14 15 15	13 14 14 14 15	13 13 14 14	13 13 13 13	12 12 13 13	12 12 12 13	12 12 12 12 13	11 12 12 12 12
45 46 47 48 49	16 17 17 17 18	16 16 16 17 17	15 16 16 16 17	15 15 15 16 16	14 15 15 15 16	14 14 15 15	14 14 14 15	13 14 14 14 14	13 13 14 14 14	13 13 13 13 14
50	18	17	17	16	16	16	15	15	14	14

$$a = tan - i \frac{n}{d}$$
.

n				DEN	OMIN	ATOR	OR I	NUMI	ERAT	or (d or	e n).				
or d.	55	60	65	70	75	80	85	90	95	100	105	110	115	120	125	130
50 52 54 56 58	42° 43 44	40° 41 42 43 44	38° 39 40 41 42	36° 37 38 39 40	34° 35 36 37 38	32° 33 34 35 36	30° 31 32 33 34	29° 30 31 32 33	28° 29 30 31 31	27° 27 28 29 30	25° 26 27 28 29	24° 25 26 27 28	23° 24 25 26 27	23° 23° 24 25° 26	22° 23 23 24 25	21° 22 22 23 24
60 62 64 66 68		45	43 44 45	41 42 42 43 44	39 40 40 41 42	37 38 39 40 40	35 36 37 38 39	34 35 35 36 37	32 33 34 35 36	31 32 33 33 34	30 31 31 32 33	29 29 30 31 32	28 28 29 30 31	27 27 28 29 30	26 26 27 28 29	25 25 26 27 28
70 72 74 76 78				45	43 44 45	41 42 43 44 44	39 40 41 42 43	38 39 39 40 41	36 37 38 39 39	35 36 37 37 38	34 34 35 36 37	32 33 34 35 35	31 32 33 33 34	30 31 32 32 33	29 30 31 31 32	28 29 30 30 31
80 82 84 86 88						45	43 44 45	42 42 43 44 44	40 41 41 42 43	39 39 40 41 41	37 38 39 39 40	36 37 37 38 39	35 35 36 37 37	34 34 35 36 36	33 33 34 35 35	32 32 33 33 34
90 92 94 96 98								45	43 44 45	42 43 43 44 44	41 41 42 42 43	39 40 41 41 42	38 39 39 40 40	37 37 38 39 39	36 36 37 38 38	35 35 36 36 37
100 102 104 106 108										45	44 44 45	42 43 43 44 44	41 42 42 43 43	40 40 41 41 42	39 39 40 40 41	38 38 39 39 40
110 112 114 116 118												45	44 44 45	43 43 44 44 45	41 42 42 43 43	40 41 41 42 42
120 122 124 126 128														45	44 44 45	43 43 44 44 45
130			1										ļ			45

TABLE 41.

<i>n</i>				DE	NOMIN	ATOR	OR	NUME	RATO	or (d	OR #	ı).			
d.	130	135	140	145	150	155	160	165	170	175	180	185	190	1 9 5	200
50 52 54 56	21° 22 22 23	20° 21 22 23	20° 20 21 22	19° 20 20 21	18° 19 20 20	18° 19 19	17° 18 19	17° 17 18	16° 17 18 18	16° 17 17 18	16° 16 17 17	15° 16 16 17	15° 15 16 16	14° 15 15	14° 15 15 16
58 60 62 64 66 68	24 25 25 26 27 28	23 24 25 25 26 27	23 24 25 25 26	22 23 24 24 25	22 22 23 24 24	21 21 22 22 23 24	20 21 21 22 22	19 20 21 21 22 22	19 20 21 21 21	19 20 20 21 21	18 19 20 20	17 18 19 19 20 20	17 18 18 19 19	17 18 18 19	17 17 18 18
70 72 74 76 78	28 29 30 30 31	27 28 29 29	27 27 28 28 28	26 26 27 28 28	25 26 26 27 27	24 25 26 26 27	23 24 24 25 25 26	23 24 24 25 25	22 23 24 24 24 25	22 22 23 23 24	21 22 22 22 23 23	21 21 22 22 22 23	20 21 21 22 22	20 20 21 21 21	19 20 20 21 21
80 82 84 86 88	32 32 33 33 34	31 31 32 32 33	30 30 31 32 32	29 29 30 31 31	28 29 29 30 30	27 28 28 29 30	27 27 28 28 29	26 26 27 28 28	25 26 26 27 27	25 25 26 26 26	24 24 25 26 26	23 24 24 25 25	23 23 24 24 25	22 23 23 24 24	22 22 23 23 24
90 92 94 96 98	35 35 36 36 37	34 34 35 35 36	33 33 34 34 35	32 32 33 34 34	31 32 32 33 33	30 31 31 32 32	29 30 30 31 31	29 29 30 30 31	28 28 29 29 30	27 28 28 29 29	27 27 28 28 29	26 26 27 27 28	25 26 26 27 27	25 25 26 26 27	24 25 25 26 26
100 102 104 106 108	38 38 39 39 40	37 37 38 38 39	36 36 37 37 38	35 35 36 36 37	34 34 35 35 36	33 33 34 34 35	32 33 33 34 34	31 32 32 33 33	30 31 31 32 32	30 30 31 31 32	29 30 30 30 31	28 29 29 30 30	28 28 29 29 30	27 28 28 29 29	27 27 27 28 28
110 112 114 116 118	40 41 41 42 42	39 40 40 41 41	38 39 39 40 40	37 38 38 39 39	36 37 37 38 38	35 36 36 37 37	35 35 35 36 36	34 34 35 35 36	33 33 34 34 35	32 33 33 34 34	31 32 32 33 33	31 32 32 33	30 31 31 31 32	29 30 30 31 31	29 29 30 30 31
120 122 124 126 128	43 43 44 44 45	42 42 43 43 43	41 41 42 42 42	40 40 41 41 41	39 39 40 40 40	38 38 39 39 40	37 37 38 38 39	36 36 37 37 38	35 36 36 37 37	34 35 35 36 36	34 34 35 35 35	33 33 34 34 35	32 33 33 34 34	32 32 32 33 33	31 32 32 33
130 132 134 136 138	45	44 44 45	43 43 44 44 45	42 42 43 43 44	41 41 42 42 43	40 40 41 41 42	39 40 40 40 41	38 39 39 39 40	37 38 38 39 39	37 37 37 38 38	36 36 37 37 37	35 35 36 36 37	34 35 35 36 36	34 34 34 35 35	33 33 34 34 35
140 142 144 146 148			45	44 44 45	43 43 44 44 45	42 42 43 43 44	41 42 42 42 43	40 41 41 42 42	39 40 40 41 41	39 39 39 40 40	38 38 39 39 39	37 38 38 38 39	36 37 37 38 38	36 36 36 37 37	35 35 36 36 37
150					45	44	43	42	41	41	40	39	38	38	37

RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

ENGLISH MEASURES.

 R_c = radius of critical curvature in miles. V_c High = maximum speed in miles per hour on isohar of critical curvature. V_s = speed along straight line isohars = 0.5 V_c . V Low = speed in Low along isohar of curvature R_c . V Low = 0.4142 V_c .

The table is computed for a density of the air, ρ = .0010, which represents the conditions in the free air at an elevation of, roughly, one mile. Values for any other density can be readily found by dividing each or any of the tabulated values by the ratio of the densities, as, for ex-

ample, for surface conditions divide by $1.2 = \frac{.0010}{.0012}$ and so on.

Lati-						d (m	iles)					
tude:		100	125	150	175	200	250	300	400	500	600	800
10°	R_c V_c High V_s V Low	8160 372 186 154	6530 298 149 123	5440 248 124 103	4660 212 106 88.0	4080 186 93.0 77.0	3260 149 74·4 61.6	2720 124 62.0 51.3	2040 93.0 46.5 38.5	1630 74 · 4 37 · 2 30 · 8	1360 62.0 31.0 25.7	1020 46.5 23.2 19.2
20	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{V Low} \end{array}$	2100 189 94.4 78.2	1680 151 75.5 62.5	1400 126 62.9 52.1	1200 108 54.0 44.7	1050 94 · 4 47 · 2 39 · 1	841 75·5 37·8 31·3	701 62.9 31.4 26.1	526 47.2 23.6 19.6	420 37.8 18.9 15.7	350 31.5 15.8 13.0	263 23.6 11.8 9.8
25	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	1380 153 76.4 63.3	1100 122 61.1 50.6	918 102 50.9 42.2	787 87.3 43.6 36.2	688 76.4 38.2 31.6	551 61.1 30.6 25.3	459 50.9 25.4 21.1	344 38.2 19.1 15.8	275 30.6 15.3 12.7	230 25.5 12.8 10.6	172 19. 1 9. 5 7. 9
30	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{V} \ ext{Low} \end{array}$	984 129 64.5 53.5	787 103 51.6 42.8	656 86. I 43. 0 35. 7	562 73.8 36.9 30.6	492 64.5 32.2 26.7	393 51.6 25.8 21.4	328 43.0 21.5 17.8	246 32.3 16.2 13.4	197 25.8 12.9 10.7	164 21.5 10.8 8.9	123 16. 1 8. 1 6. 7
35	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{V} \ ext{Low} \end{array}$	747 112 56.3 46.6	598 90.0 45.0 37.3	498 75.0 37.5 31.1	427 64.3 32.2 26.6	374 56.3 28.2 23.3	299 45.0 22.5 18.6	249 37·5 18.8 15.5	187 28. I 14. O 11. 6	150 22.5 11.2 9.3	125 18.8 9.4 7.8	93·4 14·1 7·0 5·8
40	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	595 100 50, 2 41.6	476 80.3 40.2 33.3	397 66.9 33.4 27.7	340 57·4 28.7 23.8	298 50. 2 25. I 20. 8	238 40. 2 20. 1 16. 7	198 33.5 16.8 13.9	149 25. I 12. 6 10. 4	119 20.1 10.0 8.3	99.2 16.7 8.4 6.9	74.4 12.6 6.3 5.2
45	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{V} \ ext{Low} \end{array}$	492 91.3 45.6 37.8	393 73.0 36.5 30.2	328 60.9 30.4 25.2	281 52.2 26.1 21.6	246 45.6 22.8 18.9	197 36.5 18.2 15.1	164 30.4 15.2 12.6	123 22.8 11.4 9.4	98.4 18.3 9.2 7.6	82.0 15.2 7.6 6.3	61.5 11.4 5.7 4.7
50	R _c V _c High V _s V Low	419 84.3 42.1 34.9	335 67.4 33.7 27.9	279 56. 2 28. 1 23. 3	240 48.2 24.1 20.0	210 42.1 21.0 17.4	168 33·7 16.8 14.0	140 28.1 14.0 11.6	105 21.1 10.6 8.7	83.8 16.9 8.4 7.0	69.9 14.0 7.0 5.8	52.4 10.5 5.3 4.4
55	R _c V _c High V _s V Low	366 78.8 39.4 32.6	293 63.0 31.5 26.1	244 52.5 26.2 21.7	209 45.0 22.5 18.6	183 39·4 19.7 16.3	147 31.5 15.8 13.0	122 26.3 13.2 10.9	91.6 19.7 9.8 8.2	73·3 15.8 7·9 6.5	61.1 13.1 6.6 5.4	45.8 9.8 4.9 4.1
60	R _c V _c High V _s V Low	328 74·5 37·3 30·9	262 59.6 29.8 24.7	219 49.7 24.8 20.6	187 42.6 21.3 17.6	164 37·3 18.6 15.5	131 29.8 14.9 12.3	109 24.8 12.4 10.3	82.0 18.6 9.3 7.7	65.6 14.9 7.4 6.2	54·7 12.4 6.2 5.1	41.0 9.3 4.7 3.9
65	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	299 71.2 35.6 29.5	240 57.0 28.5 23.6	200 47·5 23.8 19.7	171 40.7 20.4 16.9	150 35.6 17.8 14.7	120 28.5 14.2 11.8	99.8 23.7 11.8 9.8	74.8 17.8 8.9 7.4	59.9 14.2 7.1 5.9	49.9 11.9 6.0 4.9	37·4 8.9 4·4 3·7

TABLE 42. RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

ENGLISH MEASURES.

Lati-						d (mile	s)					
tude:		100	125	150	175	200	250	300	400	500	600	800
70°	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{V Low} \end{array}$	278 68.7 34.3 28.5	223 55.0 27.5 22.8	186 45.8 22.9 19.0	159 39·3 19.6 16.3	139 34·3 17·2 14·2	27.5 13.8 11.4	92.8 22.9 11.4 9.5	69.6 17.2 8.6 7.1	55·7 13·7 6·8 5·7	46.4 11.4 5.7 4.7	34.8 8.6 4.3 3.6
75	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	264 66.8 33.4 27.7	211 53·5 26.8 22.2	176 44.6 22.3 18.5	151 38.2 19.1 15.8	132 33·4 16.7 13.8	105 26.7 13.4 11.1	87.9 22.3 11.2 9.2	65.9 16.7 8.4 6.9	52.7 13.4 6.7 5.6	43.9 11.1 5.6 4.6	33.0 8.4 4.2 3.5
80	R _c V _c High V _s V Low	254 65.5 32.8 27.1	203 52.4 26.2 21.7	169 43·7 21.8 18.1	145 37·5 18.8 15·5	127 32.8 16.4 13.6	101 26.2 13.1 10.9	84.5 21.8 10.9 9.0	63.4 16.4 8.2 6.8	50.7 13.1 6.6 5.4	42.3 10.9 5.4 4.5	31.7 8.2 4.1 3.4
85	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	248 64.8 32.4 26.8	198 51.8 25.9 21.5	165 43.2 21.6 17.9	142 37.0 18.5 15.3	124 32.4 16.2 13.4	99.1 25.9 13.0 10.7	82.6 21.6 16.8 8.9	62.0 16.2 8.1 6.7	49.6 13.0 6.5 5.4	41.3 10.8 5.4 4.5	31.0 8.1 4.0 3.4
90	R_c V_c High V_s V Low	246 64.6 32.3 26.8	197 51.6 25.8 21.4	164 43.0 21.5 17.8	140 36.9 18.4 15.3	123 32·3 16.2 13.4	98.4 25.8 12.9 10.7	82.0 21.5 10.8 8.9	61.5 16.1 8.0 6.7	49.2 12.9 6.4 5.3	41.0 10.8 5.4 4.5	30.7 8.1 4.0 3.3

TABLE 43.

RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

METRIC MEASURES.

 R_c = radius of critical curvature in kilometers. V_c High = maximum speed in meters per second on isobar of critical curvature. V_s = speed along straight line isobars = 0.5 V_c . V Low = speed in Low along isobar of curvature R_c . V Low = 0.4142 V_c .

The remarks in heading of Table 42 relative to the density of the air apply equally to Table 43.

Lati-					<i>d</i> (1	kilomet	ers)					
tude:		100	125	150	175	200	250	300	400	500	600	800
10°	R _c V _c High V _s V Low R _c V _c High V _s V Low	8330 105 52.7 43.5 2140 53.5 26.7 22.2	6660 84.3 42.2 34.9 1710 42.8 21.4	5550 70.2 35.1 29.1 1430 35.6 17.8	4760 60.2 30.1 24.9 1220 30.5 15.2 12.6	4160 52.7 26.4 21.8 1070 26.7 13.4 11.1	3330 42.1 21.0 17.4 857 21.4 10.7 8.9	2780 35.1 17.6 14.5 714 17.8 8.9 7.4	2080 26.3 13.2 10.9 536 13.4 6.7 5.6	1670 21.1 10.6 8.7 429 10.7 5.4 4.4	1390 17.6 8.8 7.3 357 8.9 4.4 3.7	1040 13.2 6.6 5.5 268 6.7 3.4 2.8
25	R _c V _c High V _s V Low	1400 43·3 21.6 17.9	1120 34.6 17.3 14.3	936 28.8 14.4 11.9	802 24.7 12.4 10.2	702 21.6 10.8 8.9	562 17.3 8.6 7.2	468 14.4 7.2 6.0	351 10.8 5.4 4.5	281 8.7 4.4 3.6	234 7.2 3.6 3.0	175 5·4 2.7 2.2
30	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	1003 36.6 18.3 15.2	802 29.3 14.6 12.1	669 24.4 12.2 10.1	573 20.9 10.4 8.7	501 18.3 9.2 7.6	401 14.6 7.3 6.0	334 12.2 6.1 5.1	251 9.1 4.6 3.8	201 7·3 3·6 3·0	167 6.1 3.0 2.5	125 4.6 2.3 1.9

SMITHSONIAN TABLES.

TABLE 43.
RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT
WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

METRIC MEASURES.

Lati-					d (1	kilomet	ers)					
ude:		100	125	150	175	200	250	300	400	500	600	800
35°	R_c V_c High V_s V Low	762 31.9 15.9 13.2	610 25.5 12.8 10.6	508 21.3 10.6 8.8	435 18. 2 9. 1 7. 5	381 15.9 8.0 6.6	305 12.8 6.4 5.3	254 10.6 5.3 4.4	191 8.0 4.0 3.3	152 6.4 3.2 2.7	127 5·3 2.6 2.2	95·3 4.0 2.0 1.7
40	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	607 28.4 14.2 11.8	485 22.8 11.4 9.4	405 19.0 9.5 7.9	347 16.3 8.2 6.8	303 14.2 7.1 5.9	243 11.4 5.7 4.7	202 9·5 4·8 3·9	152 7.1 3.6 2.9	121 5·7 2.8 2.4	101 4.7 2.4 1.9	75.8 3.6 1.8
45	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	501 25.9 12.9 10.7	401 20.7 10.4 8.6	334 17.2 8.6 7.1	287 14.8 7.4 6.1	251 12.9 6.4 5·3	201 10.3 5.2 4.3	167 8.6 4.3 3.6	125 6.5 3.2 2.7	100 5.2 2.6 2.2	83.6 4.3 2.2 1.8	62.7 3.2 1.6
50	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	427 23.9 11.9 9.9	342 19.1 9.6 7.9	285 15.9 8.0 6.6	244 13.6 6.8 5.6	214 11.9 6.0 4.9	9.5 4.8 3.9	142 8.0 4.0 3.3	107 6.0 3.0 2.5	85.5 4.8 2.4 2.0	7I.2 4.0 2.0 I.7	53.4 3.0 1.5
55	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	374 22.3 11.2 9.2	299 17.9 9.0 7.4	249 14.9 7.4 6.2	213 12.8 6.4 5.3	187 11.2 5.6 4.6	149 8.9 4.4 3.7	125 7·4 3·7 3.1	93.4 5.6 2.8 2.3	74·7 4·5 2·2 1·9	62.3 3.7 1.8 1.5	46. 2. 1. 1.
60	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	334 21.1 10.6 8.7	267 16.9 8.4 7.0	223 14. 1 7.0 5.8	191 12.1 6.0 5.0	167 10.6 5.3 4.4	134 8.4 4.2 3.5	7.0 3.5 2.9	83.6 5.3 2.6 2.2	66.9 4.2 2.1 1.7	55·7 3·5 1.8 1.4	41.8 2.0 1.5
65	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	305 20. 2 10. 1 8. 4	244 16.1 8.0 6.7	204 13.4 6.7 5.6	174 11.5 5.8 4.8	153 10. 1 5. 0 4. 2	122 8. 1 4. 0 3. 4	102 6.7 3.4 2.8	76.3 5.0 2.5 2.1	61.0 4.0 2.0 1.7	50.9 3.4 1.7 1.4	38.: 2.: 1.:
70	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	284 19.5 9.7 8.1	227 15.6 7.8 6.5	189 13.0 6.5 5.4	162 11.1 5.6 4.6	9.7 4.8 4.0	7.8 3.9 3.2	94.6 6.5 3.2 2.7	71.0 4.9 2.4 2.0	56.8 3.9 2.0 1.6	47·3 3·2 1.6 1.3	35. 2. 1.
75	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{V} \ ext{Low} \end{array}$	269 18.9 9.5 7.8	215 15.1 7.6 6.3	179 12.6 6.3 5.2	154 10.8 5.4 4.5	134 9.5 4.8 3.9	107 7.6 3.8 3.1	89.6 6.3 3.2 2.6	67.2 4.7 2.4 1.9	53.7 3.8 1.9 1.6	44.8 3.2 1.6 1.3	33.0 2 1.
80	R_c V_c High V_s V Low	259 18.6 9.3 7.7	207 14.9 7.4 6.2	172 12.4 6.2 5.1	148 10.6 5.3 4.4	129 9.3 4.6 3.9	103 7·4 3·7 3.1	86.2 6.2 3.1 2.6	64.6 4.6 2.3 1.9	51.7 3.7 1.8 1.5	43. I 3. I I. 6 I. 3	32. 2. 1.
85	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	253 18.4 9.2 7.6	202 14.7 7.4 6.1	168 12.2 6.1 5.1	144 10.5 5.2 4.3	126 9.2 4.6 3.8	7·3 3.6 3.0	84. 2 6. I 3. 0 2. 5	63.2 4.6 2.3 I.9	50. 5 3. 7 1. 8 1. 5	42. I 3. I 1. 6 1. 3	31. 2. 1. 1.
90	R_c V_c High V_s V Low	251 18.3 9.1 7.6	201 14.6 7.3 6.0	167 12.2 6.1 5.1	143 10.4 5.2 4.3	9. I 4. 6 3. 8	7·3 3.6 3.0	83.6 6.1 3.0 2.5	62.7 4.6 2.3 1.9	50. I 3. 7 I. 8 I. 5	41.8 3.0 1.5 1.2	31. 2. 1.

REDUCTION OF TEMPERATURE TO SEA LEVEL.

English measures	•	٠	٠	•	•	•	•	•	•	•	•	•	•	•	٠	•	TABLE 44
Metric measures																	TADIE 45

REDUCTION OF TEMPERATURE TO SEA LEVEL.

ENGLISH MEASURES.

Rate of decrease of		DIF	FERE	NCES	BETW		TEE D AT			-	AT AN	Y ALTI	TUDE	
temper- ature. 1°F.						A	LTITUC	DE IN	FEET.					
for every	100	200	300	400	500	600	700	800	900	1000	2000	3000	4000	5000
Feet.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.
200	0.50	1.00	1.50	2.00	2°50	3.00	3°50	4°00	4°50	5.00	10.00	15.00	20.00	25.00
205	0.49	0.98	1.46	1.95	2.44	2.93 2.86	3.41	3.90	4.39	4.88	9.76	14.63	19.51	24.39
215	0.48	0.95	1.43	1.90	2.38 2.33	2.79	3.33 3.26	3.81 3.72	4.29	4.76 4.65	9.52 9.30	13.95	18.60	23.81 23.26
220	0.47	0.93	1.36	1.82	2.27	2.73	3.18	3.64	4.19	4.55	9.30	13.63	18.18	23.20
220	0.43	0.91	1.30	1.02	2.27	2.73	3.10	3.04	4.09	4.33	9.09	13.03	10.10	22.72
230	0.43	0.87	1.30	1.74	2.17	2.61	3.04	3.48	3.91	4-35	8.70	13.04	17.39	21.74
240	0.42	0.83	1.25	1.67	2.08	2.50	2.92	3-33	3.75	4.17	8.33	12.50	16.67	20.83
250	0.40	0.80	1.20	1.60	2.00	2.40	2.80	3.20	3.60	4.00	8.00	12.00	16.00	20.00
260	0.38	0.77	1.15	1.54	1.92	2.31	2.69	3.08	3.46	3.85	7.69	11.54	15.38	19.23
270	0.37	0.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	7.41	11.11	14.81	18.52
280	0.36	0.71	1.07	1.43	1.79	2.14	2.50	2.86	3.21	3-57	7.14	10.71	14.29	17.86
290	0.34	0.69	1.03	1.38	1.73	2.07	2.41	2.76	3.10	3.45	6.90	10.34	13.79	17.24
300	0.33	0.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	-	6.67	10.00	13.33	16,67
310	0.32	0.65	0.97	1.29	1.61	1.94	2.26	2.58	2.90	3.23	6.45	9.68	12,90	16.13
320	0.31	0.62	0.94	1.25	1.56	1.87	2.19	2.50	2.81	3.12	6.25	9.37	12.50	15.62
	5-						ĺ			J				0.1
340	0.29	0.59	0.88	1.18	1.47	1.76	2.06	2.35	2.65	2.94	5.88	8.82	11.76	14.71
360	0.28	0.56	0.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	5.56	8.33	11.11	13.89
380	0.26	0.53	0.79	1.05	1.32	1.58	1.84	2.10	2.37	2.63	5.26	7.89	10.53	13.16
400	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00	2.25	2.50	5.00	7.50	10.00	12.50
420	0.24	0.48	0.71	0.95	1.19	1.43	1.67	1.90	2.14	2.38	4.76	7.14	9.52	11.90
440	0.23	0.45	0.68	0.91	1.14	1.36	1.59	1.82	2.05	2,27	4.55	6.82	9.09	11.36
460	0,22	0.43	0.65	0.87	1.09	1.30	1.52	1.74	1.96	2.17	4.35	6.52	8.70	10.87
48o	0.21	0.42	0.62	0.83	1.04	1.25	1.46	1.67	1.87	2.08	4.17	6.25	8.33	10.42
500	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2.00	4.00	6.00	8.00	10.00
520	0.19	0.38	0.58	0.77	0.96	1.15	1.35	1.54	1.73	1.92	3.85	5.77	7.69	9.62
540			2 -6	0.7	0.00	1.11	T 20	, 10	7 6-	. 0-	2 70		,,,-	0.36
	0.19	0.37	0.56	0.74	0.93	i	1.30	1.48	1.67	1.85	3.70	5.56	7.41	9.26
560	0.18	0.36	0.54	0.71	o.89 o.86	1.07	1.25	1.43	1.61	1.79	3.57	5.36	7.14	8.93
580 600	0.17	0.34	0.52	0.69	0.83	1.03	1.21	1 ~	1.55	1.72	3.45	5.17	6.90	
620	o. 17 o. 16	0.33	0.50	0.65	0.81	0.97	1 .	1.33	1.50	1.67	3.33	5.00		8.33 8.06
020	0.10	0.32	0.40	0.05	0.01	0.97	1.13	1.29	1.45	1.61	3.23	4.04	6.45	0.00
650	0.15	0.31	0.46	0.62	0.77	0.92	1.08	1.23	1.38	1.54	3.08	4.62	6.15	7.69
700	0.14	0.29	0.43	0.57	0.71	0.86	1.00	1.14	1.29	1.43	2.86	4.29	5.71	7.14
750	0.13	0.27	0.40	0.53	0.67	0.80	0.93	1.07	1.20	1.33	2.67	4.00	5.33	6.67
800	0.12	0.25	0.37	0.50	0.62	0.75	0.87	1.00	1.12	1.25	2.50	3.75	5.00	6.25
850	0.12	0.24	0.35	0.47	0.59	0.71	0.82	0.94	1.06	1.18	2.35	3.53	4.71	5.88
900	0.11	0.22	0.33	0.44	0.56	0.67	0.78	0.89	1.00	1.11	2.22	3-33	4.44	5.56
l	•		<u> </u>			<u> </u>	<u> </u>	<u>' </u>	<u> </u>	•		1	1	

Tabular values are to be added to the observed temperature to obtain the temperature at sea level.

REDUCTION OF TEMPERATURE TO SEA LEVEL.

METRIC MEASURES.

Rate of decrease		DIFFE	RENCE	S BETV					AT AN	Y ALT	ITUDE	
of					ANI	AT SI	EA LEV	EL.				
temper- ature.					AL	TITUDE I	N METER	S.				
for every	100	200	300	400	500	600	700	800	900	1000	2000	3000
m.	c.	c.	C.	c.	c.	c.	c.	c.	c.	c.	c.	C.
100	1:00	2,00	3.00	4.00	5.00	6.00	7.00	8.00	9.00	10.00	20.00	30.00
IO2	0.98	1.96	2.94	3.92	4.90	5.88	6.86	7.84	8.82	9.80	19.61	29.41 28.85
104	0.96	1.92	2.88	3.85	4.81	5.77	6.73 6.60	7.69	8.65	9.62	19.23 18.87	28.30
106	0.94	1.89	2.83	3.77	4.72	5.66		7.55	8.49	9.43	18.52	27.78
108	0.93	1.85	2.78	3.70	4.63	5.56	6.48	7.41	8.33	9.26	10.52	27.70
110	0.91	1.82	2.73	3.64	4.55	5-45	6.36	7.27	8.18	9.09	18.18	27.27
115	0.87	1.74	2.61	3.48	4.35	5.22	6.09	6.96	7.83	8.70	17.39	26.09
120	0.83	1.67	2.50	3.33	4.17	5.00	5.83	6.67	7.50	8.33	16.67	25.00
125	0.80	1.60	2.40	3.20	4.00	4.80	5.60	6.40	7.20	8.00	16.00	24.00
130	0.77	1.54	2.31	3.08	3.85	4.62	5.38	6.15	6.92	7.69	15.38	23.08
135	0.74	1.48	2,22	2.96	3.70	4.44	5.19	5.93	6.66	7.41	14.81	22.22
140	0.71	1.43	2.14	2.86	3.57	4.29	5.00	5.71	6.43	7.14	14.29	21.43
145	0.69	1.38	2.07	2.76	3.45	4.14	4.83	5.52	6.21	6.90	13.79	20.69
150	0.67	1.33	2.00	2.67	3.33	4.00	4.67	5.33	6.00	6.67	13.33	20.00
155	0.65	1.29	1.94	2.58	3.23	3.87	4.52	5.16	5.81	6.45	12.90	19.35
160	0.62	1.25	1.87	2.50	3.12	3.75	4.37	5.00	5.62	6.25	12.50	18.75
170	0.59	1.18	1.76	2.35	2.94	3.53	4.12	4.70	5.29	5.88	11.76	17.65
180	0.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.56	11.11	16.67
190	0.53	1.05	1.58	2,10	2.63	3.16	3.68	4.21	4.74	5.26	10.53	15.79
200	0.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	10.00	15.00
210	0.48	0.95	1.43	1.90	2.38	2.86	3.33	3.81	4.29	4.76	9.52	14.29
220	0.45	0.91	1.36	1.82	2.27	2.73	3.18	3.64	4.09	4.55	9.09	13.64
230	0.43	0.87	1.30	1.74	2.17	2.61	3.04	3.48	3.91	4.35	8.70	13.04
240	0.42	0.83	1.25	1.67	2.08	2.50	2.92	3.33	3.75	4.17	8.33	12.50
250	0.40	0.80	1.20	1.60	2,00	2.40	2.80	3.20	3.60	4.00	8.00	12.00
260			1.15	7.54	1.92	2.31	2.69	3.08	3.46	3.85	7.69	11.54
	0.38	0.77	1.15	1.54	1.85	2.22	2.59	2.96	3.43	3.70	7.41	11.11
270 280	0.37 0.36	0.74	1.07	1.43	1.79	2.14	2.50	2.86	3.21	3.70	7.14	10.71
290	-	0.71	1.07	1.38	1.79	2.07	2.41	2.76	3.10	3.45	6.90	10.34
300	0.34	0.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	6.67	10,00
		'							2.81	i	6.25	
320	0.31	0.62	0.94	1.25	1.56	1.87	2.19	2.50	2.65	3.12	5.88	9.37 8.82
340	0.29	0.59	0.88	1.18	1.47	1.76	2.06	2.35	1	2.94 2.78	1 .	
360	0.28	0.56	0.83	1.11	1.39	1.67	1.94	2,22	2.50	2.78	5.56 5.26	8.33 7.89
380	0.26	0.53	0.79	1.05	1.32	1.58	1.84	2.10	2.37		5.00	7.50
400	0.25	0.50	0.75	1.00	1.25	1.50	1.75			2.50		
420	0.24	0.48	0.71	0.95	1.19	1.43	1.67	1.90	2.14	2.38	4.76	7.14
440	0.23	0.45	0.68	0.91	1.14	1.36	1.59	1.82	2.05	2.27	4.55	6.82
460	0.22	0.43	0.65	0.87	1.09	1.30	1.52	1.74	1.96	2.17	4.35	6.52
480	0.21	0.42	0.62	0.83	1.04	1.25	1.46	1.67	1.87	. 2.08	4.17	6.25
500	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2,00	4.00	6.00
·	Tabul	0= 22012	ies ate	to be	added	to the	obsett	ved ter	nnerat	ure to	obtain	

Tabular values are to be added to the observed temperature to obtain the temperature at sea level.

BAROMETRICAL TABLES.

Reduction of the barometer to standard temperature —
English measures Table 46
Metric measures
Reduction of the mercurial barometer to standard gravity.
Direct reduction from local to standard gravity Table 48
Reduction through variation with latitude —
English measures TABLE 49
Metric measures Table 50
Determination of heights by the barometer. English measures.
Values of 60368 (1 + 0.0010195 \times 36) $log \frac{29.90}{B}$ Table 51
Term for temperature Table 52
Correction for gravity and weight of mercury Table 53
Correction for average degree of humidity Table 54
Correction for the variation of gravity with altitude Table 55
Determination of heights by the barometer — Metric and dynamic measures.
Values of 18400 $\log \frac{760}{B}$ Table 56
Values for 18400 $log \frac{1013.3}{B}$ Table 57
Temperature correction factor Table 58
Temperature correction (0.00367 $\theta \times Z$) Table 59
Correction for humidity Table 60
Correction for humidity. Auxiliary to Table 58 Table 61
Correction for gravity and weight of mercury Table 62
Correction for the variation of gravity with altitude Table 63
Difference of height corresponding to a change of o.1 inch in the
barometer — English measures Table 64
Difference of height corresponding to a change of I millimeter in the barometer — Metric measures Table 65
Determination of heights by the barometer.
Formula of Babinet
Barometric pressures corresponding to the temperature of the
boiling point of water —
English measures Table 67
Metric measures

TABLE 46.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

Attach	ed			HEIG	HT OF	тне ва	ROMETE	R IN IN	ICHES.		
Ther	ter -						1				
Fahre heit		19.0	19.5	20.0	20.5	21.0	21.5	22.0	22,5	23.0	23.5
F		Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0.0	0	+0.050	+0,051	+0.052	+0.053	+o.o55	+0.056	+0.057	+0.059	+0.060	+o.o61
+0.	5	+0.049	+0.050	+0.051	+0.053	+0.054	+0.055	+0.056	+0.058	+0.059	+0.06o
I.		.048	049	.050	.052	.053	.054	.055	.057	.058	.059
I.		.047	.048	.049	.051	.052	.053	.054	.056	.057	.058
2. 2.		.046 .045	.047 .046	.049 .048	.050 .049	.051	.052 .051	.053 .052	.055 .054	.056 .055	.057 .056
3.0	o	+0.044	+0.046	+0.047	+0.048	+0.049	+0.050	+0.051	+0.053	+0.054	+0.055
3.		.043	.045	.046	.047	.048	.049	.050	.051	•O53	.054
4.		.043	.044	.045	.046	.047	.048	.049	.050	.052	.053
4.		.042	.043	.044	.045	.046	.047	.048		.051	
5.	°l	.041	.042	.043	.044	.045	.046	.047	.048	.049	.051
5.			+0.041					+0.046			
6.		.039	.040	.041	.042	.043	.044	.045	.046	.047 .046	.048 .047
6.		.038 .037	.039	.040	.041 .040	.042	.043	.044	.045	.045	.047 .046
7. 7.		.037	.038		.039	.040	.041	.043		.044	.045
8.			_		İ	10.020	+0.040	+0.041	+0.042	±0.042	+0.044
8.	5	.035	.036	.037	.038	.038	.039	.040	.041	.042	.043
9.		.034	.035	.036	.037	.038	.038	.039	.040	.041	.042
9.		.033	.034	.035	.036		.037	.038	.039	.040	.041
IÓ.		.032	.033	.034	.035	.036	.036	.037	.038	.039	.040
10.	5	+0.031	+0.032	+0.033	+0.034	+0.035	+0.035	+0.036	+0.037	+0.038	+0.039
II.		.030	.031	.032	.033	.034	.034	.035	.036	.037	.038
11.		.030	,030	.031	.032	.033	.034		.035	.036	.037
12.		.029	.030	.030	.031		.033	.033			.036
12.	·5	.028	.029	1 -	.030		.032			.034	.c34
13.		+0.027						+0.031			
13.		.026	.027	.028	.028	.029	.030	.030	.031	.032	.032
14.		.025 .024	.026	.027 .026	.027	.028	.029	.029	.030	.031	.031
14.		.024	.023	.025	.025	.026	.027	.027	.028	.029	.029
			1	_	+0.024	L-0.025	La 026	+0.026	10 027	+0.027	+0.028
15. 16.		.022	+0.023	023	.024	.024	.025	.025	.026	.026	.027
16.		.021	.022	.023	.023	.023	.024	.024	.025	.025	.026
17.		.020	.021	.021	.022	.022	.023	1 '	.024	.024	.025
17.		.019	.020	.020	.021	.021	.022	.022	.023	.023	.024
18.	0	+0.018	+0.019	+0.019	+0.020	+0.020	+0.021	+0.021	+0,022	+0.022	+0.023
18.	.5	.017	.018	.018	.019	.019	,020	.020	.021	.021	.022
19.	.0	.017	.017	.018	.018	.018	.019	,019	.020	.020	.021
19.		.016	.016	.017	.017	.017	.018	.018	.019	.019	.02C
20.		.015	.015	.016	.016	.016	.017	.017	.018	.018	.018
20	.5	+0.014	+0.014	+0.015	+0.015	+0.016	+0.016	+0.016 .015	+0.017	+0.017	+0.017
21.	.0	.013	.014	.014	.014	.015	.015	.015	.016	.016	.016
21.	٠5	.012	.013	.013	.013	.014	.014	.014	.015	.015	.015
22.		110.	.012	.012	.012	.013	.013	.013	.014	.014	.014
11	_		1.				1	l .]		
23.		+0,010	+0.010	+0.010		+0.011		110.0+	+0.012	+0.012	+0.012
23.		.009	.009	.009	.010	.010	.010	.009	.010	.010	.010
24. 24.		.003	.007	.008	.009	.008	.008	.008	.009	.009	.009
25.		.006	.006	.007	.007	.007	.007	:007	.008	.008	.008
						<u> </u>	<u> </u>	<u>L.,</u>	<u> </u>	<u> </u>	<u> </u>

Attached		<u></u>	HEIG	HT OF		ROMETE	R IN J	ICHES.		
Ther- mometer										
Fahren- heit.	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
25°5	+0.005	+0.006	+0.006	+0.006	+0.006	+0.006	+0,006		+0.007	+0.007
26.0	.005	.005	.005	.005	.005	.005	.005	.005	.005	.006
26.5	.004	.004	.004	.004	.004	.004	.004	.004	.004	.005
27.0 27.5	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
28.0	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0,001	+0.001
28.5	0,000	0,000	0,000	0.000	0.000	0,000	0,000	0.000	0.000	0.000
29.0	-0.001	-0.001	-0,001	-0,001	-0.001	-0.001	-0.001	-0.001	-0.001	-0,001
29.5	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
30.0	.002	.002	.002	.003	.003	.003	.003	.003	.003	.003
30.5	-0,003	-0.003	-0.003	-0,003	-0.004	-0.004	-0.004	-0.004	-0,004	-0.004
31.0	.004	.004	.004	.004	.005	.005	.005	.005	.005	.005
31.5	.005	.005	.005	.005	.005	.006	.006	.006	.006	.006
32.0	.006	.006	.006	.006	.006	.007	.007	.007	.007	.007
32.5	.007	.007	.007	.007	.007	.000	.008	.000	.000	
33.0	-0.008	-o.oo8	-0.00 8	-0.008	-0.008	-0.009	-0.009	-0.009	-0.009	-0.009
33.5	.008	.009	.009	.009	.009	.010	.010	.olo	.010	.010
34.0	.009	.010	.010	.010	.010	.OIO	.011	.011	.011	.011
34.5	.010	.010	.011	.011	.011	.011	.012	.012	.012	.013
35.0	.011	.oii	.012	.012	.012	.012	.013	.013	.013	.014
35.5	-0.012	-0.012	-0,012	-0.013	-0.013	-0.013	-0.014	-0.014	-0.014	-0.015
36.0	.013	.013	.013	.014	.014	.014	.015	.015	.015	.016
36.5	.014	.014	.014	.015	.015	.015	.016	.016	.016	.017
37.0	.014	.015	.015	.016	.016	.016	.017	.017	.017	.018
37.5	.015	.016	.016	.017	.017	.017	.018	.018	,019	.019
38.0	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.019	-0.019	-0,020	-0.020
38.5	.017	.017	.018	.018	.019	.019	.020	.020	.021	.021
39.0	.018	.018	.019	.019	.020	.020	.021	.021	.022	.022
39.5	.019	.019	.020	.020	.021	.021	.022	.022	.023	.023
40.0	.020	.020	.021	.021	.022	.022	.023	.023	.024	.024
40.5	-0,020	-0.021	-0.022	-0.022	-0,023	-0.023	-0.024	0.024	-0.025	-0.025
41.0	.021	.022	.022	.023	.024	.024	.025	.025	.026	.026
41.5	.022	.023	.023	.024	.025	.025	.026	.026	.027	.027
42.0	.023	.024	.024	.025	.025	.026	.027	.027	.028	.029
42.5	.024	.025	.025	.026	.026	.027	.028	.028	.029	.030
43.0	-0.025	-0.025	-0.026	-0.027	-0.027	-0.028	-0.029	-0.029	-0.030	-0.031
43.5	.026	.026	.027	.028	.028	.029	.030	.030	.031	.032
44.0	.026	.027	.028	.029	.029	.030	.031	.031	.032	.033
44.5	.027	.028	.029	.030	.030	.031	.032	.032	.033	.034
45.0	.028	.029	.030	.030	.031	.032	.033	.033	.034	.035
45.5	-0.029	-0.030	-0.031	-0.031	-0,032	-0.033	-0.034	-0.034	-0.035	-0.036
46.0	.030	.031	.031	.032	.033	.034	.035	.035	.036	.037
46.5	.031	.032	.032	.033	.034	.035	.036	.036	.037	.038
47.0	.032	.032	.033	.034	.035	.036	.037	.037	.038	.039
47.5	.033	.033	.034	.035	.036	.037	.038	.038	.039	.040
48.0	-0.033	-0.034	-0.035	-0.036	-0.037	-0.038	-0.039	-0.040	-0.040	-0.041
48.5	.034	.035	.036	.037	.038	.039	.040	.041	.041	.042
49.0	.035	.036	.037	.038	.039	.040	.041	.042	.042	.043
49.5	.036	.037	.038	.039	.040	.041	.042	.043	.044	.044
50.0	.037	.038	.039	.040	.041	.042	.043	.044	0.45	.046

				ENGL	<u></u>	ASURE				
Attached Ther- mometer			HEIG	HT OF	тне ва	ROMETE	R IN IN	CHES.		
Fahren- heit.	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
50°5	-0.038	-0.039	-0.040	-0.041	-0.042	-0.043	-0.044	-0.045	-0.046	-0.047
51.0	.039	.040	.041	.042	.043	.044	.045	.046	0.47	.048
51.5	.039	.040	.041	.042	.044	.045	.046	.047	.048	.049
52.0	.040	.041	.042	.043	.044	.046	.047	.048	.049	.050
52.5	.041	.042	.043	.044	.045	.047	l '	.049	.050	.051
53.0	-0.042	-0.043	-0.044	-0.045	-0.046	-0.047	-0.049	-0.050	-0.051	-0.052
53.5	.043	.044	.045	.046	.047	.048	.050	.051	.052	.053
54.0	.044	.045	.046	.047	.048	.049	.051	.052	.053	.054
54-5 55.0	.045	.046	.047 .048	.048	.049	.050	.052	.053	.054	.055
	.045	.047	Ţ	.049	.050	.051	.053	.054	.055	.056
55.5	-0.046	-0.047	-0.049	-0.050	-0.051	-0.052	-0.054	-0.055	-0.056	-0.057
56.0	.047	.048	.050	.051	.052	.053	.055	.056	.057	.058
56.5	.048	.049	.050	.052	.053	.054	.056	.057	.058	.059
57.0 57.5	.049	.050	.051	.053	.054	.055	.057	.058	.059 .060	.060 .061
	.0 50	.051	.052	.054	.055	.056	.0 58	•059	.000	.001
58.0	-0.051	-0.052	-0.053	-0.055	-0.056	-0.057	-0.059	-0,060	-0.061	-0.063
58.5	.051	.053	.054	.055	.057	.058	.06o	.061	.062	.064
59.0	.052	.054	.055	.056	.058	.059	.061	.062	.063	.065
59.5	.053	.055	.056	.057	.059	.060	.061	.063	.064	.066
60.0	.054	.055	.057	.05 8	.060	.061	.062	.064	.065	.067
60.5	-0.055	-0.056	-0.058	-0.059	-0. 061	-0.062	-0.063	-0.065	-0.066	-0.068
61.0	.056	.057	.059	.060	.062	.063	.064	.066	.067	.069
61.5	.057	.058	.06o	.061	.062	.064	.065	.067	.068	.070
62.0	.057	.059	.060	.062	.063	.065	.066	.068	.069	.071
62.5	.058	.060	.061	.063	.064	.066	.067	.069	.071	.072
63.0	-0.059	-0.061	-0.062	-0.064	-0.065	-0.067	-0.068	-0.070	-0.072	-0.073
63.5	.060	.062	.063	.065	.066	0.68	.069	.071	.073	.074
64.0	.061	.062	.064	.066	.067	.069	.07ó	.072	.074	.075
64.5	.062	.063	.065	.067	.068	.070	.071	.073	.075	.076
65.0	.063	.064	.066	.067	.069	.071	.072	.074	.076	.077
65.5	-0.063	-0.065	-0.067	-0.068	-0.070	-0.072	-0.073	-0.075	-0.077	-0.078
66.0	.064	.066	.068	•069	.071	.073	.074	.076	.078	.079
66.5	.065	.067	.069	.070	.072	.074	.075	.077	.079	.081
67.0	.066	.068	.069	.071	.073	.075	.076	.078	.080	.082
67.5	.067	.069	.070	.072	.074	.076	.077	•079	.081	.083
68.0	-0.068	-0.069	-0.071	-0.073	-0.075	-0.077	-0.078	-o.o8o	-0.082	-0.084
68.5	.069	.070	.072	.074	.076	.078	.079	.081	.083	.085
69.0	.069	.071	.073	.075	.077	.079	.080	.082	.084	.086
69.5	.070	.072	.074	.076	.078	.079	180.	.083	.085	.087
70.0	.071	.073	.075	.077	.079	.080	.082	.084	.086	.088
70.5	-0.072	-0.074	-0.076	-0. 078	-0.080		-0.083	-o.o85	-o.o8 ₇	-0.089
71.0	.073	.075	.077	.079	.080		.084	.086	.088	.090
71.5	.074	.076	.078	.079	.081	.083	.085	.087	.089	.091
72.0	.075	.076	.078	.080	.082	.084	.086	.088	.090	.092
72.5	.075	.077	.079	.081	.083	.085	.087	.089	.091	.093
73.0	-0.076	-0.078	-0.080	-0.082	-0.084	0.086	-o.o88	-0.090	-0.092	-0.094
73.5	.077	.079	.081	.083	.085	.087	.089	.091	.093	.095
74.0	.078	. 0 80	.082	.084	.086	.088	.090	.092	.094	.096
74.5	.079	.081	.083	.085	.087	.089	.091	.093	.095	.097
75.0	.080	.082	.084	.086	.088	.090	.092	.094	.096	.099
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					OF WE					
Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN IN	CHES.		
Fahren- heit.	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
75°.5		-0.083		-0.087	-0.089	-0.091	-0.093	-0.095	-0.097	-0.100
76.0	.081	.084	.086	.088	.090	.092	.094	.096	.098	.101
76.5	.082	.084	.087	.089	.091	.093	.095	.097	.100	.102
77.0	.083	.085	.087	.090	.092	.094	.096	.098	.101	.103
77.5	.084	.086	.088	.091	.093	.095	.097	.099	.102	.104
78.0	-0.085	-0.087	-0.089	-0.091	-0.094	-0.096	-0.098	-0.100	-0.103	-0.105
78.5	.086	.088	.090	.092	.095	.097	.099	.101	.104	, 106
79.0	.086	.089	.091	.093	.096	.098	.100	.102	.105	.107
79.5	.087	.090	.092	.094	.097	.099	.101	.103	.106	.108
80.0	.088	.091	.093	.095	.097	.100	.102	.104	.107	.109
80.5	-0.089	-0.091	-0.094	-0.096	-0.098	-0.101	-0.103	-0.105	-0.108	-0.110
81.0	.090	.092	.095	.097	.099	.102	.104	.106	.109	.111
81.5	.091	.093	.096	.098	.100	.103	.105	.107	.IIO	.112
82.0	.092	.094	.096	.099	.101	.104	.106	.108	.111	.113
82.5	.092	.095	.097	,100	.102	.105	.107	.109	.112	.114
83.0	-0.093	~0.096	-0.098	-0.101	-0.103	-0.106	-0.108	-0,111	-0.113	-0.115
83.5	.094	.097	.099	.102	.104	.107	.109	.112	.114	.117
84.0	.095	.098	.100	.103	.105	.108	.110	.113	.115	.118
84.5	.096	.098	.101	.103	.106	.108	.III	.114	.116	.119
85.0	.097	.099	.102	.104	.107	.109	.112	.115	.117	.120
85.5	-0.098	-0.100	-0.103	-0.105	-0.108	-0.110	-0.113	-0.116	-0.118	-0.121
86.0	.098	.101	.104	.106	.109	.111	.114	.117	.119	.122
86.5	.099	.102	.105	.107	.110	.112	.115	.118	.120	.123
87.0	.100	.103	.105	•108	.111	.113	.116	.119		.124
87.5	.101	.104	.106	.109	.112	.114	.117	.120	.122	.125
88.0	0, 102	-0.105			-0.113	o.115	-o.118	-0.121		-0.126
88.5	.103	.105	.108	.111	.114	.116	.119	.122	.124	.127
89.0	.104	.106	.109	.112	.114	.117	.120	.123	.125	.128
89.5	.104	.107	.110	.113	.115	.118	.121	.124	.126	.129
90.0	.105	.108	.111	.114	.116	.119	.122	.125	.127	.130
	-0.106		-0.112	-0.114	-0.117				-0.128	
91.0	.107	.110	.113	.115	.118	.121	.124	.127	.129	.132
91.5	.108	.III	.113	.116	.119	.122	.125	.128		.133
92.0	.109	.112	.114	.117	.120	.123	.126	.129		.134
92.5	.110	.112	.115	.118	.121	.124	.127	.130	.133	.135
93.0	-0.110	-0.113	-0.116	-0.119	-0.122	-0.125	-o.128	-0.131		-0.137
93.5	.111	.114	.117	.120	.123	.120	.129	.132	135	.138
94.0	.112	.115	.118	.121	.124	.127	.130	.133	.136	.139
94.5	.113	.116	.119	.122	.125	.128	.131	.134	.137	.140
95.0	.114	.117	.120	.123	.126	.129	.132	.135	.138	.141
95.5	-0.115						-0.133			
96.0	.115	.119		.125			-134	.137		
96.5	.116	.119	.122	.126	.129	.132	.135	.138	.141	.144
97.0	.117	.120	.123	.126	.130	.133	.136	.139	.142	.145
97.5		.121	.124	.127	1.130	.134	.137	.140	.143	.146
98.0	-0.119	-O. I 22	-o. 125	-0.128	-0.131	-o.135	-o.138	-0.141	-0.144	-0.147
98.5	.120	.123	.126	.129	.132	.135	.139	.142	.145	.148
99.0	.121	.124	.127	.130	.133	.136	.140	.143	.146	.149
99.5	,121	.125	.128	.131	.134	.137	.141	.144	.147	.150
100.0	.122	.126	.129	.132	.135	.138	.142	.145	.148	.151
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Attached Ther- mometer		-	HEIG	HT OF	THE BA	ROMETI	R IN II	NCHES.		
Fahren- heit.	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0.0	⊹0.06 3	+0.063	+0.064	+0.064	+0.065	+0.065	+0.066	+0.066	+0.067	+0.067
+0.5	+0.061	+0.062	+0.063	+0.063	+0.064	+0.064	+0.065	+0.065	+0.066	+0.066
1.0	.060	.061	.061	.062	.062	.063	.063	.064	.064	.065
1.5 2.0	.059 .058	.060	.060 .059	.061	.061 .060	.062	.062 .061	.063 .062	.063	.064
2.5	.057	.058	.058	.059	.059	.059	.060	.060	.061	.061
3.0	+0.056	+0.056					+0.059		+0.060	+0.060
3.5	.055	.055	.056	.056	.057	.057	.058	.058	.059	.059 .058
4.0 4.5	.054	.054	.055	.055 .054	.056 .054	.056	.057 .055	.057 .056	.057 .056	.057
5.0	.052	.052	.052	.053	.053	.054	.054	.055	.055	.056
5.5	+0.051	+0.051				+0.053				
6.0	.049	.050	.050	.051	.051	.052	.052	.052	.053	.053
6.5 7.0	.048	.049	.049	.050	.050	.050	.051	.051	.052	.052 .051
7.5	.046	.047	.047	.047	.048	.048	.048	.049	.049	.050
8.0	+0.045						+0.047			+0.048
8.5	.044	.044	.045	.045	.045	.046	.046	.047	.047	.047 .046
9.0	.043	.043	.044	.044	.044	.045	.045	.045	.046	.045
9.5 10.0	.042 .041	.041	.041	.043	.043	.042	.043	.043	.043	.044
10.5	+0.040	+0.040	+0.040	+0.041	+0.041			+0.042	+0.042	
11.0	.039	.039	.039	.039	.040	.040	.040	.041	.041	.041
11.5	.037	.038	.038	.038	.039	.039	.039	.040 .038	.040	.040 .039
12.0	.035	.037 .036	.037	.037 .036	.036	.037	.037	.037	.038	.038
13.0	+0.034	+0.034	+0.035	+0.035		+0.036	+0.036	+0.036	+0.036	
13.5	.03,3	.033	.034	.034	.034	.034	.035	.035	.035	.036
14.0	.032	.032	.032	.033	.033	.033	.034	.034	.034	.034
14.5 15.0	.031	.031	.030	.032	.032	.032	.032	.033	.033	.032
15.5	+0.029	+0.029	+0.029	+0.029	+0.030	+0.030	+0.030	+0.030	+0.031	+0.031
16.0	.028	.028	.028	.028	.028	.029	.029	.029	.029	.030
16.5	.026	.027	.027	.027	.027	.028	.028	.028	.028	.028
17.0 17.5	.025	.026	.026 .025	.026	.026 .025	.026	.027 .026	.027 .026	.027 .026	.026
18.0	+0.023	+0.023	+0.024	+0.024	+0.024	+0.024	+0.024	+0.025	+0.025	+0.025
18.5	.022	.022	.022	.023	.023	.023	.023	.023	.024	.024
19.0	.021	.021	.021	.022	.022	.022	.022	.022	.022	.023
19.5 20.0	.020	.020	.020	.020	.02I .0I9	.021	.021	.02I .020	.021	.02I .020
20.5		1 -	+0.018	-	-	1		+0.019	+0.019	+0.019
21.0	.017	.017	.017	.017	.017	.017	.017	.018	.018	.018
21.5	,016	.016	.016	.016		.016	.016	.016	.017	.017
22.0 22.5	.014	.015	.015	.015	.015	.015	.015	.015	.015	.016 .014
23.0		+0.012		+0.013			1	+0.013	1	+0.013
23.5	.011	.01.1	.011	.011	.012	.012	.012	.012	.012	.012
24.0	.010	.010	.010	.010	.010	.011	110.	.011	.011	110,
24.5	.009	.009	.009	.009	.009	.009	.009	.010	.010.	.010
25.0				1			.550	.550		,

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN I	NCHES.		
Fahren- heit.	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8
F.	Inch.									
25°5	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007
26.0	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
26.5	.005	.005	.005	.005	.005	.005	.005	.005	.005	.005
27.0	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
27.5			,003	.003	.003	.003	.003	.003	.003	.003
28.0		+0,001			+0.001	+0.001				+0.001
28.5	0.000	0.000	0.000	0,000	0,000	0,000	0.000	0.000	0.000	0,000 -0,001
29.0	.002	.002	.002	.002	.002	,002	.002	.002	.002	.002
29.5 30.0	.002	.003	.003	.002	.002	.003	.002	.002	.002	.002
	Ů					·	ľ			Ĭ
30.5	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004
31.0	.005	.005	.005	.005	.005	.005	.005	.005	.006	.006
31.5	.007	.007	.007	.008	.008	.007	.007	.007	.007	.007
32.0 32.5	.007	.007	.007	.009	.009	.009	.009	.009	.009	.000
li i			1	_		_	_		-	_
33.0	-0.010	-0.010	-0.010	-0. 010	-0.010	-0.010	-0.010	-0.010	-0.010	-0.010
33.5	.011	.011	110.	.011	.011	.011	.011	110.	.011	.011
34.0	.012	.012	.012	.012	.012	.012	.012	.012	.012	.013
34.5	.013	.013	.013	.013	.013	.013	.013	.014	.014	.014
35.0	.014		.014	.014	.014	.014	.015	.015	.015	.015
35.5	-0.015	-0.015	-0.015	—ი.015	-0.015	-0.016	-0.016	-0.016	-0. 016	-0.016
36.0	.016	.016	.016	.016	.017	.017	.017	.017	.017	.017
36.5	.017	.017	.017	.018	.018	.018	.018	.018	.018	.018
37.0	.018	810. 910.	.019	.019	.019	.019	.019	.019	.019	.019
37.5	.019							.020	.021	.021
38.0	-0.020	-0.021	-0.021	-0.021	-0.021	-0.021	-0.021	-0.022	-0.022	-0.022
38.5	.021	.022	,022	.022	.022	.022	.023	.023	.023	.023
39.0	.023	.023	.023	.023	.023	.024	.024	.024	.024	.024
39.5	.024	.024	.024	.024	.024	.025 .026	.025	.025	.025	.025
40.0										
40.5	-0.026	-0.026	-0.026	-0.026	-0.027	-0.027	-0.027	-0.027	-0.028	-0.028
41.0	.027	.027	.027	.028	.028	.028	.028	.029	.029	.029
41.5			.030	.029	.029	.029	.029	.030	.030	.030
42.0 42.5	.029	.029	.030	.030	.030	.030 .031	.031	.031	.031	.031
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43.0	-0.031 .032	-0.032	-0.032 .033	-0.032 .033	-0.032	-0.033 .034	-0.033 .034	-0.033 .034	-0.033 .035	-0.034 .035
43.5 44.0	.032	.033	.033	.033	.035	.034	.035	.034	.035	.035
44.5	.035	.035	.035	.034	.035	.035	.035	.035	.037	.037
45.0	.036	.036	.036	.037	.037	.037	.037	.038	.038	.038
45.5	-0.037	-0.037	-0.037	-0.038	-0.038	-0.038	-0.039	-0.039	-0.039	-0.039
46.0	.038	.038	.038	.039	.039	.039	.040	.040	.040	.041
46.5	.039	.039	.040	.040	.040	.041	.041	.041	.041	.042
47.0	.040	.040	.041	.041	.041	.042	.042	.042	.043	.043
47-5	.041	.041	.042	.042	.042	.043	.043	.043	.044	.044
48.0 48.5	-0.042 .043	-0.042 .044	-0.043 .044	-0.043 .044	-0.044 .045	-0.044 .045	-0,044 .045	-0,045 .046	-0.045 .046	-0.045 .046
49.0	.043	.044	.045	.044	.045	.045	.043	.047	.047	.048
49.5	.045	.046	.046	.047	.047	.047	.048	.048	.048	.049
50.0	.046	.047	.047	.048	.048	.048	.049	.049	.050	.050
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Attached Ther-			нею	HT OF	THE BA	ROMETE	R IN I	NCHES.		
mometer Fahren- heit.	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
50°5	-0.048	-0.048	-0.048	-0.049	-0.049	-0.050	-0.050	-0.050	-0.051	-0.051
51.0	.049	.049	.049	.050	.050	.051	.051	.051	.052	.052
51.5	.050	.050	.051	.051	.051	.052	.052	.053	.053	-053
52.0	.051	.051	.052	.052	.053	.053	.053	.054	.054	.055
52.5	.052	.052	.053	.053	.054	.054	.055	.055	.055	.056
53.0	-0.053	-0.053	-0.054	-0.054	-0.055	-0.055	-0.056	-0.056	-0.057	-0.057
53.5	.054	.055	.055	-055	.056	.056	.057	.057	.058	.058
54.0 54.5	.055 .056	.056	.056	.057	.057	.057 .059	.058	.058 .060	.059	.059
55.0	.057	.058	.058	.059	.059	.060	.060	.061	.061	.062
55.5	-0.058	-0.059	-0.059	-0.060	-0.060	-0.061	_0 . 061	-0.062	-0.062	-0.063
56.0	.060	.060	.060	.061	.061	.062	.062	.063	.063	.064
56.5	.061	.061	.062	.062	.063	.063	.064	.064	.065	.065
57.0	.062	.062	.063	.063	.064	.064	.065	.065	.066	.066
57.5	.063	.063	.064	.064	.065	.065	.066	.066	.067	.067
58.0	-0.064	-0.064	-0.065	-0.065	_o.o66	_o.o66	0.067	-0.068	-0.068	0.069
58.5	.065	.065	.066	.067	.067	.068	.068	.069	.069	.070
59.0	.066	.067	.067	.068	.068	.069	.069	.070	.07ó	.071
59.5	.067	.068	.068	.069	.069	.070	.070	.071	.072	.072
60.0	.068	.069	.069	.070	.070	.071	.072	.072	.073	.073
60.5	-0.069	0.070	0.070	-0.071	-0.072	-0.072	-0.073	-0.073	-0.074	-0.074
61.0	.070	.071	.072	.072	.073	.073	.074	.074	.075	.076
61.5	.071	.072	.073	.073	.074	.074	.075	.076	.076	.077
62.0	.073	.073	.074	.074	.075	.076	.076	.077	.077	.078
62.5	.074	.074	·º75	.075	.076	.077	.077	.078	.078	.079
63.0	-0.075	-0.075	-0.076	-0.077	-0.077	-0.078	-o.o ₇ 8	-0.079	-0.080	-0.080
63.5	.076	.076	.077	.078	.078	.079	.080	.08o	.081	.081
64.0	.077	.077	.078	.079	.079	.080	.081	.081	.082	.082
64.5	.078	.079	.079	.080	.081	.081	.082	.082	.083	.084
65.0	.079	.080	.080	.081	.082	.082	.083	.084	.084	.085
65.5	-0.080	-0.081	0.081	-0.082	-o.o83	-0.083	-0.084	-0.085	-0.085	-0.086
66.0	.081	.082	.083	.083	.084	.085	.085	.086	.087	.087
66.5	.082	.083	.084	.084	.085	.086	.086	.087	.088	.088
67.0	.083	.084	.085	.085	.086	.087	.087	.088	.089	.090
67.5	.084	.085	.086	.087	.087	.088	.089	.089	.090	.091
68.0	0.085	-o.o86	-0.087	-o.o88	-0.088	-0.089	-0.090	-0.090	-0.091	-0.092
68.5	.087	.087	.088	.089	.089	.090	.091	.092	.092	.093
69.0	.088	.088	.089	.090	.091	.091	.092	.093	-093	.094
69.5	.089	.089	.090	.091	.092	.092	.093	.094	.095	.095
70.0	.090	.091	.091	.092	.093	.094	.094	.095	.096	.097
70.5	-0.091	-0.092	-0.092	-0.093	-0.094	-0.095	-0.095	-0.096	-0.097	0.098
71.0	.092	.093	.094	.094	.095	.096	.097	.097	.098	.099
71.5	.093	.094	.095	.095	.096	.097	.098	.098	.099	.100 .101
72.0 72.5	.094	.095	.096 .097	.096 .098	.097	.098	.099	100.	.100	.101
1		-		- 1				İ		
73.0	-0.096	-0.097	-0.098	-0.099	-0.100	-0.100	-0.101	-0.102	-0.103	-0.104
73.5	.097	.098	.099	.100	.101	.101	.102	.103	.104	.105
74.0	.098	.099	.100	.101 .102	.102	.103	.103	.104	.105	.106
74.5 75.0	.100	.100	.101	.102	.103	.104	.105	.105 .106	.106	.107 .108
73.0	.101	.101	.102	.103		.103		.100	.10/	.100

Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN IN	ICHES.		
Fahren- heit.	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
75°5	-0.102	-0.103	-0.103	-0.104	-o.1o5	-0.106	-0.107	-0.108	-0.108	-0.109
76.0	.103	.104	.104	.105	.106	.107	.108	.109	.110	.110
76.5	.104	.105	.106	.106	.107	.108	.109	.110	.III	.112
77.0	.105	.106	.107	.108	.108	.109	.IIO	.111	.112	.113
77.5	.106	.107	.108	.109	.110	.110	.111	.112	.113	.114
78.0	-0.107	-0.108	-0.109	-0.110	-0.111	-0.112	-o.II2	-0.113	-0.114	-0.115
78.5	.108	.109	.110	.III	.112	.113	.114	.114	.115	.116
79.0	.109	.110	.111	.112	.113	.114	.115	.116	.117	.117
79.5	.110	.III	.112	.113	.114	.115	.116	.117	.118	.119
80.0	.111	.112	.113	.114	.115	.116	.117	.118	.119	.120
80.5	-0.112	-0.113	-0.114	-0.115	-0.116	-0.117	-0.118	-0.119	-0.120	-0.121
81.0	.114	.115	.115	.116	.117	.118	.119	.120	.121	.122
81.5	.115	.116	.117	.118	.118	.119	.120	.121	.122	.123
82.0	.116	.117	811.	.119	.120	.121	.122	.122	.123	.124
82.5	.117	.118	.119	.120	.121	.122	.123	.124	.125	.126
83.0	-0.118	-0.119	-0.120	-0.121	-0.122	-0.123	-0.124	-0.125	-0.126	-o.127
83.5	.119	.120	.121	.122	.123	.124	.125	.126	.127	.128
84.0	.120	.121	.122	.123	.124	.125	.126	.127	.128	.129
84.5	.121	.122	.123	.124	.125	.126	.127	.128	.129	.130
85.0	.122	.123	.124	.125	.126	.127	.128	.129	.130	.131
85.5	-0.123	-0.124	-0.125	-0.126	-0.127	-0.128	-0.129	-0.130	-0.131	-0.133
86.o	.124	.125	.126	.127	.128	.130	.131			
		.125	.128					.132	.133	.134
86.5	.125 .126	.128		.129	.130	.131	.132	.133	.134	.135
87.0	.128	.120	.129	.130	.131	.132	.133	.134	.135	.136
87.5	l	1	.130	.131	.132	.133	.134		.136	.137
88.0	-0.129	-0.130	-0.131	-0.132	-0.133	-0.134	—o. 135	-0.136	-o.137	-o.138
88.5	.130	.131	.132	.133	.134	-135	.136	.137	.138	.139
89.0	.131	.132	.133	.134	.135	.136	.137	.138	.140	.141
89.5	.132	.133	.134	.135	.136	.137	.138	.140	.141	.142
90.0	.133	.134	.135	.136	.137	.138	.140	.141	.142	.143
90.5	-o.134	-0.135	-0.136	-0.137	-01.39	-0.140	-0.141	-0.142	-0.143	-0.144
91.0	.135	.136	.137	.138	.140	.141	.142	.143	.144	.145
91.5	.136	.137	.138	.140	.141	.142	.143	.144	.145	.146
92.0	.137	.138	.140	.141	.142	.143	.144	.145	.146	.148
92.5	.138	.139	.141	.142	.143	.144	.145	.146	.148	.149
93.0	-0.139	-0.141	-0.142	-0.143	-0.144	-0.145	-0.146	-0.148	-0.149	-0.150
93.5	.140	.142	.143	.144	.145	.146	.148	.149	.150	.151
94.0	.142	.143	.144	.145	.146	.147	.149	.150	.151	.152
94.5	.143	.144	.145	.146	.147	.149	.150	.151	.152	.153
95.0	.144	.145	.146	.147	.149	.150	.151	.152	.153	.154
95.5	-0.145	-0.146	-0.147	-0.148	-0.150	-0.151	-0.152	-0.153	-0.154	-0.156
96.0	.146	.147	.148	.150	.151	.152	.153	.154	.156	.157
96.5	.147	.148	.149	.151	.152	.153	.154	.156	.157	.158
97.0	.148	.149	.150	.152	.153	.154	.155	.157	.158	.159
97.5	•149	.150	.152	.153	.154	.155	.157	.158	.159	.166
98.0	-0.150	-0.151	-0.153	-0.154	-0.155	-0.156	-0.158	-0.159	-0.160	-0.161
98.5	.151	.153	.154	.155	.156	.158	.159	.160	.161	.163
99.0	.152	154	.155	.156	-157	.159	.160	.161	.162	.164
99.5	.153	.155	.156	.157	.159	.160	.161	.162	.164	.165
100.0	.154	.156	.157	.158	.160	.161	.162	.163	.165	.166
			07	l 0°	<u> </u>		1	<u> </u>		

Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN IN	CHES.		
Fahren- heit.	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
F. 0°0	Inch. +0.068	Inch. +0.068	Inch.	Inch. 0.069	Inch.	Inch.	Inch.	Inch.	Inch. +0.072	Inch.
			-	٠ -			•			
+ 0.5 1.0	+0.067 .065	.066	.066	.067	.067	.068	.068	.069	+0.071 .069	.070
1.5	.064	.065	.065	.066	.066	.067	.067	.068	.068	.069
2.0 2.5	.063 .062	.064 .062	.064 .063	.065 .063	.065 .064	.065 .064	.066 .065	.066 .065	.067 .066	.067 .066
3.0		+0.061			+0.063				+0.064	
3.5	.059	.060	.060	.060	.061 .060	.062 .061	.062 .061	.063 .061	.063 .062	.064 .062
4.0 4.5	.o58 .o57	.059	.059	.058	.059	.059	.060	.060	.062	.062
5.0	.056	.056	.057	.057	.058	.058	.059	.059	.059	.060
5.5 6.0				+0.056				+0.058		+0.059
6.5	.054 .052	.054	.054	.055	.055	.056	.056 .055	.056 .055	.057 .056	.057 .056
7.0	.051	.052	,052	.052	.053	.053	.054	.054	.054	.055
7.5	.050	.050	.051	.051	.052	.052	.052	.053	.053	.053
8.0										+0.052
8.5	.048 .046	.048	.048 .047	.049	.049 .048	.049	.050 .049	.050 .049	.051 .049	.051 .050
9.0 9.5	.045	.046	.046	.046	.047	.047	.047	.048	.048	.048
10.0	.044	.044	.045	.045	.045	.046	046	046	.047	.047
10.5	+0.043							+0.045		+0.046
11.0	.042	.042	.042	.043	.043	.043	.044	.044	.044	.045
11.5 12.0	.041 .039	.041	.041	.041	.042	.042 .041	.042	.043	.043	.043
12.5	.038	.038	.039	.039	.039	.040	.040	.040	.040	.041
13.0	+0.037	+0.037						+0.039		+0.040
13.5	.036	.036	.036	.037	.037	.037	.037	.038	.038	.038
14.0 14.5	.035	.035	.035	.035	.036	.036	.036	.036	.037	.037 .036
15.0	.032	.032	.033	.033	.033	.033	.034	.034	.034	.034
15.5		+0.031							+0.033	
16.0	.030	.030	.030	.031	.031	.031	.031	.031	.032	.032
16.5 17.0	.029	.029	.029	.029	.030	.030	.030	.030	.030	.031
17.5	.026	.027	.027	.027	.027	.027	.028	.028	.028	.028
18.0	+0.025	+0.025		+0.026	+0.026	+0.026		+0.026	+0.027	+0.027
18.5	.024	.024	.024	.024	.025	.025	.025	.025	.025	.026
19.0 19.5	.023	.023	.023	.023	.023	.024	.024	.024	.024	.024
20.0	.020	.021	.021	.021	.021	.021	.021	.021	.023	.022
20.5 21.0	+0.019 810.	+0.019 810.	+0.020	+0.020 .018	+0.020			+0.020 .019	+0.020	+0.021 .019
21.5	.013	.017	.017	.017	.019	.019	.019	.019	610. 810.	.019
22.0	.016	.016	.016	.016	.016	.016	.016	.017	.017	.017
22.5	.014	.015	.015	.015	.015	.015	.015	.015	.015	.015
23.0	+0.013		+0.014	+0.014	+0.014	+0.014		+0.014		+0.014
23.5	.012	.012	.012	.012	.012	.013	.013	.013	.013	.013
24.0 24.5	110. 010.	.010	010.	.010	.010	.010	.010	.012	.010	.110
25.0	.009	.009	.009	.009	.009	.009	.009	.009	.009	.009
JI	I			<u> </u>		<u></u>	<u></u>		ــــــــــــــــــــــــــــــــــــــ	L

Attached Ther-			HEIC	HT OF	THE BA	ROMETI	ER IN I	NCHES.		
mometer				i		1	· · · · · · · · · · · · · · · · · · ·	<u> </u>	1	1
Fahren- heit.	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
25°5	+0.007	+0.007	+0.008	+0.008	+0.008	+0.008	+0.008	+0.008	+0.008	+0.008
26.0 26.5	.006	.006	.006	.006	.006	.006	.006	.007	.007	.007
27.0	.005	.005	.005	.005	.005	.005	.005	.005	.005	.005
27.5	.003	.004	.004	.004	.004	.004	.004	.004	.004	.004
28.0	+0.001	+0.001	+0.002		+0.002	+0.002	+0.002	+0.002	+0.002	.003 +0.002
28.5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0,000	0.000
29.0	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
29.5	.002	,002	.002	,002	.002	.002	.002	.002	.002	.002
30.0	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
30.5	-0.004	-0.004	-0.004	-0 005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005
31.0	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
31.5	.007	.007	.007	.007	.007	.007	.007	.007	.007	.007
32.0	.008	.008	.008	.008	.008	.008	.008	.008	.008	.009
32.5	.009	.009	.009	.009	.009	.009	.010	.010	.010	.010
33.0	-0.010	-0.010	-0.010	-0.011	-0.011	-0.011	-0.011	-0.011	-0.011	-0.011
33.5	.011	.012	.012	.012	.012	.012	.012	.012	.012	.012
34.0	.013	.013	.013	.013	.013	.013	.013	.013	.013	.014
34.5	.014	.014	.014	.014	.014	.014	.014	.015	.015	.015
35.0	.015	.015	.015	.015	.015	.016	.016	.016	.016	.016
35.5	~0. 016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017
36.0	.017	.018	810,	.018	.018	.018	.018	.018	.018	.019
36.5	.019	.019	.019	.019	.019	.019	.019	.020	.020	.020
37.0	.020	.020	.020	.020	.020	.021	.021	.021	.021	.021
37.5	.021	.021	.021	.021	.022	.022	.022	.022	.022	.022
38.0	-0.022	-0.022	-0.022	-0.023	-0.023	-0.023	-0.023	-0.023	-0.023	-0.024
38.5	.023	.023	.024	.024	.024	.024	.024	.025	.025	.025
39.0	.024	.025	.025	.025	.025	.025	.026	.026	.026	.026
39.5	.026	.026	.026	.026	.026	.027	.027	.027	.027	.027
40.0	.027	.027	.027	.027	.028	.028	.028	.028	.028	.029
40.5	-0.028	-0.028	-0.028	-0.029	-0.029	-0.029	-0.029	-0.030	-0.030	-0.030
41.0	.029	.029	.030	.030	.030	.030	.031	.031	.031	.031
41.5	.030	.031	150.	.031	.031	.032	.032	.032	.032	.032
42.0	.032	.032	.032	.032	.033	.033	.033	.033	.033	.034
42.5	.033	.033	.033	.033	.034	.034	.034	.034	.035	.035
43.0	-0.034	-0.034	-0.034	-0.035	-0.035	-0.035	-0.035	- 0.036	-0.036	-0.036
43.5	.035	.035	.036	.036	.036	.036	.037	.037	.037	.037
44.0	.036	.037	.037	.037	.037	.038	.038	.038	.038	.039
44.5	.037	.038	.038	.038	.039	.039	.039	.039	.040	.040
45.0	.039	.039	.039	.039	.040	.0 40	.040	.041	.041	.041
45.5 46.0	-0.040	-0.040	-0. 040	-0.041	-0.041	-0.041	-0.042	-0.042	-0.042	-0.043
	.041	.041	.042	.042	.042	.043	.043	.043	.043	.044
40.5 47.0	.042	.042	.043	.043	.043	.044	.044	.044 .046	.045	.045 .046
47.5	.045	.045	.044	.046	.045	.045	.045 .047	.040	.046	.048
48.0	-0.046	-0.046	-0.046	-0.047	- 0.047	-0.047	-0. 048	-0.048	-0.048	-0.049
48.5	.047	.047	.048	.048	.048	.049	.049	.049	.050	.050
49.0	.048	.048	.049	.049	.049	.050	.050	.051	.051	.051
49.5	.049	.050	.050	.050	.051	.051	.051	.052	.052	.053
50.0	.050	.051	.051	.052	.052	.052	.053	.053	.053	.054
<u> </u>										

Attached Ther- mometer			HEIG	HT OF 7	THE BA	ROMETE	R IN IN	CHES.		
Fahren- heit.	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
F	Inch.	, Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
50°5	-0.052	-0.052	-0.052	-0. 053	-0.053	-0.054	-0.054	-0.054	-o.o55	-o.o55
51.0	.053	.053	.054	.054	.054	.055	.055	.056	.056	.056
51.5	.054	.054	.055 .056	.055	.056	.056 .057	.056	.057 .058	.057	.058
52.0 52.5	.055 .056	.055 .057	.057	.056 .058	.057 .058	.058	.059	.059	.060	.060
53.0	-0.057	-o.o ₅ 8	-0.058	-0.059	-0.059	<u></u> 0.060	-0.060	-0.061	-0.061	-0.061
53.5	.059	.059	.059	.060	.060	.061	.061	.062	.062	.063
54.0	.060	.060	.061	.061	.062	.062	.063	.063	.063	.064
54.5	.061	.061	.062	.062	.063	.063	.064	.064	.065	.065
55.0	.062	.063	.063	.064	.064	.064	.065	.065	.066	.066
55.5	-0.063	-0.064	-0.064	-0.065	-0.065	-0.066	-0.066	-0.067	-0.067	-0.068
56.0	.064	.065	.065	.066	.066	.067	.067	.068	.068	.069
56.5	.066	.066 .067	.067 .068	.067 .068	.068 .069	.068	.069 .070	.069 .070	.070 .071	.070 .071
57.0	.067	.069	.069	.070	.009	.009	.071	.072	.072	.073
57.5		-		-	·			-		
58.0	-0.069	-0.070	-0.070	-0.071	-0.07 I	-0.072	-0.072	-0.073	-0.073	-0.074
58.5	.070	.071	.071	.072	.072	.073	.074	.074	.075	.075 .076
59.0	.072	.072	.073 .074	.073 .074	.074	.074 .075	.075 .076	.075	.077	.078
59·5 60.0	.073 .074	.073	.075	.074	.076	.077	.077	.078	.078	.079
60.5		-0. 076	-0.076	0.077	-0.077	-0.078	-0. 078	-0.079	-0.080	-0.080
61.0	-0.075 .076	.077	.077	-0.077 .078	-0.077 .079	.079	.080	.080	.081	.081
61.5	.077	.078	.079	.079	.080	.080	.081	.082	.082	.083
62.0	.079	.079	.08o	.080	.081	.082	.082	.083	.083	.084
62.5	.080	.080	.081	.082	.082	.083	.083	.084	.085	.085
63.0	-0.081	-0.082	-0.082	-0.083	-0.083	-0.084	-0.085	-0.085	-0.086	-o.o86 ·
63.5	.082	.083	.083	.084	.085	.085	.086	.086	.087	.088
64.0	.083	.084	.085	.085	.086	.086	.087	.088	.088	.089
64.5	.084	.085	.086	.086	.087	.088	.088	.089	.090	.090
65.0	.0 86	.086	.087	.088	.000	.009	.090	.090	.091	.092
65.5	-0.087	-0.087	·· o.o88	-0.089	-0.089	-0.090	-0.091	-0.091	-0.092	-0.093
66.0	.088	.089	.089	.090	.091	.091	.092	.093	.093	.094
66.5	.089	.090	.090	.091	.092	.093	.093	.094	.095	.095
67.0 67.5	.090	.091	.092	.092	.093	.094	.094	.095	.097	.097
1		-		· ·						
68.0	-0.093	-0.093	-0.094	-0.095	-0.095	-0.096 .097	-0.097 .098	-0.098 .099	-0.098	-0.099 .100
68.5 69.0	.094	.095	.095	.096	.097	.097	.099	.100	.101	.102
69.5	.095	.097	.098	.098	.099	.100	.101	.101	.102	.103
70.0	.097	.098	.099	.100	,100	.101	.102	.103	.103	.104
70.5	-0.098	-0.099	-0.100	-0,101	_o.101	-0.102	-0.103	-0.104	-0.105	-0.105
71.0	.100	.100	.101	.102	.103	.103	.104	.105	.106	.107
71.5	.ioi	.102	.102	.103	.104	.105	.105	.106	.107	.108
72.0	.102	.103	.104	.104	.105	.106	.107	.107	.108	.109
72.5	.103	.104	.105	.106	.106	.107	.108	.109	.109	.110
73.0	-0.104	-0.105	-0.106	-0.107	-0.108	-0.108	-0.109	-0.110	-0.111	-0.112
73.5	.105	.106	.107	.108	.109	.IIO	.110	.III.	.112	.113
74.0	.107	.107	.108	.109	.110	.111	.112	.112	.113	.114
74.5	.108	.109	.109	.110	.112	.113	.113	.115	114	.115
75.0	19			<u> </u>	1			1		

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Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN IN	CHES.		
Fahren- heit.	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
75°5	-0.110	-0.111	-O. I I 2	-0.113	-0.114		-o.115	-o.116		-o.118
76.0	.III	.112	.113	.114	.115	.116	.116	.117	.118	.119
76.5	.113	.113	.114	.115	.116	.117	.118	.119	.119	.120
77.0	.114	.115	.115	.116	.117	.118	.119	.120	.121	.122
77.5	.115	.116	.117	.117	.118	.119	.120	.121	.122	.123
78.0	-0.116	-0.117	-0.118	-0.119	-0.120		-0.121	-0.I22	-0.123	-0.124.
78.5	.117	.118	.119	.120	.121	.122	.123	.123	.124	.125
79.0	.118	.119	.120	.121	.122	.123	.124	.125	.126	.127
79.5	.120	.120	.121	.122	.123	.124	.125	.126	.127	.128
80.0	.121	.122	.123	.123	.124	.125	.126	.127	.128	.129
80.5	-0. I 22	-0.123	-0.124	-0.125	-0.126	- 0.127	-0.127	- 0.128	-0.129	
81.0	.123	.124	.125	.126	.127	.128	.129	.130	.131	.132
81.5	.124	.125	.126	.127	.128	.129	.130		.132	
82.0	.125	.126	.127	.128	.129	.130	.131	.132	.133	.134
82.5	.127	.128	.128	.129	.130	.131	.132	.133	.134	.135
83.0	-0.128	-0,129	-0.130	-0.131	-0.132	-0.133	-0.134	-o.135	-0.136	-o.137
83.5	.129	.130	.131	.132	.133	.134	-135	.136	.137	.138
84.0	.130	.131	.132	.133	.134	.135	.136	.137	.138	.139
84.5	.131	.132		.134	.135	.136	.137	.138	.139	.140
85.0	.132	.133	.134	.135	.136	.137	.138	.139	.141	.142
85.5	-0.134	-0.135	-0.136	-0.137	-0.138	-0. I 30	-0.140	-0.141	-0. I42	-0.143
86.0	.135	.136	.137	.138	.139	.140	.141	.142	.143	.144
86.5	.136	.137	.138	.139	.140	.141		.143	.144	.145
87.0	.137	.138	.139	.140	.141	.142			.145	.147
87.5	.138	.139	.140	.141	.142	.144	.145	.146	.147	.148
88.0	-0.139	0. 140	-0.142	-0.143	-0.144	-0.145	-0.146	-0.14 7	-0.148	-0.149
88.5	.141	.142	.143	.144	.145	.146	.147	.148	.149	.150
89.0	.142	.143	.144	.145	.146	.147	.148	•149	.150	.152
89.5	.143	.144	.145	.146	.147	.148	•149	.151	.152	•153
90.0	.144	.145	.146	.147	.148	.150	.151	.152	.153	.154
90.5	-0.145	-0.146					-0.152		-0.154	
91.0	.146	.147	.149	.150	.151	.152	.153	.154	•155	.157
91.5	.148	.149	.150	.151	.152	.153	.154	.155	.157	.158
92.0 92.5	.149 .150	.150 .151	.151	.152	.153	.154 .156	.156	.157 .158	.158 .159	.159 .160
93.0	_								-0.160	
21 .	-0.151	-0.152		-0.155	-0.156	→0.157 .158	-0.158	-0.159 .160	.162	-0.161 .163
93.5	.152	.153	.155	.156	.157		.159 .160	.162		.164
94.0 94.5	·153	.155 .156	.156	.157 .158	.158	.159 .160	.160	.163	.163	.165
95.0	.155 .156	.150	.157 .158	.159	.160	.162	.163	.164	.165	.166
95.5				•	_0.760	-0.762	→0. 164	-0.765	_0.767	-0.16g
95.5 96.0	-0.157 .158	→0.158 .159	-0.159 .160		.163		.165		.168	
96.5	.159	.160	.162	.163	.164	.165	.167	.168	.169	.170
97.0	.160	.162	.163	.164	.165	.167	.168	.169	.170	.171
97.5	.162	.163	.164	.165	.166	.168	.169	.170	.171	.173
98.0	–0. 163	-0. 164	-o.165	-0.166	-0.168	-0.169	-0.170	-0.171	-0.173	-0.174
98.5	.164	.165	.166	.168	.169	1.170	.171	.173	.174	.175
99.0	.165	.166	.168	.169	.170	.171	.173	.174	.175	.176
99.5	.166	.167	.169	.170	.171	.173	.174	.175	.176	.178
100.0	.167	.169	.170	.171	.172	.174	-175	.176	.178	.179
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Attached Ther-			HEIG	HT OF 1	THE BA	ROMETE	R IN IN	ICHES.		
mometer Fahren- heit.	28.0	28.2	28.4	28.6	28.8	29.0	29.2	29.4	29.6	29.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0°0	+0.073	+0.074	+0.074	+0.075	+0.075	+0.076	+0.076	+0.077	+0.077	+0.078
⊹0.5	+0.072	+0.072	+0.073	+0.073	+0.074	+0.074	+0.075	+0.075	+0.076	+0.076
1.0	.070	.071	.071	.072	.072	.073	.073	.074	.074	.075
1.5	.069	.070	.070	.071	.071	.072	.072	.073	.073	.074
2.0 2.5	.068	.068	.069	.069	.070	.070	.071	.071	.072	.072 .071
3.0	i .		+0.066	+0.067	+0.067	_	+o.o68	+0.069	+0.069	+0.070
3.5	+0.065 .064	+0.066	.065	.065	.066	.066	.067	.067	.068	.068
4.0	.063	.063	.064	.064	.065	.065	.065	.066	.066	.067
4.5	.062	.062	.062	.063	.063	.064	.064	.065	.065	.065
5.0	.060	.061	.061	.062	.062	.062	.063	.063	.064	.064
5.5	+0.059	+0.059	+0.060		+0.061		+0.062		+0.062	+0.063
6.0	.058	.058	.059	.059	.059	.060	.060	.059	.061	.060
6.5 7.0	.056	.057 .056	.057 .056	.058	.058	.058	.059 .057	.058	.058	.059
7.5	.054	.054	.055	.055	.055	.056	.056	.057	.057	.057
8.0	+0.053	+0.053	+0.053	+0.054	+0.054	+0.054	+0.055	+0.055	+0.056	+0.056
8.5	.051	.052	.052	.052	.053	.053	.053	.054	.054	.055
9.0	.050	.050	.051	.051	.051	.052	.052	.053	.053	.053
9.5	.049	.049	.049	.050	.050	.050	.051	.051	.052	.052
10.0	.047	.048	.048	.048	.049	.049	.050	.050	.050	.051
10.5	+0.046	+0.047	+0.047	+0.047	+0.048		+0.048	+0.049	+0.049	+0.049
0.11	.045	.045	.046	.046	.046	.047	.047	.047	.047	.048
II.5 I2.0	.044	.044	.044	.045	.045	.045	.046	.046	.046	.046
12.5	.041	.041	.043	.042	.042	.043	.043	.043	.043	.044
13.0		+0.040	+0.040	+0.041	+0.041	+0.041	+0.042	+0.042	+0.042	+0.042
13.5	.039	039	.039	.039	.040	.040	.040	.040	.041	.041
14.0	.037	.038	.038	.038	.038	.039	.039	.039	.039	.040
14.5	.036	.036	.037	.037	.037	.037	.038	.038	.038	.038
15.0	.035	.035	.035	.035	.036	.036	.036	.036	.037	.037
15.5	+0.033		+0.034		+0.034	+0.035	+0.035	+0.035	+0.035	+0.036
16.0	.032	.032	.033	.033	.033	.033	.034	.034	.034	.034
16.5 17.0	.031	.031	.031	.032	.032	.032	.032	.032	.033	.033
17.5	,028	.029	.029	.029	.029	.029	.030	.030	.030	.030
18.0	+0,027	+0.027	+0.027	+0.028	+0.028	+0.028	+0,028	+0.028	+0,029	+0.029
18.5	.026	.026	.026	.026	.027	.027	.027	.027	.027	.027
19.0	.025	.025	.025	.025	.025	.025	.026	.026	.026	.026
19.5	.023	.023	.024	.024	.024	.024	.024	.024	.025	.025
20.0	.022	.022	.022	.022	.023	.023	.023	.023	.023	.023
20.5		+0.021			+0,021	+0.021	+0.022			+0.022
21.0	.019	.020	.020	.020			.020	.020	.021	.021
21.5 22.0	.017	.017	.017	.017	.019	.017	.019	.019	.019	.019
22.5	.016	.016	.016	.016	.016	.016	.016	.016	.016	.017
23.0	+0.01/	+0.014	+0.015	+0.015	+0,015	+0.015	+0.015	+0.015	+0.015	+0.015
23.5	.013	.013	.013	.or3	.013	.014	.014	.014	.014	.014
24.0	.012	.012	.012	.012	.012	.012	.012	.012	.012	.013
24.5	110.	110.	110.	110.	110.	110.	110.	.011	.010	110.
25.0	.009	.009	.009	.009	.009	.010	.010	.010	.010	.010

	ENGLISH WEASURES.										
Attached Ther- mometer		HEIGHT OF THE BAROMETER IN INCHES.									
Fahren- heit.	28.0	28.2	28.4	28.6	28.8	29.0	29.2	29.4	29.6	29.8	
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	
25°5	+0.008				+0.008	+0.008	+0.008	+0.008	+0.008	+0.008	
26.0	.007	.007	.007	.007	.007	.007	.007	.007	.007	.007	
26.5	.005	,005	.005	.006	.006	.006	.006	.006	.006	.006	
27.0 27.5	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
28.0	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	
28.5	0.000	0.000	0.000	0.000	0.000	0,000	0.000	0,000	0.000	0,000	
29.0	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	
29.5	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
30.0	.003	.004	.004	.004	.004	.004	.004	.004	.004	.004	
30.5	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	
31.0	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	
31.5	.007	.007	.007	.007	.008	.008	.008	.008	.008	.008	
32.0 32.5	.010	.009	.009	.009	.009	.009	.009	.010	.009	.010	
33.0	-0.011	-0.011	-0.011	-0.011	-0.011	-0.012	-0.012	-0.012	-0.012	-0.012	
33.5	.012	.012	.013	.013	.013	.013	.013	.013	.013	.013	
34.0	.014	.014	.014	.014	.014	.014	.014	.014	.014	.015	
34.5	.015	.015	.015	.015	.015	.015	.016	.016	.016	.016	
35.0	.016	.016	.016	.017	.017	.017	.017	.017	.017	.017	
35.5	-0.017	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.019	
36.0 36.5	.019 .020	.019	.019	.019	.019	.019	.020	.020 .021	.020	.020 .021	
37.0	.021	.021	.022	.022	.021	.021	.022	.021	.021	.023	
37.5	.023	.023	.023	.023	.023	.023	.024	.024	.024	.024	
38.0	-0.024	-0.024	-0.024	-0.024	-0.024	-0.025	-0.025	-0.025	0.025	-0.025	
38.5	.025	.025	.025	.026	.026	.026	.026	.026	.027	.027	
39.0	.026	.027	.027	.027	.027	.027	.027	.028	.028	.028	
39.5 40.0	.028	.028	.028	.028	.028	.029	.029	.029 .030	.029	.029	
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40.5	-0.030	-0.030	-0.031	-0.031	-0.031	-0.031		-0.032		-0.032	
41.0 41.5	.031	.032	.032	.032	.032	.033	.033	.033	.033	.033	
42.0	.034	.034	.034	.035	.035	.035	.035	.036	.036	.036	
42.5	.035	.035	.036	.036	.036	.036	.037	.037	.037	.037	
43.0	-0.036	-0.037	-0.037	-0.037	-0.038	0.038	-0.038	-0.038	-0.039	-0.039	
43.5	.038	.038	.038	.039	.039	.039	.039	.040	.040	.040	
44.0	.039	.039	.040	.040	.040	.040	.041	.041	.041	.042	
44.5 45.0	.040	.041	.041	.041	.041	.042	.042	.042	.043	.043	
45.5	-0.043	-0.043	-0.043	-0.044	-0.044	-0.044		0.045	-0.045	-0.046	
46.0	.044										
46.5	.045	.046	.046	.046	.047	.047	.047	.048	.048	.048	
47.0	.047	.047	.047	.048	.048	.048	.049	.049	.049	.050	
47.5	.048	.048	.049	.049	.049	.050	.050	.050	.051	.051	
48.0	-0.049	-0.050	-0.050	-0.050	-0.051	-0.051	-0.051	-0.052	-0.052	-0.052	
48.5	.050	.051	.051	.052	.052	.052	.053	.053	.053	.054	
49.0 49.5	.052	.052	.052	.053	.053	.054	.054	.054	.055	.055	
50.0	.054	.055	.055	.055	.056	.056	.057	.057	.057	.058	
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	ENGLISH MEASURES.									
Attached Ther- mometer	HEIGHT OF THE BAROMETER IN INCHES.									
Fahren- heit.	28.0	28.2	28.4	28.6	28.8	29.0	29.2	29.4	29.6	29.8
F.	Inch.	Inch.	Inch.	Inch.	Jnch.	Inch.	Inch.	Inch.	Inch.	Inch.
50°5	-0.055	-0.056	-0.056	-0.057	-0.057	-0.057	-0.058	-0.058	-0.059	-0.059
51.0	.057	.057	.058	.058	.058	.059	.059	.060	.060	.060
51.5	.058	.058	.059	.059	.060	.060	.061	.061	.061	.062
52.0	.059	.060	.060	.061	.061	.061	.062	.062	.063	.063
52.5	.061	.061	.061	.062	.062	.063	.063	.064	.064	.064
53.0	-0.062	-0.062	-0.063	-0.063	-0.064			-0.065	-0.065	-0.066
53.5	.063	.064	.064	.064	.065	.065	.066	.066	.067	.067
54.0	.064	.065	.065	.066	.066	.067	.067	.068	.068	.068
54.5	.066	.066	.067	.067	.067	.068	.068	.069	.069	.070
55.0	.067	.067	.008	.008	.069	.069	.070	.070	.071	.071
55.5	-0.068	-0.069	-0.069	-0.070	-0.070	-0.071	-0.071	-0.072	-0.072	-0.073
56.0	.069	.070	.070	.071	.071	.072	.072	.073	.073	.074
56.5	.071	.071	.072	.072	.073	.073	.074	.074	.075	.075
57.0	.072	.072	.073	.073	.074	.075	.075	.076	.076	.077
57•5	.073	.074	.074	.075	•075	.076	.076	.077	.077	.078
58.0	-0.074	-0.075	-0. 076	-0.076	-0.077	-0.077	-0. 078	-0.078	-0.079	-0.079
58.5	.076	.076	.077	.077	.078	.078	.079	.080	.080	.081
59.0	.077	.078	.078	.079	.079	.080	.080	.081	.081	.082
59.5	.078	.079	.079	.080	.081	.081	.082	.082	.083	.083
60.0	.080	.080	.081	.081	.082	.082	.083	.084	.084	.085
60.5	-o.o81	-0.081	-0.082	-0.083	-0.083	-0.084	-0.084	-0.085	- 0.085	o. o86
61.0	.082	.083	.083	.084	.084	.085	.086	.086	.087	.087
61.5	.083	.084	.085	.085	.086	.086	.087	.087	.088	.089
62.0	.085	.085	.086	.086	.087	.088	.088	.089	.089	.090
62.5	.086	.086	.087	.088	.088	.089	.090	.090	.091	.091
63.0	-0.087	-0. 088	-0.088	-0.089	-0.090	-0.090	-0.091	-0.091	-0.092	-0.093
63.5	.088	.089	.090	.090	.091	.092	.092	.093	.693	•094
64.0	.090	.090	.091	.092	.092	.093	.093	.094	.095	.095
64.5 65.0	.091 .092	.092	.092	.093 .094	.093	.094	.095 .096	.095 .097	.096 .097	.097
	.092	.093	.093	.094	.095	.095	.090		.09/	.090
65.5	-0.093	-0.094	-0.095	-0.095	-0.096	-0.097	-0.097	-0. 098	-0.099	-0.099
66.0 66.5	.095	.095	.096	.097	.097	.098	.099	.099	.100	.101 .102
67.0	.096	.097 .098	.097 .099	.098	.099	.099	.101	.101	.101	.102
67.5	.098	.099	.100	.101	.101	.102	.103	.103	.104	.105
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68.0	-0.100	-0.100	-0.101	-0.102	-0.103	-0.103	-0.104	-0.105	-0.105	-0.106
68.5	.101	.102	.102	.103	.104	.105	.105	.106	.107	.107
69.0 69.5	.102 .104	.103	.104 .105	.104 .106	.105 .106	.106 .107	.107 .108	.107	.108	.109
70.0	.105	.106	.105	.107	.108	.109	.109	.110	.111	.112
70.5	-0.106	-o. 107	-0.108	-0.108	-0.109	-0.110	-0.111	-0.111	-0.II2	-0.113
71.0	.107	.108	.109	.110	011.	.111	.112	.113	.113	.114
71.5	.109	.109	.11ó	.111	.112	.112	.113	.114	.115	.116
72.0	.110	.111	.111	.112	.113	.114	.115	.115	.116	.117
72.5	.111	.112	.113	.113	.114	.115	.116	.117	.117	.118
73.0	-0.112	-0.113	-0.114	-0.115	-0.116	-0.116	-0.117	-0.118	-0.119	-o.120
73.5	.114	.114	.115	.116	.117	.118	.118	.119	.120	,121
74.0	.115	.116	.117	.117	.118	.119	.120	.121	.121	.122
74.5	.116	.117	.118	.119	.119	.120	.121	.122 .123	.123 .124	.124 .125
75.0	•••/	.110	•119	.120	••••			23	•••4	•••5

Attached	THE PARTY OF MANY PARTY OF THE									
Ther- mometer	HEIGHT OF THE BAROMETER IN INCHES.									
Fahren- heit.	28.0	28.2	28.4	28 6	28 8	29.0	29.2	29.4	29.6	29.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
75°5	-0.119	-0.119	-0.120	-0.121	-0,122	-0.123	-0.124	-o. 125	-0.125	-0.126
76.0	.120	.121	.122	.122	.123	.124	.125	.126	.127	.128
76.5	.121	.122	.123	.124	.125	.125	.126	.127	.128	.129
77.0 77.5	.122 .124	.123	.124	.125	.126	.127	.128	.129	.131	.130 .132
78.0	-0.125	- 0.126	-0.127	-0.128	-0. 129	-0. I29	-0.130	-0.131	-0.132	-0.133
78.5	.126	.127	.128	.129	.130	.131	.132	.133	.133	.134
79.0	.127	.128	.129	.130	.131	.132	.133	.134	.135	.136
79.5	.129	. 130	.131	.131	.132	•133	.134	· 135	.136	.137
80.0	.130	.131	.132	.133	•134	.135	.136	.136	.137	.138
80.5	-0.131	-0.132	-0.133	-0.134	-0.135	-0.136	-o.137	-0.138	-0.139	-0.140
81.0	.132	.133	.134	•135	.136	.137	.138	.139	.140	.141
81.5	.134	.135	.136	.137	.138	.139	.139	.140	.141	.142
82.0	.135	.136	.137	.138	.139	.140	.141	.142	.143	.144
82.5	.136	.137	.138	.139	.140	.141	.142	.143	.144	.145
83.0	-0.138	-0.139	-0.139	-0.140	-0.141	-0.142	-0.143	-0.144	-o. 145	-0.146
83.5	.139	.140	.141	.142	.143	.144	.145	.146	.147	.148
84.0	.140	.141	.142	.143	.144	.145	.146	.147	.148	.149
84.5	.141	.142	.143	.144	•145	.146	.147	.148	.149	.150
85.0	.143	.144	.145	.146	.147	.148	.149	.150	.151	.152
85.5	-0.144	-0.145	-0.146	-0.147	-0.148	-0.149	-0.150	-0.151	-0.152	-o.153
86.0	.145	.146	.147	.148	.149	.150	.151	.152	.153	.154
86.5	.146	.147	.148	.149	.151	.152	.153	.154	.155	.156
87.0	.148	.149	.150	.151	.152	.153	.154	.155	.156	.157
87.5	.149	.150	.151	.152	.153	.154	.155	.156	.157	.158
88.0	-0.150	-0.151	-0.152	-0.153	-0.154	-o.155	-0.157	-o.158	-0.159	-0.160
88.5	.151	.152	.154	.155	.156	.157	.158	.159	.160	.161
89.0	.153	.154	.155	.156	.157	.158	.159	.160	.161	.162
89.5	.154	.155	.156	.157	.158	.159	.160	.162	.163	.164
90.0	.155	.156	.157	.158	.160	.161	.162	.163	.164	.165
90.5	-0.156	-0.1 <u>5</u> 7	-0.159	-0.160	-0.161	-o. 162	-0.163	- 0. 164	-0.165	 0. 166
91.0	.158	.159	.160	.161	.162	.163	.164	.166	.167	.168
91.5	.159	.160	.161	.162	.163	.165	.166	.167	. 168	.169
92.0	.160	.161	.162	.164	.165	.166	.167	.168	.169	.170
92.5	.161	.163	.164	.165	.166	. 167	.168	.169	.171	.172
93.0	-0.163	-0.164	-0.165	-0.166	-0.167	-o. 168		-0.171	-0.172	-0.173
93.5	.164	.165	.166	.167	.169	.170	.171	.172	.173	.174
94.0	.165	.166	.168	.169	.170	.171	.172	.173	.175	.176
94.5	.166	.168	.169	.170	.171	.172	.174	.175	.176	.177
95.0	.168	.169	.170	.171	.172	.174	.175	.176	.177	.178
95.5	-0.169		-0.171	-0.173	-0.174			-0.177	-0.179	-0.180
96.0	.170	.171	.173		.175	.176	.177	.179	.180	.181
96.5	.171	.173	.174	.175	.176	.178	.179	.181	.183	.182 .184
97.0 97.5	.173 .174	.174	.175	.176 .178	.178	.179 .180	.181	.183	.184	.185
!					-0.180	-o.181	-0. 183	-0.184	-0.185	– 0. 186
98.0	—o. 175	-0.176	-0.178	-0.179	-0.180	.183	-0.183 .184	.185	.187	.188
98.5	.176	.178	.179	.180 .182	.183	.184	.185	.187	.188	.189
99.0	.178 .179	.179	.182	.183	.184	.185	.187	.188	.189	.199
99.5	.179	.182	.183	.184	.185	.187	.188	.189	.191	.192
100,0		.102	.103	.104		,		,		3=

	ENGLISH WEASURES.									
Attached Ther- mometer	HEIGHT OF THE BAROMETER IN INCHES.									
Fahren- heit.	29.8	30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0.0	+0.078	+0.078	+0.079	+0.079	+0.080	+0.080	+0.081	+0.081	+0.082	+0.082
0.5	+0.076	+0.077	+0.077	+0.078	+0.078	+0.079	+0.079	+0.080	+0.080	+0.081
1.0	.075	.076	.076	.077	.077	.078	.078	.079	.079	.080
1.5	.074	.074	.075	.075	.076	.076	.077	.077	.078	.078
2.0	.072	.073	.073	.074	.074	.075	.075	.076	.076	.077
2.5	.071	.071	.072	.072	.073	.073	.074	1	.075	075
		+0.070				+0.072				+0.074
3.5 4.0	.068 .067	.069	.069	.070	.070	.070	.071	.071 .070	.072	.072 .071
4.5	.065	.066	.066	.067	.067	.068	.068	.069	.069	.069
5.0	.064	.065	.065	.065	.066	.066	.067	.067	.068	.068
5.5	+0.062	+0.063	+0.06₄	+0.064	+0.064	+0.065	+0.065	+0.066	+0.066	+0.067
6.0	.061	.062	.062	.063	.063	.063	.064	.064	.065	.065
6.5	.060	.060	.061	.061	.062	.062	.062	.063	.063	.064
7.0	.059	.059	.059	.060	.060	.061	.061	.061	.062	.062
7.5	.057	.058	.058	.058	.059	.059	.060	.060	.060	.061
8.0	+0.056	+0.056	+0.057	+0.057	+0.057	+0.058	+0.058	+0.059	+0.059	+0.059
8.5	.055	.055	.055	.056	.056	.056	.057	.057	.058	.058
9.0	.053	.054	.054	.054	.055	.055	.055	.056	.056	.056
9.5 10.0	.052	.052	.053 .051	.053 .052	.053	.054 .052	.054 .053	.054	.055	.055 .054
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10.5 11.0		+0.049 .048								+0.052
11.5	.048	.048	.048 .047	.049 .047	.049 .048	.049 .048	.050	.050	.050	.051
12.0	.045	.045	.046	.046	.046	.047	.047	.047	.048	.049
12.5	.044	.044	.044	.045	.045	.045	.045	.046	.046	.046
13.0	+0.042	+0.043	+0.043	+0.043	+0.044	+0.044	+0.044	+0.044	+0.045	+0.045
13.5	.041	.041	.042	.042	.042	.042	.043	.043	.043	.043
14.0	.040	.040	.040	.040	.041	.041	.041	.042	.042	.042
14.5	.038	.039	.039	.039	.039	.040	.040	.040	.040	.041
15.0	.037	.037	.037	.038	.038	.038	.038	.039	.039	.039
15.5		+0.036				+0.037				+0.038
16.0	.034	.034	.035	.035	.035	.035	.036	.036	.036	.036
16.5 17.0	.033	.033	.033	.034	.034	.034	.034	.034	.035	.035
17.5	.032	.030	.031	.031	.031	.031	.031	.033	.032	.033
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18.0 18.5	+0.029 .027	+0.029	.028	.028	+0.030	+0.030	.029	+0.030	.029	+0.031 .029
19.0	.026	.026	.026	.027	.027	.027	.029	.029	.029	.029
19.5	.025	.025	.025	.025	.025	.026	.026	.026	.026	.026
20.0	.023	.024	.024	.024	.024	.024	.024	.024	.025	.025
20.5	- 0.022	+0.022	+0.022	+0.022	+0.023	+0.023	+0.023	+0.023	+0.023	+0.023
21.0	.021	.021	.021	.021	.021	.021	.022	.022	.022	.022
21.5	.019	.019	.020	.020	.020	.020	.020	.020	.020	.020
22.0 22.5	.018 .017	.018	.018	.018	.018	.019	.019	.019	.019	.019 810.
ti i	•					[1			
23.0	+0.015		+0.015		+0.016			+0.016		+0.016
23.5 24.0	.014 .013	.014	.014	.014	.014	.014	.014	.015	.015	.015
24.5	.013	.013	.013	.013	.013	.012	.013	.013	.013	.013
25.0	.010	.010	.010	.010	.010	.010	.010	.010	0.10	.010
L		1	<u> </u>	!	<u> </u>	<u> </u>	I .			1

Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETI	R IN I	NCHES.		
Fahren- heit.	29.8	30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
25.5	+0.008	+0.009	+0.009	+0.009	+0.009	+0.009	+0.009	+0.009	+0.009	+0.009
26.0	.007	.007	.007	.007	.007	.007	.007	.007	.008	.008
26.5	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
27.0	.004	.004	.004	.005	.005	.005	.005	.005	.005	.005
27.5	.003	.003	,003	,003	.003	.003	.003	.003	.003	.003
28.0	+0,002	+0.002	+0.002	+0,002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002
28.5	0.000	0,000	0.000	0.000	0.000	0,000	0,000	0.000	0.000	0.000
29.0	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
29.5	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
30.0	.004	.004	.004	.004	,004	.004	.004	.004	.004	.004
30.5	0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005
31.0	.006	.006	•006	.007	.007	.007	.007	.007	.007	.007
31.5	.008	.008	.008	.008	.008	,008	.008	.008	.008	.008
32.0	.009	.009	.009	.009	.009	.009	.009	.010	.oro	.010
32.5	.010	.011	.011	.011	.011	.011	.011	110.	.011	.011
33.0	-0.012	-0.012	-0.012	-0.012	-0,012	-0.012	-0.012	-0.012	-0.012	-o.or3
33.5	.013	.or3	.013	.013	.014	.014	.014	.014	.014	.014
34.0	.015	.015	.015	.015	.015	.015	.015	.015	.015	.015
34.5	.016	.016	.016	.016	.016	.016	.017	.017	.017	.017
35.0	.017	.017	.017	.018	.018	.018	.018	.018	.018	.018
35.5	-0.019	-0.019	-0.019	-0.019	-0,019	-0.019	-0.019	-0.019	-0.020	-0.020
36.0	.020	.020	.02Ó	.020	.020	.021	.021	.021	.021	.021
36.5	.021	.021	.022	.022	.022	.022	.022	.022	.022	.023
37.0	.023	.023	.023	.023	.023	.023	.024	.024	.024	.024
37-5	.024	.024	.024	.024	.025	.025	.025	.025	.025	.025
38.0	-0.025	-0.026	-0.026	-0.026	-0.026	-0.026	-0.026	-0.027	-0.027	-0.027
38.5	.027	.027	.027	.027	.027	.028	.028	.028	.028	.028
39.0	.028	.028	.028	.029	.029	.029	.029	.029	.030	.030
39.5	.029	.030	.030	.030	.030	.030	.031	.031	.031	.031
40.0	.031	.031	.031	.031	.032	.032	.032	.032	.032	.033
40.5	-0.032	-0.032	-0.033	-0.033	-0.033	-0.033	-0.033	-0.034	-0.034	-0.034
41.0	.033	.034	.034	.034	.034	.035	.035	.035	.035	.035
41.5	.035	.035	.035	.035	.036	.036	.036	.036	.037	.037
42.0	.036	.036	.037	.037	.037	.037	.038	.038	.038	.038
42.5	.037	.038	.038	.038	.038	•039	.039	.039	•040	.040
43.0	-0.039	-0.039	-0.039	-0.040	-0.040	-0.040	-0.040	-0.041	-0.041	-0.04T
43.5	.040	.040	.041	.041	.041	.042	.042	.042	.042	.043
44.0	.042	.042	.042	.042	.043	.043	.043	.043	.044	.044
44.5	.043	.043	.043	.044	.044	.044	.045	.045	.045	.045
45.0	.044	.045	.045	.045	.045	.046	.046	.046	.047	.047
	-0.046	-0.046	-0.046	-0.047	-0.047	-0.047	-0.047	-0.048	-0.048	-0.048
46.0	.047	.047	.048	.048	.048	.049	.049	.049	.049	.050
46.5	.048	.049	.049	.049	.050	.050	.050	.051	.051	.051
47.0	.050	.050	.050	.051	.051	.051	.052	.052	.052	.053
47.5	.051	.051	.052	.052	.052	.053	.053	.053	.054	•054
48.0	-0.052 -	-0.053	-0.053	-0.053	-0.054	- 0.054	-0.054 ·	-0.055	-0.055	-0.055
48.5	.054	.054	.054	.055	.055	.055	.056	.056	.057	.057
49.0	.055	.055	.056	.056	.057	.057	.057	.058	.058	.058
49.5	.056	.057	.057	.058	.058	.058	.059	.059	.059	.060
50.0	.058	.058	.058	.059	.059	.060	.060	.060	.061	.061

Attached Ther- mometer			HEIG	нт ог	THE BA	ROMETE	R IN II	iches.		
Fahren- heit.	29.8	30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
50°5	-0.059	-0.059	-0.060	- 0.060	-0.061	-0.061	-0.061	-0.062	-0.062	-o.o <u>6</u> 3
51.0	.060	.061	.061	.062	.062	.062	.063	.063	.064	.064
51.5	.062	.062	.063	.063	.063	.064	.064	.065	.065	.065
52.0	.063 .064	.064 .065	.064	.064 .066	.065	.065 .067	.066 .067	.066 .067	.066 .068	.067 .068
52.5		_		. 1						
53.0	-0.066	-o.o66	-0.067	-0.067	- 0.068	-0.068	o.o68	-0.069	-0.069	-0.070
53 5	.067 .068	.068	.068	.069	.069	.069 .071	.070 .071	.070 .072	.071 .072	.071
54.0	.070	.070	.071	.071	.072	.072	.073	.073	.074	.074
5 4 -5 55.0	.071	.072	.072	.073	.073	.074	.074	.075	.075	.075
55.5				-0.074	-0.074	-0.075	-0.075	-0.076	-0.076	-0.077
56.0	-0.073 .074	-0.073 .074	-0.074 .075	.075	.076	.076	.077	.077	.078	.078
56.5	.074	.074	.076	.073	.077	.078	.078	.079	.079	.080
57.0	.073	.077	.078	.078	.079	.079	.080	.080	.081	.081
57.5	.078	.078	.079	.079	.080	.081	.081	.082	.082	.083
58.0	-0.079	-o.o8o	-0.080	-0.081	-o.o81	-0.082	-0.082	-0.083	-0.084	-0.084
58.5	.081	.081	.082	.082	.083	.083	.084	.084	.085	.085
59.0	.082	.083	.083	.084	.084	.085	.085	.086	.086	.087
59-5	.083	.084	.084	.085	.086	.086	.087	.087	.088	.088
60.0	.085	.085	.086	.086	.087	.087	.088	.089	.089	.090
60.5	-0.086	-0.087	-0.087	-0.088	-0.088	-0.089	-0.089	-0.090	-0.091	-0.091
61.0	.087	.088	.089	.089	.090	.090	.091	.091	.092	.093
61.5	.089	.089	.090	.090	.091	.092	.092	.093	.093	.094
62.0	.090	.091	.091	.092	.092	.093	.094	.094	.095	.095
62.5	.091	.092	.093	.093	•094	.094	.095	.096	.096	.097
63.0	0.093	-0.093	-0.094	-0.095	-0.095	-0.096	-0.096	-0.097	-0.098	-0.098
63.5	.094	.095	.095	.096	.097	.097	.098	.098	.099	.100
64.0	.095	.096	.097	.097	.098	.099	.099	.100	.101	.101
64.5	.097	.097	.098	.099	.099	.100	.101	.IOI	.102	.103
65.0	.098	.099	.099	.100	.101	.101	,IO2	.103	.103	.104
65.5	-0.099	-0.100	-0,101	-0,101	-0.102	-0.103	-0.103	-o. 104	-0.105	-0.105
66.0	.iói	.101	.102	.103	.103	.104	.105	.106	.106	.107
66.5	.102	.103	.103	.104	.105	.106	.106	.107	.108	.108
67.0	.103	.104	.105	.106	.106	.107	.108	.108	.109	.110
67.5	.105	.106	.106	.107	.108	.108	.109	.IIO	.IIO	.111
68.0	-0.106	-0.107	-0.108	-0.108	-0.109	-0.110	-0.110	-o.III	-0.112	-0.113
68.5	.107	.108	.109	.110	.110	.111	.112	.113	.113	.114
69.0	.109	.110	.110	.111	.112	.112	.113	.114	.115	.115
69.5	.110	.111	.112	.112	.113	.114	.115	.115	.116	.117
70.0	.112	.112	.113	,	.115	.115	.110		.11/	.110
70.5	-0.113	-0.114	-0.114	-0.115	-0.116	-0.117	-0.117	-0.118	-0.119	-0.120
71.0	.114	.115	.116	.116	.117	.118	.119	.120 .121	.120	.121
71.5 72.0	.116	.118	.117	.119	.119	.119	.120	.121	.123	.123
72.5	.118	.119	.120	.121	.121	.122	.123	.124	.125	.125
73.0	-0.120	-0.120	-0.121	-0.122	-0.123	-0.124	-0.124	-0.125	-0.126	-0.127
73.5	.121	.122	.123	.123	.124	.125	.126	.127	.127	.128
74.0	.121	.122	.123	.125	.126	.126	.127	.128	.129	.130
74.5	.124	.124	.125	.126	.127	.128	.129	.129	.130	.131
75.0	.125	.126	.127	.127	.128	.129	.130	.131	.132	.132
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1				ENGLIS		ASURES				
Attached Ther- mometer			HEIG	HT OF T	HE BAR	OMETE	R IN IN	CHES.		
Fahren- heit.	29.8	30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
75°5	-o. 126	-0.127	-0.12 8	-0.129	-0.130		-0.131	-o.132	-o.133	- 0.134
76.0	.128	.128	.129	.130	.131	.132	.133	.134	.134	•135
76.5	.129	.130	.131	.132	.132	.133	.134	135	.136	.137
77.0	.130	.131	.132	.133	.134	.135	.136	.136	.137	.138
77.5	.132	.133	.133	.134	.135	.136	.137	.138	.139	.140
78.0	-0.133	-0.134	-0.135	-0.136	-0. 137	-0.137	-0.138	-o.139	-0.140	-0.141
78.5	.134	.135	.136	.137	.138	.139	.140	.141	.142	.142
79.0	.136	.137	.137	.138	.139	.140	.141	.142	.143	.144
79.5	.137	.138	.139	.140	.141	.142	.143	.143	.144	.145
80.0	.138	.139	.140	.141	.142	•143	.144	.145	.146	.147
80.5	-0. 140	-0.141		-0.142	-0.143	-0.144	- 0.145	-0.146	-o.147	- 0.148
81.0	.141	.142	.143	.144	.145	.146	.147	.148	.149	.150
81.5	.142	.143	.144	.145	.146	.147	.148	.149		.151
82.0	.144	.145	.146	.147	.148	.149	.149	.150	.151	.152
82.5	•145	.146	.147	.148	.149	.150	.151	.152	•153	•154
83.0	-0. 146	-0.147	-0.148	-0.149	-0.150	-0.151	-0.152	0.153	-0.154	-0.155
83.5	.148	.149	.150	.151	.152	.153	.154	.155	.156	.157
84.0	.149	.150	.151	.152	.153	.154	.155	.156	.157	.158
84.5	.150	.151	.152	.153	.154	.155	.156	.157	.158	.159
85.0	.152	.153	.154	.155	.156	.157	.158	.159	.160	.161
85.5	-0.153	-0.154	-0.155	-0.156	-0.157	-o.158	- 0.159	- 0.160	-0.161	-o.162
86.o	.154	.155	.156	.158	.159	.160	.161	.162	.163	.164
86.5	.156	.157	.158	.159	.160	.161	.162	.163	.164	.165
87.0	.157	.158	.159	.160	.161	.162	.163	.164	.166	.167
87.5	.158	.159	.161	.162	.163	.164	.165	.166	.167	.168
88.0	-0.160	-0.161		-0.163				- 0.167	-0. 168	-0.169
88.5	.161	.162	.163	.164	.165	.166	.168	.169	.170	.171
89.0	.162	.164	.165	.166	.167	.168	.169	.170	.171	.172
89.5	.164	.165	.166	.167	.168	.169	.170	.171	.173	.174
90.0	.165	.166	.167	.168	.170	.171	.172	.173	.174	.175
90.5	-0.166	-0.168		-0.170		- 0.172		-0.174	-0.175	-0.176
91.0	.168	.169	.170	.171	.172	.173	•175	.176	.177	.178
91.5	.169	.170	.171	.173	.174	·175	.176	.177.	.178	.179
92.0	.170	.172	.173	.174	.175	.176	.177	.178	.180	.181
92.5	.172	.173	.174	•175	.176	.178	•179	.180	.181	.182
93.0	-0.173	-0.174	-0.175	-0.177	-0. 178	- 0.1 <u>7</u> 9	-0.180	-0.181		-o.184
93.5	.174	.176		.178	.179	.180	.181	.183	.184	.185
94.0	.176	.177	.177 .178	.179	.180	.182				.186
94.5	.177	.178	.179	.181	.182	.183	.184	.185	.187	.188
95.0	.178	.180	.181	.182	.183	.184	.186	.187	.188	.189
95.5	-0.180	-0.181	-0.182	-0.183	-o.185	-o.186	-o.187	o, 188	-0.189	
96.0	.181	.182	.184	.185	.186		.188			
96.5	.182	.184	.185	.186	.187	.189	.190	.191	.192	.193
97.0	.184	.185	.186	.187	.189	.190	.191	.192	.194	.195
97.5	.185	.186	.188	.189	.190	.191	.193	.194	.195	.196
98.0	-o.186	-0.188	-0.189	-0.190	-0.191	-0.193	-0.194	-0.195	-0.196	-0.198
98.5	.188	.189	.190	.192	.193	.194	.195	.197	.198	.199
99.0	.189	.190	.192	.193	.194	.195	.197	.198	.199	.201
99.5	.190	.192	.193	.194	.196	.197	.198	.199	.201	.202
100.0	.192	.193	.194	.196	•197	.198	.200	.201	.202	.203
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FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION TO BE SUBTRACTED.

Attached Ther-			F	EIGHT	OF T	не ва	ROMET	ER IN	MILLI	метен	RS.		
mometer Centi- grade.	440	450	460	470	480	490	500	510	520	530	540	550	560
c.	mm. mm.	mm.	mm.	mm.									
0:0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.5	.04	.04	.04	.04	.04	.04	.04	.04 .08	.04 .08	.04	.04	.04	.05
1.0	.07	.07	.08	.08	.08	.08	.08	.12	.13	.09	.09 .13	.09	.09 .14
1.5 2.0	.14	.15	.15	.15	.16	.16	.16	.17	.17	.17	.18	.18	.18
2.5	0.18	0.18	0.19	0.19	0.20	0.20	0.20	0.21	0.21	0.22	0.22	0.22	0.23
3.0 3.5	.22 .25	.22	.23 .26	.23	.24	.24	.24	.29	.30	.30	.31	.31	.32
3.3 4.0	.29	.29	.30	.31	.31	.32	.33	.33	.34	-35	.35	.36	.37
4.5	.32	∙33	•34	•35	.35	.36	•37	∙37	.38	∙39	.40	.40	.41
5.0	0.36	0.37	0.38	0.38	0.39	0.40	0.41	0.42	0.42	0.43	0.44	0.45	0.46
5.5 6.0	.40	.40	.41	.42 .46	·43 ·47	.44 .48	·45	.46 .50	.47 .51	.48 .52	.48 .53	.49 .54	.50 ∙55
6.5	·43 ·47	·44 .48	·45	.50	.51	.52	.53	.54	.55	.56	.57	.58	.59
7.0	.50	.51	∙53	.54	.55	.56	-57	.58	•59	.61	.62	.63	.64
7.5	0.54	0.55	0.56	0.58	0.59	0.60	0.61	0.62	0.64	0.65	0.66	0.67	0.69
80	.57	.59	.60 .64	.61	.63	.64 .68	.65	.67 .71	.68 .72	.69	.70 ·75	.72 .76	·73 ·78
8.5 9.0	.61 .65	.66	.68	.65 .69	.67	.72	.73	·75	.76	·73 ·78	.79	.81	.82
9.5	.68	.70	.71	.73	.74	.76	.77	.79	.81	.82	.84	.85	.87
10.0	0.72	0.73	0.75	0.77	0.78	0.80	0.82	0.83	0.85	0.86	o.88	0.90	0.91
10.5	.75	.77 .81	.79	.8o .84	.82	.84 .88	.86	.87 .91	.89	.91 •95	.92 .97	·94	.96 1.00
11.0 11.5	.79 .83	.84	.86	.88	.90	.92	.94	.96	.98	.99	1.01	1.03	1.05
12.0	.86	.88	.90	.92	•94	.96	.98	1.00	1.02	1.04	1.06	1.08	1.10
13.0	0.93	0.95	0.97	1.00	1.02	1.04	1.06	1.08	1.10	1.12	1.14	1.17	1.19
14.0	1.00	1.03	1.05	1.07	1.10	I.12 I.20	I.14 I.22	1.16	1.19	I.2I I.30	I.23 I.32	I.25 I.34	1.28 1.37
15.0 16.0	1.08	I IO	I.I2 I.20	1.15	I.17 I.25	1.28	1.30	1.33	1.36	1.38	1.41	1.43	1.46
17.0	1.22	1.25	1.27	1.30	1.33	1.36	1.38	1.41	1.44	1.47	1.50	1.52	1.55
18.0	1.29	1.32	1.35	1.38	1.41	1.44	1.47	1.50	1.52	1.55	1.58	1.61	1.64
19.0	1.35	1.39	1.42	1.45	1.49	1.52	1.55	1.58	1.61	1.64 1.73	1.67 1.76	1.70 1.79	1.73 1.82
20.0 21.0	1.43	I.47 I.54	1.50	1.53	1.56	1.67	1.71	1.74	1.78	1.81	1.85	1.88	1.91
22.0	1.58	1.61	1.65	1.68	1.72	1.75	1.79	1.83	1.86	1.90	1.93	1.97	2.01
23.0	1.65	1.68	1.72	1.76	1.80	1.83	1.87	1.91	1.95	1.98	2.02	2.06	2.10
24.0	1.72	1.76	1.80	1.84	1.87	1.91	1.95	1.99	2.03	2.07	2.11	2.15	2.19
25.0 26.0	1.79	1.83	1.87	1.91	2.03	1.99	2.03	2.07 2.16	2.11	2.16 2.24	2.20 2.28	2.24	2.28 2.37
20.0 27.0	1.86	1.98	1.95 2.02	1.99 2.06	2.11	2.15	2.20	2.24	2.28	2.33	2.37	2.41	2.46
28.0	2.00	2.05	2.09	2.14	2.18	2.23	2.28	2.32	2.37	2.41	2.46	2.50	2.55
29.0	2.07	2.12	2.17	2.22	2.26	2.31	2.36	2.40		2.50	2.55	2.59	2.64
30.0	2.15	2.19	2.24	2.29	2.34	2.39	2.44	2.49 2.57	2.54	2.58 2.67	2.63	2.68	2.73
31.0 32.0	2.22 2.29	2.27 2.34	2.32	2.37 2.44	2.42	2.55	2.60	2.65	2.70	2.76	2.81	2 86	2.91
33.0	2.36	2.41	2.47	2.52	2.57	2.63	2.68	2.73	2.79	2.84	2.89	2.95	3.00
34.0	2.43	2.48	2.54	2.60	2.65	2.71	2.76	2.82		2.93 -3.01	2.98	3.04	3.09 3.18
35.0	2.50	2.55	2.61	2.67	2.73	2.78	2.04	2.90	2.93	3.01	.3.07	3.13	3,10

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	EIGHT O	F THE B		ER	н	EIGHT O	F THE B		ER
Attached Ther- mometer.	0:0	0°2	0°4	0°6	0°8	0:0	0°2	0°4	0°6	0°8
c. 0° 1 2 3 4	mm. 0.00 .09 .18 .27 .37	mm. 0.02 .11 .20 .29	mm. 0.04 .13 .22 .31 .40	mm. 0.05 .15 .24 .33 .42	mm. 0.07 .16 .26 .35	mm. 0.00 .09 .19 .28	mm. 0.02 .11 .20 .30	mm. 0.04 .13 .22 .32 .41	mm. 0.06 .15 .24 .34 .43	mm. 0.07 .17 .26 .35 .45
5 6 7 8 9	0.46 •55 •64 •73 •82	0.48 •57 .66 •75	0.49 .58 .68 .77 .86	0.51 .60 .69 .79 .88	0.53 .62 .71 .80	0.47 .56 .65 .74 .84	0.48 .58 .67 .76 .86	0.50 .60 .69 .78 .87	0.52 .61 .71 .80 .89	0.54 .63 .73 .82
10 11 12 13 14	0.91 1.00 1.10 1.19 1.28	0.93 1.02 1.11 1.20 1.30	0.95 1.04 1.13 1.22 1.31	0.97 1.06 1.15 1.24 1.33	0.99 1.08 1.17 1.26 1.35	0.93 1.02 1.12 1.21 1.30	0.95 1.04 1.13 1.23 1.32	0.97 1.06 1.15 1.25 1.34	0.99 1.08 1.17 1.26 1.36	1.00 1.10 1.19 1.28 1.37
15 16 17 18 19	1.37 1.46 1.55 1.64 1.73	1.39 1.48 1.57 1.66 1.75	1.41 1.50 1.59 1.68	1.42 1.51 1.61 1.70 1.79	1.44 1.53 1.62 1.71 1.81	1.39 1.49 1.58 1.67 1.76	1.41 1.50 1.60 1.69 1.78	1.43 1.52 1.62 1.71 1.80	1.45 1.54 1.63 1.73 1.82	1.47 1.56 1.65 1. 7 5 1.84
20 21 22 23 24	1.82 1.91 2.01 2.10 2.19	1.84 1.93 2.02 2.11 2.20	1.86 1.95 2.04 2.13 2.22	1.88 1.97 2.06 2.15 2.24	1.90 1.99 2.08 2.17 2.26	1.86 1.95 2.04 2.13 2.23	1.87 1.97 2.06 2.15 2.24	1.89 1.99 2.08 2.17 2.26	1.91 2.00 2.10 2.19 2.28	1.93 2.02 2.11 2.21 2.30
25 26 27 28 29	2.28 2.37 2.46 2.55 2.64	2.30 2.39 2.48 2.57 2.66	2.31 2.40 2.49 2.59 2.68	2.33 2.42 2.51 2.60 2.69	2.35 2.44 2.53 2.62 2.71	2.32 2.41 2.50 2.59 2.69	2.34 2.43 2.52 2.61 2.71	2.35 2.45 2.54 2.63 2.72	2.37 2.47 2.56 2.65 2.74	2.39 2.48 2.58 2.67 2.76
30 31 32 33 34	2.73 2.82 2.91 3.00 3.09	2.75 2.84 2.93 3.02 3.11	2.77 2.86 2.95 3.04 3.13	2.78 2.87 2.97 3.06 3.15	2.80 2.89 2.98 3.07 3.16	2.78 2.87 2.96 3.06 3.15	2.80 2.89 2.98 3.07 3.17	2.82 2.91 3.00 3.09 3.18	2.83 2.93 3.02 3.11 3.20	2.85 2.94 3.04 3.13 3.22
35	3.18	3.20	3.22	3.24	3.25	3.24	3.26	3.28	3.29	3.31

TABLE 47.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н		F THE B	AROMET	ER	н	EIGHT O	F ТНЕ В i 90 m n		ER
Attached Ther- mometer.	0:0	0°2	0°.4	0:6	0:8	0:0	0°2	0?4	0.6	0°8
C 0° 1 2 3 4 5	mm. 0.00 .09 .19 .28 .38 0.47 .57	mm. 0.02 .11 .21 .30 .40 0.49 .59	mm. 0.04 .13 .23 .32 .42 0.51	mm. 0.06 .15 .25 .34 .44 0.53	mm. 0.08 .17 .27 .36 .45	mm. 0.00 .10 .19 .29 .39 0.48 .58	mm. 0.02 .12 .21 .31 .40 0.50 .60	mm. 0.04 .13 .23 .33 .42 0.52 .62	mm. 0.06 .15 .25 .35 .44 0.54	mm. 0.08 .17 .27 .37 .46 0.56
7	.66	.68	.70	.72	•74	.67	.69	.71	.73	•75
8	.76	.78	.79	.81	•83	•77	.79	.81	.83	.85
9	.85	.87	.89	.91	•93	.87	.89	.90	.92	•94
10	0.95	0.96	0.98	1.00	1.02	0.96	0.98	1.00	1.02	1.04
11	1.04	1.06	1.08	1.10	1.12	1.06	1.08	1.10	1.12	1.14
12	1.13	1.15	1.17	1.19	1.21	1.15	1.17	1.19	1.21	1.23
13	1.23	1.25	1.27	1.29	1.30	1.25	1.27	1.29	1.31	1.33
14	1.32	1.34	1.36	1.38	1.40	1.35	1.37	1.38	1.40	1.42
15	1.42	1.44	1.46	1.47	1.49	1.44	1.46	1.48	1.50	1.52
16	1.51	1.53	1.55	1.57	1.59	1.54	1.56	1.58	1.60	1.61
17	1.61	1.62	1.64	1.66	1.68	1.63	1.65	1.67	1.69	1.71
18	1.70	1.72	1.74	1.76	1.78	1.73	1.75	1.77	1.79	1.81
19	1.79	1.81	1.83	1.85	1.87	1.83	1.84	1.86	1.88	1.90
20	1.89	1.91	1.93	1.95	1.96	1.92	1.94	1.96	1.98	2.00
21	1.98	2.00	2.02	2.04	2.06	2.02	2.04	2.06	2.07	2.09
22	2.08	2.10	2.11	2.13	2.15	2.11	2.13	2.15	2.17	2.19
23	2.17	2.19	2.21	2.23	2.25	2.21	2.23	2.25	2.27	2.28
24	2.26	2.28	2.30	2.32	2.34	2.30	2.32	2.34	2.36	2.38
25	2.36	2.38	2.40	2.41	2.43	2.40	2.42	2.44	2.46	2.48
26	2.45	2.47	2.49	2.51	2.53	2.49	2.51	2.53	2.55	2.57
27	2.55	2.57	2.58	2.60	2.62	2.59	2.61	2.63	2.65	2.67
28	2.64	2.66	2.68	2.70	2.72	2.69	2.70	2.72	2.74	2.76
29	2.73	2.75	2.77	2.79	2.81	2.78	2.80	2.82	2.84	2.86
30	2.83	2.85	2.87	2.88	2.90	2.88	2.90	2.91	2.93	2.95
31	2.92	2.94	2.96	2.98	3.00	2.97	2.99	3.01	3.03	3.05
32	3.02	3.03	3.05	3.07	3.09	3.07	3.09	3.11	3.12	3.14
33	3.11	3.13	3.15	3.16	3.18	3.16	3.18	3.20	3.22	3.24
34	3.20	3.22	3.24	3.26	3.28	3.26	3.28	3.30	3.31	3.33
35	3.30	3.3I	3.33	3.35	3.37	3.35	3.37	3-39	3.41	3.43

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O'-CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	H		г тне в 00 mm		ER	H	EIGHT O	F THE B		ER
Attached Ther- mometer.	0:0	0°2	0°.4	0:6	0:8	0:0	0°2	0°.4	0 °6	0:8
C. 0° 1 2	mm. 0.00 .10 .20	mm. 0.02 .12 .22 .31	mm. 0.04 .14 .24 .33	mm. 0.06 .16 .25	mm. 0.08 .18 .27	mm. 0.00 .10 .20	mm. 0.02 .12 .22 .32	mm. 0.04 .14 .24 .34	mm. 0.06 .16 .26 .36	mm. 0.08 .18 .28 .38
4 5 6 7 8	.39 0.49 .59 .69 .78	.41 0.51 .61 .70 .80	.43 0.53 .63 .72 .82	.45 0.55 .65 .74 .84	.47 0.57 .67 .76 .86	.40 0.49 .59 .69 .79	.41 0.51 .61 .71 .81	.43 0.53 .63 .73 .83	.45 0.55 .65 .75 .85	•47 •57 •67 •77 •87 •97
10 11 12, 13	0.98 1.08 1.17 1.27 1.37	1.00 1.10 1.19 1.29 1.39	1.02 1.12 1.21 1.31 1.41	1.04 1.13 1.23 1.33 1.43	1.06 1.15 1.25 1.35	0.99 1.09 1.18 1.28 1.38	1.01 1.10 1.20 1.30 1.40	1.03 1.12 1.22 1.32 1.42	1.05 1.14 1.24 1.34 1.44	1.07 1.16 1.26 1.36 1.46
15 16 17 18 19	1.47 1.56 1.66 1.76 1.86	1.49 1.58 1.68 1.78 1.88	1.51 1.60 1.70 1.80 1.90	1.53 1.62 1.72 1.82 1.91	1.54 1.64 1.74 1.84 1.93	1.48 1.58 1.68 1.77 1.87	1.50 1.60 1.70 1.79 1.89	1.52 1.62 1.71 1.81 1.91	1.54 1.64 1.73 1.83 1.93	1.56 1.66 1.75 1.85 1.95
20 21 22 23 24	1.95 2.05 2.15 2.25 2.34	1.97 2.07 2.17 2.26 2.36	1.99 2.09 2.19 2.28 2.38	2.01 2.11 2.21 2.30 2.40	2.03 2.13 2.23 2.32 2.42	1.97 2.07 2.17 2.26 2.36	1.99 2.09 2.19 2.28 2.38	2.01 2.11 2.21 2.30 2.40	2.03 2.13 2.23 2.32 2.42	2.05 2.15 2.24 2.34 2.44
25 26 27 28 29	2.44 2.54 2.63 2.73 2.83	2.46 2.56 2.65 2.75 2.85	2.48 2.58 2.67 2.77 2.87	2.50 2.60 2.69 2.79 2.89	2.52 2.61 2.71 2.81 2.91	2.46 2.56 2.66 2.75 2.85	2.48 2.58 2.68 2.77 2.87	2.50 2.60 2.70 2.79 2.89	2.52 2.62 2.71 2.81 2.91	2.54 2.64 2.73 2.83 2.93
30 31 32 33 34	2.93 3.02 3.12 3.22 3.31	2.94 3.04 3.14 3.24 3.33	2.96 3.06 3.16 3.25 3.35	2.98 3.08 3.18 3.27 3.37	3.00 3.10 3.20 3.29 3.39	2.95 3.05 3.15 3.24 3.34	2.97 3.07 3.16 3.26 3.36	2.99 3.09 3.18 3.28 3.38	3.01 3.11 3.20 3.30 3.40	3.03 3.13 3.22 3.32 3.42
35	3.41	3.43	3.45	3-47	3.49	3.44	3.46	3.48	3.50	3.52

TABLE 47.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	H		F THE B		ER	н		F ТНЕ В 615 mm		ER
Attached Ther- mometer.	0:0	0°2	0°4	0°6	0°8	0:0	0°2	0°.4	0.6	0.8
C. 0° 1 2 3 4	mm. 0.00 .10 .20 .30	mm. 0.02 .12 .22 .32 .42	mm. 0.04 .14 .24 .34	mm. 0.06 .16 .26 .36	mm. 0.08 .18 .28 .38 .48	mm. 0.00 .10 .20 .30	mm. 0.02 .12 .22 .32	mm. 0.04 .14 .24 .34	mm. 0.06 .16 .26 .36	mm. 0.08 .18 .28 .38 .48
5 6 7 8 9	0.50 .60 .70 .80	0.52 .62 .72 .82	0.54 .64 .74 .84	0.56 .66 .76 .86	0.58 .68 .78 .88	0.50 .60 .70 .80	0.52 .62 .72 .82 .92	0.54 .64 .74 .84	0.56 .66 .76 .86	0.58 .68 .78 .88 .98
10 11 12 13 14	0.99 1.09 1.19 1.29 1.39	1.01 1.11 1.21 1.31 1.41	1.03 1.13 1.23 1.33 1.43	1.05 1.15 1.25 1.35 1.45	1.07 1.17 1.27 1.37 1.47	1.00 1.10 1.20 1.30 1.40	I.02 I.12 I.22 I.32 I.42	I.04 I.14 I.24 I.34 I.44	1.06 1.16 1.26 1.36 1.46	1.08 1.18 1.28 1.38 1.48
15 16 17 18	1.49 1.59 1.69 1.79 1.89	1.51 1.61 1.71 1.81 1.91	1.53 1.63 1.73 1.83 1.93	1.55 1.65 1.75 1.85 1.95	1.57 1.67 1.77 1.87	1.50 1.60 1.70 1.80 1.90	1.52 1.62 1.72 1.82 1.92	1.54 1.64 1.74 1.84 1.94	1.56 1.66 1.76 1.86 1.96	1.58 1.68 1.78 1.88 1.98
20 21 22 23 24	1.99 2.09 2.18 2.28 2.38	2.01 2.10 2.20 2.30 2.40	2.03 2.12 2.22 2.32 2.42	2.05 2.14 2.24 2.34 2.44	2.07 2.16 2.26 2.36 2.46	2.00 2.10 2.20 2.30 2.40	2.02 2.12 2.22 2.32 2.42	2.04 2.14 2.24 2.34 2.44	2.06 2.16 2.26 2.36 2.46	2.08 2.18 2.28 2.38 2.48
25 26 27 28 29	2.48 2.58 2.68 2.78 2.88	2.50 2.60 2.70 2.80 2.90	2.52 2.62 2.72 2.82 2.91	2.54 2.64 2.74 2.84 2.93	2.56 2.66 2.76 2.86 2.95	2.50 2.60 2.70 2.80 2.90	2.52 2.62 2.72 2.82 2.92	2.54 2.64 2.74 2.84 2.94	2.56 2.66 2.76 2.86 2.96	2.58 2.68 2.78 2.88 2.98
30 31 32 33 34	2.97 3.07 3.17 3.27 3.37	2.99 3.09 3.19 3.29 3.39	3.01 3.11 3.21 3.31 3.41	3.03 3.13 3.23 3.33 3.43	3.05 3.15 3.25 3.35 3.45	3.00 3.10 3.20 3.30 3.40	3.02 3.12 3.22 3.32 3.42	3.04 3.14 3.24 3.34 3.44	3.06 3.16 3.26 3.36 3.46	3.08 3.18 3.28 3.38 3.48
35	3.47	3.49	3.51	3 ⋅53	3-55	3.49	3.51	3 ·53	3.55	3.57

TABLE 47.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	eight oi	г тне в 20 mm		er.	H	еіонт о 6	г тне в 25 mm		ER
Attached Ther- mometer.	0°0	0°2	0:4	0°6	0°8	0:0	0°2	0°4	0:6	0.8
C. 0° 1 2 3 4	mm. 0.00 .10 .20 .30 .40	mm. 0.02 .12 .22 .32 .43	mm. 0.04 .14 .24 .34 .45	mm. 0.06 .16 .26 .36	mm. 0.08 .18 .28 .38 .49	mm. 0.00 .10 .20 .31 .41	mm. 0.02 .12 .22 .33 .43	mm. 0.04 .14 .24 .35 .45	mm. 0.06 .16 .27 .37 .47	mm. 0.08 .18 .29 •39 •49
5 6 7 8 9	0.51 .61 .71 .81	0.53 .63 .73 .83 .93	0.55 .65 .75 .85 .95	0.57 .67 .77 .87	0.59 .69 .79 .89	0.51 .61 .71 .82 .92	0.53 .63 .73 .84 .94	0.55 .65 .75 .86 .96	0.57 .67 .78 .88 .98	0.59 .69 .80 .90
10 11 12 13 14	1.01 1.11 1.21 1.31 1.41	1.03 1.13 1.23 1.33 1.43	1.05 1.15 1.25 1.35 1.46	1.07 1.17 1.27 1.37 1.48	1.09 1.19 1.29 1.39 1.50	1.02 1.12 1.22 1.32 1.43	1.04 1.14 1.24 1.34 1.45	1.06 1.16 1.26 1.37 1.47	1.08 1.18 1.28 1.39 1.49	1.10 1.20 1.30 1.41 1.51
15 16 17 18 19	1.52 1.62 1.72 1.82 1.92	1.54 1.64 1.74 1.84	1.56 1.66 1.76 1.86 1.96	1.58 1.68 1.78 1.88 1.98	1.60 1.70 1.80 1.90 2.00	1.53 1.63 1.73 1.83 1.93	1.55 1.65 1.75 1.85	1.57 1.67 1.77 1.87 1.97	1.59 1.69 1.79 1.89 1.99	1.61 1.71 1.81 1.91 2.01
20 21 22 23 24	2.02 2.12 2.22 2.32 2.42	2.04 2.14 2.24 2.34 2.44	2.06 2.16 2.26 2.36 2.46	2.08 2.18 2.28 2.38 2.48	2.10 2.20 2.30 2.40 2.50	2.04 2.14 2.24 2.34 2.44	2.06 2.16 2.26 2.36 2.46	2.08 2.18 2.28 2.38 2.48	2.10 2.20 2.30 2.40 2.50	2.12 2.22 2.32 2.42 2.52
25 26 27 28 29	2.52 2.62 2.72 2.82 2.92	2.54 2.64 2.74 2.84 2.94	2.56 2.66 2.76 2.86 2.96	2.58 2.68 2.78 2.88 2.98	2.60 2.70 2.80 2.90 3.00	2.54 2.64 2.74 2.85 2.95	2.56 2.66 2.76 2.87 2.97	2.58 2.68 2.78 2.89 2.99	2.60 2.70 2.80 2.91 3.01	2.62 2.72 2.82 2.93 3.03
30 31 32 33 34	3.02 3.12 3.22 3.32 3.42	3.04 3.14 3.24 3.34 3.44	3.06 3.16 3.26 3.36 3.46	3.08 3.18 3.28 3.38 3.48	3.10 3.20 3.30 3.40 3.50	3.05 3.15 3.25 3.35 3.45	3.07 3.17 3.27 3.37 3.47	3.09 3.19 3.29 3.39 3.49	3.11 3.21 3.31 3.41 3.51	3.13 3.23 3.33 3.43 3.53
35	3.52	3-54	3.56	3.58	3.60	3-55	3.57	3.59	3.61	3.63

TABLE 47.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED

	н		F ТНЕ В 30 mm		ER	н		F ТНЕ В 35 mn		ER
Attached Ther- mometer.	0:0	0°2	0°.4	0.6	0:8	0:0	0°2	0:4	0:6	0.8
0°	mm. 0.00 .10	mm. 0.02 .12	mm. 0.04 .14	mm. 0.06 .16	mm. 0.08	mm. 0.00 .10	mm. 0.02	mm. 0.04 .15	mm. 0.06	mm. 0.08 .19
2 3 4	.21 .31 .41	.23 .33 .43	.25 .35 .45	.27 .37 .47	.29 .39 .49	.21 .31 .41	.23 .33 .44	.25 .35 .46	.27 •37 .48	.29 .39 .50
5 6 7 8	0.51 .62 .72 .82	0.53 .64 •74 .84	o.56 .66 .76 .86	0.58 .68 .78 .88	0.60 .70 .80 .90	0.52 .62 .73 .83	0.54 .64 .75 .85	0.56 .66 .77 .87	0.58 .68 .79 .89	0.60 .70 .81
9 10 11	.92 1.03 1.13	•95 1.05 1.15	·97 1.07 1.17	.99 1.09 1.19	I.II I.2I	•93 1.04 1.14	.95 1.06 1.16	.97 1.08 1.18	.99 1.10 1.20	I.02 I.12 I.22
12 13 14	1.23 1.34 1.44	1.25 1.36 1.46	1.27 1.38 1.48	1.29 1.40 1.50	1.31 1.42 1.52	1.24 1.35 1.45	1.26 1.37 1.47	1.28 1.39 1.49	1.30 1.41 1.51	1.33 1.43 1.53
15 16 17 18	1.54 1.64 1.74 1.85 1.95	1.56 1.66 1.77 1.87 1.97	1.58 1.68 1.79 1.89	1.60 1.70 1.81 1.91 2.01	1.62 1.72 1.83 1.93 2.03	1.55 1.66 1.76 1.86 1.96	1.57 1.68 1.78 1.88 1.99	1.59 1.70 1.80 1.90 2.01	1.61 1.72 1.82 1.92 2.03	1.63 1.74 1.84 1.94 2.05
20 21 22 23 24	2.05 2.15 2.26 2.36 2.46	2.07 2.17 2.28 2.38 2.48	2.09 2.19 2.30 2.40 2.50	2.11 2.21 2.32 2.42 2.52	2.13 2.24 2.34 2.44 2.54	2.07 2.17 2.27 2.38 2.48	2.09 2.19 2.29 2.40 2.50	2.11 2.21 2.31 2.42 2.52	2.13 2.23 2.34 2.44 2.54	2.15 2.25 2.36 2.46 2.56
25 26 27 28 29	2.56 2.66 2.77 2.87 2.97	2.58 2.68 2.79 2.89 2.99	2.60 2.70 2.81 2.91 3.01	2.62 2.73 2.83 2.93 3.03	2.64 2.75 2.85 2.95 3.05	2.58 2.69 2.79 2.89 2.99	2.60 2.71 2.81 2.91 3.01	2.62 2.73 2.83 2.93 3.03	2.64 2.75 2.85 2.95 3.05	2.66 2.77 2.87 2.97 3.08
30 31 32 33 34	3.07 3.17 3.28 3.38 3.48	3.09 3.19 3.30 3.40 3.50	3.11 3.21 3.32 3.42 3.52	3.13 3.23 3.34 3.44 3.54	3.15 3.25 3.36 3.46 3.56	3.10 3.20 3.30 3.40 3.51	3.12 3.22 3.32 3.42 3.53	3.14 3.24 3.34 3.44 3.55	3.16 3.26 3.36 3.47 3.57	3.18 3.28 3.38 3.49 3.59
35	3.58	3.60	3.62	3.64	3.66	3.61	3.63	3.65	3.67	3.69

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	еіснт о 6	F THE B i40 mm		ER	н	EIGHT O	г тне в 645 mm		ER
Attached Ther- mometer.	0:0	0°2	0:4	0°6	0°8	0:0	0°2	0°4	0°6	0°8
C. ° 1234 5678	mm. 0.00 .10 .21 .31 .42 0.52 .63 .73 .84	mm. 0.02 .13 .23 .33 .44 0.54 .65 .75 .86	mm. 0.04 .15 .25 .36 .46 0.56 .67 .77	mm. 0.06 .17 .27 .38 .48 0.59 .69 .79	mm. 0.08 .19 .29 .40 .50 0.61 .71 .81	mm. 0.00 .11 .21 .32 .42 0.53 .63 .74	mm. 0.02 .13 .23 .34 .44 0.55 .65 .76 .86	mm. 0.04 .15 .25 .36 .46 0.57 .67 .78 .88	mm. 0.06 .17 .27 .38 .48 0.59 .69 .80	mm. 0.08 .19 .29 .40 .51 0.61 .72 .82
9 10 11 12 13 14	.94 1.04 1.15 1.25 1.36 1.46	.96 1.06 1.17 1.27 1.38 1.48	1.09 1.19 1.29 1.40 1.50	1.00 1.11 1.21 1.31 1.42 1.52	1.02 1.13 1.23 1.34 1.44 1.54	.95 1.05 1.16 1.26 1.37 1.47	.97 1.07 1.18 1.28 1.39 1.49	.99 1.09 1.20 1.30 1.41 1.51	1.01 1.12 1.22 1.32 1.43 1.53	1.03 1.14 1.24 1.35 1.45 1.56
16 17 18 19 20	1.67 1.77 1.88 1.98	1.69 1.79 1.90 2.00	1.71 1.81 1.92 2.02	1.73 1.83 1.94 2.04	1.75 1.86 1.96 2.06	1.68 1.79 1.89 2.00	1.70 1.81 1.91 2.02	1.72 1.83 1.93 2.04	1.74 1.85 1.95 2.06	1.77 1.87 1.97 2.08
21 22 23 24	2.19 2.29 2.40 2.50	2.21 2.31 2.42 2.52	2.23 2.33 2.44 2.54	2.25 2.35 2.46 2.56	2.27 2.37 2.48 2.58	2.20 2.31 2.41 2.52	2.23 2.33 2.43 2.54	2.25 2.35 2.46 2.56	2.27 2.37 2.48 2.58	2.29 2.39 2.50 2.60
25 26 27 28 29	2.60 2.71 2.81 2.91 3.02	2.62 2.73 2.83 2.93 3.04	2.64 2.75 2.85 2.95 3.06	2.66 2.77 2.87 2.98 3.08	2.69 2.79 2.89 3.00 3.10	2.62 2.73 2.83 2.94 3.04	2.64 2.75 2.85 2.96 3.06	2.66 2.77 2.87 2.98 3.08	2.69 2.79 2.89 3.00 3.10	2.71 2.81 2.92 3.02 3.12
30 31 32 33 34	3.12 3.22 3.33 3.43 3.53	3.14 3.24 3.35 3.45 3.55	3.16 3.27 3.37 3.47 3.58	3.18 3.29 3.39 3.49 3.60	3.20 3.31 3.41 3.51 3.62	3.14 3.25 3.35 3.46 3.56	3.17 3.27 3.37 3.48 3.58	3.19 3.29 3.39 3.50 3.60	3.21 3.31 3.42 3.52 3.62	3.23 3.33 3.44 3.54 3.64
35	3.64	3.66	3.68	3.70	3.72	3.67	3.69	3.71	3.73	3.75

TABLE 47.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	EIGHT O	F ТНЕ В 5 0 m n		ER	н	ексит о 6	F ТНЕ В 555 mm		ER
Attached Ther- mometer.	0.0	0°2	0°.4	0.6	0°8	0:0	0°2	0:4	0:6	0°8
c. 0° 1 2 3 4	mm. 0.00 .11 .21 .32 .42	mm. 0.02 .13 .23 .34 .45	mm. 0.04 .15 .25 .36 .47	mm. 0.06 .17 .28 .38 .49	mm. 0.08 .19 .30 .40 .51	mm. 0.00 .11 .21 .32 .43	mm. 0.02 .13 .24 .34 .45	mm. 0.04 .15 .26 .36 .47	mm. 0.06 .17 .28 .39 .49	mm. 0.09 .19 .30 .41 .51
6 7 8 9	0.53 .64 .74 .85 .95	.66 .76 .87 .98	.68 .78 .89 1.00	.70 .81 .91 1.02	.72 .83 .93 1.04	.64 .75 .85 .96	.66 .77 .88 .98	.68 .79 .90 1.00	.71 .81 .92 1.03	.73 .83 .94 1.05
11 12 13 14	1.17 1.27 1.38 1.48	1.19 1.29 1.40 1.50	1.21 1.31 1.42 1.53	1.23 1.34 1.44 1.55	1.25 1.36 1.46 1.57	1.17 1.28 1.39 1.49	1.20 1.30 1.41 1.52	1.22 1.32 1.43 1.54	1.24 1.35 1.45 1.56	1,26 1,37 1,47 1,58
16 17 18 19	1.69 1.80 1.91 2.01	1.72 1.82 1.93 2.03	1.74 1.84 1.95 2.05	1.76 1.86 1.97 2.07	1.78 1.88 1.99 2.10	1.71 1.81 1.92 2.03	1.73 1.84 1.94 2.05	1.75 1.86 1.96 2.07	1.77 1.88 1.98 2.09	1.79 1.90 2.01 2.11
21 22 23 24 25	2.22 2.33 2.43 2.54	2.24 2.35 2.45 2.56	2.26 2.37 2.47 2.58	2.29 2.39 2.50 2.60	2.31 2.41 2.52 2.62	2.24 2.35 2.45 2.56	2.26 2.37 2.47 2.58	2.28 2.39 2.49 2.60	2.30 2.41 2.52 2.62	2.32 2.43 2.54 2.64
26 27 28 29 30	2.75 2.85 2.96 3.06	2.77 2.87 2.98 3.08	2.79 2.90 3.00 3.11 3.21	2.81 2.92 3.02 3.13	2.83 2.94 3.04 3.15	2.77 2.88 2.98 3.09	2.79 2.90 3.00 3.11 3.21	2.81 2.92 3.02 3.13	2.83 2.94 3.05 3.15 3.26	2.85 2.96 3.07 3.17 3.28
31 32 33 34 35	3.27 3.38 3.48 3.59 3.69	3.30 3.40 3.51 3.61	3.32 3.42 3.53 3.63 3.74	3.34 3.44 3.55 3.65	3.36 3.46 3.57 3.67 3.78	3.30 3.41 3.51 3.62 3.72	3.32 3.43 3.53 3.64 3.74	3.34 3.45 3.55 3.66 3.76	3.36 3.47 3.57 3.68 3.79	3.38 3.49 3.60 3.70 3.81

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	Н		F THE E	SAROMET	ER	н		F THE E		ER
Attached Ther- mometer.	0:0	0°2	0:4	0°6	0:8	0°0	0°2	0°4	0°6	0°8
C. 0° 1	mm. 0.00	mm, 0.02	mm. 0.04 .15	mm. 0.06	mm. 0.09	mm. 0.00	mm. 0.02	mm. 0.04	mm. 0.07	mm. 0.09 .20
3 4	.22 .32 .43	•24 •34 •45	.26 .37 .47	.28 •39 •50	.30 .41 .52	.22 .33 .43	•24 •35 •46	.26 .37 .48	.28 .39 .50	.30 .41 .52
5 6 7 8 9	0.54 .65 .75 .86	0.56 .67 .78 .88	0.58 .69 .80 .90	0.60 .71 .82 .93 1.03	0.62 •73 •84 •95	0.54 .65 .76 .87	0.56 .67 .78 .89	0.59 .69 .80 .91	0.61 .72 .82 .93 1.04	0.63 •74 •85 •95
10 11 12 13	1.08 1.18 1.29 1.40	1.10 1.21 1.31 1.42 1.53	1.12 1.23 1.33 1.44 1.55	1.14 1.25 1.36 1.46	1.16 1.27 1.38 1.48 1.59	1.08 1.19 1.30 1.41 1.52	1.11 1.21 1.32 1.43 1.54	1.13 1.24 1.34 1.45 1.56	1.15 1.26 1.37 1.47 1.58	1.17 1.28 1.39 1.50 1.60
15 16 17 18	1.61 1.72 1.83 1.93	1.63 1.74 1.85 1.96 2.06	1.66 1.76 1.87 1.98 2.08	1.68 1.78 1.89 2.00	1.70 1.81 1.91 2.02 2.13	1.63 1.73 1.84 1.95	1.65 1.76 1.86 1.97	1.67 1.78 1.88 1.99 2.10	1.69 1.80 1.91 2.01	1.71 1.82 1.93 2.04 2.14
20 21 22 23 24	2.15 2.26 2.36 2.47 2.58	2.17 2.28 2.38 2.49 2.60	2.19 2.30 2.41 2.51 2.62	2.21 2.32 2.43 2.53 2.64	2.23 2.34 2.45 2.56 2.66	2.17 2.27 2.38 2.49 2.60	2.19 2.29 2.40 2.51 2.62	2.21 2.32 2.42 2.53 2.64	2.23 2.34 2.45 2.55 2.66	2.25 2.36 2.47 2.57 2.68
25 26 27 28 29	2.68 2.79 2.90 3.00 3.II	2.71 2.81 2.92 3.03 3.13	2.73 2.83 2.94 3.05 3.15	2.75 2.85 2.96 3.07 3.18	2.77 2.88 2.98 3.09 3.20	2.70 2.81 2.92 3.03 3.13	2.73 2.83 2.94 3.05 3.16	2.75 2.85 2.96 3.07 3.18	2.77 2.88 2.98 3.09 3.20	2.79 2.90 3.01 3.11 3.22
30 31 32 33 34	3.22 2.32 3.43 3.54 3.64	3.24 3.35 3.45 3.56 3.67	3.26 3.37 3.47 3.58 3.69	3.28 3.39 3.49 3.60 3.71	3.30 3.41 3.52 3.62 3.73	3.24 3.35 3.46 3.56 3.67	3.26 3.37 3.48 3.59 3.69	3.29 3.39 3.50 3.61 3.71	3.31 3.41 3.52 3.63 3.74	3.33 3.44 3.54 3.65 3.76
35	3-75	3.77	3.79	3.81	3.84	3.78	3.80	3.82	3.84	3.86

TABLE 47.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	EIGHT O	F THE E		ER	н	EIGHT O	F ТНЕ 1		ER
Attached Ther- mometer.	0:0	0°2	0°4	0.6	0.8	0:0	0°2	0.4	0.6	0.8
C. 0° 1 2 3 4 5 6 7 8	mm. 0.00 .11 .22 .33 .44 0.55 .66 .77	mm. 0.02 .13 .24 .35 .46 0.57 .68	mm. 0.04 .15 .26 .37 .48 0.59 .70 .81	mm. 0.07 .18 .28 .39 .50 0.61 .72 .83	mm. 0.09 .20 .31 .42 .53 0.63 .74	mm. 0.00 .11 .22 .33 .44 0.55 .66 .77 .88	mm. 0.02 .13 .24 .35 .46 0.57 .68 .79	mm. 0.04 .15 .26 .37 .48 0.60 .71 .82	mm. 0.07 .18 .29 .40 .51 0.62 .73 .84	mm. 0.09 .20 .31 .42 .53 0.64 .75 .86
9 10 11 12 13 14	.87 .98 1.09 1.20 1.31 1.42 1.53	.90 I.01 I.11 I.22 I.33 I.44 I.55	.92 1.03 1.14 1.25 1.35 1.46 1.57	1.05 1.16 1.27 1.38 1.49 1.59	1.07 1.18 1.29 1.40 1.51 1.62	.99 1.10 1.21 1.32 1.43 1.54	1.01 1.12 1.23 1.34 1.45 1.56	1.04 1.14 1.25 1.36 1.47 1.58	.95 1.06 1.17 1.28 1.39 1.50 1.61	.97 1.08 1.19 1.30 1.41 1.52 1.63
15 16 17 18 19 20	1.64 1.75 1.86 1.96 2.07	1.66 1.77 1.88 1.99 2.09	1.68 1.79 1.90 2.01 2.12	1.70 1.81 1.92 2.03 2.14	1.72 1.83 1.94 2.05 2.16	1.65 1.76 1.87 1.98 2.09	1.67 1.78 1.89 2.00 2.11	1.69 1.80 1.91 2.02 2.13	1.72 1.83 1.94 2.04 2.15	1.74 1.85 1.96 2.07 2.18
21 22 23 24 25 26	2.29 2.40 2.51 2.62 2.72 2.83	2.31 2.42 2.53 2.64 2.75 2.85	2.33 2.44 2.55 2.66 2.77 2.88	2.36 2.46 2.57 2.68 2.79 2.90	2.38 2.49 2.59 2.70 2.81 2.92	2.31 2.42 2.53 2.64 2.74 2.85	2.33 2.44 2.55 2.66 2.77 2.88	2.35 2.46 2.57 2.68	2.37 2.48 2.59 2.70 2.81	2.39 2.50 2.61 2.72 2.83
27 28 29 30	2.94 3.05 3.16 3.27	2.65 2.96 3.07 3.18 3.29 3.40	2.98 3.09 3.20 3.31	3.01 3.11 3.22 3.33	3.03 3.14 3.24 3.35 3.46	2.96 3.07 3.18 3.29	2.99 3.09 3.20 3.31	2.90 3.01 3.12 3.23	2.92 3.03 3.14 3.25 3.36	2.94 3.05 3.16 3.27 3.38
31 33 33 34 35	3.37 3.48 3.59 3.70 3.81	3.40 3.50 3.61 3.72 3.83	3.42 3.53 3.63 3.74 3.85	3.44 3.55 3.66 3.76 3.87	3.40 3.57 3.68 3.79 3.89	3.40 3.51 3.62 3.73 3.84	3.42 3.53 3.64 3.75 3.86	3.44 3.55 3.66 3.77 3.88	3.47 3.57 3.68 3.79 3.90	3.49 3.60 3.71 3.81 3.92

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	Н	EIGHT O	F THE E	-	ER	п		F THE 1		ER
Attached Ther- mometer.	0°0	0°2	0°4	0°6	0.8	0:0	0°2	0°4	0.6	0.8
c. 0° 1 2 3 4 56 78	mm. 0.00 .11 .22 .33 .44 0.56 .67 .78 .89	mm. 0.02 .13 .24 .36 .47 0.58 .69 .80 .91	mm. 0.04 .16 .27 .38 .49 0.60 .71 .82 .93	mm. 0.07 .18 .29 .40 .51 0.62 .73 .84 .95	mm. 0.09 .20 .31 .42 .53 0.64 .75 .87	mm. 0.00 .11 .22 .34 .45 0.56 .67 .78 .89	mm. 0.02 .13 .25 .36 .47 0.58 .69 .80	mm. 0.04 .16 .27 .38 .49 0.60 .72 .83 .94	mm. 0.07 .18 .29 .40 .51 0.63 .74 .85	mm. 0.09 .20 .31 .43 .54 0.65 .76 .87 .98
9	1.00	1.02	1.04	1.06	1.09	1.01	1.03	1.05	1.07	1.09
10	1.11	1.13	1.15	1.18	1.20	1.12	1.14	1.16	1.18	1.21
11	1.22	1.24	1.26	1.29	1.31	1.23	1.25	1.27	1.30	1.32
12	1.33	1.35	1.37	1.40	1.42	1.34	1.36	1.38	1.41	1.43
13	1.44	1.46	1.49	1.51	1.53	1.45	1.47	1.50	1.52	1.54
14	1.55	1.57	1.60	1.62	1.64	1.56	1.59	1.61	1.63	1.65
15	1.66	1.68	1.71	1.73	1.75	1.67	1.70	1.72	1.74	1.76
16	1.77	1.79	1.82	1.84	1.86	1.79	1.81	1.83	1.85	1.87
17	1.88	1.91	1.93	1.95	1.97	1.90	1.92	1.94	1.96	1.99
18	1.99	2.02	2.04	2.06	2.08	2.01	2.03	2.05	2.07	2.10
19	2.10	2.13	2.15	2.17	2.19	2.12	2.14	2.16	2.19	2.21
20	2.21	2.24	2.26	2.28	2.30	2.23	2.25	2.27	2.30	2.32
21	2.32	2.35	2.37	2.39	2.41	2.34	2.36	2.39	2.41	2.43
22	2.43	2.46	2.48	2.50	2.52	2.45	2.47	2.50	2.52	2.54
23	2.54	2.57	2.59	2.61	2.63	2.56	2.59	2.61	2.63	2.65
24	2.66	2.68	2.70	2.72	2.74	2.67	2.70	2.72	2.74	2.76
25	2.77	2.79	2.81	2.83	2.85	2.79	2.81	2.83	2.85	2.87
26	2.88	2.90	2.92	2.94	2.96	2.90	2.92	2.94	2.96	2.99
27	2.99	3.01	3.03	3.05	3.07	3.01	3.03	3.05	3.07	3.10
28	3.10	3.12	3.14	3.16	3.18	3.12	3.14	3.16	3.18	3.21
29	3.21	3.23	3.25	3.27	3.29	3.23	3.25	3.27	3.30	3.32
30	3.32	3·34	3.36	3.38	3.40	3.34	3.36	3.38	3.41	3.43
31	3.43	3·45	3.47	3.49	3.51	3.45	3.47	3.49	3.52	3.54
32	3.54	3·56	3.58	3.60	3.62	3.56	3.58	3.61	3.63	3.65
33	3.64	3·67	3.69	3.71	3.73	3.67	3.69	3.72	3.74	3.76
34	3.75	3·78	3.80	3.82	3.84	3.78	3.80	3.83	3.85	3.87
35	3.86	3.89	3.91	3.93	3.95	3.89	3.91	3.94	3.96	3.98

TABLE 47.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н		F THE 1	SAROMET	ER	. н	EIGHT O	F THE 1		ER
Attached Ther- mometer.	0°0	0°2	0°4	0°6	0.8	0°0	0°2	0:4	0.6	0.8
c. 0° 1 2	mm. 0.00 .11 .23	mm. 0.02 .14 .25	mm. 0.05 .16 .27	mm. 0.07 .18 .29	mm. 0.09 .20 .32	mm. 0.00 .11 .23	mm. 0.02 .14 .25	mm. 0.05 .16 .27	mm. 0.07 .18 .30	mm. 0.09 .20 .32 .43
4 5 6 7 8	•45 •.56 •.68 •.79 •.90	.47 0.59 .70 .81	0.61 .72 .83	.52 0.63 .74 .86 .97	•54 •.65 •.77 •.88 •.99	•45 ••57 •68 •79 •91	.48 0.59 .70 .82 .93	.50 0.61 .73 .84 .95	•52 •.64 •75 •.86 •.98	•54 •.66 •77 •88 •.00
9	1.01	1.04	1.06	1.08	1.10	1.02	1.04	1.07	1.09	1.11
10	1.13	1.15	1.17	1.19	1.22	1.13	1.16	1.18	1.20	1.22
11	1.24	1.26	1.28	1.31	1.33	1.25	1.27	1.29	1.31	1.34
12	1.35	1.37	1.39	1.42	1.44	1.36	1.38	1.41	1.43	1.45
13	1.46	1.48	1.51	1.53	1.55	1.47	1.50	1.52	1.54	1.56
14	1.57	1.60	1.62	1.64	1.66	1.59	1.61	1.63	1.65	1.68
15	1.69	1.71	1.73	1.75	1.78	1.70	1.72	1.74	1.77	1.79
16	1.80	1.82	1.84	1.87	1.89	1.81	1.83	1.86	1.88	1.90
17	1.91	1.93	1.96	1.98	2.00	1.92	1.95	1.97	1.99	2.01
18	2.02	2.05	2.07	2.09	2.11	2.04	2.06	2.08	2.11	2.13
19	2.13	2.16	2.18	2.20	2.22	2.15	2.17	2.20	2.22	2.24
20	2.25	2.27	2.29	2.31	2.34	2.26	2.29	2.31	2.33	2.35
21	2.36	2.38	2.40	2.43	2.45	2.38	2.40	2.42	2.44	2.47
22	2.47	2.49	2.52	2.54	2.56	2.49	2.51	2.53	2.56	2.58
23	2.58	2.60	2.63	2.65	2.67	2.60	2.62	2.65	2.67	2.69
24	2.69	2.72	2.74	2.76	2.78	2.71	2.74	2.76	2.78	2.80
25	2.81	2.83	2.85	2.87	2.90	2.83	2.85	2.87	2.89	2.92
26	2.92	2.94	2.96	2.99	3.01	2.94	2.96	2.98	3.01	3.03
27	3.03	3.05	3.07	3.10	3.12	3.05	3.07	3.10	3.12	3.14
28	3.14	3.16	3.19	3.21	3.23	3.16	3.19	3.21	3.23	3.25
29	3.25	3.27	3.30	3.32	3.34	3.28	3.30	3.32	3.34	3.37
30	3.36	3.39	3.41	3.43	3.45	3.39	3.41	3.43	3.46	3.48
31	3.48	3.50	3.52	3.54	3.56	3.50	3.52	3.55	3.57	3.59
32	3.59	3.61	3.63	3.65	3.68	3.61	3.64	3.66	3.68	3.70
33	3.70	3.72	3.74	3.77	3.79	3.73	3.75	3.77	3.79	3.81
34	3.81	3.83	3.85	3.88	3.90	3.84	3.86	3.88	3.90	3.93
35	3.92	3.94	3-97	3-99	4.01	3.95	3-97	3-99	4.02	4.04

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	EIGHT O	F ТНЕ В '00 mm		ER	Н	EIGHT O	F ТНЕ В '05 m n		er
Attached Ther- mometer.	0:0	0°2	0°4	0°6	0°8	0:0	0°2	0°4	0°6	0°8
C. 0° 1 2 3 4	mm. 0.00 .11 .23 .34 .46	mm. 0.02 .14 .25 .37 .48	mm. 0.05 .16 .27 .39	mm. 0.07 .18 .30 .41 .53	mm. 0.09 .21 .32 .43 .55	mm. 0.00 .12 .23 .35 .46	mm. 0.02 .14 .25 .37 .48	mm. 0.05 .16 .28 .39	mm. 0.07 .18 .30 .41 .53	mm. 0.09 .21 .32 .44
5	0.57	0.59	0.62	0.64	0.66	0.58	0.60	0.62	0.64	0.67
6	.69	.71	•73	•75	.78	.69	.71	•74	.76	.78
7	.80	.82	•85	•87	.89	.81	.83	•85	.87	.90
8	.91	.94	•96	•98	1.00	.92	.94	•97	.99	I.01
9	1.03	1.05	•1.07	1.10	1.12	1.04	1.06	1.08	1.10	I.13
10	1.14	1.16	1.19	1.21	1.23	1.15	1.17	1.20	1.22	1.24
11	1.26	1.28	1.30	1.32	1.35	1.26	1.29	1.31	1.33	1.36
12	1.37	1.39	1.42	1.44	1.46	1.38	1.40	1.43	1.45	1.47
13	1.48	1.51	1.53	1.55	1.57	1.49	1.52	1.54	1.56	1.59
14	1.60	1.62	1.64	1.67	1.69	1.61	1.63	1.65	1.68	1.70
15	1.71	1.73	1.76	1.78	1.80	1.72	1.75	1.77	1.79	1.81
16	1.82	1.85	1.87	1.89	1.92	1.84	1.86	1.88	1.91	1.93
17	1.94	1.96	1.98	2.01	2.03	1.95	1.98	2.00	2.02	2.04
18	2.05	2.07	2.10	2.12	2.14	2.07	2.09	2.11	2.14	2.16
19	2.17	2.19	2.21	2.23	2.26	2.18	2.20	2.23	2.25	2.27
20	2.28	2.30	2.32	2.35	2.37	2.30	2.32	2.34	2.36	2.39
21	2.39	2.42	2.44	2.46	2.48	2.41	2.43	2.46	2.48	2.50
22	2.51	2.53	2.55	2.57	2.60	2.52	2.55	2.57	2.59	2.62
23	2.62	2.64	2.67	2.69	2.71	2.64	2.66	2.68	2.71	2.73
24	2.73	2.76	2.78	2.80	2.82	2.75	2.78	2.80	2.82	2.84
25	2.85	2.87	2.89	2.91	2.94	2.87	2.89	2.91	2.94	2.96
26	2.96	2.98	3.01	3.03	3.05	2.98	3.00	3.03	3.05	3.07
27	3.07	3.10	3.12	3.14	3.16	3.10	3.12	3.14	3.16	3.19
28	3.19	3.21	3.23	3.25	3.28	3.21	3.23	3.25	3.28	3.30
29	3.30	3.32	3.34	3.37	3.39	3.32	3.35	3.37	3.39	3.41
30	3.41	3.44	3.46	3.48	3.50	3.44	3.46	3.48	3.51	3.53
31	3.53	3.55	3.57	3.59	3.62	3.55	3.57	3.60	3.62	3.64
32	3.64	3.66	3.68	3.71	3.73	3.66	3.69	3.71	3.73	3.76
33	3.75	3.77	3.80	3.82	3.84	3.78	3.80	3.82	3.85	3.87
34	3.87	3.89	3.91	3.93	3.96	3.89	3.92	3.94	3.96	3.98
35	3.98	4.00	4.02	4.05	4.07	4.01	4.03	4.05	4.07	4.10

TABLE 47.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTEO.

	H		г тне в '10 mm	AROMETI	er	н	EIGHT O	F ТНЕ В 715 mm		ER
Attached Ther- mometer.	0:0	0°2	0°4	0:6	0.8	0:0	0°2	0°.4	0:6	0°8
c. 0° 1 2 3 4 5 6 7 8 9	mm. 0.00 .12 .23 .35 .46 0.58 .70 .81 .93 1.04	mm. 0.02 .14 .26 .37 .49 0.60 .72 .83 .95 1.07	mm. 0.05 .16 .28 .39 .51 0.63 .74 .86 .97 1.09	min. 0.07 .19 .30 .42 .53 0.65 .76 .88 1.00 1.11	mm. 0.09 .21 .32 .44 .56 0.67 .79 .90 1.02 1.13	mm. 0.00 .12 .23 .35 .47 0.58 .70 .82 .93 1.05	mm. 0.02 .14 .26 .37 .49 0.61 .72 .84 .96 1.07	mm. 0.05 .16 .28 .40 .51 0.63 .75 .86 .98 1.10	mm. 0.07 .19 .30 .42 .54 0.65 .77 .89 1.00 1.12	mm. 0.09 .21 .33 .44 .56 0.68 .79 .91 1.03 1.14
10 11 12 13 14	1.16 1.27 1.39 1.50 1.62	1.18 1.30 1.41 1.53 1.64	1.20 1.32 1.44 1.55 1.67	1.23 1.34 1.46 1.57 1.69	1.25 1.37 1.48 1.60 1.71	1.17 1.28 1.40 1.52 1.63	1.19 1.31 1.42 1.54 1.65	1.21 1.33 1.45 1.56 1.68	1.24 1.35 1.47 1.58 1.70	1.26 1.38 1.49 1.61 1.72
16 17 18 19	1.74 1.85 1.97 2.08 2.20	1.76 1.87 1.99 2.10 2.22	1.76 1.90 2.01 2.13 2.24	1.92 2.04 2.15 2.27	1.94 2.06 2.17 2.29	1.75 1.86 1.98 2.10 2.21	1.77 1.89 2.00 2.12 2.24	1.79 1.91 2.03 2.14 2.26	1.93 2.05 2.17 2.28	1.64 1.96 2.07 2.19 2.30
20 21 22 23 24	2.31 2.43 2.54 2.66 2.77	2.33 2.45 2.57 2.68 2.80	2.36 2.47 2.59 2.70 2.82	2.38 2.50 2.61 2.73 2.84	2.40 2.52 2.63 2.75 2.86	2.33 2.44 2.56 2.68 2.79	2.35 2.47 2.58 2.70 2.81	2.37 2.49 2.61 2.72 2.84	2.40 2.51 2.63 2.75 2.86	2.42 2.54 2.65 2.77 2.88
25 26 27 28 29	2.89 3.00 3.12 3.23 3.35	2.91 3.03 3.14 3.25 3.37	2.93 3.05 3.16 3.28 3.39	2.96 3.07 3.19 3.30 3.42	2.98 3.09 3.21 3.32 3.44	2.91 3.02 3.14 3.25 3.37	2.93 3.05 3.16 3.28 3.39	2.95 3.07 3.19 3.30 3.42	2.98 3.09 3.21 3.32 3.44	3.00 3.12 3.23 3.35 3.46
30 31 32 33 34	3.46 3.58 3.69 3.81 3.92	3.48 3.60 3.71 3.83 3.94	3.51 3.62 3.74 3.85 3.97	3.53 3.65 3.76 3.87 3.99	3.55 3.67 3.78 3.90 4.01	3.49 3.60 3.72 3.83 3.95	3.51 3.62 3.74 3.86 3.97	3.53 3.65 3.76 3.88 3.99	3.56 3.67 3.79 3.90 4.02	3.58 3.69 3.81 3.92 4.04
35	4.03	4.06	4.08	4.10	4.13	4.06	4.09	4.11	4.13	4.16

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	H	EIGHT O	F THE B		ER	н	EIGHT O	я тне і 725 mn		ER
Attached Ther- mometer.	0:0	0°2	0°4	0.6	0.8	000	0°2	0.4	0.6	0:8
C. 0° I 2	mm. 0.00 .12 .24	mm. 0.02 .14 .26	mm. 0.05 .16	mm. 0.07 .19	mm. 0.09 .21 ·33	mm. 0.00 .12 .24	mm. 0.02 .14 .26	mm. 0.05 .17 .28	mm. 0.07 .19 .31	mm. 0.09 .21 .33
3 4 5 6	.35 .47 0.59	.38 .49 o.61	.40 .52 0.63	.42 .54 0.66	.45 .56 0.68	.36 .47 0.59	.38 .50 0.62	.40 .52 0.64	•43 •54 •.66	.45 .57 0.69
7 8 9	.71 .82 .94 1.06	.73 .85 .96 1.08	.75 .87 .99	.78° .89 1.01 1.13	.80 .92 1.03 1.15	.71 .83 .95 1.06	.73 .85 .97 1.09	.76 .88 .99	.78 .90 1.02 1.14	.80 .92 1.04 1.16
10 11 12 13 14	1.17 1.29 1.41 1.53 1.64	1.20 1.31 1.43 1.55 1.67	1.22 1.34 1.46 1.57 1.69	1.24 1.36 1.48 1.60 1.71	1.27 1.39 1.50 1.62 1.74	1.18 1.30 1.42 1.54 1.65	1.21 1.32 1.44 1.56 1.68	1.23 1.35 1.47 1.58 1.70	1.25 1.37 1.49 1.61 1.73	1.28 1.39 1.51 1.63 1.75
1 5 16 17 18 19	1.76 1.88 1.99 2.11 2.23	1.78 1.90 2.02 2.13 2.25	1.81 1.92 2.04 2.16 2.27	1.83 1.95 2.06 2.18 2.30	1.85 1.97 2.09 2.20 2.32	1.77 1.89 2.01 2.13 2.24	1.80 1.91 2.03 2.15 2.27	1.82 1.94 2.05 2.17 2.29	1.84 1.96 2.08 2.20 2.31	1.87 1.98 2.10 2.22 2.34
20 21 22 23 24	2.34 2.46 2.58 2.69 2.81	2.37 2.48 2.60 2.72 2.83	2.39 2.51 2.62 2.74 2.86	2.41 2.53 2.65 2.76 2.88	2.44 2.55 2.67 2.79 2.90	2.36 2.48 2.60 2.71 2.83	2.38 2.50 2.62 2.74 2.85	2.41 2.53 2.64 2.76 2.88	2.43 2.55 2.67 2.78 2.90	2.45 2.57 2.69 2.81 2.92
25 26 27 28 29	2.93 3.04 3.16 3.28 3.39	2.95 3.07 3.18 3.30 3.42	2.97 3.09 3.21 3.32 3.44	3.00 3.11 3.23 3.35 3.46	3.02 3.14 3.25 3.37 3.49	2.95 3.07 3.18 3.30 3.42	2.97 3.09 3.21 3.32 3.44	3.00 3.11 3.23 3.35 3.46	3.02 3.14 3.25 3.37 3.49	3.04 3.16 3.28 3.39 3.51
30 31 32 33 24	3.51 3.63 3.74 3.86 3.98	3.53 3.65 3.77 3.88 4.00	3.56 3.67 3.79 3.91 4.02	3.58 3.70 3.81 3.93 4.05	3.60 3.72 3.84 3.95 4.07	3.53 3.65 3.77 3.89 4.00	3.56 3.68 3.79 3.91 4.03	3.58 3.70 3.82 3.93 4.05	3.60 3.72 3.84 3.96 4.07	3.63 3.75 3.86 3.98 4.10
35	4.09	4.11	4.14	4.16	4.18	4.12	4.14	4.17	4.19	4.21

TABLE 47.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	EIGHT O	THE B		ER.	н	EIGHT O	7 THE B. 735 mn		ER
Atfached Ther- mometer.	0:0	0°2	0°,4	0:6	0.8	0:0	0.2	0:4	0.6	0:8
c. 0°	mm.	mm. 0.02	mm. 0.05	mm.	mm.	mm.	mm. 0.02	mm. 0.05	mm. 0.07	mm. O.IO
1 2 3	.12 .24 .36	.14 .26 .38	.17 .29 .41	.19 .31 .43	.21 -33 -45	.12 .24 .36	.14 .26 .38	.17 .29 .41	.19 .31 .43	.22 •34 .46
4	.48	.50	-52	-55	-57	.48	.50	∙53	•55	.58
5 6 7 8	0.60 .71 .83	0.62 -74 -86	o.64 .76 .88	0.67 .79 .91	0.69 .81 .93	0.60 .72 .84	0,62 •74 .86	o.65 •77 .89	0.67 •79 •91	0.70 .82 .94
8 9	.95 1.07	.98 1.10	I.00 I.I2	I.02 I.14	1.05 1.17	.96 1.08	.98 1.10	I.01 I.13	1.03 1.15	1.06
10 11 12 13 14	1.19 1.31 1.43 1.55 1.67	1.21 1.33 1.45 1.57 1.69	1.24 1.36 1.48 1.59 1.71	1.26 1.38 1.50 1.62 1.74	1.29 1.40 1.52 1.64 1.76	1.20 1.32 1.44 1.56 1.68	1.22 1.34 1.46 1.58 1.70	1.25 1.37 1.49 1.61 1.72	1.27 1.39 1.51 1.63 1.75	1.29 1.41 1.53 1.65 1.77
15 16 17 18	1.78 1.90 2.02 2.14 2.26	1.81 1.93 2.05 2.16 2.28	1.83 1.95 2.07 2.19 2.31	1.86 1.97 2.09 2.21 2.33	1.88 2.00 2.12 2.23 2.35	1.80 1.92 2.04 2.15 2.27	1.82 1.94 2.06 2.18 2.30	1.84 1.96 2.08 2.20 2.32	1.87 1.99 2.11 2.23 2.35	1.89 2.01 2.13 2.25 2.37
20 21 22 23 24	2.38 2.50 2.61 2.73 2.85	2.40 2.52 2.64 2.76 2.87	2.42 2.54 2.66 2.78 2.90	2.45 2.57 2.68 2.80 2.92	2.47 2.59 2.71 2.83 2.94	2.39 2.51 2.63 2.75 2.87	2.42 2.54 2.66 2.77 2.89	2.44 2.56 2.68 2.80 2.92	2.46 2.58 2.70 2.82 2.94	2.49 2.61 2.73 2.85 2.97
25 26 27 28 29	2.97 3.09 3.20 3.32 3.44	2.99 3.11 3.23 3.35 3.46	3.02 3.13 3.25 3.37 3.49	3.04 3.16 3.28 3.39 3.51	3.06 3.18 3.30 3.42 3.54	2.99 3.11 3.23 3.35 3.46	3.01 3.13 3.25 3.37 3.49	3.04 3.16 3.27 3.39 3.51	3.06 3.18 3.30 3.42 3.54	3.08 3.20 3.32 3.44 3.56
30 31 32 33 34	3.56 3.68 3.79 3.91 4.03	3.58 3.70 3.82 3.94 4.05	3.61 3.72 3.84 3.96 4.08	3.63 3.75 3.87 3.98 4.10	3.65 3.77 3.89 4.01 4.12	3.58 3.70 3.82 3.94 4.06	3.61 3.73 3.84 3.96 4.08	3.63 3.75 3.87 3.99 4.11	3.65 3.77 3.89 4.01 4.13	3.68 3.80 3.92 4.03 4.15
35	4.15	4.17	4.20	4.22	4.24	4.18	4.20	4.22	4.25	4.27

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	В	EIGHT O	F THE 1740 mn	-	ER	H		F THE 1		ER
Attached Ther- mometer.	0°0	0°2	0%4	0:6	0.8	0:0	0°2	0°4	0:6	0°8
c. 0° 1 2 3 4	mm. 0.00 .12 .24 .36 .48	mm. 0.02 .15 .27 .39	mm. 0.05 .17 .29 .41 .53	mm. 0.07 .19 .31 .44	mm. 0.10 .22 .34 .46 .58	mm. 0.00 .12 .24 .37 .49	mm. 0.02 .15 .27 .39	mm. 0.05 .17 .29 .41	mm. 0.07 .19 .32 .44 .56	mm. 0.10 .22 .34 .46 .58
5 6 7 8 9	0.60 .72 .85 .97 I.09	0.63 .75 .87 .99	0.65 .77 .89 1.01 1.13	0.68 .80 .92 1.04 1.16	0.70 .82 .94 1.06 1.18	0.61 .73 .85 .97 1.09	0.63 .75 .88 1.00	0.66 .78 .90 1.02 1.14	0.68 .80 .92 1.05 1.17	0.71 .83 .95 1.07 1.19
10	1.21	1.23	1.26	1.28	1.30	1.22	1.24	1.26	1.29	1.31
11	1.33	1.35	1.38	1.40	1.42	1.34	1.36	1.38	1.41	1.43
12	1.45	1.47	1.50	1.52	1.54	1.46	1.48	1.51	1.53	1.55
13	1.57	1.59	1.62	1.64	1.66	1.58	1.60	1.63	1.65	1.68
14	1.69	1.71	1.74	1.76	1.78	1.70	1.72	1.75	1.77	1.80
15	1.81	1.83	1.86	1.88	1.90	1.82	1.85	1.87	1.89	1.92 ·
16	1.93	1.95	1.98	2.00	2.03	1.94	1.97	1.99	2.01	2.04
17	2.05	2.07	2.10	2.12	2.15	2.06	2.09	2.11	2.14	2.16
18	2.17	2.19	2.22	2.24	2.27	2.18	2.21	2.23	2.26	2.28
19	2.29	2.31	2.34	2.36	2.39	2.31	2.33	2.35	2.38	2.40
20	2.41	2.43	2.46	2.48	2.51 °	2.43	2.45	2.47	2.50	2.52
21	2.53	2.55	2.58	2.60	2.63	2.55	2.57	2.59	2.62	2.64
22	2.65	2.67	2.70	2.72	2.75	2.67	2.69	2.72	2.74	2.76
23	2.77	2.79	2.82	2.84	2.87	2.79	2.81	2.84	2.86	2.88
24	2.89	2.91	2.94	2.96	2.99	2.91	2.93	2.96	2.98	3.01
25	3.01	3.03	3.06	3.08	3.11	3.03	3.05	3.08	3.10	3.13
26	3.13	3.15	3.18	3.20	3.22	3.15	3.17	3.20	3.22	3.25
27	3.25	3.27	3.30	3.32	3.34	3.27	3.29	3.32	3.34	3.37
28	3.37	3.39	3.42	3.44	3.46	3.39	3.42	3.44	3.46	3.49
29	3.49	3.51	3.54	3.56	3.58	3.51	3.54	3.56	3.58	3.61
30	3.61	3.63	3.66	3.68	3.70	3.63	3.66	3.68	3.70	3.73
31	3.73	3.75	3.78	3.80	3.82	3.75	3.78	3.80	3.82	3.85
32	3.85	3.87	3.89	3.92	3.94	3.87	3.90	3.92	3.95	3.97
33	3.97	3.99	4.01	4.04	4.06	3.99	4.02	4.04	4.07	4.09
34	4.09	4.11	4.13	4.16	4.18	4.11	4.14	4.16	4.19	4.21
35	4.21	4.23	4.25	4.28	4.30	4.23	4.26	4.28	4.31	4.33

TABLE 47.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н	EIGHT O	F ТНЕ В. 50 mm		ER	н	EIGHT O	F THE B '55 mm		ER
Attached Ther- mometer.	0;0	0°2	0.4	0.6	0%8	000	0°2	0:4	0.6	0°8
C. 0° 1 2 3 4 5 6 7 8 9	mm. 0.00 .12 .25 .37 .49 0.61 .73 .86 .98 1.10	mm. 0.02 .15 .27 .39 .51 0.64 .76 .88 1.00 1.13	mm. 0.05 .17 .29 .42 .54 0.66 .78 .91 1.03 1.15	mm. 0.07 .20 .32 .44 .56 0.69 .81 .93 1.05 1.17	mm. 0.10 .22 .34 .47 .59 0.71 .83 .95 1.08 1.20	mm. 0.00 .12 .25 .37 .49 0.62 .74 .86 .99 I.11	mm. 0.02 .15 .27 .39 .52 0.64 .76 .89 1.01 1.13	mm. 0.05 .17 .30 .42 .54 0.67 .79 .91 1.03 1.16	mm. 0.07 .20 .32 .44 .57 0.69 .81 .94 1.06 1.18	mm. 0.10 .22 .35 .47 .59 0.71 .84 .96 1.08 1.21
11 12 13 14	1.22 1.35 1.47 1.59 1.71	1.25 1.37 1.49 1.61 1.74	1.39 1.52 1.64 1.76	1.42 1.54 1.66 1.78	1.44 1.56 1.69 1.81	1.23 1.35 1.48 1.60 1.72	1.38 1.50 1.62 1.75	1.40 1.53 1.65 1.77	1.43 1.55 1.67 1.80	1.45 1.58 1.70 1.82
. 15 16 17 18 19	1.83 1.96 2.08 2.20 2.32	1.86 1.98 2.10 2.22 2.34	1.88 2.00 2.13 2.25 2.37	1.91 2.03 2.15 2.27 2.39	1.93 2.05 2.17 2.30 2.42	1.85 1.97 2.09 2.21 2.34	1.87 1.99 2.12 2.24 2.36	1.89 2.02 2.14 2.26 2.38	1.92 2.04 2.16 2.29 2.41	1.94 2.07 2.19 2.31 2.43
20 21 22 23 24	2.44 2.56 2.69 2.81 2.93	2.47 2.59 2.71 2.83 2.95	2.49 2.61 2.73 2.86 2.98	2.52 2.64 2.76 2.88 3.00	2.54 2.66 2.78 2.90 3.03	2.46 2.58 2.70 2.83 2.95	2.48 2.61 2.73 2.85 2.97	2.51 2.63 2.75 2.87 3.00	2.53 2.65 2.78 2.90 3.02	2.56 2.68 2.80 2.92 3.05
25 26 27 28 29	3.05 3.17 3.29 3.41 3.54	3.07 3.20 3.32 3.44 3.56	3.10 3.22 3.34 3.46 3.58	3.12 3.24 3.37 3.49 3.61	3.15 3.27 3.39 3.51 3.63	3.07 3.19 3.31 3.44 3.56	3.09 3.22 3.34 3.46 3.58	3.12 3.24 3.36 3.49 3.61	3.14 3.27 3.39 3.51 3.63	3.17 3.29 3.41 3.53 3.66
30 31 32 33 34	3.66 3.78 3.90 4.02 4.14	3.68 3.80 3.92 4.04 4.17	3.71 3.83 3.95 4.07 4.19	3.73 3.85 3.97 4.09 4.21	3.75 3.87 4.00 4.12 4.24	3.68 3.80 3.92 4.05 4.17	3.71 3.83 3.95 4.07 4.19	3.73 3.85 3.97 4.10 4.22	3.75 3.88 4.00 4.12 4.24	3.78 3.90 4.02 4.14 4.27
35	4.26	4.29	4.31	4.33	4.36	4.29	4.31	4.34	4.36	4.39

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н		F THE В		ER	Н		г тив в '65 mn	BAROMET	ER
Attached Ther- mometer.	0:0	0°2	0°4	0°6	0°8	0.0	0°2	0°4	0°6	0°8
C. 0° 1 2 3 4	mm. 0.00 .12 .25 .37 .50	mm. 0.02 .15 .27 .40	mm. 0.05 .17 .30 .42 .55	mm. 0.07 .20 .32 .45 .57	mm. 0.10 .22 .35 .47 .60	mm. 0.00 .13 .25 .37	mm. 0.03 .15 .27 .40 .52	mm. 0.05 .17 .30 .42 .55	mm. 0.07 .20 .32 .45 .57	mm. 0.10 .22 .35 .47 .60
5 6 7 8 9	0.62 .74 .87 .99	0.65 •77 .89 1.02 1.14	0.67 •79 •92 1.04 1.17	0.69 .82 .94 1.07 1.19	0.72 .84 .97 1.09	0.62 •75 •87 1.00	0.65 •77 •90 1.02	0.67 .80 .92 1.05 1.17	0.70 .82 .95 1.07 1.20	0.72 .85 .97 I.10 I.22
10	1.24	1.26	1.29	1.31	1.34	1.25	1.27	1.30	1.32	1.35
11	1.36	1.39	1.41	1.44	1.46	1.37	1.40	1.42	1.45	1.47
12	1.49	1.51	1.54	1.56	1.59	1.50	1.52	1.55	1.57	1.60
13	1.61	1.64	1.66	1.68	1.71	1.62	1.65	1.67	1.70	1.72
14	1.73	1.76	1.78	1.81	1.83	1.75	1.77	1.80	1.82	1.85
15	1.86	1.88	1.91	1.93	1.96	1.87	1.89	1.92	1.94	1.97
16	1.98	2.01	2.03,	2.06	2.08	1.99	2.02	2.04	2.07	2.09
17	2.10	2.13	2.15	2.18	2.20	2.12	2.14	2.17	2.19	2.22
18	2.23	2.25	2.28	2.30	2.33	2.24	2.27	2.29	2.32	2.34
19	2.35	2.38	2.40	2.43	2.45	2.37	2.39	2.42	2.44	2.47
20	2.47	2.50	2,52	2.55	2.57	2.49	2.52	2.54	2.57	2.59
21	2.60	2.62	2,65	2.67	2.70	2.62	2.64	2.66	2.69	2.71
22	2.72	2.75	2,77	2.80	2.82	2.74	2.76	2.79	2.81	2.84
23	2.84	2.87	2,89	2.92	2.94	2.86	2.89	2.91	2.94	2.96
24	2.97	2.99	3,02	3.04	3.07	2.99	3.01	3.04	3.06	3.09
25	3.09	3.12	3.14	3.16	3.19	3.11	3.14	3.16	3.19	3.21
26	3.21	3.24	3.26	3.29	3.31	3.23	3.26	3.28	3.31	3.33
27	3.34	3.36	3.39	3.41	3.43	3.36	3.38	3.41	3.43	3.46
28	3.46	3.48	3.51	3.53	3.56	3.48	3.51	3.53	3.56	3.58
29	3.58	3.61	3.63	3.66	3.68	3.61	3.63	3.66	3.68	3.70
30	3.71	3.73	3.75	3.78	3.80	3.73	3.75	3.78	3.80	3.83
31	3.83	3.85	3.88	3.90	3.93	3.85	3.88	3.90	3.93	3.95
32	3.95	3.98	4.00	4.02	4.05	3.98	4.00	4.03	4.05	4.08
33	4.07	4.10	4.12	4.15	4.17	4.10	4.13	4.15	4.17	4.20
34	4.20	4.22	4.25	4.27	4.29	4.22	4.25	4.27	4.30	4.32
35	4.32	4.34	4.37	4.39	4.42	4.35	4-37	4.40	4.42	4.45

TABLE 47.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н		F ТНЕ В 70 mm	AROMET	ER	н	EIGHT O	F THE F 75 mm		ER
Attached Ther- mometer.	0:0	0:2	0°.4	0.6	0:8	0:0	0°2	0°.4	0%	0°8
c. 0° 1 2 3 4 5 6 7 8	mm. 0.00 .13 .25 .38 .50 0.63 .75	nm. 0.03 .15 .28 .40 .53 0.65 .78	mm. 0.05 .18 .30 .43 .55 0.68 .80	mm. 0.08 .20 .33 .45 .58 0.70 .83 .958	mm. 0.10 .23 .35 .48 .60 0.73 .85	mm. 0.00 .13 .25 .38 .51 0.63 .76 .89	mm. 0.03 .15 .28 .40 .53 0.66 .78	mm. 0.05 .18 .30 .43 .56 0.68 .81	mm. 0.08 .20 .33 .46 .58 0.71 .83	mm. 0.10 .23 .35 .48 .61 0.73 .86
9 10 11 12 13 14	1.01 1.13 1.26 1.38 1.51 1.63 1.76	1.03 1.16 1.28 1.41 1.53 1.66 1.78	1.06 1.18 1.31 1.43 1.56 1.68 1.81	1.08 1.21 1.33 1.46 1.58 1.71 1.83	1.11 1.23 1.36 1.48 1.61 1.73 1.86	1.14 1.26 1.39 1.52 1.64 1.77	1.04 1.16 1.29 1.42 1.54 1.67 1.79	1.06 1.19 1.31 1.44 1.57 1.69 1.82	1.09 1.21 1.34 1.47 1.59 1.72 1.84	1.11 1.24 1.36 1.49 1.62 1.74 1.87
15 16 17 18 19	1.88 2.01 2.13 2.26 2.38	1.91 2.03 2.16 2.28 2.41 2.53	1.93 2.06 2.18 2.31 2.43	1.96 2.08 2.21 2.33 2.46	1.98 2.11 2.23 2.36 2.48	1.89 2.02 2.15 2.27 2.40	1.92 2.05 2.17 2.30 2.42	1.94 2.07 2.20 2.32 2.45	1.97 2.10 2.22 2.35 2.47	2.00 2.12 2.25 2.37 2.50
21 22 23 24 25	2.51 2.63 2.76 2.88 3.01 3.13	2.53 2.66 2.78 2.91 3.03 3.16	2.50 2.68 2.81 2.93 3.06	2.50 2.71 2.83 2.96 3.08	2.73 2.86 2.98 3.11	2.52 2.65 2.77 2.90 3.03	2.55 2.67 2.80 2.93 3.05	2.57 2.70 2.83 2.95 3.08	2.72 2.85 2.98 3.10	2.02 2.75 2.88 3.00 3.13
26 27 28 29	3.26 3.38 3.51 3.63	3.28 3.41 3.53 3.65	3.31 3.43 3.56 3.68	3.33 3.46 3.58 3.70	3.36 3.48 3.60 3.73 3.85	3.28 3.40 3.53 3.65	3.30 3.43 3.55 3.68	3.33 3.45 3.58 3.70	3.35 3.48 3.60 3.73	3.38 3.50 3.63 3.75 3.88
31 32 33 34 35	3.88 4.00 4.13 4.25	3.90 4.03 4.15 4.28	3.93 4.05 4.18 4.30	3.95 4.08 4.20 4.33	3.98 4.10 4.23 4.35	3.90 4.03 4.15 4.28	3.93 4.05 4.18 4.30	3.95 4.08 4.20 4.33	3.98 4.10 4.23 4.35	4.00 4.13 4.25 4.38

TABLE 47.

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTEO.

METHO MENOCILES

	н		F ТНЕ В '80 mm		ER	H		F ТИЕ В '85 mn		ER
Altached Ther- mometer.	0:0	0°2	0°4	0:6	0:8	0.0	0°2	0°4	0°6	0.8
C. 0° 1 2 3 4	mm. 0.00 .13 .25 .38	mm. 0.03 .15 .28 .41 .53	mm. 0.05 .18 .31 .43 .56	mm. 0.08 .20 .33 .46 .59	mm. 0.10 .23 .36 .48 .61	mm. 0.00 .13 .26 .38 .51	mm. 0.03 .15 .28 .41 .54	mm. 0.05 .18 .31 .44 .56	mm. 0.08 .21 •33 .46 •59	mm. 0.10 .23 .36 .49 .62
5 6 7 8 9	0.64 .76 .89 1.02	0.66 .79 .92 1.04 1.17	0.69 .81 .94 1.07 1.20	0.71 .84 .97 1.09	0.74 .87 .99 1.12 1.25	0.64 •77 •90 1.02 1.15	0.67 .79 .92 1.05 1.18	0.69 .82 .95 1.08 1.20	0.72 .85 .97 I.10 I.23	0.74 .87 1.00 1.13 1.25
10 11 12 13 14	I.27 I.40 I.53 I.65 I.78	1.30 1.42 1.55 1.68 1.81	1.32 1.45 1.58 1.70 1.83	1.35 1.48 1.60 1.73 1.86	1.37 1.50 1.63 1.75 1.88	1.28 1.41 1.54 1.66 1.79	1.31 1.43 1.56 1.69 1.82	1.33 1.46 1.59 1.71 1.84	1.36 1.48 1.61 1.74 1.87	1.38 1.51 1.64 1.77 1.89
15 16 17 18	1.91 2.03 2.16 2.29 2.41	1.93 2.06 2.19 2.31 2.44	1.96 2.08 2.21 2.34 2.46	1.98 2.11 2.24 2.36 2.49	2.01 2.13 2.26 2.39 2.51	1.92 2.05 2.17 2.30 2.43	1.94 2.07 2.20 2.33 2.45	1.97 2.10 2.22 2.35 2.48	2.00 2.12 2.25 2.38 2.51	2.02 2.15 2.28 2.40 2.53
20 21 22 23 24	2.54 2.67 2.79 2.92 3.05	2.57 2.69 2.82 2.94 3.07	2.59 2.72 2.84 2.97 3.10	2.62 2.74 2.87 3.00 3.12	2.64 2.77 2.89 3.02 3.15	2.56 2.68 2.81 2.94 3.07	2.58 2.71 2.84 2.96 3.09	2.61 2.73 2.86 2.99 3.12	2.63 2.76 2.89 3.01 3.14	2.66 2.79 2.91 3.04 3.17
25 26 27 28 29	3.17 3.30 3.42 3.55 3.68	3.20 3.32 3.45 3.58 3.70	3.22 3.35 3.47 3.60 3.73	3.25 3.37 3.50 3.63 3.75	3.27 3.40 3.53 3.65 3.78	3.19 3.32 3.45 3.57 3.70	3.22 3.34 3.47 3.60 3.73	3.24 3.37 3.50 3.62 3.75	3.27 3.40 3.52 3.65 3.78	3.29 3.42 3.55 3.67 3.80
30 31 32 33 34	3.80 3.93 4.05 4.18 4.31	3.83 3.95 4.08 4.21 4.33	3.85 3.98 4.11 4.23 4.36	3.88 4.00 4.13 4.26 4.38	3.90 4.03 4.16 4.28 4.41	3.83 3.95 4.08 4.21 4.33	3.85 3.98 4.11 4.23 4.36	3.88 4.00 4.13 4.26 4.39	3.90 4.03 4.16 4.28 4.41	3.93 4.06 4.18 4.31 4.44
35	4.43	4. 46	4.48	4.51	4.53	4.46	4.49	4.51	4.54	4.56

TABLE 47.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	В	-	F THE 1		ER	F		OF THE 1		YER
Attached Ther- mometer.	0°0	0°2	0°4	0°6	0°8	0:0	0°2	0:4	0.6	0°8
C. 0° 1 2 3 4	mm. 0.00 .13 .26 .39	mm. 0.03 .15 .28 .41	mm. 0.05 .18 .31 .44	mm. 0.08 .21 .34 .46 .59	mm. 0.10 .23 .36 .49 .62	mm. 0.00 .13 .26 .39	mm. 0.03 .16 .29 .42 .55	mm. 0.05 .18 .31 .44 .57	mm. 0.08 .21 .34 .47 .60	mm. 0.10 .23 .36 .49
5 6 7 8 9	0.64 •77 .90 1.03 1.16	0.67 .80 .93 1.06 1.19	0.70 .83 .95 1.08 1.21	0.72 .85 .98 1.11 1.24	0.75 .88 I.01 I.13 I.26	0.65 .78 .91 1.04 1.17	0.67 .80 .93 1.06 1.19	0.70 .83 .96 1.09	0.73 .86 .99 1.12 1.24	0.75 .88 1.01 1.14 1.27
10 11 12 13 14	1.29 1.42 1.55 1.67 1.80	1.31 1.44 1.57 1.70 1.83	1.34 1.47 1.60 1.73 1.85	1.37 1.49 1.62 1.75 1.88	1.39 1.52 1.65 1.78 1.91	1.30 1.43 1.56 1.68 1.81	1.32 1.45 1.58 1.71 1.84	1.35 1.48 1.61 1.74 1.87	1.37 1.50 1.63 1.76 1.89	1.40 1.53 1.66 1.79 1.92
15 16 17 18	1.93 2.06 2.19 2.32 2.44	1.96 2.09 2.21 2.34 2.47	1.98 2.11 2.24 2.37 2.50	2.01 2.14 2.26 2.39 2.52	2.03 2.16 2.29 2.42 2.55	1.94 2.07 2.20 2.33 2.46	1.97 2.10 2.23 2.36 2.49	1.99 2.12 2.25 2.38 2.51	2.02 2.15 2.28 2.41 2.54	2.05 2.18 2.30 2.43 2.56
20 21 22 23 24	2.57 2.70 2.83 2.96 3.08	2.60 2.73 2.85 2.98 3.11	2.62 2.75 2.88 3.01 3.14	2.65 2.78 2.91 3.03 3.16	2.67 2.80 2.93 3.06 3.19	2.59 2.72 2.85 2.98 3.10	2.61 2.74 2.87 3.00 3.13	2.64 2.77 2.90 3.03 3.16	2.67 2.79 2.92 3.05 3.18	2.69 2.82 2.95 3.08 3.21
25 26 27 28 29	3.21 3.34 3.47 3.60 3.72	3.24 3.37 3.49 3.62 3.75	3.26 3.39 3.52 3.65 3.77	3.29 3.42 3.54 3.67 3.80	3.31 3.44 3.57 3.70 3.83	3.23 3.36 3.49 3.62 3.75	3.26 3.39 3.52 3.64 3.77	3.28 3.41 3.54 3.67 3.80	3.31 3.44 3.57 3.70 3.82	3.34 3.46 3.59 3.72 3.85
30 31 32 33 34	3.85 3.98 4.11 4.23 4.36	3.88 4.00 4.13 4.26 4.39	3.90 4.03 4.16 4.29 4.41	3.93 4.06 4.18 4.31 4.44	3.95 4.08 4.21 4.34 4.46	3.88 4.00 4.13 4.26 4.39	3.90 4.03 4.16 4.29 4.42	3.93 4.06 4.18 4.31 4.44	3.95 4.08 4.21 4.34 4.47	3.98 4.11 4.24 4.36 4.49
35	4-49	4.51	4.54	4.57	4.59	4.52	4.54	4-57	4.59	4.62

CORRECTIONS TO REDUCE BAROMETRIC READINGS TO STANDARD CRAVITY.

$$C = \frac{(g_l - g)}{g} B$$

(WITH $\mathbf{g}_t \! < \! \mathbf{g}$ the correction is to be subtracted; with $\mathbf{g}_t \! > \! \mathbf{g}$, it is to be added.)

				ВА	ROMETEI	READIN	G <i>B</i> ,			
g ₁ — g	1.0	2.0	3.0	4.0	5.0	6.0	7.0.	8.0	9.0	10.0
Dynes.	Dyne,	Dyne.	Dyne.	Dyne.	Oyne.	Dyne,	Dyne.	Оуле.	Oyne,	Dyne.
0.1	-	0.00020		, ,	0.00051	0.00061	, -	0.00082	0.00002	0.00102
0.2	00020	00041	00061	00082	00102	00122	00143	00163	00184	00204
0.3	00031	00061	00002	00122	00153	00184	00214	00245	00275	00306
0.4	00041	00082	. 00122	00163	00204	00245	00286	00326	00367	00408
0.5	00051	00102	00153	00204	00255	00306	00357	00408	00459	00510
0.6	0.00061	0.00122	0.00184	0.00245	0.00306	0.00367	0.00428	0.00489	0.00551	0.00612
0.7	00071	00143	00214	00286	00357	00428	00500	00571	00642	00714
0.8	00082	00163	00245	00326	00408	00489	00571	00653	00734	00816
0.9	00092	00184	00275	00367	00459	00551	00642	00734	00826	00918
1.0	00102	00204	00306	00408	00510	00612	00714	00816	00918	01020
1.1	0.00112	0.00224	0.00337		0.00561	0.00673	0.00785	0.00897	0.01010	0.01122
1.2	00122	00245	00367	00489	00612	00734	00857	00979	01101	01224
1.3	00133	00265	00398	00530	00663	00795	00928	01061	01193	01326
1.4	00143	00286	00428	00571	00714	00857	00999	01142	01285	01428
1.5	00153	00306	00459	00612	00765	00018	01071	01224	01377	01530
1.6	0.00163	0.00326	0.00489		0.00816	0.00979	0.01142	0.01305	0.01468	0.01632
1.7	00173	00347	00520	00693	00867	01040	01213	01387	01560	01734
1.8	00184	00367	00551	00734	00918	01101	01285	01468	01652	01835
1.9	00194	00387	00581	00775	00 969	01162	01356	01550	01744	01937
2,0	00204	00408	00612	00816	01020	01224	01428	01632	01835	02039
2.1		0.00428	0.00642		0.01071				0.01927	
2.2	00224	00449	00673	00897	01122	01346	01570	01795	02019	02243
2.3	00235	00469	00704	00938	01173	01407	01642	01876	02111	02345
2.4	00245	00489	00734	00979	01224	01468	01713	01958	02203	02447
2.5	00255	00510	00765	01020	01275	01530	01785	02039	02294	02549
2.6	0.00265	0.00530			0.01326			0.02121		0.02651
2.7	00275	00551	00826	01101	01377	01652	01927	02203	02478	02753
2.8	00286	00571	00857	01142	01428	01713	01999	02284	02570	02855
2.9	00296	00591	00887	01183	01479	01774	02070	02366	02661	02958
3.0	00306	00612	00918	01224	01530	01835	02141	02447	02753	03059
3.1	0.00316	0.00632	0.00948		0.01581	0.01897	0.02213	0.02529	0.02845	0.03161
3.2	00326	00653	00979	01305	01632	01958	02284	02610	02937	03263
3.3	00337	00673	01010	01346	01683	02019	02356	02692	03029	o 3365
3.4	00347	00693	01040	01387	01734	02080	02427	02774	03120	03467
3.5	00357	00714	01071	01428	01785	02141	02498	02855	03212	03569
3.6	0.00367	0.00734	0.01101	0.01468	0.01835	0.02203	0.02570	0.02937	0.03304	0.03671
3.7	00377	00755	01132	01509	01886	02264	02641	03018	03396	03773
3.8	00387	.00775	01162	01550	01937	02325	02712	03.100	03487	
3.9	00398	00795	01193	01591	01988	02386	02784	03182	03579	03977
4.0	00408	00816	01224	01632	02039	02447	02855	03263	03671	04079
	<u> </u>	<u> </u>	1	<u> </u>	1	<u> </u>	<u> </u>	1	1	<u></u>

TABLE 49.

REDUCTION OF THE BAROMETER TO STANDARD CRAVITY. ENGLISH MEASURES.

FROM LATITUDE 0° TO 45°, THE CORRECTION IS TO BE SUBTRACTED.

Lati- tude.	19			HEIGHT OF THE BAROMETER IN INCHES.													
tude.	19 20 21 22 23 24 25 26 27 28 29 30																
		20	21	22	23	24	25	26	27	28	29	30					
	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	ľnch.	Inch.	Inch.	Inch.	Inch.	Inch.					
0°	-0.051	-0.054	-0.056	-0.059	-0.0 62	-0.064	-0.067	-0.070	-0.072	-0.075	-0.0 78	-0.080					
5	-0.050 0.050	-0.053 0.052	-0.055 0.055	-0.058 0.058	-0.061 0.060	-0.063 0.063	-0.066 0.066	-0.069 0.068	-0.07I	-0.074 0.073	-0.077 0.076						
	0.040	0.052	0.055	0.057	0.060	0.062	0.065	0.068	0.070	0.073	0.075						
7 8	0.049	0.052	0.054		0.059	0.062	0.064	0.067	0.070	0.072	0.075						
	0.048	0.051	0.054	~	0.059	0.061	0.064	0.066	0,069	0.071	0.074	0.076					
9	0.040	0.051	0,034	0.030					,	·	• •						
10	-0.048	-0.050	-0.053	-0.055	-0.058		-0.063	-0.0 66			-0.073						
II	0.047	0.050	0.052	0.055	0.057	0.060		0.065	0.067	0.070	0.072						
12	0.047	0.049	0.051	0.054	0.056		0.061	0.064	0.066	0.069	0.071						
13	0.046	o. o 48	0.051	0.053	0.055	0.058			0.065	0.068	0.070						
14	0.045	0.047	0.050	0.052	0.055	0.057	0.059	0.062	0.0 64	0.066	0.069	0.071					
15	-0.044	-0.047	-0.049	-0.051	-0.053	- 0.0 56	-0.058										
16	0.043	0.046	0.048	0.050	0.052	0.055	0.057	0.059	0.062	0.064	0.066						
17	0.042	0.045	0.047	0.049	0.051	0.053	0.056	0.058	0.060	0.062							
18	0.041	0.044	0.046	0.048	0.050	0.052	0.054	0.057	0.059	0.0 61	0.063	0.065					
19	0.040	0.042	0.045	0.047	0.049	0.051	0.053	0.055	0.057	0.059	0.0 62	0.064					
20	-0.039	-0.041	-0.043	-0.045	-0.047	-0.050	-0.052	-0.054	-0.056	-0.058	-0.060	-0.062					
21	0.038				0.046				0.054	0.056							
22	0.037	0.030					0.040	0.050		0.054							
23	0.036	0.038				0.045	0.047	0.049		0.053							
24	0.034	0.036				0.043	0.045	0.047	0.049	0.051							
25	-0.033	-0.035	-0.037	-0.038	-0.040	-0.042	-0.043	-0.045	-0.047	-0.040	-0.050	-0.052					
26	0.032	0.033		0.037	0.038		0.042		0.045	0.047	0.048						
27	0.030	0.032		0.035	0.037	0.038	0.040		0.043	0.045							
28	0.020	0.030					0.038			0.043							
29	0.027	0.029			0.033	0.035	0.036		0.039	0.040							
30	- 0.0 26	-0.027	-0.029	-0.030	-0.031	-0.033	-0.034	-0.035	-0.037	-0.038	-0.040	-0.041					
31	0.024	0.026			0.030		0.032		0.035	0.036							
32	0.023	0.024					0.030			0.034							
33	0.021	0.022					0.028		0.030	0.031							
34	0.020	0.021			0.024		0.026	-									
35	-0.018	-0.019	-0.020	-0.021	-0.022	0.023	-0.024	-0.025	-0.026	-0.027	-0.027	-0.028					
36	0.016		0.018				0.022		0.023	0.024							
37	0.015	0.015	_		0.018					0.022							
38	0.013	0.013		0.015					_	0.019	(
39	0.013	0.012					0.015			0.017							
40	-0.010	-0.070	-0.011	-0.011	-0.012	-0.012	-0.013	-0.013	-0.014	-0.0T4	-0.015	-0.015					
41	0.008					0.012	0.010		0.011								
42	0.006	0.006		0.007	0.007	0.008				i	1						
	0.004	0.005		0.005		l .											
43 44	0.003		0.003	0.003	0.003	0.003	0.003	I .	1	1							
45	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001					

REDUCTION OF THE BAROMETER TO STANDARD GRAVITY.

ENGLISH MEASURES.

FROM LATITUDE 46° TO 90° THE CORRECTION IS TO 8E ADDED.

Lati- tude.	19															
		20	21	22	23	24	25	26	27	28	29	30				
1	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.				
45°	-0.001	-0.001	-0.001		!	-0.001	4	-0.001	l	-0.001	-0.001	-0.001				
46	+0.001	±0.001	+0.001	±0.00⊺	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001				
47	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.004		0.004	0.004	0.004				
48	0.004	0.005	0.005	0.005	0.005	0.006	0.006		0.006	0.006		0.007				
49	0.006	0.006	0.007	0.007	0.007	0.008			0.000	0.000		0.010				
50	0.008	0.008	0.009	0.000	0.010	0.010		0.011	0.011	0.012		0.012				
5l	1 - 070	10070		10077	10010	10.070	10.074	10050	10074	10014	10075					
1 1							+0.013				+0.015					
52	0.011	0.012		0.013	0.014	0.014	0.015	0.015	0.016	0.016		0.018				
53	0.013	0.014	0.014	0.015		0.016	0.017		0.018	0.019		0.020				
54	0.015	0.015	0.016	0.017		0.019	0.019	0.020	0.021	0.022		0.023				
55	0.016	0.017	0.018	0.019	0.020	0.021	0.021	0.022	0.023	0.024	0.025	0.026				
56	+0.018	+0.019	+0.020	+0.021	+0.022	+0.023	+0.024	+0.024	+0.026	+0.026	+0.027	+0.028				
57	0.020	0.021	0.022	0.023	0.024	0.025	0.026	0.027	0.028	0.029	0.030	0.031				
58	0.021	0.022	0.023	0.025	0.026	0.027	0.028	0.029	0.030	0.031	0.032	0.033				
59	0.023	0.024	0.025	0.026	0.028	0.020	0.030	0.031		0.033	0.035	0.036				
60	0.024	0.026	0.027	0.028	0.029	0.031	0.032	0.033	0.034	0.036	0.037	0.038				
61	±0.026	±0.027	⊥o o28	±0.020	±0.021	+0.022	+0.024	+0.025	+0.027	40.028	+0.039	±0.04T				
62	0.027	0.020	0.030	0.032	0.033	0.034	0.036	0.037	0.039	0.040	0.042					
		- 1			0.035	0.036	0.038	0.030				0.043				
63	0.029	0.030	0.032	0.033				0,	0.041	0.042	0.044	0.045				
64	0.030	0.032	0.033	0.035	0.036	0.038		0.041	0.043	0.044	0.046	0.047				
65	0.031	0.033	0.035	0.036	0.038	0.040	0.041	0.043	0.045	0.046	0.048	0.050				
66	+0.033	+0.034	+0.036						+0.047	+0.048	+0.050	+0.052				
67	0.034	0.036	0.038	0.039	0.041	0.043	0.045	0.047	0.048	0.050	0.052	0.054				
68	0.035	0.037	0.039	0.041	0.043	0.045	0.046	0.048	0.050	0.052	0.054	0.056				
69	0.036	0.038	0.040	0.042	0.044	0.046	0.048	0.050	0.052	0.054	0.056	0.058				
70	0.038	0.040	0.042	0.044	0.046	0.048	0.050	0.052	0.053	0.055	0.057	0.059				
71	+0.030	+0.041	+0.043	+0.045	+0.047	+0.040	+0.051	+0.053	+0.055	+0.057	+0.059	±0.061				
72	0.040	0.042	0.044	0.046	0.048	0.050		0.054	0.057	0.050	0.061	0.063				
73	0.041	0.043	0.045	0.047	0.049	0.052	0.054	0.056		0.060		0.064				
74	0.042	0.044	0.046	0.048		0.053	0.055	0.057	0.050	0.062	0.064	0.066				
75	0.043	0.045	0.047	0.049		0.054	0.056			0.063	0.065	0.067				
				1000	الممتا		1000	10.06-		16	6 6					
											+0.066					
77	0.044	0.047	0.049	0.051	0.054	0.056	0.058	0.061	0.063	0.065	0.068	0.070				
78	0.045	0.047	0.050	0.052	0.055	0.057	0.059	0.062		0.066		0.071				
79	0.046	0.048	0.051	0.053	0.055	0.058	0.060	0.063	0.065	0.067	0.070	0.072				
80	0.046	0.049	0.051	0.054	0.056	0.059	0.061	0.063	0.066	0.0 68	0.071	0.073				
81	+0.047	+0.040	+0.052	+0.054	+0.057	+0.050	+0.062	+0.064	+0.067	+0.06n	+0.072	+0.074				
82	0.047	0.050	0.052	0.055		0.060			0.067	0.070		0.075				
83	0.048	0.050	0.053	0.056		0.061	0.063			0.071		0.076				
84	0.048	0.051	0.053	0.056		0.061	0.064					0.076				
85	0.049	0.051	0.054			0.061	0.064		0.069							
•	+0.049	+0.052	+0.055	+0.057	+0.060	+0. 062	+0.065	+0.068	+0.070	+0.073	+0.075	+0.078				

TABLE 50.

REDUCTION OF THE BAROMETER TO STANDARD CRAVITY.

METRIC MEASURES.

FROM LATITUDE 0° TO 45°, THE CORRECTION IS TO BE SUBTRACTEO.

Lati-				HE	IGHT O	Г ТНЕ	BARO	METER	IN MII	LIMET	ERS.		-	
tude.	520	540	560	580	600	620	640	660	680	700	720	740	760	780
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
0°	-1.39	-1.45	-1.50	-1.55	-1.61	-1.66	- 1. 71	-1.77	-1.82	-I.87	-1.93	-1.98	-2.04	-2.09
5	-1.37	-1.42	-1.48	-1.53	-1.58	-1.64	-1.69	-1.74	-1.79	-1.85	-1. <u>9</u> 0		-2.00	-2.06
6	1.36	1.42	1.47	1.52	1.57	1.63	1.68	1.73	1.78	1.83	1.89 1.87	1.94	1.99	2.04
7 8	1.35 1.34	1.40 1.30	1.46 1.44	I.51 I.49	1.56 1.55	1.61	1.66 1.65	1.72 1.70	1.77 1.75	1.82 1.80	1.85	I.92 I.91	1.98 1.96	2.03 2.01
9	1.33	1.38	1.43	1.48	1.53	1.58	1.63	1.68	1.73	1.78	1.84	1.89	1.94	1.99
10	-1.31	_1.36	-1.41	-1.46	-1.51	-1.56	-1.61	-1.66	-1.71	-1.76	-1.81	-1.86	-I.Q2	-1.97
11	1.29	1.34	1.39	1.44	1.49	1.54	1.59	1.64	1.69	1.74	1.79	1.84	1.89	1.94
12	1.27	1.32	1.37	1.42	1.47	1.52	1.57	1.62	1.67	1.72	1.76	1.81	1.86	1.91
13	1.25	1.30	1.35	1.40	1.45	1.50	1.54	1.59 1.56	1.64 1.61	1.69 1.66	1.74 1.71	1.78 1.75	1.83 1.80	1.88
14	1.23	1	1.33	1.38	1.42	1.47	1.52							
15	-1.21	-1.26			-1.40	-1.44	-1.49	-1.54	-1.58	-1.63	-1.67	-1.72	-1.77	-1.81
16	1.19 1.16	1.23	1.28	1.32	I.37 I.34	1.41	1.46	1.50	1.55 1.52	1.60 1.56	1.64 1.60	1.69 1.65	1.73 1.60	1.78
17	1.13	1 -		1.26	1.31	1.35	1.39	1.44	1.48	1.52	1.57	1.61	1.65	1.70
19	1.10		1.19		1.27	1.32	1.36	1.40	1.44	1.48	1.53	1.57	1.61	1.65
20	-1.07	-1.11	-1.16		-1.24	-1.28	-1.32	-1.36	-1.40	-1.44	-1.49	-1.53	-1.57	-1.61
21	1.04	1.08	1.12	1.16	1.20	1.24	1.28	1.32 1.28	1.36	1.40	1.44	1.48	1.52	1.56
22	1.01		1.09	1.13	1.16	1.20	I.24 I.20	1.24	1.32 1.28	1.36	1.40 1.35	I.44 I.39	1.48	1.51 1.46
23 24	0.94			1.05	1.08	1.12	1.16	1.19	1.23	1.27	1.30	1.34	1.37	1.41
25	-0.90	-0.94		-1.01	-1.04	-1.08	-1.11	-1.15	-1.18	-1.22	-1.25	-1.29	-1.32	-1.36
26	0.87			0.97	1.00	1.03	1.07	1.10	1.13	1.17	1.20	1.23	1.27	1.30
27	0.83			0.92	0.96 0.91	0.99 0.94	0.97	1.05	1.08	1.12 1.06	1.15	1.18	1.21	1.24
28 29	0.79 0.75				0.86	0.89	0.92	0.95	0.98	1.01	1.04		1.10	1.12
30	-0.71	-0.74	-0.76	-0.79	-0.82	-0.85	-0.87	-0.90	-0.93		-0. 98		-1.04	-1.06
31	o .67	0.69			0.77	0.80	0.82	0.85	0.87	0.90	0.92		0.98	
32	0.62 0.58					0.74	0.77	0.79	0.82	0.84	o.86 o.80		0.91	0.94
33 34	0.54	0.56				0.64	0.66	0.68	0.70		0.74		0.79	0.81
35	- 0. 49	-0.51	-0.53	-0.55	-0.57	-0.59	- 0. 61	-0.63						
36	0.45	0.46		0.50	0.52	0.53	0.55							
37	0.40		1 . 2			0.48	0.49				0.56		0.59	
38 39	0.36 0.31						1					_		1
40	-0:26	-0.27	-0.28	-0.20	-0.30	-0.31	-0.32	-0.33	-0.34	-0.35	- 0. 36	-0.37	-0.38	-0.39
41	0.21		0.23	0.24	0.25	0.26	0.26	0.27	0.28	0.29	0.30	0.30	0.31	0.32
42	0.17						1							
43	0.12						_			1	1	4 '	1 .	
44						-0.03			1	-0.03		-0.03		
45	-0.02	-0.02	-0.03						-0.03	-0.03	0.03	0.03	0.03	0.04

REDUCTION OF THE BAROMETER TO STANDARD GRAVITY.

METRIC MEASURES.

FROM LATITUDE 46° TO 90°, THE CORRECTION IS TO BE ADDED.

				HE	IGHT (OF THE	BARO	METER	IN MI	LLIME	TERS.			
Lati- tude.	520	540	560	580	600	620	640	660	680	700	720	740	760	780
45°	mm. 0.02	mm, -0.02	mm. -0.03	mm. 0.03	mm, -0.03	mm. 0.03	mm.	mm. -0.03	mm. -0.03	mm. 0.03	mm.	mm.	mm. -0.03	mm. 0.04
46	-d-0.02 0.07	+0.03	+0.03			+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.04	+0.04
48 49	0.12 0.17	0.12 0.17	0.13	0.13	0.14 0.19	0.14	0.21	0.09 0.15 0.21	0.09	0.16	0.10	0.10 0.17 0.24	0.10 0.18 0.25	0.11 0.18 0.25
50 51 52	+0.26 0.31	+0.27 0.32	l *				+0.32	+0.33			+0.36	+0.37	+0.38	+0.39
53 54 55	0.36 0.40 0.45		0.33 0.38 0.43 0.48	0.34 0.40 0.45 0.50	0.36 0.41 0.46 0.52	0.37 0.42 0.48 0.53	0.38 0.44 0.49 0.55	0.39 0.45 0.51 0.57	0.40 0.46 0.52 0.58	0.42 0.48 0.54 0.60	0.43 0.49 0.56 0.62	0.44 0.51 0.57 0.64	0.45 0.52 0.59 0.65	0.46 0.53 0.60 0.67
56 57	+0.49	'	+0.53 0.58		Ĭ		+0.60 0.66				+0.68	+0.70	٦	+0.74
58 59 60	0.58 0.62 0.66	0.60 0.65	0.6 ₂ 0.6 ₇ 0.7 ₂	0.65 0.69 0.74	0.67 0.72 0.77	0.69 0.74 0.79	0.71 0.77 0.82	0.74 0.79 0.84	0.76 0.81 0.87	0.78 0.84 0.89	0.80 0.86 0.92	0.82 0.89 0.94	0.85 0.91 0.97	0.87 0.93 1.00
61 62	+0.71 0.74	+0.73	0.80	+0.79 0.83	0.85	+0.84 0.88	0.91	0.94	0.97	1.00	I.O2	+1.00 1.05	1.08	1.11
63 64 65	0.78 0.82 0.86	0.81 0.85 0.89	0.85 0.89 0.93	0.88 0.92 0.96	0.91 0.95 0.99	0.94 0.98 1.03	0.97 1.01 1.06	1.00 1.04 1.09	1.03 1.08 1.13	1.06 1.11 1.16	1.09 1.14 1.19	1.12 1.17 1.22	I.15 I.20 I.26	1.18
66 67 68	+0.90 0.93 0.97	+0.93 0.97	+0.97 1.00 1.04	+1.00 1.04 1.08	+1.04 1.08 1.11	+1.07 1.11 1.15	+1.10 1.15 1.19	+1.14 1.18 1.23	+1.17 1.22 1.26	+1.21 1.25 1.30	+1.24 1.29 1.34	1.33	+1.31 1.36 1.41	+1.35 1.40
69 70	1.00	1.04	1.08	1.11	1.15	1.19	1.23	1.27	1.31	1.34 1.39	1.38 1.43	1.37 1.42 1.47	1.46 1.51	1.45 1.50 1.55
71 72 73	+1.06 1.09 1.12	1.13 1.16	+1.14 1.17 1.20	+1.18 1.22 1.25	1.26 1.29	1.30 1.33	+1.31 1.34 1.37	+1.35 1.38 1.42	+1.39 1.42 1.46	+1.43 1.47 1.50	+1.47 1.51 1.55	+1.51 1.55 1.59	+1.55 1.59 1.63	+1.59 1.63 1.67
74 75	1.14	1.19	1.23 1.26	1.28	1.32 1.35	1.36 1.39	1.41 1.44	1.45 1.48	1.50	1.54 1.57	1.58	1.63 1.66	1.67	1.72
76 77 78	+1.19 1.21 1.23 1.25	+1.24 1.26 1.28 1.30	+1.28 1.31 1.33 1.35	+1.33 1.35 1.38 1.40	+1.37 1.40 1.42 1.45	+1.42 1.45 1.47 1.49	+1.47 1.49 1.52 1.54	+1.51 1.54 1.57 1.59	+1.56 1.59 1.61 1.64	+1.60 1.63 1.66 1.60	+1.65 1.68 1.71 1.73	+1.70 1.73 1.76 1.78	+1.74 1.77 1.80 1.83	+1.79 1.82 1.85 1.88
79 80 81	1.25 1.27 +1.29	1.32 +1.33	1.37	1.42	.147 +1.48	1.51	1.56 1.58	1.61 +1.63	1.66	1.71	1.76	1.81	1.86	1.90
8 ₂ 8 ₃	1.30 1.31	1.35 1.36	1.40 1.41 1.42	1.45 1.46 1.48	1.50	1.55 1.56 1.58	1.60 1.61 1.63	1.65 1.67 1.68	1.70 1.72	1.75 1.77 1.78	1.80 1.82 1.83	1.85 1.87 1.88	1.90 1.92	1.95 1.97
8 ₅	1.33	1.38	1.43	1.49	1.54	1.59	1.64	1.69 +1.72	1.74	1.79	1.84	1.90	1.95	2.00
84 85	1.32 1.33	1.37 1.38	I.42 I.43	1.48 1.49	1.53 1.54	1.58 1.59	1.63 1.64	1.68 1.69	1.73 1.74	1.78 1.79	1.8 ₃ 1.8 ₄	1.88	1.93 1.95	2.00

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Values of 60368 [1 + 0.0010195 \times 36] log $\frac{29.90}{B}$.

Barometric Pressure. B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
12.00	24814	24791	24769	24746	24723	24701	24678	24656	24633	24611
12.10	24588	24566	24543	24521	24499	24476	24454	24431	24409	24387
12.20	24365	24342	24320	24298	24276	24253	24231	24209	24187	24165
12.30	24143	24121	24098	24076	24054	24032	24010	23988	23966	23944
12.40	23923	23901	23879	23857	23835	23813	23791	23770	23748	23726
12.50	23704	23682	23661	23639	23617	23596	23574	23552	23531	23509
12.60	2 3488	23466	23445	23423	23402	23380	23359	23337	23316	23294
12.70	23273	23251	23230	23209	23187	23166	23145	23123	23102	23081
12.80	23060	23038	23017	22996	22975	22954	22933	22911	22890	22869
12.90	22848	22827	22806	22785	22764	22743	22722	22701	2268ი	22659
13.00	22638	22617	22596	22576	22555	22534	22513	22492	22471	22451
13.10	22430	22409	22388	22368	22347	22326	22306	22285	22264	22244
13.20	22223	22203	22182	22162	22141	22121	22100	22080	22059	22039
13.30	22018	21998	21977	21957	21937	21916	21896	21876	21855	21835
13.40	21815	21794	21774	21754	21734	21713	21693	21673	21653	21633
13.50	21612	21592	21572	21552	21532	21512	21492	21472	21452	21432
13.60	21412	21392	21372	21352	21332	21312	21292	21272	21252	21233
13.70	21213	21193	21173	21153	21134	21114	21094	21074	21054	21035
13.80	21015	20995	20976	20956	20936	20917	20897	20878	20858	20838
13.90	20819	20799	20780	20760	20741	20721	20702	20682	20663	20643
14.00	20624	20605	20585	20566	20546	20527	20508	20488	20469	20450
14.10	20431	20411	20392	20373	20354	20334	20315	20296	20277	20258
14.20	20238	20219	20200 20010	20181	20162	20143	20124	20105	20086	20067
14.30 14.40	20048 19858	19839	19821	19991	199 72 19783	19953 19764 i	19934 19745	19915	19896 19708	19877
			_					-		
14.50	19670	19651	19633	19614	19595	19577	19558	19539	19521	19502
14.60	19483	19465	19446 19261	19428 19242	19409 19224	19390 19206	19372	19353	19335	19316
14.70	19298 19114	19279 19095	19201	19242	19040	19200	19187 19004	19169 1898 5	19150 18967	19132
14.60	18931	18912	18894	18876	18858	18840	18821	18803	18785	18949 18767
15.00	18749	18731	18713	18694	18676	18658	18640	18622	18604	18586
15.10	18568	18550	18532	18514	18496	18478	18460	18442	18425	18407
15.20	18389	18371	18353	18335	18317	18300	18282	18264	18246	18228
15.30	18211	18193	18175	18157	18140	18122	18104	18086	18069	18051
15.40	18033	18016	17998	17981	17963	17945	17928	17910	17893	17875
15.50	17858	17840	17823	17805	17788	17770	17753	17735	17718	17700
15.60	17683	17665	17648	17631	17613	17596	17578	17561	17544	17526
15.70	17509	17492	17474	17457	17440	17423	17405	17388	17371	17354
15.80	17337	17319	17302	17285	17268	17251	17234	17216	17199	17182
15.90	17165	17148	17131	17114	17097	17080	17063	17046	17029	17012
16.00	16995	16978	16961	16944	16927	16910	16893	16876	16859	16842
16.10	16825	16808	16792	16775	16758	16741	16724	16707	16691	16674
16.20	16657	16640	16623	16607	16590	16573	16557	16540	16523	16506
16.30	16490	16473	16456	16440	16423	16406	16390	16373	16357	16340
16.40	16324	16307	16290	16274	16257	16241	16224	16208	16191	16175
16.50	16158	16142	16125	16109	16092	16076	16060	16043	16027	16010
16.60	15994	15978	15961	15945	15929	15912	15896	15880	15863	15847
16.70	15831	15815	15798 15636	15782	15766 15604	15750	15733	15717	15701	15685
16.80 16.90	15669	15652		_	15443	15427	15572 15411	15556	15539	15523
17.00	15507	15491	15475	15459	15443	15267	l -	15395	15379	15363
17.00	15347	15331	15315	15299	15203	1320/	15251	15235	15219	15203

DETERMINATION OF HEIGHTS BY THE BAROMETER.

ENGLISH MEASURES.

Values of 60368 [1 + 0.0010195 \times 36] $\log \frac{29.90}{B}$.

								В		
Barometric Pressure B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
17.00	15347	15331	15315	15299	15283	15267	15251	15235	15219	15203
17.10	15187	15172	15156	15140	15124	15108	15092	15076	15061	15045
17.20	15029	15013	14997	14982	14966	14950	14934	14919	14903	14887
17.30	14871	14856	14840	14824	14809	14793	14777	14762	14746	14730
17.40	14715	14699	14684	14668	14652	14637	14621	14606	14590	14575
17.50	14559	14544	14528	14512	14497	14481	14466	14451	14435	14420
17.60	14404	14389	14373	14358	14342	14327	14312	14296	14281	14266
17.70	14250	14235	14219	14204	14189	14173	14158	14143	14128	14112
17.80	14097	14082	14067	14051	14036	14021	14006	13990	13975	13960
17.90	13945	13930	13914	13899	13884	13869	13854	13839	13824	13808
18.00	13793	13778	13763	13748	13733	13718	13703	13688	13673	13658
18.10	13643	13628	13613	13598	13583	13568	13553	13538	13523	13508
18.20	13493	13478	13463	13448	13433	13418	13404	13389	13374	13359
18.30	13314	13329	13314	13300	13285	13270	13255	13240	13226	13211
18.40	13196	13181	13166	13152	13137	13122	13107	13093	13078	13063
18.50	13049	13034	13019	13005	12990	12975	12961	12946	12931	12917
18.60	12902	12888	12873	12858	12844	12829	12815	12800	12785	12771
18.70	12756	12742	12727	12713	12698	12684	12669	12655	12640	12626
18.80	12611	12597	12583	12568	12554	12539	12525	12510	12496	12482
18.90	12467	12453	12438	12424	12410	12395	12381	12367	12352	12338
19.00	12324	12310	12295	12281	12267	12252	12238	12224	12210	12195
19.10	12181	12167	12153	12138	12124	12110	12096	12082	12068	12053
19.20	12039	12025	12011	11997	11983	11969	11954	11940	11926	11912
19.30	11898	11884	11870	11856	11842	11828	11814	11800	11786	11772
19.40	11758	11744	11730	11716	11702	11688	11674	11660	11646	11632
19.50	11618	11604	11590	11576	11562	11548	11534	11520	11507	11493
19.60	11479	11465	11451	11437	11423	11410	11396	11382	11368	11354
19.70	11340	11327	11313	11299	11285	11272	11258	11244	11230	11217
19.80	11203	11189	11175	11162	11148	11134	11121	11107	110 9 3	11080
19.90	11066	11052	11039	11025	11011	10998	10984	10970	10957	10943
20.00	10930	10916	10903	10889	10875	10862	10848	10835	10821	10808
20.10	10794	10781	10767	10754	10740	10727	10713	10700	10686	10673
20.20	10659	10646	10632	10619	10605	10592	10579	10565	10552	10538
20.30	10525	10512	10498	10485	10472	10458	10445	10431	10418	10405
20.40	10391	10378	10365	10352	10338	10325	10312	10298	10285	10272
20.50	10259	10245	1023 2	10219	10206	10192	10179	10166	10153	10139
20.60	10126	10113	10100	10087	10074	10060	10047	10034	10021	10008
20.70	9995	9982	9968	9955	9942	9929	9916	9903	9890	9877
20.80	9864	9851	9838	9825	9812	9799	9786	9772	9759	9746
20.90	9733	9720	9707	9694	9681	9668	9655	9642	9629	9617
21.10	9604	9591	9578	9565	9552	9539	9526	9513	9500	9487
21.10	9474	9462	9449	9436	9423	9410	9397	9384	9372	9359
21.20	9346	9333	9320	9307	9295	9282	9269	9256	9244	9231
21.30	9218	9205	9193	9180	9167	9154	9142	9129	9116	9103
21.40	9091	9078	9065	9053	9040	9027	9015	9002	8989	8977
21.50	8964	8951	8939	8926	8913	8901	8888	8876	8863	8850
21.60	8838	8825	8813	8800	8788	8775	8762	8750	8737	8725
21.70	8712	8700	8687	8675	8662	8650	8637	8625	8612	8600
21.80	8587	8575	8562	8550	8538	8525	8513	8500	8488	8475
21.90	8463	8451	8438	8426	8413	8401	8389	8376	8364	8352
22.00	8339	8327	8314	8302	8290	8277	8265	8253	8240	8228

TABLE 51.

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Values of 60368 [1+0.0010195 \times 36] $\log \frac{29.90}{B}$.

								В		
Barometric Pressure. B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
22.00	8339	8327	8314	8302	8290	8277	8265	8253	8240	8228
22.10	8216	8204	8191	.8179	8167	8154	8142	8130	8118	8105
22.20	8093	8081	8069	8056	8044	8032	8020	8008 7886	7995	7983 7862
22.30 22.40	7971 7849	7959 7 ⁸ 37	7947 7825	. 7935 7813	7922 7801	7910 7789 ·	7898 7777	7765	7874 7753	7740
22.40	7949	1031	7023	7023	,001	1109	''''	11-5	7755	''45
22.50	7728	7716	7704	7692	768o	7668	7656	7644	7632	7620
22.60	7608	7596	7584	7572	7560	7548	7536	7524	7512	7500
22.70	7488	7476	7464	7452	7440	7428	7416	7404	7392	7380
22.80 22.90	7368 7249	7356 7238	7345 7226	7333 7214	732I 7202	7309 7190	7297 7178	7285 7166	7273 7155	7261 7143
22.90	7249	7230	/220	/214	/202	7.30	12,0	7100	7-55	7-43
23.00	7131	7119	7107	7096	7084	7072	7060	7048	7037	7025
23.10	7013	7001	6990	6978	6966	6954	6943	6931	6919	6907
23.20	6896	6884	6872	6861	6849	6837	6825	6814	6802 6686	6790 6674
23.30	6779 6662	6767 6651	6755 6639	6744 6628	6732 6616	6721 6604	6709 6593	6697 6581	6570	6558
23.40	2002		0039	0020	0010	0004	9393	0,002	-575	9550
23.50	6546	6535	6523	6512	6500	6489	6477	6466	6454	6443
23.60	6431	6420	6408	6397 6282	6385	6374	6362	6351	6339	6328
23.70	6316	6305	6293		6270	6259	6247	6236	6225 6110	6213
23.80 23.90	6202 6088	6190 6076	6179 6065	6167 6054	6156 6042	6145 6031	6133 6020	6122 6008	5997	6099 5986
23.90	0000	00,0	0003	0034	0042	0031	0020	0000	3771	3900
24.00	5974	5963	5952	5940	5929	5918	5906	5895	5884	5872
24.10	5861	5850	5839	5827	5816	5805	5794 5681	5782	5771	5760
24.20	5749	5737	5726	5715	5704	5693		5670	5659	5648
24.30 24.40	5637	5625	5614	5603	5592 5480	5581 5469	5570 5458	5558 5447	5547 5436	5536 5425
24.40	5525	5514	5503	5492	3400	3409	3430	3447	3430	34-3
24.50	5414	5403	5392	5381	5369	5358	5347	5336	5325	5314
24.60	5303	5292	5281	5270	5259	5248	5237	5226	5215	5204
24.70	5193	5182	5171	5160	5149	5138	5127	5116	5105	5094
24.80 24.90	5083 4974	5072 4963	5061 4952	5050 4941	5039 4930	5028 4919	5017 4908	5006 4897	4995 4886	4985 4876
24.90	49/4	4903	4902	454-	4930	42~2	7300	4001	, 4000	40,70
25.00	4865	4854	4843	4832	4821	481o	4800	4789	4778	4767
25.10	4756	4745	4735	4724	4713	4702	4691	4681	4670	4659
25.20	4648	4637	4627	4616	4605	4594	4584	4573	4562	4551
25.30 25.40	4540 4433	4530 4423	4519 4412	4508 4401	4498 4391	4487 4380	4476 4369	4465 4358	4455 4348	4444 4337
23.40	4433	4423	4412	4401		7,000		7330	-340	7331
25.50	4326	4316	4305	4295	4284	4273	4263	4252	4241	4231
25.60	4220	4209	4199	4188	4178	4167	4156	4146	4135	4125
25.70 25.80	4114 4009	4104 3998	4093 3988	4082 3977	4072 3966	4061 3956	4051 3945	4040 3935	4030 3924	4019 3914
25.90	3903	3893	3882	3872	3861	3851	3841	3830	3820	3809
					_					-
26.00	3799	3788	3778	3767	3757	3746	3736	3726 3622	3715	3705 3601
26.10 26.20	3694 3590	3684 3580	3674 3570	3663 3559	3653 3549	3642 3539	3632 3528	3518	3508	3497
26.30	3590 3487	3477	3466	3339	3349	3435	3425	3415	3404	3394
26,40	3384	3373	3363	3353	3343	3332	3322	3312	3301	3291
26.50		0.070	2060	0050	2040	2220	2270	2200	2700	3189
26.50	3281	3270	3260	3250	3240	3230	3219	3209	3199	3109
	'	<u>' </u>	<u> </u>	<u> </u>	1			<u> </u>	<u></u>	

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Values of 60368 [1+0.0010195 \times 36] $\log \frac{29.90}{B}$.

								В		
Barometric Pressure. B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
26.50 26.60	3281 3179	3270 3168	3260 3158	3250 3148	3240 3138	3230 3128	3219 3117	3209 3107	3199 3097	3189 3087
26.70 26.80 26.90	3077 2975 2874	3066 2965 2864	3056 2955 2854	3046 2945 2843	3036 2934 2833	3026 2924 2823	3016 2914 2813	3005 2904 2803	2995 2894 2793	2985 2884 2783
27.00	2773	2763	2753	2743	2733	2723	2713	2703	2 692	2682
27.10 27.20	2672 2572	2662 2562	2652 2552	2642 2542	2532 2532	2622 2522	2612 2512	2602 2502	2592 2493	258 2 2483
27.30 27.40	2473 2373	2463 2363	2453 2353	2443 2343	2433 2334	2423 2324	2413 2314	2403 2304	2393 2294	2383 2284
27.50	2274	2264	2254	2245	2235	2225	2215	2205	2195	2185
27.60 27.70	2176 2077	2166 2067	2156 2058	2146 2048	2136	2126 2028	2116	2107 2009	2097 1999	2087 1989
27.80	1979	1970	1960	1950	1940	1930	1921	1911	1901	189í
27.90	1882	1872	1862	1852	1843	1833	1823	1814	1804	1794
28.00 28.10	1784 1688	1775 1678	1765 1668	1755 1659	1746 1649	1736 1639	1726 1630	1717 1620	1707 1610	.1697 1601
28.20	1591	1581	1572	1562	1552	1543	1533	1524	1514	1504
28.30 28.40	1495 1399	1485 1389	1476 1380	1466 1370	1456	1447 1351	1437 1342	1428 1332	1418 1322	1408
28.50 28.60	1303 1208	1294	1284	1275 1180	1265	1256	1246	1237	1227	1218
28.70	1113	1199 1104	1189	1085	1170	1161	1151	1142 1047	1132 1038	1123
28.80 28.90	1019 925	1009 915	1000 906	990 896	981 887	97 2 878	962 868	953 859	943 849	934 840
29.00	831	821	812	803	793	784	775	765	756	746
29.10	737	728	718`	709	700	690	681	672	663	653
29.20 29.30	644 551	635 542	625 532	616 523	607 514	597 505	588 495	579 486	570 477	560 468
29.40	458	449	440	431	421	412	403	394	384	375
29.50 29.60	366 274	357 265	348 256	338 247	329 237	320 228	311	302 210 -	292 201	283 192
29.70	182	173	164	155	146	137	128	118	109	100
29.80 29.90	+ 91 0	+ 82 - 9	+ 73 - 18	+ 64 - 27	+ 55 - 36	+ 45 - 45	+ 36 - 55	+ 27 - 64	+ 18 - 73	+ 9 - 82
30.00	– 91	- 100	— 109	-118	- 127	– 136	– 145	– 154	– 163	– 172
30.10	 181	- 190	- 199	- 208	- 217	- 226	- 235	- 244	- 253	- 262
30.20 30.30	- 271 - 361	- 280 - 370	- 289 - 379	- 298 - 388	- 307 - 397	- 316 - 406	- 325 - 415	- 334 - 424	- 343 - 433	- 35 ² - 44 ²
30.40	– 451	– 460	- 469	– 47 8	– 486	495	- 504	-513	- 522	- 53r
30.50 30.60	- 540 - 629	- 549 - 638	- 558 - 647	- 567 - 656	- 576 - 665	- 585 - 673	.— 593 — 682	- 602 - 691	611 700	- 620 - 709
30.70 30.80	- 718 - 806	- 727 - 815	- 735 - 824	- 744 - 833	- 753 - 841	- 76 ₂ - 850	- 771 - 859	- 780 - 868	- 788 - 877	- 797 - 885
30.00	500	515	324	933	041	335	- 239	300	""	503

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Term for Temperature: 0.002039 (θ - 50°) z.

For temperatures $\left\{ \begin{array}{ll} above \ 50^{\circ} \ F. \\ below \ 50^{\circ} \ F. \end{array} \right\}$ the values are to be $\left\{ \begin{array}{ll} added. \\ subtracted. \end{array} \right.$

		- (Below 50° F.) (Subtracted.												
Mea Temper	ature.	AP	PROX	(MATI	DIFF	EREN	CE OF	HEIG	HT O	BTAIN	ED FI	ROM T	ABLE	20 .
θ	•	20	40	60	80	100	200	300	400	500	600	700	800	900
F.	F.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
49°	51°	0	0	0	0	0	0	I	1	I	1	1	2	2
48	52	0	0	0,	0	0	I	1 2	2 2	2	2 4	3 4	3 5	4
47 46	53 54	0	0	0	I	ľ	2	2	3	3 4	5	6	7	7
45	55	0	0	I	ī	1	. 2	3	4		6	7	8	
44	56	o	ŏ	ı	ī	Î	2	4		5 6	7	9	10	9
43	57 58	0	1	ľ	I	1	3		5 6	7 8	9	10	II	13
42	58	0	I	I	I	2 2	3	4 5 6	7		10 11	II	13	15 17
41	59	٥	_				4	6	7 8	9]	13	15	
40	60 61	0	I	I	2	2 2	4	7	9	10	12 13	14 16	16	18
39 38	62	١ŏ	ī	Î	2	2	5		10	12	15	17	20	22
37 36	63	1	I	2	2	3	5	7 8	11	13		19	21	24
	64	1	I	2	2	3	l	9	11	14	17	20	23	26
35	65	I	I	2	2	3 3	6	9	12	15 16	18	21	24 26	28 29
34 33	66 67	I	I	2 2	3	3	7 7	10	13	17	21	23	28	31
32	67 68	ī	ī	2	3	4	7 8	11	15	18	22	26	29	33
31	69	1	2	2	3	4	l	12	15	19	23	27	31	35
30	70	1	2	2	3	4	8	12	16	20	24	29	33	37
29 28	71	I	2 2	3	3 4	4	9	13	17	2I 22	26	30 31	34 36	39 40
20 27	72 73	I	2	3	4	4 5	9	14	19	23	28	33	38	42
26	74	I	2	3 3 3	4	5 5	IÓ	15	20	24	29	34	39	44
25	75	1	2	3	4	5	10	15	20	25	31	36	41	46
24	76	I	2	3	4	5	II	16	21	27	32	37	42	48
23 22	77 78	I	2 2	3	5	6	II	17	22	20	33	39 40	44 46	50 51
21	79	Î	2	4	5	6	12	18	24	30	35	41	47	53
20	80	1	2	4	5	6	12	18	24	31	37	43	49	
10	81	1	3	4	5 5 5 5 6	6	13	19	25	32	38	44	51	55 57
18	82	I	1 3	4	5	7	13	20	26	33	39 40	46	52 54	59 61
17 16'	83 84	I	3 3	4	8	7 7	14	21	28	34	42	49	55	62
15	85	1	3	4	6	7	14	21	29	36	43	50	57	64
14	86	ī	3	4	6	7 8	15	22	29		44	51	59 60	64 66 68
13	87 88	2	3	5	6	8	15	23	30	37 38	45 46	53		68
12 11	88 89	2 2	3	5 5 5	6	8	15,	23	31 32	39 40	48	54	62	70 72
10	90	2	3		7	8	16	24	33	41	49	57	65	73
	91	2	3	5	7	8	17	25	33	42	50	59 60	67	75 77
9 8	92	2	3	5	7	9	17	26 26	34	43	51	60	69	77
7 6	93 94	2 2	4	5 5 5 5 5	7 7	9	18	20	35 36	44	53 54	63	70 72	79 81
5	94	2	4	6	1 '	9	18	28	37	46		64	73	83
4	96	2	4	6	7 8 8	9	19	28	37 38	47 48	55 56	66	. 75	83 84 86
3	97 98	2	4	6	8 8	10	19	29	38		57	67	77	86 88
2 I		2 2	4 4	6	8	IO	20	30	39 40	49 50	59 60	70	78 80	90
o	100	2	4	6	8	10	20	31	41	51	61	71	82	92
		<u></u>	<u> </u>	1	<u> </u>	<u> </u>		1 5-	1 '	0=		1 '-		

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Term for Temperature: 0.002039 $(\theta - 50^{\circ})$ z.

For temperatures $\left\{ \begin{array}{ll} above \ 50^{\circ} \ F. \\ below \ 50^{\circ} \ F. \\ \end{array} \right\}$ the values are to be $\left\{ \begin{array}{ll} added. \\ subtracted. \end{array} \right.$

MI .	an rature.	APPR	OXIMA'	re dif	FEREN	CE OF	HEIGH	т овт	AINED	FROM	TABLE	20.
).	1000	2000	3000	4000	5000	6000	7000	8000	9000	10000	2 000 6
F. 49° 48 47	F. 51° 52 53	Feet. 2 4 6	Feet. 4 8 12	Feet. 6 12 18	Feet. 8 16 2 4	Feet. IO 20 31	Feet. 12 24 37	Feet. 14 2 9 43	Feet. 16 33 49	Feet. 18 37 55	Feet. 20 41 61	Feet. 41 82 122
46 45 44 43 42	54 55 56 57 58	8 10 12 14 16	16 20 24 29 33	31 37 43 49	33 41 49 57 65	41 51 61 71 82	49 61 73 86 98	57 71 86 100 114	65 82 98 114 130	73 92 110 128 147	102 122 143 163	204 245 285 326
41 40 39 38 37 36	59 60 61 62 63	18 20 22 24 27	37 41 45 49 53	55 61 67 73 80	73 82 90 98 106	92 102 112 122 133	110 122 135 147 159	128 143 157 171 186	147 163 179 196 212	165 184 202 220 239	204 224 245 265	367 408 449 489 530
36 35 34 33 32 31	64 65 66 67 68 69	31 33 35 37 39	57 61 65 69 73 77	92 98 104 110	114 122 130 139 147 155	143 153 163 173 184 194	171 184 196 208 220 232	200 214 228 243 257 271	228 245 261 277 294 310	257 275 294 312 330 349	285 306 326 347 367 387	571 612 652 693 734 775
30 29 28 27 26	70 71 72 7.3 74	41 43 45 47 49	82 86 90 94 98	122 128 135 141 147	163 171 179 188 196	204 214 224 234 245	245 257 269 281 294	285 300 314 328 343	326 343 359 375 391	367 385 404 422 440	408 428 449 469 489	816 856 897 938 979
25 24 23 22 21	75 76 77 78 79	51 53 55 57 59	102 106 110 114 118	153 159 165 171	204 212 220 228 236	255 265 275 285 296	306 318 330 343 355	357 371 385 400 414	408 424 440 457 473	459 477 495 514 532	510 530 551 571 591	1020 1060 1101 1142 1183
20 19 18 17 16	80 81 82 83 84	61 63 65 67 69	122 126 130 135 139	184 190 196 202 208	245 253 261 269 277	306 316 326 336 347	367 379 391 404 416	428 442 457 471 485	489 506 522 538 555	551 569 587 606 624	612 632 652 673 693	1223 1264 1305 1346 1387
15 14 13 12	85 86 87 88 89	71 73 75 77 80	143 147 151 155 159	214 220 226 232 239	285 294 302 310 318	357 367 377 387 398	428 440 453 465 477	500 514 528 542 557	571 587 604 620 636	642 661 679 697 716	714 734 754 775 795	1427 1468 1509 1550 1590
10 98 76	90 91 92 93 94	82 84 86 88 90	163 167 171 175 179	245 251 257 263 269	326 334 343 351 359	408 418 428 438 449	489 502 514 526 538	571 585 599 614 6 2 8	652 669 685 701 718	734 75 2 771 789 807	816 836 856 877 897	1631 1672 1713 1754 1794
5 4 3 2	95 96 97 98	92 94 96 98	184 188 192 196 200	275 281 287 294 300	367 375 383 391 400	459 469 479 489 500	551 563 575 587 599	64 2 657 671 685 699	734 750 767 783 799	826 844 862 881 899	918 938 958 979 999	1835 1876 1917 1957 1998
Ô	100	102	204	306	408	510	612	714	816	918	1020	2039

ENGLISH MEASURES.

Correction for Gravity and Weight of Mercury: $z(0.002540 \cos 2 \phi - 0.000007 \cos^2 2 \phi + 0.00244)$.

Latitude.	APP	ROXIMA	TE DIE	FEREN	CE OF	HEIGH'	г овта	INED I	rom T	ABLES	51-52.
φ	500	1000	1500	2000	2500	3000	3500	4000	4500	5000	5500
0° 2 4 6	Feet. +3 3 3 2	Feet. +5 5 5 5	Feet. +8 8 8 8	Feet. + IC IO IO IO	Feet. +13 13 13 13	Feet. +15 15 15 15	Feet. +18 18 18 18	Feet. +20 20 20 20 20	Feet. +23 23 23 23 23 22	Feet. +25 25 25 25 25 25	Feet. +28 28 28 28 27
1 0 -12 14 16 18	+2 2 2 2 2	+5 5 5 5	+7 7 7 7 7	+10 10 9 9	+12 12 12 12 11	+15 15 14 14 14	+17 17 17 16 16	+20 19 19 19	+22 22 21 21 21	+25 24 24 23 23	+27 27 26 26 26 25
20 22 24 26 28	+2 2 2 2 2	+4 4 4 4	+7 6 6 6 6	+ 9 9 8 8 8	10	+13 13 13 12 12	+16 15 15 14 14	+18 17 17 16 16	+20 19 19 18 18	+22 22 21 20 20	+24 24 23 22 21
30 32 34 36 38	+2 2 2 2 2	+4 4 3 3 3	+6 5 5 5 5	+ 8 7 7 6 6	+ 9 9 9 8 8	+11 10 10 9	+13 13 12 11	+15 14 14 13 12	+17 16 15 15	+19 18 17 16	+21 20 19 18 17
40 42 44	1 1	+3 3 3	+4 4 4	+ 6 5 5	+ 7 7 6	+ 9 8 8	+10 9 9	+12 11 10	+13 12 11	+14 13 13	+16 15 14
45	+1	+2	+4	+ 5	+ 6	+ 7	+ 9	+10	+11	+12	+13
46 48 50	+1	+2 2 2	+4 3 3	+ 5 4 4	+ 6 5 5	+ 7 6 6	+ 8 8 7	+ 9 9 8	+11 9	+12 11 10	+13 12 11
52 54 56 58 60	+1 1 1	+2 2 1 1	+3 2 2 2 2 2	+ 4 3 3 3 2	+ 4 4 4 3 3	+ 5 5 4 4 3	+ 6 6 5 4 4	+ 7 6 6 5 4	+ 8 7 7 6 5	+ 9 8 7 6 6	+10 9 8 7 6
62 64 66 68 70	0 0 0 0	0 1 1	+1	+ 2 2 1 1	+ 2 2 2 1 1	+ 3 2 2 2 1	+ 3 3 2 2 1	+ 4 4 3 2 2	+ 4 3 3 2 2	+ 5 4 3 3 2	+ 5 4 3 3 2
72 74 76 78 80	00000	0000	0 0 0 0	0 0 0 0	+ I 0 0 0	+ I	+ I	+ I	+ 1 0 0	+ I	+ I 0 0

ENGLISH MEASURES.

Correction for Gravity and Weight of Mercury: $z(0.002640 \cos 2\phi - 0.000007 \cos^2 2\phi + 0.00244)$.

Latitude.	AP	PROXIM	ATE DI	FFERE	NCE OF	HEIGH!	г ОВТАІ	NED FI	ROM TAI	BLES 5	1-52.
φ	6000	7000	8000	9000	10000	11000	12000	13000	14000	15000	20000
0° 2 4 6 8	Feet. +30 30 30 30 30	Feet. +35 35 35 35 35 35	Feet. +41 40 40 40 40	Feet. +46 46 45 45 45	Feet. +51 50 50 50	Feet. + 56 56 55 55 55	Feet. +61 61 61 61 60	Feet, +66 66 66 66 65	Feet. +71 71 71 71 70	Feet. + 76 76 76 76 76 75	Feet. -101 101 101 100 99
10	+29	+34	+39	+44	+49	+54	+59	+64	+69	+74	+ 98
12	29	34	39	44	48	53	58	63	68	73	97
14	29	33	38	43	48	52	57	62	67	71	95
16	28	33	37	42	47	51	56	61	65	70	93
18	27	32	37	41	46	50	55	59	64	68	91
20	+27	+31	+36	+40	+45	+49	+53	+58	+62.	+67	+ 89
22	26	30	35	39	43	48	52	56	61	65	87
24	25	29	34	38	42	46	50	55	59	63	84
26	24	28	32	37	41	45	49	53	57	61	81
28	23	27	31	35	39	43	47	51	55	59	78
30	+23	+26	+30	+34	+38	+41	+45	+49	+53	+56	+ 75
32	22	25	29	32	36	40	43	47	50	54	72
34	21	24	27	31	34	38	41	44	48	51	68
36	20	23	26	29	32	36	39	42	46	49	65
38	18	22	25	28	31	36	37	40	43	46	61
40	+17	+20	+23	+26	+29	+32	+35	+38	+41	+43	+ 57
42	16	10	22	24	27	30	33	35	38	41	54
44	15	18	20	23	25	28	30	33	35	38	50
45	+15	+17	+19	+22	+24	+27	+29	+32	+34	+37	+ 49
46	+14	+16	+19	+21	+23	+26	+28	+30	+33	+35	+ 46
48	13	15	17	19	22	24	26	28	30	32	43
50	12	14	16	18	20	22	24	26	28	30	40
52 54 56 58 60	+11 10 9 8 7	+13 11 10 9 8	+14 13 12 10 9	+16 15 13 11 10	+18 - 16 - 14 - 13 - 11	+20 18 16 14 12	+22 19 17 15	+23 21 19 17 14	+25 23 20 18 16	+27 24 22 19 17	+ 36 32 29 26 22
62	+ 6	+ 7	+ 8	+ 9	+10	+11	+11	+12	+13	+14	+ 19
64	5	6	6	7	8	9	10	10	11	12	16
66	4	5	5	6	7	7	8	9	9	10	13
68	3	4	4	5	5	6	6	7	7	8	11
70	2	3	3	4	4	4	5	5	6	6	8
72 74 76 78 80	+ 2 + 1 + 1 0 0	+ 2 + 1 + 1 0 0	+ 2 + 2 + 1 0	+ 3 + 2 + 1 0	+ 3 + 2 + 1 - 0 - 1						

ENGLISH MEASURES.

Correction for an Average Degree of Humidity.

Temper- ature. 500 1000 2000 3000 4000 5000 6000 7000 F. Feet. Feet. Feet. Feet. Feet. Feet. Feet. Feet. -20° 0 0 0 0 0 0 0 0 + 1	Feet. + I 2 3 4 4 4 5	9000 Feet. + I 2 3 4 4	Feet. + I 2 3	Feet. + 2 4 6
$ \begin{vmatrix} -20^{\circ} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & $	+ I 2 3 4 4 4 4	+ I 2 3 4 4	+ I 2 3	+2
$ \begin{vmatrix} -16 & 0 & 0 & 0 & +1 & +1 & +1 & +1 & 1 \\ -12 & 0 & 0 & +1 & 1 & 1 & 2 & 2 & 2 \end{vmatrix} $	2 3 4 4 4	2 3 4 4	3	
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	3 4 4 4	3 4 4	3	6
-8 0 0 I I 2 2 3 3	4 4	4	1 .	,
	4 4	4	4	9
-6 0 0 I 1 2 2 3 3			5 6	10
$egin{bmatrix} -4 & 0 & +1 & 1 & 2 & 2 & 3 & 3 & 4 \\ -2 & 0 & 1 & 1 & 2 & 2 & 3 & 4 & 4 \end{bmatrix}$		5 6	6	II I2
		6		14
+ 2 0 I I 2 3 4 4 5	5 6	7	7 7 8	15 16
	7	7 8		16 18
8 0 1 2 3 4 4 5 6 7	7 8	9	9 10	19
10 + 1 1 2 3 4 5 6 7	8	9	10	21
	9	10 11	11 12	22 24
16 1 1 3 4 5 6 8 9	10	11	13	25
18 1 1 3 4 5 7 8 9	11	12	13	27
20 I I 3 4 6 7 9 10 22 I 2 3 5 6 8 9 II	11 12	13	14 15	29 31
24 I 2 3 5 7 8 10 II	13	15	16	33
26	14 15	16 17	17 19	35 37
30 I 2 4 6 8 10 12 14	16	18	20	41
32 I 2 4 7 9 II I3 16	18	20	22	44
34 I 2 5 7 10 12 15 17 36 I 3 5 8 11 13 16 19	19 21	22 24	24 27	49 53
38 1 3 6 9 12 15 18 21	23	26	29	59
	26 28	29	32	64
	31	32 35	35 39	71 77 84
44 2 4 8 12 15 19 23 27 46 2 4 8 13 17 21 25 29 48 2 5 9 14 18 23 27 32	34 37	35 38 41	4 2 46	
	37 40	, ,	50	92 99
52 3 5 11 16 21 27 32 37	43	45 48	53	107
54 3 6 11 17 23 29 34 40 56 3 6 12 18 24 30 37 43	46 49	51 55	57 6 1	114
58 3 6 13 19 26 32 39 45	52	55 58	65	130
60 3 7 14 21 27 34 41 48 62 4 7 14 22 29 36 43 51	55	62	69	137
62 4 7 14 22 29 36 43 51 64 4 8 15 23 30 38 46 53	55 58 6 1	65 69	7 2 76	145 152
66 4 8 16 24 32 40 48 56	64	72	8o	160
68 4 8 17 25 34 42 50 59 70 4 9 18 26 35 44 53 61	67	76 70	84	168
72 5 9 18 27 37 46 55 64	70 73	79 82	88 91	175 183
76 5 10 20 30 40 49 59 69 80 5 11 21 32 43 53 64 75	79 85	89 96	99 106	198
84 6 11 23 34 46 57 68 80	91	103	114	213 228
88 6 12 24 37 49 61 73 85	97	110	122	2 43
92 6 13 26 39 52 65 78 91 96 7 14 27 41 55 68 82 96	103	123	129 137	259 274

ENGLISH MEASURES.

Correction for the Variation of Gravity with Altitude: $\frac{z \, (z + 2 \, h_{\rm p})}{R}$.

Approx-			н	EIGHT	of Lo	WER S	TATIO	N IN F	EET (/	i _o).		
difference				1		Γ΄	1	í	1	1		· · · · ·
cf height. Z.	0	1000	2000	3000	4000	5000	6000	7000	8000	9000	10000	12000
Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
500	0	0	0	0	0	0	0	o.	0	0	0	+1
1000	0	0	0	0	0	+ 1	+1	+1	+1	+ 1	+1	I
1500	0	0	0	+1	+1	1	I	I	I	1	2	2
2000	0	0	+1	I	I	1	I	2	2	2	2	2
2500	0	+ r	I	I	r	I	2	2	2	2	3	3
3000	. 0	I	I	1	2	2	2	2	3	3	3	4
3500	+ r	I	1	2	2	2	3	3	3	4	4	5
4000	I	I	2	2	2	3	3	3	4_	4	. 5	5 6
4500	1	I	2	2	3	3	4	4	4	5	5	0
5000	I	2	2	3	3	4	4	5	5	6	6	7
5500	I	2	3	3	4	4	5	5	6	6	7	8
6000	2	2	3	3	4	5	5	6	6	7	7	9
6500 7000	2	3	3	4	5	5 6	6 6	6	7	8	8	9
7000	2	3	4	4	5			7	٥	٥	9	10
7500	3	3	4	5	6	6	7	8	8	9	10	11
8000	3	4	5	5 6		7 8	8 8	8	9 10	10	II	12
8500 9000	3	4 5	5 6	6	7	8		9 10	11	11 12	12 12	13 14
9500	4 4	5	6	7	8	9	9	11	12	13	13	15
9300	4	3		(9	10			-3	-3	-3
10000	5	6	7	8	9	10	II	11	12	13	14	16
11000	6	7	8	9	10	11	12	13	14	15	16	18
12000	7	8	9	ю	11	13	14	15	16	17	18	21
13000	8	9	11	12	13	14	16	17	18	19	21	23
14000	9	11	12	13	15	16	17	19	20	21	23	25
15000	11	12	14	15	17	18	19	21	22	24	25	28
16000	12	14	15	17	18	20	21	23	25	26	28	31
17000	14	15	17	19	20	22	24	25	27	28	30	
18000	16	17	19	21	22	24	26	28	30	31		ļ
19000	17	19	21	23	25	26	28	30	32			
20000	19	21	23	25	27	29	31					

METRIC MEASURES.

Values of 18400 $\log \frac{760}{B}$.

Barometric Pressure.	0	ı	2	3	4	5	6	7	8	9
mm. 300 310 320 330 340	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	7428	7401	7375	7348	7322	7296	7270	7244	7218	7192
	7166	7140	7115	7089	7064	7038	7013	6987	6962	6937
	6912	6887	6862	6838	6813	6789	6764	6740	6715	6691
	6666	6642	6618	6594	6570	6546	6522	6498	6475	6451
	6428	6405	6381	6358	6334	6311	6288	6265	6242	6219
350	6196	6173	6151	6128	6106	6083	6061	6038	6016	5993
360	5971	5949	5927	5905	5883	5861	5839	5817	5795	5773
370	5752	5739	5709	5687	5666	5644	5623	5602	5581	5560
380	5539	5518	5497	5476	5455	5434	5414	5393	5373	5352
390	5332	5311	5291	5270	5250	5229	5209	5189	5169	5149
400	5129	5109	5089	5069	5049	5029	5010	4990	4971	4951
410	4932	4912	4893	4873	4854	4834	4815	4796	4777	4758
420	4739	4720	4701	4682	4663	4644	4625	4606	4588	4569
430	4551	4532	4514	4495	4477	4458	4440	4422	4404	4386
440	4368	4350	4332	4314	4296	4278	4260	4242	4224	4206
450	4188	4170	4152	4134	4117	4099	4082	4064	4047	4029
460	4012	3994	3977	3959	3942	3925	3908	3891	3874	3857
470	3840	3823	3806	3789	3772	3755	3738	3721	3705	3688
480	3672	3655	3639	3622	3606	3589	3573	3556	3540	3523
490	3507	3490	3474	3458	3442	3426	3410	3394	3378	3362
500	3346	3330	3314	3298	3282	3266	3250	3235	3219	3203
510	3188	3172	3157	3141	3126	3110	3095	3079	3064	3048
520	3033	3017	3002	2986	2971	2955	2940	2925	2910	2895
530	2880	2865	2850	2835	2820	2805	2790	2775	2760	2745
540	2731	2716	2701	2687	2672	2657	2643	2628	2613	2599
550	2584	2570	2555	2541	2526	2512	2497	2483	2468	2454
560	2440	2426	2411	2397	2383	2369	2355	2341	2327	2313
570	2299	2285	2271	2257	2243	2229	2215	2201	2188	2174
580	2160	2146	2133	2119	2105	2092	2078	2064	2051	2037
590	2023	2010	1996	1983	1969	1956	1942	1929	1915	1902
600	1889	1875	1862	1848	1835	1822	1809	1796	1783	1770
610	1757	1744	1731	1718	1705	1692	1679	1666	1653	1640
620	1627	1614	1601	1588	1576	1563	1550	1537	1525	1512
630	1499	1486	1474	1461	1448	1436	1423	1411	1398	1386
640	1373	1361	1348	1336	1323	1311	1298	1286	1273	1261
650	1249	1236	1224	1212	1199	1187	1175	1163	1151	1139
660	1127	1115	1103	1091	1079	1067	1055	1043	1031	1019
670	1007	995	983	971	960	948	936	924	913	901
680	889	877	866	854	842	831	819	807	796	784
690	772	761	749	738	726	715	703	692	680	669
700	657	646	635	623	612	601	589	578	567	555
710	544	533	521	510	499	487	476	465	454	443
720	432	421	410	399	388	377	366	355	344	333
730	322	311	300	289	278	267	256	245	234	224
740	213	202	19 2	181	170	160	149	138	128	117
750	+ 106	+ 95	+ 85	+ 74	+ 64	+ 53	+ 43	+ 32	+ 22	+ 11
760	0	- 10	- 21	- 31	42	- 52	- 63	- 73	- 83	- 94
770	104	- 115	- 125	- 136	146	- 156	- 166	- 177	- 187	- 197

DETERMINATION OF HEIGHTS BY THE BAROMETER. DYNAMIC MEASURES.

Values of 18400 log $\frac{1013.3}{B}$

						- В				
Baro- metric Pressure	0	1	2	3	4	5	6	7	8	9
mb.	m.	m.	m,	m.	m,	m.	m,	111.	m.	m.
o	8	55306	49767	46527	44228	42445	40988	39756	38689	37748
10	36906	36144	35448	34809	34217	33666	33150	32665	32209	31777
20	31367	30977	30605	30250	29910	29584	29270	28969	28678	28397
30	28127	27865	27611	27365	27126	26895	26670	26451	26238	26031
40	25828	25630	25438	25250	25066	24887	24711	24539	24371	24206
50	24043	23886	23731	23579	23430	23283	23139	22998	22859	22722
60	22588	22456	22326	22198	22072	21948	21827	21706	21587	21471
70 80	21356	21242	21131	21021	20012 10800	20805 19804	20699 19711	20594 19618	20491	20389
90	19348	19259	19172	19995	19000	18916	18832	18749	19527 18667	19437 18586
									. !	-
100	18506	18426	18347	18269	18192	18116	18040	17965	17891	17817
110	17744	17672	17600	17529	17459	17389	17320	17251	17183	17115
120	17049	16982	16917	16851 16227	16787 16167	16722 16108	16659	16596	16533	16471
130	16409	16348	16287	15647	15592	15536	16048 15482	15990 15427	15932	15874
							15402		15373	15319
150	15266	15212	15160	15107	15055	15004	14952	14901	14850	14800
160	14750	14700	14650	14601	14553	14504	14456	14408	14360	14312
170	14265	14218	14172	14125	14079	14034	13988	13943	13898	13853
180	13809	13764	13720	13677	13633	13590	13547	13504	13461	13419
	13377	13335	13293	13251	13210	13169	13128	13087	13047	13007
200	12967	12927	12887	12848	12808	12769	12730	12692	12653	12615
210	12577	12539	12501	12463	12426	12389	12352	12315	12278	12242
220	12205	12169	12133	12097	12061	12026	11990	11955	11920	11885
230	11850	11815	11781	11746	11712	11678	11644	11610	11577	11543
240	11510	11476	11443	11410	11378	11345	11312	11280	11248	11216
250	11184	11152	11120	11088	11057	11025	10994	10 963	10932	10901
260	10870	10839	10809	10778	10748	10718	10688	10658	10628	10598
270	10569	10539	10510	10480	10451	10422	10393	10364	10335	10307
280	10278	10249	10221	10193	10165	10137	10108	10081	10053	10025
290	9997	9970	9943	9915	9888	9861	9834	9807	9780	9753
300	9727	9700	9674	9647	9621	9594	9568	9542	9516	9490
310	9465	9439	9413	9388	9362	9337	9311	9286	9261	9236
320	9211	9186	9161	9136	9111	9087	9062	9038	9014	8989
330	8965	8941	8917	8893	8869	8845	8821	8797	8773	8750
340	8726	8703	8679	8656	8633	8610	8587	8564	. 8541	8518
350	8495	8472	8449	8427	8404	8381	8359	8336	8314	8292
360	8270	8247	8225	8203	8181	8159	8138	8116	8094	8073
370	8051	8029	8008	7986	7965	7943	7922	7901	7880	7859
.380	7838	7817	7796	7775	7754	7733	7712	7692	7671	7651
390	7630	7610	7589	7569	7548	7528	7508	7488	7468	7448
400	7428	7408	7388	7368	7348	7328	7309	7289	7269	7250
410	7230	7211	7191	7172	7153	7133	7114	7095	7076	7057 6868
420	7038	7019	7000	6981	6962	6943	6924	6906	6887	
430	6850 6666	6831	6813 6630	6794	6776	6757	6739 6558	6721	6703	6684
440			_							6504
450	6487	6469	6451	6433	6416	6398	6381	6363	6346	6328
460	6311	6294	6276	6250	6242	6225	6207	6190	6173	6156
470	6139	6122	6105	6088	6071	6055	6038	6021	6004	5987
480	5971	5954	5937	5921	5904	5888	5871	5855	5839	5822
490	5806	5790	5773	5757	5741	5725	5709	5693	5677	5661

DETERMINATION OF HEIGHTS BY THE BAROMETER. DYNAMIC MEASURES.

Values of 18400 $\log \frac{1013.3}{B}$

						- B				
Barometric Pressure	0	1	2	3	4	5	6	7	8	9
mb.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
500	5645	5629	5613	5597	5581	5565	5549	5533	5518	5502
510	5486	547 I	5455	5439	5424	5408	5393	5377	5362	5346
520	5331	5316	5300	5285	5270	5 ² 55	5239	5224	5200	5194
530	5179	5164	5149	5134	5119	5104	5089	5074	5059	5044
540	5030	5015	5000	4985	4971	4956	4941	4927	4912	4898
550	4883	4868	4854	4839	4825	4811	4796	4782	4768	4753
560	4739	4725	4710	4696	4682	4668	4654	4640	4626	4612
570	4598	4583	4569	4556	4542	4528	4514	4500	4486	4472
580	4459	4445	4431	4417	4404	4390	4376	4363	4349	4335
590	4322	4308	4295	4281	4268	4254	4241	4228	4214	4201
600	4188	4174	4161	4148	4134	4121	4108	4095	4082	4069
610	4056	4042	4029	4016	4003	3990	3977	3964	3951	3939
620	3926	3913	3900	3887	3874	3861	3849	3836	3823	3810
630	3798	3785	3772	3760	3747	3735	3722	3709	3697	3684
640	3672	3659	3647	3635	3622	3610	3597	3585	3573	3560
650	3548	3536	3523	3511	3499	3487	3475	3462	3450	3438
660	3426	3414	3402	3390	3378	3366	3354	3342	3330	3318
670	3306	3294	3282	3270	3258	3246	3235	3223	3211	3199
680	3187	3176	3164	3152	3141	3129	3117	3106	3004	3082
690	3071	3059	3048	3036	3025	3013	3002	2990	2979	2967
700	2956	2944	2933	2922	2910	2899	2888	2876	2865	2854
710	2842	2831	2820	2800	2798	2786	2775	2764	2753	2742
720	2731 2621	2720	2708	2697	2686	2675	2664	2653	2642	2631
730	2512	2609	2599	2588	2577 246g	2566	2555	2544	2533	2523
740	_	2501	2490	2479		2458	2447	2437	2426	2415
750	2405	2394 2288	2383	2373	2362	2351	2341	2330	2320	2309
760 770	2299 21 9 4	2200	2278	2267 2163	2257	2246	2236	2225	2215	2205
770 780	2194 2001	2081	2071	2060	2153 · 2050	2142 2040	2132 2030	2122	2112	2101
790	1989	1979	1969	1959	1949	1939	1929	1919	2009 1909	1999 1899
800	188g	1879	186g		1849					1 1
810	1789	1780	1770	1859 1760	1750	1839	1829	1819	1809	1799
820	1602	1682	1672	1662	1653	1740 1643	1731 1633	1721 1623	1711 1614	1701 1604
830	1595	1585	1575	1566	1556	1547	1537	1527	1518	1508
840	1499	1489	1480	1470	1461	1451	1442	1433	1423	1414
850	1404	1395	1386	1376	1367	1357	1348	1339	1329	1320
860	1311	1302	1292	1283	1274	1357	1255	1246		1320
870	1218	1209	1200	1191	1182	1173	1164	1154	1237 1145	1136
88o	1127	1118	1100	1100	1001	1082	1073	1064	1055	1046
890	1037	1028	1019	1010	1001	992	983	974	965	956
900	048	939	930	921	QI2	903	894	886	877	868
910	859	850	842	833	824	815	807	798	780	781
920	772	763		746	737	729	720	711	703	694
930	772 686	677	755 668	660	651	643	634	626	617	608
940	600	592	583	575	566	558	549	541	53 ²	524
950	516	507	499	490	482	474	465	457	448	440
960	432	424	415	407	399	390	382	374	365	357
970	349	341	332	324	316	308	300	292	283	275
980	267	259	251	243	234	226	218	210	202	194
990	186	178	170	162	154	146	138	130	122	114
1000	100	98	90	82	74	66	58	50	42	34
1010	26	18	10	2	- 6	- 13	— 21	- 29	- 37	- 45
1020	- 53	- 61	- 68	- 76	- ·84	- 92	-100	-107	-115	-123
1030	-131	-138	-146	-154	- 162	-169	-177	- 185	-192	- 200
1040	- 208	-215	-223	-231	- 238 .	<u> - 246 </u>	-254	<u>- 261 </u>	- 269	- 277

DETERMINATION OF HEIGHTS BY THE BAROMETER. METRIC MEASURES.

Temperature correction factor, $a = .00367 \theta$.

Multiply approximate altitudes, determined from table 56 or 57. by values of a corresponding to mean temperature, θ , of air column. Add, if θ is above o C; subtract, if below o C.

Mean Tame 0	.0	.1	,2	.3	.4	.5	.6	.7	.8	.9
Temp. θ										
	u.	u.	u.	a.	u.	u.	u.	u.	u.	u.
0	0.000	0.000	100.0	0.001	0.001	0.002	0.002	0.003	0.003	0.003
I	.004	.004	.004	.005	.005	.006	.006	.006	.007	.007
2	.007	.008	.008	.008	.009	.009	.010	.010	.010	.011
3	.011	.011	.012	.012	.012	.013	.013	.014	.014	.014
4	.015	.015	.015	.016	.016	.017	.017	.017	.018	.018
5	.018	019	.019	.519	.020	.020	.021	.021	.021	.022
6	.022	.022	.023	.023	.023	.024	.024	.025	.025	.025
7 8	.026	.026	.026	.027	.027	.028	.028	.028	.029	.029
	.029	.030	.030	.030	.031	.031	.032	.032	.032	.033
9	.033	.033	.034	.034	.034	.035	.035	.0 36	.0 36	.036
10	.037	.037	.037	.038	.038	.039	.039	.039	.040	.040
11	.040	.041	.041	.041	.042	.042	.043	.043	.043	.044
12	.044	.044	.045	.045	.04 6	.046	.046	.047	.047	.047
13	.048	.048	.048	.049	.049	.050	.050	.050	.051	.051
14	.051	.052	.052	.552	.053	.053	.054	.054	.054	.055
ll 15 i	.055	.055	.056	.056	.057	.057	.057	.058	.058	.058
16	.059	.059	.059	.060	.060	.061	.061	.061	.062	.062
17	.062,	.063	.063	.063	.064	.064	.065	.065	.065	.066
18	.066	.066	.067	.067	.068	.068	.o68	.o6g	.060	.060
19	.070	.070	.070	.071	.071	.072	.072	.072	.0.73	.073
20	.073	.074	.074	.075	.075	.075	.076	.076	.076	.077
21	.077	.077	.078	.078	.079	.079	.070	.080	.080	.080
22	.081	.081	.081	.082	.082	.083	.083	.083	.084	.084
23	.084	.085	.085	.086	.086	.086	.087	.087	.087	.088
24	.088	.088	.089	.080	.090	.090	.000	.091	.001	.001
u 1	i			1	1 1	-			-	
25 26	.092	.092	.092	.003	.093	.094	.094	.094	.095	.095
	.095	.090	.100	.100	.101	.101	.101	.102	.102	.102
27 28	.099 .103	.103	.103	.104	.104	.101	.105	.105	.106	.106
29	.106	.107	.107	.108	.108	.108	.100	.100	.100	.110
•								_	_	
30	.110	.IIO	.III	.111	.112	.112	.112	.113	.113	.113
31	.114	.114	.115	.115	.115	.116	.116	.116	.117	.117
32	.117	.118	.110	.119	.119	.119 .123	.120	.120 .124	.120 .124	.121
33	.121	.121	.126	.126	.126	.123	.123	.124	.128	.124
34	.125	.125			ŀ				ł	
35	.128	.129	.129	.130	.130	.130	.131	.131	.131	.132
36	.132	.132	.133	.133	.134	.134	.134	.135	.135	.135
37	.136	.136	.137	.137	.137	.138	.138	.138	.139	.139
38	.139	.140	.140	.141	.141	.141	.142	.142	.142	.143
39	.143	.143	.144	.144	.145	.145	.145	.146	.146	.146
40	.147	.147	.148	.148	.148	.149	.149	.149	,150	.150
41	.150	.151	.151	.152	.152	.152	.153	.153	.153	.154
42	.154	.155	.155	-155	.156	7156،	.156	.157	.157	،157
43	.158	.158	.159	.159	.159	.160	.160	.160	.161	.161
44	.161	.162	.162	.163	.163	.163	.164	,164	.164	.165
45	.165	.166	.166	.166	.167	.167	,167	.168	,168	.168
46	.169	.169	.170	.170	.170	.171	.171	.171	.172	.172
47	.172	.173	.173	.174	.174	.174	.175	.175	.175	.176
48	.176	.177	.177	.177	.178	,178	.178	.179	.179	.179
49	.180	.180	.181	.181	181,	.182	.182	.182	.183	.183
50	.184	.184	.184	.185	,185	.185	.186	.186	.186	.187
						<u></u> _		<u> </u>		

METRIC MEASURES.

Term for Temperature: $0.00367 \theta \times z$.

For temperatures { above o° C. } the values are to be { added. subtracted.

					perov		· ,			`	subtra		
Approx- imate differ-	114	EAN	TEMP	ERAT	URE C	F AIE	COLU	JMN IN	CENT	IGRAD	E DEGI	REES (θ).
ence of height. Z.	I°	2°	3°	4°	5°	6°	7°	8°	9°	10°	20°	30°	40°
m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
100	0	1	1	1	2	2	3	3	3	4	7	11	15
200	1	1	2	3	4	i 4	5 8	3 6	7	7	15	22	29
300	1	2	3	4	6	7	8	9	10	11	22	33	44
400	I	3	4	6	7	9	10	12	13	15	29	44	59
500	2	4	6	.7	9	11	13	15	17	18	37	55	73
600	2	4	7 8	9	ΙÍ	· 13	15 18	15 18	20	22	44	55 66	73 88
700	3	5	8	10	13	15 18		21	23	26	51	77 88	103
800	3		9	12	15		21	23	26	29	59 66		117
900	3	7	10	13	17	20	23	26	30	33	66	99	132
1000	4	7 8	11	15	18	22	26	29	33	37	73 81	110	147
1100	4		12	16	20	24	28	32	33 36	40	8r	121	161
1200	4	9	13	18	22	26	31	35 38	40	44	88	132	176
1300	5	IO	14	19	24	29	33 36	38	43	48	95	143	191
1400	5	10	15	21	26	31	36	41	46	51	103	154	206
1500	6	11	17	22	28	33	39	44	50	55	110	165	220
1600	6	12	18	23	29	35	41	47	53 56	59 62	117	176	235
1700	6	12	19	25	31	37	44	50	56		125	187	250
1800	7	13	20	26	33	40	46	53	59 63	66	132	198	264
1900	7	14	21	28	35	42	49	56	63	70	139	209	279
2000	7	15	22	29	37	44	51	59	66	73	147	220	294
2100	7 8	15 16	23	31	39	46	54	62	69	77	154 161	231	308
2200	8		24	32	40	48	57	65 68	73 76	81	161	242	323 338
2300	8	17	25	34	42	51	59		76	84	169	253	338
2400	9	18	26	35	44	53	62	70	79	8,8	176	264	352
2500	9	18	28	37	46	55	64	73	83	92	184	275	367
2 600	ΙÓ	19	29	37 38	48	57	67	73 76	83 86	95	191	275 286	382
2700	10	20	30	40	50	59 62	69	79 82	89	99	198	297	396
2800	10	21	31	41	51		72		92	103	206	308	411
2900	11	21	32	43	53	64	75	85	96	106	213	319	426
3000	11	22	33	44	55	66	77	88	99	110	220	330	440
3100	11	23	34	46	57	68	80	91	102	114	228	341	455
3200	12	23	35	47 48	59 61	70	82	94	106	117	235	352	470 484
3300	12	24	36			73	85	97	109	121	242	363	
3400	12	25	37	50	62	75	87	100	112	125	250	374	499
3500	13	26	39	51	64	77	90	103	116	128	257	385	514
3600	13	26	40	53	66	79	92	106	119	132	264	396	528
3700	14	27	41	54	68	81		109	122	136	272	407	543
3800	14	28	42	56	70	84	95 98	112	126	139	279	418	558
3900	14	29	43	57	72	86	100	115	129	143	286	429	573
4000	15	29	44	50	72	88	103	117	122	147	2 94	440	587
5000	18	37	44	59 73	73 92	110	128	147	132 165	183	294 367	440 551	724
6000	22	44	55 66	73 88	110	132	154	176	198	220	440	551 661	734 881
7000	26	51	77	103	128	154	180	205	231	257	514	771	1028
	-	-	''	"		"			J-	٥,	0-7	,,-	
													·

METRIC MEASURES.

Correction for Humidity: Values of 10000 β .

$$\beta = 0.378 \frac{e}{b} = 0.378 \frac{e_1 + e_0}{B + B_0}$$

Mean Vapor Pressure.			MEAN	BARC	METR	ic Pri	ESSUR	B +		ETER:	$s\left(\frac{B}{}\right)$	$\frac{+B_{\circ}}{2}$	•	
$e = \frac{\theta_1 + \theta_0}{2}$	500	520	540	560	580	600	620	640	660'	680	700	720	740	760
mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm,	mm.	mm.
1	· 8	7	7	7	7	6	6	6	6	6	5	5	5	5
2	15	15	14	14	13	13	12	12	11	11	11	11	10	10
3	23	22	21	20	20	19	18	18	17	17	16	16	15	15
4	30	29	28	27	26	25	24	24	23	22	22	21	20	20
5 6 7 8 9	38	36	35	34	33	31	30	30	29	28	27	26	26	25
	45	44	42	41	39	38	37	35	34	33	32	32	31	30
	53	51	49	47	46	44	43	41	40	39	38	37	36	35
	60	58	56	54	52	50	49	47	46	44	43	42	41	40
	68	65	63	61	59	57	55	53	52	50	49	47	46	45
10	76	73	70	68	65	63	61	59	57	56	54	53	51	50
11	83	80	77	74	72	69	67	65	63	61	59	58	56	55
12	91	87	84	81	78	76	73	71	69	67	65	63	61	60
13	98	95	91	88	85	82	79	77	74	72	70	68	66	65
14	106	102	98	95	91	88	85	83	80	78	76	74	72	70
15	113	109	105	101	98	95	91	89	86	83	81	79	77	75
16	121	116	112	108	104	101	98	94	92	89	86	84	82	80
17	129	124	119	115	111	107	104	100	97	94	92	89	87	85
18	136	131	126	122	117	113	110	106	103	100	97	95	92	90
19	144	138	133	128	124	120	116	112	109	106	103	100	97	95
20	151	145	140	135	130	126	122	118	115	111	108	105	102	99
21	159	153	147	142	137	132	128	124	120	117	113	110	107	104
22	166	160	154	149	143	139	134	130	126	122	119	116	112	109
23	174	167	161	155	150	145	140	136	132	128	124	121	117	114
24	181	174	168	162	156	151	146	142	137	133	130	126	123	119
25	189	182	175	169	163	157	152	148	143	139	135	131	128	124
26	197	189	182	175	169	164	159	154	149	145	140	137	133	129
27	204	196	189	182	176	170	165	159	155	150	146	142	138	134
28	212	204	196	189	182	176	171	165	160	156	151	147	143	139
29	219	211	203	196	189	183	177	171	166	161	157	152	148	144
30	227	218	210	203	196	189	183	177	172	167	162	158	153	149
31	234	225	217	209	202	195	189	183	178	172	167	163	158	154
32	242	233	224	216	209	202	195	189	183	178	173	168	163	159
33	249	240	231	223	215	208	201	195	189	183	178	173	169	164
34	257	247	238	230	222	214	207	201	195	189	184	179	174	169
35	265	254	245	236	228	220	213	207	200	195	189	184	179	174
36	272	262	252	243	235	227	219	213	206	200	194	189	184	179
37	280	269	259	250	241	233	226	219	212	206	200	194	189	184
38	287	276	266	257	248	239	232	224	218	211	205	200	194	189
39	295	283	273	263	254	246	238	230	223	217	211	205	199	194
40	302	291	280	270	261	252	244	236	229	222	216	210	204	199

METRIC MEASURES.

Correction for Humidity: 10000 $\beta \times z$.

Top argument: Values of 10000 β obtained from page Side argument: Approximate difference of height (z).

	510	Cargo	ment	. пр	PIOXIII	nate di	II CI CIIC	01 11	engint (Z }·		
Approximate Difference		,				10	οοο β.		1			
of Height. Z.	25	50	75	100	125	150	175	200	225	250	275	300
m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
100	0.3	0.5	0.8	1.0	1.3	1.5	1.8	2.0	2.3	2.5	2.8	3.0
200	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0
300	0.8	1.5	2.3	3.0	3.8	4.5	5.3	6.0	6.8	7.5	8.3	9.0
400	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0
500	1.3	2.5	3.8	5.0	6.3	7.5	8.8	10.0	11.3	12.5	13.8	15.0
600	1.5	3.0	4.5	6.0	7.5	9.0	10.5	12.0	13.5	15.0	16.5	18.0
700	1.8	3.5	5.3	7.0	8.8	10.5	12.3	14.0	15.8	17.5	19.3	21.0
800	2.0	4.0	6.0	8.0	10.0	12.0	14.0	16.0	18.0	20.0	22.0	24.0
900	2.3	4.5	6.8	9.0	11.3	13.5	15.8	18.0	20.3	22.5	24.8	27.0
1000	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0	27.5	30.0
1100	2.8	5.5	8.3	11.0	13.8	16.5	19.3	22.0	24.8	27.5	30.3	33.0
1200	3.0	6.0	9.0	12.0	15.0	18.0	21.0	24.0	27.0	30.0	33.0	36.0
1300	3.3	6.5	9.8	13.0	16.3	19.5	22.8	26.0	29.3	32.5	35.8	39.0
1400	3.5	7.0	10.5	14.0	17.5	21.0	24.5	28.0	31.5	35.0	38.5	42.0
1500	3.8	7.5	11.3	15.0	18.8	22.5	26.3	30.0	33.8	37.5	41.3	45.0
1600	4.0	8.0	12.0	16.0	20.0	24.0	28.0	32.0	36.0	40.0	44.0	48.0
1700	4.3	8.5	12.8	17.0	21.3	25.5	29.8	34.0	38.3	42.5	46.8	51.0
1800	4.5	9.0	13.5	18.0	22.5	27.0	31.5	36.0	40.5	45.0	49.5	54.0
1900	4.8	9.5	14.3	19.0	23.8	28.5	33.3	38.0	42.8	47.5	52.3	57.0
2000	5.0	10.0	15.0	20.0	25.0	30.0	35.0	40.0	45.0	50.0	55.0	60.0
2100	5.3	10.5	15.8	21.0	26.3	31.5	36.8	42.0	47.3	52.5	57.8	63.0
2200	5.5	11.0	16.5	22.0	27.5	33.0	38.5	44.0	49.5	55.0	60.5	66.0
2300	5.8	11.5	17.3	23.0	28.8	34.5	40.3	46.0	51.8	57.5	63.3	69.0
2400	6.0	12.0	18.0	24.0	30.0	36.0	42.0	48.0	54.0	60.0	66.0	72.0
2500	6.3	12.5	18.8	25.0	31.3	37.5	43.8	50.0	56.3	62.5	68.8	75.0
2600	6.5	13.0	19.5	26.0	32.5	39.0	45.5	52.0	58.5	65.0	71.5	78.0
2700	6.8	13.5	20.3	27.0	33.8	40.5	47.3	54.0	60.8	67.5	74.3	81.0
2800	7.0	14.0	21.0	28.0	35.0	42.0	49.0	56.0	63.0	70.0	77.0	84.0
2900	7.3	14.5	21.8	29.0	36.3	43.5	50.8	58.0	65.3	72.5	79.8	87.0
3000	7.5	15.0	22.5	30.0	37.5	45.0	52.5	60.0	67.5	75.0	82.5	90.0
3100	7.8	15.5	23.3	31.0	38.8	46.5	54.3	62.0	69.8	77.5	85.3	93.0
3200	8.0	16.0	24.0	32.0	40.0	48.0	56.0	64.0	72.0	80.0	88.0	96.0
3300	8.3	16.5	24.8	33.0	41.3	49.5	57.8	66.0	74.3	82.5	90.8	99.0
3400	8.5	17.0	25.5	34.0	42.5	51.0	59.5	68.0	76.5	85.0	93.5	102.0
3500 3600 3700 3800 3900	8.8 9.0 9.3 9.5 9.8	17.5 18.0 18.5 19.0	26.3 27.0 27.8 28.5 29.3	35.0 36.0 37.0 38.0 39.0	43.8 45.0 46.3 47.5 48.8	52.5 54.0 55.5 57.0 58.5	61.3 63.0 64.8 66.5 68.3	70.0 72.0 74.0 76.0 78.0	78.8 81.0 83.3 85.5 87.8	87.5 90.0 92.5 95.0 97.5	96.3 99.0 101.8 104.5 107.3	105.0 108.0 111.0 114.0 117.0
4000	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0	110.0	120.0
5000	12.5	25.0	37.5	50.0	62.5	75.0	87.5	100.0	112.5	125.0	137.5	150.0
6000	15.0	30.0	45.0	60.0	75.0	90.0	105.0	120 0	135.0	150.0	165.0	180.0
7000	17.5	35.0	52.5	70.0	87.5	105.0	122.5	140.0	157.5	175.0	192.5	210.0

METRIC MEASURES.

Correction for Humidity: Values of $\frac{1}{2} \left(\frac{0.378_0^4}{0.00367} \right)$

Top argument: Values of e. Side argument: Values of b. Auxiliary to Table 58.

Air					V	APOR P	RESSUE	E mm					
Pres- sure.	0.5	1	2	3	4	5	6	7	8	9	10	20	30
mm. 780	^о с.	°c.	°c.	о _с	°c.	о _с ,	°c,	°c,	°c,	°c. 0.6	°c.	°c.	°c.
760 740	0.0	.T	.ı I.	.2	.3 .3	•3 •4	.4 .4	.5 .5	·5 .6	.6 .6	·7 ·7	1.4 1.4	2.0 2.I
720 700	9 9	.1	.I .2	.2	·3 ·3	•4 •4	·4 •4	∙5 •5	.6 .6	.6 •7	·7	1.4	2.1
680 660	9 9	ı. ı.	.2	.2	•3 •3	•4 •4	·4 ·5	.5 .5	.6 .6	.7 .7	.8 .8	1.5 1.6	
640 620 600	0 0 0	I. I.	.2 .2 .2	.2 .2 .3	•3 •3 •3	·4 ·4 ·4	∙5 •5 •5	.6 .6	.6 .7 .7	.7 .8 .8	.8 .8 .9	1.6 1.7 1.7	
580 560 540 520 500	00000	1. 1. 1. 1.	.2 .2 .2 .2	·3 ·3 ·3 ·3	.4 .4 .4 .4	.4 .5 .5 .5	.5 .6 .6 .6	.6 .5 .7 .7	.7 .7 .8 .8	.8 .8 .9	.9 .9 1.0		
480 460 440 420 400	.1 .1 .1 .1	.1 .1 .1	.2 .2 .2 .2 .3	·3 ·4 ·4 ·4	.4 .4 .5 .5	.5 .6 .6 .6	.6 ·7 ·7 ·7	.8 .8				•	
380 360 340 320 300	1. 1. 1. 1.	.I .I .2 .2	.3 .3 .3 .3	.4 .4 .4 .5	.6								
280 260 240 220 200	.1 .1 .1 .1	.2 .2 .2 .2	.4 .4 .4										7.00
180 160 140 120 100	.1 .2 .2 .2	·3 ·4 ·4 ·5											
80 60 40 20 10	.3 .4 .6 1.3 2.6			_				t					

DETERMINATION OF HEIGHTS BY THE BAROMETER. DYNAMIC MEASURES.

Correction for Humidity: Values of $\frac{1}{2} \left(\frac{0.378_0^6}{0.00367} \right)$

Top argument: Values of e. Side argument: Values of b. Auxiliary to Table 58.

Air				-		VAPO	R PRE	SSURE	mb.					
Pres- sure.	0.5	1	2	3	4	5	6	7	8	9	10	20	30	40
mb. 1080 1060	°c. o.o	°c. o.o	°c. 0.1	°C. 0.1	°C. 0.2	°C. 0.2	°c. o.3	°c. 0.3	°c. 0.4 •4	°c. 0.4 •4	°c. 0.5 •5	°C, 1.0	°c. 1.4 1.5	°c. 1.9
1040 1020 1000	.o .o .o	.0 I. I.	.1 .1 .1	.I .2 .2	.2 .2 .2	.2 .3 .3	·3 ·3 ·3	·3 ·4 ·4	.4 .4 .4	.4 .5 .5	•5 •5 •5	I.0 I.0	1.5 1.5 1.5	2.0 2.0 2.I
980 960 940 920 900	.0 .0 .0 .0 .0	1. I. I. I.	 I. I.	.2 .2 .2 .2	.2 .2 .2 .2	.3 .3 .3 .3	·3 ·3 ·3 ·3 ·3	.4 .4 .4 .4	.4 .4 .4 .4	•5 •5 •5	.5 .5 .6 .6	1.1 1.1 1.1 1.1	1.6 1.6 1.6 1.7	2.I 2.I 2.2 2.2 2.3
880 860 840 820 800	0000	I. I. I. I.	1. 1. 1. 1. 1.	.2 .2 .2 .2 .2	.2 .2 .2 .3 .3	·3 ·3 ·3 ·3 ·3	.4 .4 .4 .4	.4 .4 .4 .4 .4	.5 .5 .5 .5	.5 .5 .6 .6	.6 .6 .6 .6	1.2 1.2 1.2 1.3 1.3	1.8 1.8 1.8 1.9	2.3
780 760 740 720 700	00000	 	.1 .1 .1 .1	.2 .2 .2 .2	·3 ·3 ·3 ·3 ·3	.3 .3 .3 .4 .4	.4 .4 .4 .4	.5 .5 .5 .5	.5 .6 .6	.6 .6 .6 .7	.7 .7 .7 .7	1.3 1.4 1.4 1.4 1.5	2.0	
680 660 640 620 600	.0	.I .I .I	.2 .2 .2 .2 .2	.2 .2 .2 .2 .2	·3 ·3 ·3 ·3 ·3	.4 .4 .4 .4	.5 .5 .5 .5	.5 .6 .6	.6 .6 .6 .7 .7	.7 .7 .7 .7	.8 .8 .8			
580 560 540 520 500	.0 .0 .0	I. I. I. I.	.2 .2 .2 .2	·3 ·3 ·3 ·3	.4 .4 .4 .4	.4 .5 .5 .5	.5 .6 .6 .6	.6 .6 .7 .7	.7 .7 .8 .8	.8				
480 460	I. I.	1. 1.	.2	-3	.4 .4	.5 .6	.6 .7	.8 .8			Air Pres-	VAPO	R PRES	SSURE
440 420	I.	I. I.	.2	·3 ·4 ·4	•5 •5	.6 .6	·7			}	Sure.	0.5	1	2
380 360 340 320 300	1. 1. 1. 1. 1.	.I .I .2 .2	·3 ·3 ·3 ·3 ·3 ·3 ·3	.4 .4 .4 .5 .5	.5 .6 .6 .6	.6 .7 .7 .8	.8				mb. 180 160 140 120	°C1 .2 .2 .2 .2 .3	°c. ·3 ·3 ·4 ·4	°c. .6 .6
280 260 240 220 200	.I .I .I .I	.2 .2 .2 .2 .2	.4 .4 .4 .5 .5	.6 .6 .6 .7	.7						* 80 60 40 20 10	.3 .4 .6 1.3 2.6		

METRIC MEASURES.

Correction for Gravity and Weight of Mercury : z (0.002640 cos 2 ϕ - 0.000007 cos^2 2 ϕ + 0.00244).

Approximate		LATITUDE (\$\phi\$)														
difference of Height, Z.	o°	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	75°
Meters. 100 200 300 400	m. I I 2 2	m. [1 2 2	m. O I I 2	m. O I I 2	m. O I I 2	m. O I I 2	m. O I I	m. O I I	m. O I I	m. 0 0 I	m. 0 U I	m. 0 0	m. 0 0 0 0	m. 0 0	m. 0 0 0	m. 0 0 0
500 600 700 800 900	3 3 4 4 5	3 3 4 4 5	2 3 3 4 4	2 3 3 4 4	2 3 3 4 4	2 3 3 4	2 2 3 3 3	2 2 2 3 3	1 2 2 2 3	I 1 2 2 2	I I I 2 2	I I I I	I I I I	0 I I I	0 0 0 0	0 0 0 0
1000 1100 1200 1300 1400	5 6 6 7 7	5 6 6 7 7	5 5 6 6 7	5 6 6 7	4 5 5 6 6	4 5 5 6	4 4 5 5 5	3 4 4 4 5	3 3 4 4	2 3 3 3 3	2 2 2 3 3	2 2 2 2 2 2	I I I I 2	I I I	0 0 1 1	0 0 0 0
1500 1600 1700 1800 1900	8 9 9	8 8 9 9	7 8 8 9	7 8 8 8 9	7 7 8 8 8	6 7 7 7 8	6 6 6 7 7	5 6 6 6	4 5 5 5 5	4 4 4 5	3 3 4 4	2 2 3 3 3	2 2 2 2 2	I I I	I I I I	0 0 0 0
2000 2100 2200 2300 2400	10 11 11 12 12	10 11 11 12 12	10 10 11 11 12	9 10 10 11	9 10 10	8 9 9 9	8 8 8 9	7 7 7 8 8	6 6 7 7	5 5 6 6	4 4 4 5 5	3 3 4 4	2 2 2 3 3	I 2 2 2 2	I I I	0 0 0 0
2500 2600 2700 2800 2900	13 13 14 14 15	13 13 14 14	12 13 13 14 14	12 12 13 13 14	11 12 12 12 13	10 11 11 12	9 10 10 11	8 9 9 9	7 8 8 8 8	6 6 7 7 7	5 5 6 6	4 4 4 4	3 3 3 3	2 2 2 2 2	I I I I	0 0 0 0
3000 3100 3200 3300 3400	15 16 16 17	15 16 16 17	15 16 16 16	14 15 15 16 16	13 14 14 15 15	12 13 13 14 14	11 12 12 12 13	10 11 11 11	9 9 9 10	7 8 8 8 8	6 6 6 7 7	5 5 5 5	3 3 4 4 4	2 2 2 2	I I I I	0 0 0 0
3500 3600 3700 3800 . 3900	18 18 19 19	18 18 19 19	17 18 18 19	17 17 17 18 18	16 16 16 17	14 15 15 16 16	13 14 14 14 15	12 12 12 13 13	10 11 11	9 9 9 9	7 7 7 8 8	5 5 6 6 6	4 4 4 4	3 3 3 3	I 1 2 2 2	I I I I
4000 4500 5000 5500 6000	20 23 25 28 30	20 23 25 28 30	20 22 25 27 29	19 21 24 26 28	18 20 22 24 27	17 19 21 23 25	15 17 19 21 23	13 15 17 18 20	12 13 14 16 17	10 11 12 13 15	8 9 10 11 12	6 7 8 8 9	4 5 6 6 7	3 3 4 4 4	2 2 2 2 2	I I I
6500 7000	33 35	33 35	32 34	31 33	29 31	27 29	24 26	22 23	19 20	16 17	13 14	10	7 8	5 5	3 3	I

METRIC MEASURES.

Correction for the variation of gravity with altitude: $\frac{z\,(z+2\,h_{
m o})}{R}$

												R			
Approxi- mate difference	HEIGHT OF LOWER STATION IN METERS (h _o). 0 200 400 600 800 1000 1200 1400 1600 1800 2000 2500 3000 4000														
of height. Z.	0	200	400	600	800	1000	1200	1400	1600	1800	2000	2500	3000	4000	
meters.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	
. 200	0	0	О	0	0	υ	О	0	0	o	О	0	О	0	
300	0	0	U	0	0	0	0	0	0	0	0	0	0	0	
400	0	0	0	0	0	0	0	0	0	0	0	0	0	I	
500	0	0	0	0	0	0	О	О	0	0	0	0	1	I	
600 700	0	0	0	0	0	0	0	0	0	0	0 I	I	I	I	
800	0	0	0	0	0	0	0	0	I	I	ī	ī	I	I	
900	О	0	0	0	0	0	0	I	1	1	1	1	1	1	
1000	0	0	0	0	0	o	1	ı	1	1	ı	1	I	ı	
1100	О	0	О	0	0	1	1	1	1	1	1	1	1	2	
1200	0	0	0	0	I	I	I	I	I	I	I	I	I	2 2	
1300 1400	0	0	0	I	I	I I	I	I I	I I	I	I	I	1 2	2	
				١.	Ţ		-								
1500 1600	0	0 I	I	I	I	I	I	I	I	I	I	2 2	2 2	2 2	
1700	0	1	1	1	I	r	I	I	1	I	2	2	2	3	
1800	I	I	I	I	I	I	I	ī	I	2	2	2	2	3	
1900	I	I	1	I	I	I	I	I	2	2	2	2	2	3	
2000	I	I	I	I	I	I	I	2	2	2	2	2	3	3	
2100 2200	I	ľ	I	I	I	I	1 2	2 2	2 2	2	2 2	2	3	3 3 4	
2300	I	ī	ī	ī	I	2	2	2	2	2	2	3	3	4	
2400	I	1	1	1	2	2	2	2	2	2	2	3	3	4	
2500	1	1	ı	1	2	2	2	2	2	2	3	3	3	4	
2600	I	I	I	2	2	2	2	2	2	3	3	3	4	4	
2700 2800	I	I	I 2	2 2	2 2	2 2	2	2	3 3	3	3	3	4	5	
2900	ī	2	2	2	2	2	2	3	3	3	3	4	4	5 5 5	
3000	1	2	2	2	2	2	3	3	3	3	3	4	4	5	
3100	2	2	2	2	2	2	3	3	3	3 3	3 4	4	4	5 5 6	
3200 3300	2	2 2	2 2	2 2	3	3	3	3	3	3 4	4	4 4	5 5	6	
3400	2	2	2	2	3	3	3	3	4	4	4	4	5	6	
3500	2	2	2	3	3	3	3	3	4	4	4	5	5	6	
3600	2	2	2	3	3		3	4	4	4	4	5	5 6	7	
3700	2	2	3	3	3	3 3 3	4	4	4	4	4	5 5	6	7 7	
3800 3900	2	3	3	3	3	3 4	4	4	4	4 5	5	5	6	7 7	
4000	,	-	_			'			1	_	-	6	6	8	
4500	3	3	3	3	4 4	4 5	4 5	5	5	5 6	5 6		7	9	
5000	4	4	5	5	5	5	5 6	5	5	7 8	7 8	7 8	9	10	
5500 6000	5 6	5	5	6	6 7	6 8	7 8	8	8	8	8	9 IO	10	12 13	
	1		1	'			1		_				1		
6500 7000	7 8	7 8	7	8	8	9 10	9 10	9	10	10	11	12	13	15 16	
,,,,,,	Ľ]	9	9										
<u> </u>	·				_							·			

DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF 0.1 INCH IN THE BAROMETER.

ENGLISH MEASURES.

Baro- metric		MEAN	ı Temi	PERATU	RE OF	THE	AIR IN	FAHR	ENHEI'	r dege	REES.	
Pres- sure.	30°	35°	40°	45°	50°	55°	60°	65°	70°	75°	80°	85°
Inches	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
22.0	119.2	120.5	121.8	123.1	124.4	125.8	127.1	128.5	129.8	131.2	132.5	133.9
.2	118.2	119.4	120.7	122.0	123.3	124.7	126.0	127.3	128.7	130.0	131.3	132.7
·4 .6	117.1	118.3	119.6	120.9	122.2 121.1	123.6	124.9 123.8	126.2 125.1	127.5	128.8	130.2	131.5
.8	115.0	117.3	117.5	119.8	121.1	122.5	123.0	124.0	125.3	126.6	127.9	129.2
	5		7.5				,		0-5		,	
23.0	114.0	115.3	116.5	117.8	119.0	120.3	121.6	122.9	124.2	125.5	126.8	128.1
.2	113.1	114.3	115.5	116.8	118.0	119.3	120.6	121.8	123.1	124.4	125.7	127.0
•4	112.1	113.3	114.5	115.8	117.0	118.3	119.5	120.8	122.1	123.3	124.6	125.9
.6 .8	III.I	112.3	113.5	114.8	116.0	117.3	118.5	119.8	121.0	122.3	123.5	124.8
,°	110.2	111.4	112.6	113.8	115.1	116.3	117.5	110.0	120.0	121.3	122.5	123.8
24.0	109.3	110.5	111.7	112.9	114.1	115.3	116.5	117.8	119.0	120.2	121.5	122.7
.2	108.4	109.5	110.7	111.9	113.1	114.4	115.6	116.8	11 8. 0	119.2	120.5	121.7
.4	107.5	108.6	109.8	111.0	112.2	113.4	114.6	115.9	117.1	118.3	119.5	120.7
.6	106,6	107.8	108.9	110.1	111.3	112.5	113.7	114.9	116.1	117.3	118.5	119.7
.8	105.8	106.9	108.1	109.2	110.4	111.6	112.8	114.0	115.2	116.4	117.6	118.8
25.0	104.9	106.0	107.2	108.3	109.5	110.7	111.9	113.1	114.2	115.4	116.6	117.8
.2	104.1	105.2	106.3	107.5	108.7	109.8	111.0	112,2	113.3	114.5	115.7	116.9
.4	103.3	104.4	105.5	106.6	107.8	109.0	110.1	111.3	112.4	113.6	114.8	116.0
.6	102.5	103.6	104.7	105.8	107.0	108.1	109.3	110.4	111.6	112.7	113.9	115.1
.8	101.7	102.8	103.9	105.0	106.1	107.3	108.4	109.6	110.7	111.9	113.0	114.2
26.0	100.9	102.0	103.1	104.2	105.3	106.4	107.6	108.7	109.9	III.O	112.1	113.3
.2	100.1	101.2	102.3	103.4	104.5	105.6	106.8	107.9	109.0	IIO.I	111.3	112.4
.4	99.4	100.4	101.5	102.6	103.7	104.8	106.0	107.1	108.2	109.3	110.4	111.6
.6	98.6	99.7	100.7	101.8	102.9	104.0	105.2	106.3	107.4	108.5	109.6	110.7
.8	97.9	98.9	100.0	ror.r	102.2	103.3	104.4	105.5	106.6	107.7	108.8	109.9
27.0	97. I	98.2	99.2	100.3	101.4	102.5	103.6	104.7	105.8	106.9	108,0	109.1
.2	96.4	97.5	98.5	99.Ğ	100.7	ror.8	102.8	103.9	105.0	106.í	107.2	108.3
•4	95.7	96.8	97.8	98.9	99.9	101.0	102.1	103.2	104.2	105.3	106.4	107.5
.6	95.0	96.1	97.I	98.1	99.2	100.3	101.3	102.4	103.5	104.6	105.6	106.7
.8	94.3	95-4	96.4	97.4	98.5	99.6	100.6	101.7	102.7	103.8	104.9	105.9
28.0	93.7	94.7	95.7	96.7	97.8	98.8	99.9	ror.o	102.0	103.1	104.1	105.2
.2	93.0	94.0	95.0	96. r	97.1	98.1	99.2	100.2	101.3	102.3	103.4	104.4
.4	92.4	93.4	94.4	95.4	96.4	97.5	98.5	99.5	100.6	101.6	102.7	103.7
.6	91.7	92.7	93-7	94.7	95.7	96.8	97.8	98.8	99.9	100.9	101.9	103.0
.8	91.1	92.1	93.1	94.1	95.1	96.1	97.1	98.2	99.2	100.2	101.2	102.3
29.0	90,4	91.4	92.4	93.4	94.4	95.4	96.5	97.5	98.5	99.5	100.5	101.6
.2	89.8	90.8	91.8	92.8	93.8	94.8	95.8	96.8	97.8	98.8	99.9	100.9
.4	89.2	90.2	91.1	92.1	93. r	94.1	95.1	96.1	97.1	98.2	99.2	100.2
.6	88.6	89.6	90.5	91.5	92.5	93.5	94.5	95.5	96.5	97.5	98.5	99.5
.8	88.0	89.0	89.9	90.9	91.9	92.9	93.9	94.9	95.8	96.8	97.8	98.8
30.0	87.4	88.4	89.3	90.3	91.3	92.3	93.2	94.2	95.2	96.2	97.2	98.2
30.0	86.8	87.8	88.7	89.7	90.7	91.7	93.2	93.6	94.6	95.6	96.5	97.5
.4	86.3	87.2	88.2	89.1	90.1	91.1	92.0	93.0	94.0	94.9	95.9	96.9
.6	85.7	86.7	87.6	88.5	89.5	90.5	91.4	92.4	93.3	94.3	95-3	96.2
.8	85.2	86.1	87.0	88.0	88.9	89.9	90.8	91.8	92.7	93.7	94-7	95.6
1]		<u> </u>	<u> </u>	<u> </u>				

DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF 1 MILLIMETER IN THE BAROMETER.

METRIC MEASURES.

Barometric	1	MEAN T	EMPERA	ATURE C	F THE	AIR IN	CENTIG	RADE D	EGREES	·
Pressure.	— 2°	O°	2°	4°	6°	8°	10°	12°	I4°	16°
mm.	Meters.									
760	10.48	10.57	10.65	10.73	10.81	10.89	10.98	11.06	11.15	11.23
750	10,62	10.71	10.79	10.87	10.95	11.04	11.13	11.21	11.30	11.38
740 730	10.77 10.91	10.85	10.93	II.02 II.I7	11.10	11.19	11.28	11.36	11.45	11.54 11.70
720	11.06	11.15	11.24	11.32	11.42	11.51	11.59	11.68	11.77	11.86
710	11.22	11.31	11.40	11.48	11.58	11.67	11.75	11.85	11.94	12.03
700	11.38	11.47	11.56	11.65	11.74	11.83	11.92	12.02	12.11	12.20
690 680	11.55 11.72	11.63	11.72	11.82	11.91	12.00	12.09	12.19	12.28	12.38
670	11.89	11.98	12.07	12.17	12.26	12.36	12.46	12.55	12.65	12.75
660	12.07	12.16	12.26	12.35	12.45	12.55	12.65	12.74	12.84	12.94
650	12.26	12.35	12.45	12.54	12,64	12.74	12.84	12.94	13.04	13.14
640 630	12.45 12.65	12.55 12.75	12.64	12.74	12.84	12.94 13.15	13.04 13.25	13.14	13.24	13.35 13.56
620	12.85	12.75	13.05	13.15	13.04	13.36	13.46	13.35 13.57	13.45	13.78
610	13.06	13.17	13.27	13.37	13.47	13.58	13.68	13.79	13.89	14.01
600	13.28	13.39	13.49	13.59	13.70	13.80	13.91	14.02	14.13	14.24
590 580	13.51	13.62	13.72	13.82	13.93	14.03	14.15	14.26	14.37	14.48
570	13.74	13.85	13.96 14.20	14.06 14.31	14.17 14.42	14.28 14.53	14.39 14.64	14.51 14.76	14.62 14.88	14.73 14.99
560	14.23	14.34	14.45	14.57	14.68	14.79	14.90	15.02	15.14	15.25
	1	MEAN T	EMPERA	TURE O	F THE	AIR IN	CENTIG	RADE D	EGREES	
Barometric Pressure.	18°	20°	22°	24°	26°	28°	30°	32°	34°	36°
mm.	Meters.									
760	11.32	11.41	11.49	11.58	11.66	11.75	11.84	11.92	12.01	12,10
750	11.47	11.56	11.64	11.73	11.82	11.91	12.00	12.08	12.17	12,26
740 730	11.63 11.79	11.72 11.88	11.80	11.89	11.98	12.07 12.23	12.16	12.24 12.41	12.33	12.42
720	11.95	12.04	12.13	12.22	12.32	12.40	12.49	12.58	12.68	12.77
710	12.12	12.21	12.30	12.39	12.49	12.58	12.67	12.76	12.86	12.95
700	12.29	12.39	12.48	12.57	12.67	12.76	12.85	12.94	13.04	13.13
690 680	12.47	12.57 12.75	12.66	12.75	12.85	12.94 13.13	13.04	13.13	13.23	13.32
670	12,85	12.75	13.04	13.14	13.23	13.33	13.43	13.52	13.42	13.52
660	13.04	13.14	13.24	13.34	13.43	13.53	13.63	13.73	13.83	13.93
650	13.24	13.34	13.44	13.54	13.64	13.74	13.84	13.94	14.04	14.15
640 630	13.45 13.66	13.55	13.65	13.75	13.85	13.96 14.18	14.06 14.28	14.15	14.26	14.37
620	13.88	13.70	14.09	14.20	14.30	14.16	14.20	14.62	14.49	14.83
610	14.11	14.21	14.32	14.43	14.54	14.64	14.75	14.86	14.96	15.07
600	14.35	14.45	14.56	14.67	14.78	14.89	15.00	15.11	15.21	15.32
590 580	14.59 14.84	14.70	14.81	14.92	15.03	15.14 15.40	15.25 15.52	15.36	15.47 15.74	15.59 15.86
570	15.10	15.21	15.33	15.44	15.56	15.40	15.79	15.91	16.02	16.14
560	15.37	15.48	15.60	15.72	15.84	15.95	16.07	16.19	16.30	16.42
				<u> </u>		<u> </u>	J	<u> </u>		

Formula of Babinet.

$$Z = C\frac{B_o - B}{B_o + B}$$

$$C \text{ (in feet)} = 52494 \left[I + \frac{t_o + t - 64}{900} \right] - \text{English Measures.}$$

$$C \text{ (in metres)} = 16000 \left[I + \frac{2(t_o + t)}{1000} \right] - \text{Metric Measures.}$$

In which Z = Difference of height of two stations in feet or metres.

 $B_{\rm o},\,B={
m Barometric}$ readings at the lower and upper stations respectively, corrected for all sources of instrumental error.

 t_0 , t = Air temperatures at the lower and upper stations respectively.

Values of C.

ENGLISH MEASURES.

METRIC MEASURES.

1/2 (t _o + t).	log C.	c.
F.		Feet.
10°	4.69834	49928
15	.70339	50511
20	.70837	51094
25	.71330	51677
30	.71818	52261
35	4.72300	52844
40	.72777	53428
45	.73248	54011
50	.73715	54595
55	.74177	55178
60	4.74633	55761
65	.75085	56344
70	·75532	56927
75	•75975	57511
8o	.76413	58094
	•	
85	4.76847	58677
90	.77276	59260
95	.77702	59844
100	.78123	60427
		J

½ (t _o + t).	log C.	c.
c.		Metres.
-10°	4.18639	15360
-8	.19000	15488
-6	.19357	15616
-4	.19712	15744
- 2	.20063	15872
0	4.20412	16000
+2	.20758	16128
4	.21101	16256
6	.21442	16384
8	.21780	16512
10	4.22115	16640
12	.22448	16768
14	.22778	16896
16	.23106	17024
18	.23431	17152
20	4.23754	17280
22	.24075	17408
24	.24393	17536
26	.24709	17664
28	.25022	17792
30		
	4.25334	17920
32	.25643	18048
34	.25950	18176
36	.26255	18304

TABLE 67.
BAROMETRIC PRESSURES CORRESPONDING TO THE TEMPERATURE
OF THE BOILING POINT OF WATER.

ENGLISH MEASURES.

Tempera-	1									
ture.	.0	1	.2	.3	.4	.5	.6	.7	.8	.9
F.	Inches.	inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
185°	17.075	17.112	17.150	17.187	17.224	17.262	17.300	17.337	17.375	17.413
186	17.450	17.488	17.526	17.564	17.602	17.641	17.679	17.717	17.756	17.794
187	17.832	17.871	17.910	17.948	17.987	18.026	18.065	18.104	18.143	18.182
188	18.221	18.261	18.300	18.340	18.379	18.419	18.458	18.498	18.538	18.578
189	18.618	18.658	18.698	18.738	18.778	18.818	18.859	18.899	18.940	18.980
190	19.021	19.062	19.102	19.143	19.184	19.225	19.266	19.308	19.349	19.390
191	19.431	19.473	19.514	19.556	19.598	19.639	19.681	19.723	19.765	19.807
192	19.849	19.892	19.934	19.976	20.019	20.061	20.104	20.146	20.189	20.232
193	20.275	20.318	20.361	20.404	20.447	20.490	20.533	20.577	20.620	20.664
194	20.707	20.751	20.795	20.839	20.883	20.927	20.971	21.015	21.059	21.103
195	21.148	21.192	21.237	21.282	21.326	21.371	21.416	21.461	21.506	21.551
196	21.597	21.642	21.687	21.733	21.778	21.824	21.870	21.915	21.961	22.007
197	22.053	22.099	22.145	22.192	22.238	22,284	22.331	22.377	22.424	22.471
198	22.517	22.564	22.611	22.658	22.706	22.753	22.800	22.847	22.895	22.942
199	22.990	23.038	23.085	23.133	23.181	23.229	23.277	23.325	23.374	23.422
200	23.470	23.519	23.568	23.616	23.665	23.714	23.763	23.812	23.861	23.910
201	23.959	24.009	24.058	24.108	24.157	24.207	24.257	24.307	24.357	24.407
202	24.457	24.507	24.557	24.608	24.658	24.709	24.759	24.810	24.861	24.912
203	24.963	25.014	25.065	25.116	25.168	25.219	25.271	25.322	25.374	25.426
204	25.478	25.530	25.582	25.634	25.686	25.738	25.791	25.843	25.896	25.948
205	26.001	26.054	26.107	26.160	26.213	26.266	26.319	26.373	26.426	26.480
206	26.534	26.587	26.641	26.695	26.749	26.803	26.857	26.912	26.966	27.021
207	27.075	27.130	27.184	27.239	27.294	27.349	27.404	27.460	27.515	27.570
208	27.626	27.681	27.737	27.793	27.848	27.904	27.960	28.016	28.073	28.129
209	28.185	28.242	28.298	28.355	28.412	28.469	28.526	28,583	28.640	28.697
210	28.754	28.812	28.869	28.927	28.985	29.042	29.100	29.158	29.216	29.275
211	29.333	29.391	29.450	29.508	29.567	29.626	29.685	29.744	29.803	29.862
. 212	29.921	29.981	30.040	30.100	30.159	30.219	30.279	30.339	30.399	30.459
213	30.519	30.580	30.640	30.701	30.761	30.822	30.883	30.944	31.005	31.066
214	31.127	31.199	31.250	31.311	31.373	31.435	31.497	31.559	31.621	31.683

TABLE 68.

METRIC MEASURES.

Tempera- ture.	٥.	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	mm.									
80°	355.40	356.84	358.28	359-73	361.19	362.65	364.11	365.58	367.06	368.54
81	370.03	371.52	373.01	374.51	376.02	377.53	379.05	380.57	382 .0 9	383.62
82	385.16	386.70	388.25	389.80	391.36	392.92	394-49	396.06	397.64	399-22
83	400.81	402.40	404.00	405.61	407.22	408.83	410.45	412.08	413.71	415.35
84	416.99	418.64	420.29	421.95	423.61	425.28	426.95	428.64	430.32	432.01
85	433.71	435.41	437.12	438.83	440.55	442.28	444.01	445.75	447-49	449-24
86	450.99	452-75	454-51	456.28	458.06	459.84	461.63	463.42	465.22	467.03
87	468.84	470.66	472.48	474.31	476.14	477.99	479.83 498.63	481.68	483.54	485.4 1
88	487.28	489.16 508.26	491.04 510.20	492.93 512.15	494.82	496.72 516.07	518.04	500.54 520.01	502.46 521.99	504.39 523.98
89	506.32	_	·		514.11					
90	525.97	527.97	529.98	531.99	534.01	536.04	538.07	540.11	542.15	544.21
91	546.26	548.33	550.40	552.48 573.61	554.56	556.65 577.92	558.75 580.08	560.85 582.25	562.96 584.43	565.08 586.61
92	567.20 588.80	569.33 591.00	571.47 593.20	595.4I	575.76 597.63	599.86	602.00	604.33	606.57	608.82
93 94	611.08	613.35	615.62	617.90	620.10	622.48	624.79	627.00	620.41	631.73
11			638.74	641.00	. 1	645.82	648.19	650.57	652.96	655-35
95 96	634.06	636.40 660.16	662.58	665.00	643.45 667.43	669.87	672.32	674.77	677.23	679.70
97	657.75 682.18	684.66	687.15	680.65	692.15	694.67	697.19	699.71	702.25	704.79
98	707.35	709.90	712.47	715.04	717.63	720.22	722.81	725.42	728.03	730.65
99	733.28	735.92	738.56	741.21	743.87	746.54	749.22	751.90	754-59	757.29
100	760.00	762.72	765.44	768.17	770.91	773.66	776.42	779.18	781.95	784.73

HYGROMETRICAL TABLES.

Pressure of aqueous vapor over ice — English measures	Table 69
Pressure of aqueous vapor over water — English measures	TABLE 70
Pressure of aqueous vapor over ice — Metric measures	TABLE 71
Pressure of aqueous vapor over water — Metric measures	TABLE 72
Weight of a cubic foot of saturated vapor — English measures	Table 73
Weight of a cubic meter of saturated vapor — Metric measures	TABLE 74

PRESSURE OF AQUEOUS VAPOR OVER ICE.

ENGLISH MEASURES.

31 .17228 .17306 .17386 .17466 .17546 .17626 .17707 .17788 .17869 .17950	Tempera- ture.	Vapor Pressur	Tempera ture,	Vapor Pressu	Tem re, tu	oera- re.	Vapo Pressu	r re.	Tempe ture	ra-	V: Pre	spor ssure.	Te	mpera- ture,	F	Vapor ressure.
-60° 0.00009 -45° 0.0075 -30° 0.00705 -15.0° 0.01600 -7.5° 0.02556 39 0.00107 44 0.00294 29 0.00749 14.5 0.0138 7.0 0.02658 37 0.0123 42 0.00334 27 0.0844 13.5 0.1838 7.0 0.02658 37 0.0133 41 0.00356 26 0.0866 13.0 0.1890 5.5 0.0847 0.0257 0.00131 41 0.00356 20 0.0866 13.0 0.1890 5.5 0.0847 0.00331 41 0.00356 0.0008 12.0 0.0198 4.5 0.0036 5.5 0.0847 0.0151 39 0.00404 24 0.0008 12.0 0.0198 4.5 0.0036 5.3 0.00161 38 0.0041 23 0.0160 11.5 0.0254 4.0 0.0384 52 0.0173 37 0.0048 21 0.01201 10.5 0.0217 3.0 0.0383 0.0048 21 0.01201 10.5 0.0217 3.0 0.0353 0.0058 33 0.0048 21 0.01201 10.5 0.0217 3.0 0.0253 0.00161 48 0.0026 33 0.0058 18 0.01426 0.0 0.0236 1.5 0.0326 0.0344 46 0.00258 31 0.0664 16 0.01598 8.0 0.02487 0.5 0.0371 34 0.00552 17 0.01510 8.5 0.02421 1.0 0.0344 0.00258 31 0.0664 16 0.01598 8.0 0.02487 0.5 0.03710 0.03710 0.03809 0.03849 0.03869 0	-	Inches	-	Inche	.		Inche				l Ind	chae				Inches
S9	-60°	1					I .	- 1		٥°	1			7 5°		
\$8								- 1								
57	1 58	1														1
56				"	~											
-55											.0	1890		5.5		
54	11	.0014	ı –40	. 003	70 -2	5	.000	51	-12	5	.0	1043				02024
53					, ,	-			-	_				1		
52		.0016		. 004	31	3	.010	69	11.	5	.0	2054				03084
-50	52	.0017				2	.011	33	II.	0	.0	2111		3.5		03168
40	51	.0018	5 36	. 004	88	I	.012	01	10.	5	.0	2170		3.0		03253
49	-50	.0010	8 –35	. 005	10 -2	0	.012	72	-10.	0	.0	2230	-:	2.5		03340
48	49	.0021	I 34			9								2.0		
47		.0022				·8			9.	0	. 0	2356		1.5		
Temperat. .0	47						.015	10	8.	5				1.0		03614
F. Inches.	46	.0025	8 31	.006	64	6	.015	98	8.	0	.0	2487		0.5		03710
F. Inches.	1	1	<u>, </u>		'	-	<u> </u>		·	_		<u> </u>	۲		_	
0° 0.03809 0.03829 0.03849 0.03869 0.03869 0.03890 0.03910 0.03930 0.03951 0.03971 0.03992 1.04013 0.04013 0.04055 0.04097 0.04118 0.04140 0.04161 0.04183 0.04204 0.04220 0.04220 0.04220 0.04323 0.04382 0.04040 0.04519 0.04539 0.04382 0.04040 0.04519 0.04585 0.04073 0.04782 0.04533 0.04857 0.04831 0.04657 0.04665 0.04085 0.04790 0.04733 0.04782 0.04877 0.04831 0.04856 0.04881 0.04066 0.05189 0.05215 0.05242 0.05209 0.05322 0.05320 0.05327 0.05495 0.05487 0.05487 0.05542 0.05542 0.05542 0.05542 0.05542 0.05542 0.05542 0.05270 0.05037 0.0607 0.06037 0.06037 0.06037 0.06037 0.06037 0.06047 0.06048 0.06442 0.06442 0.06442 0.06442 0.06442 0.06442 0.06442 0.06443 0.07039 0.07044 0.07039 0.07044 0.07039 0.07444 0.07039 0.07444 0.07039 0.07444 0.07039 0.07444 0.07039 0.07436 0.07429 0.07848 0.07883 0.06387 0.06037 0.06037 0.07009 0.07044 0.07039 0.07436 0.07429 0.07848 0.07833 0.06060 0.06940	Tem- perat.	.0	.1	.2	.3	_ _	.4	_	.5 /	_ •	.6	.7	_	.8	_	.9
0° 0.03809 0.03829 0.03849 0.03869 0.03869 0.03890 0.03910 0.03930 0.03951 0.03971 0.03992 1.04013 0.04013 0.04055 0.04097 0.04118 0.04140 0.04161 0.04183 0.04204 0.04220 0.04220 0.04220 0.04323 0.04382 0.04040 0.04519 0.04539 0.04382 0.04040 0.04519 0.04585 0.04073 0.04782 0.04533 0.04857 0.04831 0.04657 0.04665 0.04085 0.04790 0.04733 0.04782 0.04877 0.04831 0.04856 0.04881 0.04066 0.05189 0.05215 0.05242 0.05209 0.05322 0.05320 0.05327 0.05495 0.05487 0.05487 0.05542 0.05542 0.05542 0.05542 0.05542 0.05542 0.05542 0.05270 0.05037 0.0607 0.06037 0.06037 0.06037 0.06037 0.06037 0.06047 0.06048 0.06442 0.06442 0.06442 0.06442 0.06442 0.06442 0.06442 0.06443 0.07039 0.07044 0.07039 0.07044 0.07039 0.07444 0.07039 0.07444 0.07039 0.07444 0.07039 0.07444 0.07039 0.07436 0.07429 0.07848 0.07883 0.06387 0.06037 0.06037 0.07009 0.07044 0.07039 0.07436 0.07429 0.07848 0.07833 0.06060 0.06940	F.	Inches.	Inches.	Inches.	Inches	.	Inches.	1	nches.	ln:	ches.	Inche	s.	Inche	s.	Inches.
1		0.03800	0.03820	0. 03840		- 1	03800	ο.	03010				- 1		- 1	
3																
1	2	.04226	. 04248	.04270	. 0429	2	. 04314		04337	. 0.	4359	.043	82	. 0440	24	.04427
5 .04931 .04956 .04982 .05007 .05033 .05058 .05084 .05110 .05136 .05162 6 .05189 .05242 .05269 .05296 .05322 .05350 .05377 .05404 .05431 7 .05459 .05487 .05514 .05522 .05570 .05588 .05627 .05655 .05684 .05712 8 .05741 .05770 .05799 .05828 .05887 .05917 .05977 .05977 .05077 9 .06037 .06670 .06098 .06128 .06159 .06190 .06221 .06252 .06283 .06315 10 .06346 .06378 .06410 .06442 .06474 .06570 .06539 .06572 .06605 .06638 11 .06070 .06737 .06770 .06844 .07149 .07220 .07256 .07222 .07328 13 .07363 .07399 .07436 .07472 .07590 .07546<	3	. 04450	. 04473	. 04496	. 0451	9 .	.04543			. 0	4590					.04661
6 .05189 .05215 .05242 .05269 .05296 .053350 .05377 .05404 .05431 .70854 .05459 .05487 .05514 .05542 .05570 .05598 .05637 .05685 .05684 .05712 .0570 .05709 .05828 .05838 .06130 .06221 .05252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06241 .06570 .06604 .06975 .07000 .07044 .07079 .07114 .07149 .07184 .07220 .07256 .07202 .07328 .07363 .07339 .07436 .07472 .07509 .07546 .07583 .07621 .07658 .07696 .07925 .07964 .0803 .08042 .08082 .08051 .08101 .08201 .08201 .08241 .08281 .08281 .08321 .08362 .08505 .08565 .08566 .08608 .08650 .08692 .08734 .08777 .08819 .08862 .08905 .09345 .09364 .09364 .09311 .09355 .09300 .09335 .09345 .09362 .10032 .11038 .10186 .10235 .10284 .09360 .11033 .10333 .10333 .10332 .10342 .10482 .10532 .10582 .10633 .10683 .10734 .10785 .22 .11361 .11415 .11469 .11523 .11578 .11202 .11255 .11308 .12423 .11909 .11965 .12022 .12078 .12135 .12192 .12250 .12307 .12365 .12423 .13415 .11445 .114481 .14	4	. 04685	. 04709	. 04733	. 0475	8 .	. 04782		04807	. 0.	4831	. 048	56	. 0488	31	. 04906
6 .05189 .05215 .05242 .05269 .05296 .053350 .05377 .05404 .05431 .70854 .05459 .05487 .05514 .05542 .05570 .05598 .05637 .05685 .05684 .05712 .0570 .05709 .05828 .05838 .06130 .06221 .05252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06221 .06252 .06283 .06315 .06190 .06241 .06570 .06604 .06975 .07000 .07044 .07079 .07114 .07149 .07184 .07220 .07256 .07202 .07328 .07363 .07339 .07436 .07472 .07509 .07546 .07583 .07621 .07658 .07696 .07925 .07964 .0803 .08042 .08082 .08051 .08101 .08201 .08201 .08241 .08281 .08281 .08321 .08362 .08505 .08565 .08566 .08608 .08650 .08692 .08734 .08777 .08819 .08862 .08905 .09345 .09364 .09364 .09311 .09355 .09300 .09335 .09345 .09362 .10032 .11038 .10186 .10235 .10284 .09360 .11033 .10333 .10333 .10332 .10342 .10482 .10532 .10582 .10633 .10683 .10734 .10785 .22 .11361 .11415 .11469 .11523 .11578 .11202 .11255 .11308 .12423 .11909 .11965 .12022 .12078 .12135 .12192 .12250 .12307 .12365 .12423 .13415 .11445 .114481 .14	5	04027	04056	04082	0500	7	05022	Ι.	05058	_	r084	051	TO!	051	.6	05160
7 .05459 .05487 .05514 .05542 .05570 .05598 .05627 .05655 .05684 .05712 .05701 .05771 .05790 .05828 .05838 .05873 .05917 .05947 .05977 .05007 .05037 .05037 .05007 .05037 .05007 .05037 .05007 .05038 .06128 .06128 .06129 .06129 .06221 .06252 .06283 .06315 .06006 .06346 .06378 .06442 .06474 .06507 .06503 .06572 .06605 .06638 .07022 .07000 .07044 .07079 .07114 .07149 .07184 .07220 .07256 .07202 .07328 .13 .07363 .07399 .07436 .07472 .07509 .07546 .07583 .07621 .07658 .07696 .0803 .08042 .08082 .08052 .08525 .08566 .08608 .08650 .08692 .08734 .08777 .08819 .08862 .08065 .09405 .09435 .09481 .09526 .09572 .09618 .09614 .09711 .09757 .09804 .09994 .10042 .10090 .10138 .10683 .10734 .10785 .10284 .20 .10333 .10383 .10432 .10482 .10532 .10582 .11687 .11742 .11798 .11853 .11009 .11965 .12022 .12078 .12155 .12125 .12125 .1225 .12307 .12365 .12243 .12481 .12540 .12598 .12657 .12717 .12776 .12836 .12896 .12956 .13699 .13784 .14481 .																
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16	14	.0//33	.0///1	.07009	.0702	٦	. 07000		0/923	. 0	1904	.000	ادا	. 0002	+~	.00002
17	15	.08121	.08161	. 08201	.0824	Ι.	. o8281	٠.	08321	.0	8362	. 084	02	. 084	43	. 08484
18 .09300 .09435 .09481 .09526 .09572 .09618 .09644 .09711 .09757 .09804 19 .09851 .09898 .09946 .09994 .10042 .10090 .10138 .10186 .10235 .10284 20 .10333 .10383 .10432 .10482 .10532 .10582 .10633 .10683 .10734 .10785 21 .10836 .10888 .10940 .10992 .11044 .11096 .11149 .11202 .11255 .11308 22 .11361 .11415 .11469 .11523 .11578 .11632 .11687 .11742 .11798 .11853 23 .11965 .12202 .12078 .12135 .12210 .12250 .12367 .12276 .12276 .12276 .12276 .12276 .122836 .12280 .12265 .12307 .12365 .12423 24 .13077 .13138 .13200 .13257 .13323 .13385	16						- 1						- 1			. 08905
19																
20 .10333 .10383 .10432 .10482 .10532 .10582 .10633 .10683 .10734 .10785 21 .10836 .10888 .10940 .10992 .11044 .11096 .11149 .11202 .11255 .11308 22 .11361 .11415 .11469 .11523 .11578 .11632 .11687 .11742 .11798 .11853 23 .11900 .1965 .12022 .12078 .12135 .12192 .12250 .12307 .12365 .12423 24 .12481 .12540 .12598 .12657 .12717 .12776 .12836 .12896 .12956 .13017 25 .13077 .13138 .13200 .13261 .13323 .13385 .13447 .13510 .13573 .13636 26 .13699 .13763 .13887 .13891 .13956 .14021 .14086 .14151 .14282 27 .14348 .14415 .14484 .14							,									
21	19	.09851	. 09898	. 09946	. 0999	4	. 10042	٠	10090	. І	0138	. IOI	86	. 102	35	10284
21 .10836 .10888 .10940 .10992 .11044 .11096 .11149 .11202 .1225 .11308 22 .11361 .11415 .11469 .11523 .11578 .11632 .11687 .11742 .11798 .11853 23 .11909 .11965 .12022 .12678 .12135 .12192 .12250 .12307 .12365 .12423 24 .12481 .12540 .12598 .12675 .12717 .12776 .12836 .12896 .12956 .13017 25 .13077 .13138 .13200 .13261 .13323 .13385 .13447 .13510 .13573 .13636 26 .13690 .13763 .13827 .13891 .13956 .14021 .14866 .14151 .14216 .14282 27 .14348 .14415 .14481 .14548 .14616 .14683 .14751 .14819 .14887 .14956 28 .15024 .15993 .15874 .15947 .16020 .16093 .16167 .16241 .16315 .	20	TO	10282	10/22	. 1045	2	10532		10582	т	0622	. 106	82	ל סד.	21	T0785
22		10826														
23 .11909 .11965 .12022 .12078 .12135 .12192 .12250 .12307 .12365 .12423 .12481 .12540 .12598 .12657 .12717 .12776 .12836 .12896 .12950 .13017 .25																
24 .1248î .12540 .12598 .12657 .12717 .12776 .12836 .12896 .12956 .13017 25 .13077 .13138 .13200 .13261 .13323 .13385 .13447 .13510 .13573 .13636 .26 .13699 .13763 .13827 .13891 .13956 .14021 .14086 .14151 .14216 .14282 .27 .14348 .14415 .14481 .14548 .14616 .14683 .14751 .14819 .14887 .14956 .28 .15024 .15093 .15163 .15233 .15303 .15374 .15444 .15515 .15586 .15658 .29 .15729 .15801 .15874 .15947 .16020 .16093 .16167 .16241 .16315 .16389 .30 .16463 .16538 .16614 .16690 .16766 .16842 .16919 .16996 .17073 .17150 .31 .17228 .17306 .17386 .17466 .17546 .17546 .17626 .17707 .17788 .17869 .17950										l .	•					
25																
26 .13699 .13763 .13827 .13891 .13956 .14021 .14086 .14151 .14216 .14282 .14348 .14415 .14481 .14548 .14616 .14683 .14751 .14819 .14887 .14956 .28			, , , ₋					ŀ			·	1			-	
27 .14348																
28 .15024 .15093 .15163 .15233 .15303 .15374 .15444 .15515 .15586 .15658 .29 .15729 .15801 .15874 .15947 .16020 .16093 .16167 .16241 .16315 .16389 .30 .16463 .16538 .16614 .16690 .16766 .16842 .16919 .16996 .17073 .17150 .17228 .17306 .17386 .17466 .17546 .17546 .17626 .17707 .17788 .17869 .17950																
29 .15729 .15801 .15874 .15947 .16020 .16093 .16167 .16241 .16315 .16389 30 .16463 .16538 .16614 .16690 .16766 .16842 .16919 .16996 .17073 .17150 31 .17228 .17306 .17386 .17466 .17546 .17626 .17707 .17788 .17869 .17950							•									
30 .16463 .16538 .16614 .16690 .16766 .16842 .16919 .16996 .17073 .17150 .17228 .17306 .17386 .17466 .17546 .17546 .17626 .17707 .17788 .17869 .17950																
31 .17228 .17306 .17386 .17466 .17546 .17626 .17707 .17788 .17869 .17950	29	. 15729	. 15001	. 15074	. 1594	1	. 10020	١.	10093	. 1	.0107	. 102	41	. 103	15	. 10309
31 .17228 .17306 .17386 .17466 .17546 .17626 .17707 .17788 .17869 .17950	30	. 16463	. 16538	. 16614	. 1660	0	. 16766	١.	16842	. 1	6919	. 160	96	. 170	73	. 17150
																. 17950
	32	. 18032					•	ŀ				''		'		

PRESSURE OF AQUEOUS VAPOR OVER WATER. ENGLISH MEASURES.

Tempera- ture.	'0	.1	.2	.3	.4	٠5	.6	.7	.8	.9
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches,	Inches.	Inches.	Inches.	Inches.
32°	0.1803	0.1810	0.1818	0.1825	0.1833	0.1840	0.1847	0.1855	0.1862	0.1870
33	.1877	.1885	.1893	.1900	.1908	.1915	.1923	.1931	.1939	.1946
34	1954	.1962	.1970	.1978	.1986	.1994	.2002	.2010	.2018	.2026
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35	.2034	.2042	.2050	.2059	.2067	.2075	.2083	.2091	.2100	.2108
36	.2117	.2125	.2133	.2142	.2150	.2159	.2168	.2176	.2185	.2193
37	.2202	.2211	.2220	.2228	.2237	.2246	.2255	.2264	.2273	.2282
37 38	.2291	.2300	.2300	.2318	2327	.2336	.2345	.2355	.2364	.2373
39	.2382	.2392	.2401	.2410	.2420	.2429	.2439	.2448	.2458	.2467
		"	.							
40	.2477	.2487	.2496	.2506	.2516	.2526	.2536	.2545	-2555	.2565
41	.2575	.2585	.2595	.2606	.2616	.2626	.2636	.2646	.2656	.2667
42	.2677	.2687	.2698	.2708	.2719	.2729	.2740	.2750	.2761	.2771
43	.2782	.2793	.2804	.2814	.2825	.2836	.2847	.2858	2869	.2880
44	.2891	.2902	.2913	.2924	.2935	.2946	.2958	.2969	.2981	.2992
il i	ĺ (·				
45	.3003	.3014	.3026	.3037	.3049	.3061	.3073	.3084	.3096	.3108
46	.3120	.3132	.3144	.3156	.3167	.3179	.3191	.3203	.3216	.3228
47	.3240	.3252	.3265	-3277	.3289	.3301	.3314	.3326	.3339	.3352
48	3365	-3377	.3390	.3402	.3415	.3428	-344I	-3454	.3467	.3480
49	.3493	.3506	.3519	·3532	.3546	•3559	.3572	.3585	-3599	.3612
										-
50	.3626	.3639	.3653	.3666	.368o	.3694	.3708	.3722	.3736	-3749
51	.3763	-3777	.3791	.3805	.3820	.3834	.3848	.3862	.3876	.3890
52	.3905	.3919	-3934	.3948	.3963	.3978	-3993	.4007	.4022	.4037
53	.4052	.4067	.4082	.4097	.4112	.4127	.4142	.4157	.4172	.4187
54	.4203	.4218	.4234	.4249	.4265	.4280	.4296	.4312	.4328	4343
55	·4359	·4375	.4391	.4407	.4423	·4439	·4455	.447I	.4488	4504
56	.4521	-4537	·4554	-4570	.4587	.4603	.4620	4637	.4654	.4670
57	.4687	.4704	.4721	.4738	•4755	·4772	.4790	.4807	.4824	.4841
58	.4859	.4876	.4894	.4912	.4930	4947	.4965	.4983	.5001	.5019
59	.5037	.5055	.5073	.5091	.5110	.5128	.5146	.5164	.5183	.5201
II I			_							}
60	.5220	.5239	.5258	.5276	·5295	•5314	-5333	·5352	.5371	.5390
61	.5409	.5428	.5448	.5467	.5486	.5505	·5525	•5545	.5565	.5584
62	.5604	.5624	.5644	.5663	.5683	5703	-5724	·5744	.5764	.5784
63	.5805	.5825	.5846	.5866	.5887	.5908	.5929	•5950	.5971	.5992
64	.6013	.6034	.6055	.6076	.6097	.6118	.6140	.6161	.6183	.6204
	6	60	6	6000	600.	6006	60-0	6.0-	6.00	6.24
65	.6226	.6248	.6270	.6292	.6314	.6336	.6358	.6380	.6402	.6424
66	.6447	.6469	.6492	.6514	.6537	.6559		.6605	.6628	.6651
67 68	.6674	.6697	.6721	.6744	.6767	.6790	.6814	.6837	.7101	
60	.6909	.6932	.6956	.6980	.7004	.7028	.7053	.7077		.7125
1 09	.7150	.7174	.7199	.7224	.7249	•7274	.7299	-7324	.7348	.7373
70	7200	7424	.7449	.7474	.7500	.7526	.7552	•7577	.7603	.7629
71	7399	.7424	.7707	•77733	.7760	.7786	.7813	.7839	.7866	.7892
72	7655	.7946	.7973	.8000	.8027	.8054	.8081	.8108	.8136	.8163
73	.7919 .8191	.8219	.8247	.8274	.8302	.8330	.8358	.8386	.8414	.8442
74	.8471	.8499	.8528	.8556	.8585	.8614	.8643	.8672	.8701	.8730
' ⁺	.04/1	.0499	.03.20	.0330	.0,05	1	10043.	,2	.5,51	.5,50
75	.8760	8780	.8818	.8847	.8877	.8007	.8937	.8966	.8996	.9026
76	.9056	.9086	.9117	.9147	.0178	.9208	.9239	.9269	.9300	.9331
77	.9362	.9393	.9424	9455	.9487	.9518	.9550	.9581	.9613	.9645
78	.9677	.9709	.9741	•9773	.9805	.9837	.9870	.9902	-9935	.9968
79	1.0001	1.0033	1.0066	1.0099	1.0133	1.0166	1.0100	1.0232	1.0266	1.0300
'				- 77	-00		"			
80	1.0334	1.0367	1.0401	1.0435	1.0470	1.0504	1.0538	1.0572	1.0607	1.0641
	1		<u> </u>		<u></u>	<u> </u>				

PRESSURE OF AQUEOUS VAPOR OVER WATER. ENGLISH MEASURES.

				_	OF IVIEA					
Tempera- ture.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
80°	1.0334	1.0367	1.0401	1.0435	1.0470	1.0504	1.0538	1.0572	1.0607	1.0641
81	1.0676	1.0711	1.0746	1.0781	1.0816	1.0851	1.0887	1.0022	1.0958	1.0993
82	1.1020	1.1065	1.1101	1.1137	1.1173	1.1200	1.1246	1.1282	1.1319	1.1355
83	1.1392	1.1420	1.1466	1.1503	1.1540	1.1577	1.1615	1.1652	1.1600	1.1727
84	1.1765	1.1803	1.1841	1.1879	1.1917	1.1955	1.1994	1.2032	1.2071	1.2110
05		00					0.			
85 86	1.2149	1.2188	1.2227	1.2266	1.2305	1.2344	1.2384	1.2423	1.2463	1.2503
87	1.2543	1.2583	1.2623	1.2663	1.2704	1.2744	1.2785	1.2826	1.2867	1.2908
88	1.2949	1.2990	1.3031	1.3072	1.3114	1.3155	1.3197	1.3239		1.3323
89	1.3365	1.3407 1.3837	1.3450	1.3492 1.3925	1.3535	1.3578	1.3621	1.3664	1.3707	1.4190
11 39	1.3794	1.3037	1.3001	1.3923	1.3969	1.4013	1.4057	1.4101	1.4140	
90	1.4234	1.4279	1.4324	1.4369	1.4414	1.4459	1.4505	1.4550	1.4596	1.4642
91	1.4688	1.4734	1.4780	1.4826	1.4872	1.4918	1.4965	1.5012	1.5059	1.5106
92	1.5153	1.5200	1.5247	1.5294	1.5342	1.5390	1.5438	1.5486	1.5534	1.5582
93	1.5630	1.5678	1.5727	1.5776	1.5825	1.5874	1.5923	1.5972	1.6022	1.6071
94	1.6121	1.6171	1.6221	1.6271	1.6321	1.6371	1.6422	1.6472	1.6523	1.6574
95	1.6625	1.6676	1.6728	1.6779	1.6831	1.6882	1.6034	1.6086	1.7038	1.7000
96	1.7143	1.7195	1.7248	1.7301	1.7354	1.7407	1.7460	1.7513	1.7567	1.7620
97	1.7674	1.7728	1.7782	1.7836	1.7891	1.7945	1.8000	1.8055	1.8110	1.8165
98	1.8220	1.8275	1.8331	1.8386	1.8442	1.8498	1.8554	1.8610	1.8667	1.8723
99	1.8780	1.8837	1.8804	1.8951	1.0008	1.9065	1.9123	1.0181	1.9239	1.9297
	210,00	5,					-195			
100	1.9355	1.9413	1.9472	1.9530	1.9589	1.9648	1.9707	1.9766	1.9826	1.9885
101	1.9945	2.0005	2.0065	2.0125	2.0185	2.0245	2.0306	2.0367	2.0428	2.0489
102	2.0550	2.0611	2.0673	2.0735	2.0797	2.0859	2.0921	2.0983	2.1046	2.1108
103	2.1171	2.1234	2.1298	2.1361	2.1425	2.1488	2.1552	2.1616	2.1680	2.1744
104	2.1809	2.1874	2.1939	2.2004	2.2069	2.2134	2.2200	2.2265	2.2331	2.2397
105	2.2463	2.2520	2.2596	2.2663	2.2730	2.2797	2.2864	2.2031	2.2000	2.3067
106	2.3135	2.3203	2.3271	2.3339	2.3408	2.3477	2.3546	2.3615	2.3684	2.3753
107	2.3823	2.3893	2.3963	2.4033	2.4103	2.4173	2.4244	2.4315	2.4386	2.4457
108	2.4529	2.4600	2.4672	2.4744	2.4816	2.4888	2.4961	2.5033	2.5106	2.5179
109	2.5252	2.5325	2.5399	2.5473	2.5547	2.5621	2.5695	2.5770	2.5845	2.5919
		. 6-6-				. 6				- 46-0
110	2.5994	2.6069	2.6145	2.6220	2.6296	2.6372	2.6448	2.6524	2.6601	2.6678
111	2.6755	2.6832	2.6909	2.6986	2.7064	2.7142	2.7220	2.7298	2.7377	2.7456
112	2.7535	2.7614	2.7693	2.7772	2.7852	2.7932	2.8012	2.8092	2.8173	2.8253
113	2.8334	2.8415	2.8496	2.8577	2.8659	2.8741	2.8823	2.8905	2.8988	2.9070
114	2.9153	2.9236	2.9320	2.9403	2.9487	2.9571	2.9655	2.9739	2.9823	2.9908
115	2.9993	3.0078	3.0163	3.0248	3.0334	3.0420	3.0506	3.0592	3.0679	3.0766
116	3.0853	3.0940	3.1027	3.1115	3.1203	3.1291	3.1379	3.1467	3.1556	3.1645
117	3.1734	3.1823	3.1913	3.2003	3.2093	3.2183	3.2273	3.2364	3.2455	3.2546
118	3.2637	3.2728	3.2820	3.2912	3.3004	3.3096	3.3189	3.3282	3.3375	3.3468
119	3.3562	3.3655	3.3749	3.3843	3.3938	3.4032	3.4127	3.4222	3.4318	3.4413
120	3.4509	3.4605	3.4701	3.4797	3.4894	3.4991	3.5088	3.5185	3.5283	3.5381
121	3.4309	3.4003	3.5676	3.5774	3.5873	3.5972	3.6072	3.5103	3.6272	3.6372
121	3.5479	3.6573	3.6674	3.6775	3.6876	3.6977	3.7079	3.7181	3.7284	3.7386
122	3.7489	3.7592	3.7695	3.7799	3.7903	3.8007	3.8111	3.8215	3.8320	3.8425
123	3.8530	3.8636	3.8742	3.8848	3.8954	3.9060	3.9167	3.9274	3.9381	3.9488
11										
125	3.9596	3.9704	3.9813	3.9921	4.0030	4.0139	4.0248	4.0357	4.0467	4.0577
126	4.0687	4.0797	4.0908	4.1019	4.1131	4.1242	4.1354	4.1466	4.1578	4.1690
127	4.1803	4.1916	4.2030	4.2143	4.2256	4.2370	4.2485	4.2599	4.2714	4.2829
128	4.2945	4.3061	4.3177	4.3293	4.3410	4.3527	4.3645	4.3762	4.3880	4.3998
129	4.4116	4.4235	4.4354	4-4473	4.4592	4.4711	4.4831	4.4951	4.5072	4.5192
130	4.5313	4.5434	4.5555	4.5677	4.5798	4.5921	4.6043	4.6166	4.6289	4.6412
	1			<u> </u>		<u> </u>		1	<u> </u>	
								_		

PRESSURE OF AQUEOUS VAPOR OVER WATER. ENGLISH MEASURES.

Temper- ature.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
F.	Inches,	Inches,	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
130°	4.531	4.543	4.556	4.568	4.580	4.592	4.604	4.617	4.629	4.641
131	4.654	4.666	4.678	4.601	4.703	4.716	4.728	4.741	4.754	4.766
132	4.779	4.792	4.804	4.817	4.830	4.843	4.855	4.868	4.881	4.894
133	4.907	4.920	4.933	4.946	4.959	4.972	4.985	4.998	5.012	5.025
134	5.038	5.051	5.065	5.078	5.091	5.105	5.118	5.132	5.145	5.158
135	5.172	5.186	5.199	5.213	5.226	5.240	5.254	5.268	5.281	5.295
136	5.300	5.323	5.337	5.351	5.365	5.379	5.392	5.407	5.421	5.435
137	5.449	5.463	5.477	5.492	5.506	5.520	5-535	5.549	5.563	5.578
138	5.592	5.607	5.621	5.636	5.650	5.665	5.680	5.694	5.700	5.724
139	5.739	5.754	5.768	5.783	5.798	5.813	5.828	5.843	5.858	5.873
140	5.889	5.904	5.919	5.934	5-949	5.965	5.980	5.995	6.011	6.026
141	6.041	6.057	6.072	6.088	6.104	6.119	6.135	6.151	6.166	6.182
142	6.198	6.214	6.229	6.245	6.261	6.277	6.293	6.309	6.325	6.341
143	6.358	6.374	6.390	6.406	6.422	6.439	6.455	6.472	6.488	6.504
144	6.521	6.537	6.554	6.571	6.587	6.604	6.621	6.637	6.654	6.671
145	6.688	6.705	6.722	6.739	6.756	6.773	6.790	6.807	6.824	6.841
146	6.858	6.876	6.893	6.910	6.928	6.945	6.962	6.980	6.997	7.015
147	7.032 7.210	7.050	7.068	7.085	7.103 7.282	7.121	7.139	7.156	7.174	7.192
140	7.392	7.228	7.246 7.429	7.264 7.447	7.466	7.300 7.484	7.319 7.503	7.337 7.521	7.355 7.540	7·374 7·559
	7.392	7.410	7.429	7.447			7.303	7.321	7.340	-
150	7.577	7.596	7.615	7.634	7.653	7.672	7.69 1 7.882	7.710	7.729	7.748
151 152	7.767 7.960	7.786 7.980	7.805 8.000	7.824 8.010	7.844 8.030	7.863 8.059	7.882 8.078	7.902 8.008	7.921 8.118	7.941 8.138
153	8.158	8.178	8.198	8.218	8.238	8.258	8.278	8.208	8.319	8.339
154	8.360	8.380	8.400	8.421	8.441	8.462	8.482	8.503	8.524	8.545
	_			0.6-0		0.6	06			}
155 156	8.565 8.776	8.586 8.707	8.607 8.818	8.628 8.839	8.649 8.861	8.670 8.882	8.691 8.904	8.712 8.925	8.733 8.947	8.754 8.968
157	8.990	0.797	9.034	9.055	9.077	9.099	0.121	9.143	9.165	9.187
158	9.209	9.231	9.253	9.276	9.298	9.320	9.342	9.365	9.387	9.410
159	9.432	9.455	9.478	9.500	9.523	9.546	9.569	9.592	9.615	9.638
160	0.661	9.684	9.707	9.730	9.753	9.776	9.799	9.823	9.846	9.870
161	9.893	9.916	9.940	9.964	9.987	10.011	10.035	10.050	10.082	10.106
162	10.130	10.154	10.178	10.203	10.227	10.251	10.275	10.299	10.324	10.348
163	10.373	10.397	10.422	10.446	10.471	10.495	10.520	10.545	10.570	10.595
164	10.620	10.645	10.670	10.695	10.720	10.745	10.770	10.795	10.821	10.846
165	10.872	10.897	10.922	10.948	10.974	10.999	11.025	11.051	11.077	11.102
166	11.128	11.154	11.180	11.206	11.232	11.258	11.284	11.311	11.337	11.363
167	11.390	11.417	11.444	11.470	11.497	11.523	11.550	11.577	11.604	11.631
168	11.658	11.685	11.712	11.739	11.766	11.793	11.821	11.848	11.875	11.903
169	11.930	11.957	11.985	12.013	12.040	12.068	12.096	12.124	12.152	12.180
170	12.208	12.236	12.264	12.292	12.320	12.349	12.377	12.406	12.434	12.463
171	12.491	12.520	12.548	12.577	12.606	12.635	12.664	12.693	12.722	12.751
172	12.780	12.809	12.838	12.868	12.897	12.927 13.224	12.956	12.986	13.015	13.045
173 174	13.374	13.405	13.435	13.465	13.496	13.527	13.557	13.588	13.314	13.344
	13.680	13.711	13.742	13.773	13.804	13.835	13.867	13.898	13.929	1
1 75	13.000	14.024	14.055	14.087	14.118	14.150	14.182	13.090	13.929	13.961
177	14.310	14.342	14.374	14.406	14.438	14.471	14.503	14.536	14.568	14.601
178	14.633	14.666	14.699	14.731	14.764	14.797	14.830	14.864	14.897	14.930
179	14.963	14.996	15.030	15.063	15.097	15.130	15.164	15.197	15.231	15.265
180	15.299	15.333	15.367	15.401	15.435	15.469	15.504	15.538	15.572	15.607
		1 000			3 103		00-7	_ 303		

TABLE 70.

PRESSURE OF AQUEOUS VAPOR OVER WATER. ENGLISH MEASURES.

Tempera- ture.	.0	.1	.2	٠3	.4	.5	.6	.7	.8	.9
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
180°	15.299	15.333	15.367	15.401	15.435	15.460	15.504	15.538	15.572	15.607
181	15.641	15.676	15.710	15.745	15.780	15.815	15.850	15.885	15.020	15.955
182	15.000	16.025	16.060	16.006	16.131	16.167	16.202	16.238	16,274	16.300
183	16.345	16.381	16.417	16.453	16.480	16.525	16.561	16.598	16.634	16.670
184	16.707	16.743	16.78 o	16.817	16.853	16.890	16.927	16.964	17.001	17.038
185	17.075	17.112	17.150	17.187	17.224	17.262	17.300	17.337	17.375	17.413
186	17.450	17.488	17.526	17.564	17.602	17.641	17.679	17.717	17.756	17.794
187	17.832	17.871	17.910	17.948	17.987	18.026	18.065	18.104	18.143	18.182
188	18.221	18.261	18.300	18.340	18.379	18.419	18.458	18.498	18.538	18.578
189	18.618	18.658	18.698	18.738	18.778	18.818	18.859	18.899	18.940	18.980
190	19.021	19.062	19.102	19.143	19.184	19.225	19.266	19.308	19.349	19.390
191	19.431	19.473	19.514	19.556	19.598	19.639	19.681	19.723	19.765	19.807
192	19.849	19.892	19.934	19.976	20.010	20.061	20.104	20.146	20.189	20.232
193	20.275	20.318	20.361	20.404	20.447	20.490	20.533	20.577	20.620	20.664
194	20.707	20.751	20.795	20.839	20.883	20.927	20.971	21.015	21.059	21.103
195	21.148	21.102	21.237	21.282	21.326	21.371	21.416	21.461	21.506	21.551
196	21.507	21.642	21.687	21.733	21.778	21.824	21.870	21.015	21.061	22.007
197	22.053	22.000	22.145	22.192	22.238	22.284	22.331	22.377	22.424	22.471
198	22.517	22.564	22.611	22.658	22.706	22.753	22.800	22.847	22.805	22.942
199	22.990	23.038	23.085	23.133	23.181	23.229	23.277	23.325	23.374	23.422
200	23.470	23.510	23.568	23.616	23.665	23.714	23.763	23.812	23.861	23.910
201	23.959	24.000	24.058	24.108	24.157	24.207	24.257	24.307	24-357	24.407
202	24.457	24.507	24.557	24.608	24.658	24.700	24.759	24.810	24.861	24.012
203	24.063	25.014	25.065	25.116	25.168	25.210	25.271	25.322	25.374	25.426
204	25.478	25.530	25.582	25.634	25.686	25.738	25.791	25.843	25.896	25.948
205	26.001	26.054	26.107	26.160	26.213	26.266	26.319	26.373	26.426	26.480
206	26.534	26.587	26.641	26.695	26.749	26.803	26.857	26.912	26.066	27.021
207	27.075	27.130	27.184	27.239	27.294	27.349	27.404	27.460	27.515	27.570
208	27.626	27.681	27.737	27.793	27.848	27.004	27.060	28.016	28.073	28.120
209	28.185	28.242	28.298	28.355	28.412	28.469	28.526	28.583	28.640	28.697
210	28.754	28.812	28.869	28.927	28.985	20.042	20.100	29.158	20.216	29.275
211	29.333	20.391	29.450	29.508	29.567	29.626	20.685	29.744	29.803	29.862
212	20.021	20.081	30.040	30.100	30.150	30.210	30.279	30.339	30.399	30.459
213	30.519	30.580	30.640	30.701	30.761	30.822	30.883	30.944	31.005	31.066
214	31.127	31.189	31.250	31.311	31.373	31.435	31.497	31.559	31.621	31.683

PRESSURE OF AQUEOUS VAPOR OVER ICE. METRIC MEASURES.

Tempera- ture.	Vapor Pressure.	Tempera- ture.	Vapor Pressure.	Tempera ture.	- Vapor Pressu	re. Te	mpera- ture.	- V Pre	apor ssure,	Tempera- ture.	Vapor Pressure.
C.	mm,	C.	mm.	C.	mm	. –	C.		mm,	C.	mm.
-70°	0.0018	-60°	0.0078	-50.0°	0.020	or _	45 . 0°	° o.	0537	-40.0°	0.0964
69	0.0021	59	0.0089	49.5	0.030		44.5		0570	39.5	0. 1020
68	0.0025	58	0.0102	49.0	0.03	29	44.0		0605	39.0	0. 1080
67	0.0028	57	0.0117	48.5	0.03	50	43.5	0.	0642	38.5	0.1143
66	0.0033	56	0.0134	48.0	U, 03	73	43.0	0.	o68o	38. o	0.1209
-65	0.0038	-55	0.0153	-47.5	0.039		42.5		0721	-37.5	0. 1279
64	0.0044	54	0.0174	47.0	0.04		42.0		0765	37.0	0.1352
63	0.0051	53	0.0198	46.5	0.044		41.5		0811	36.5	0.1430
62	0.0059	52	0.0226	46.0	0.04		41.0		0 859	36.0	0.1511
61	0.0068	51	0.0256	45.5	0.050	00	40.5	0.	0910	35⋅5	0.1596
Tempera- ture.	.0	.1	.2	.3	.4	.5		.6	.7	.8	.9
	mm.	mm.	mm.	mm.	mm.	mm.		mm.	mm.	mm.	mm.
-35°	0.1686	0.1668	0.1650	0.1632	0.1614	0.150	6 0.	1579	0.156		0.1528
34	0.1880	0.1860	0.1840	0.1820	0.1800	0.178		1761	0.174	0.0	
33	0.2094	0.2072	0.2050	0.2028	0.2006	0.198		1963	0.194		
32	0.2331	0.2306	0.2281	0.2257	0.2233	0.220	9 o.	2186	0.216		1 1
31	0.2591	0.2564	0.2537	0.2510	0.2484	0.245	8 0.	243 2	0,240	6 0.2381	0.2355
-30	0.2878	0.2848	0.2818	0.2789	0.2760	0.273	1 0.	2703	0.267	4 0.2646	0.2619
29	0.3194	0.3161	0.3128	0.3096	0.3064	0.303	2 0.	3001	0.297		
28	0.3541	0.3505	0.3469	0.3433	0.3398	0.336		3329	0.329		
27	0.3923	0.3883	0.3843	0.3804	0.3766	0.372		.3689	0.365		
26	0.4341	0.4297	0.4254	0.4211	0.4169	0.412	27 0.	4085	0.404	4 0.4003	0.3963
-25	0.4800	0.4752	0.4705	0.4 658	0.4611	0.456		4519	0.447		
24	0.5303	0.5251	0.5199	0.5147	0.5096	0.504		4996	0.494		1 1 1 2 1
23	0.5854	0.5796	0.5739	0.5683	0.5628	0.557		5517	0.546		
22 21	0.6456	0.6393	0.6331	0.6270	0.6209	0.614	_	.6088	0,602		
	0.7115	0.7046	0.6978	0.6911		0.677		6713	0,664		"
-20	0.7834	0.7759	0.7685	0.7611	0.7538	0.746	6 0,	7395	0.732		
19	0.8618	0.8537	0.8456	0.8376	0.8296	0.821	7 0.	8139	0.806		
18	0.9474	0.9385	0.9297	0.9209	0.9123	0.903		8952	0.886		1
17	1.0406	1.0309	1.0213	1.0118	1.0024	0.993		9837	0.974		1 /0 0 1
16	1.1421	1.1316	1.1211	1.11 0 8	1.1005	1.090	1.	.0802	1.070	1.0602	1.0504
-15	1.2525	1.2411	1.2297	1.2184	1.2072	1.196		1852	1.174		1 9 1
14	1.3726	1.3601	1.3477	1.3355	1.3233	1.311		2993	1.287		1.2641
13	1.5029	1.4894	1.4759	1.4626	1.4495	1.436		4234	1.410		
12	1.6444	1.6297	1.6151	1.6007	1.5864	1.572		5581	1.544		
11	1.7979	1.7820	1.7662	1.7506	1.7350	1.719	10 1.	7043	1.689	2 1.6741	1.6592
-10	1.9643	1.9470	1.9299	1.9129	1.8961	1.879		8628	1,846		
9	2.1445	2.1258	2.1073	2.0889	2.0707	2.052		0347	2,016	1 222	1.9817
l š	2.3395	2.3193	2.2993	2.2794	2.2596	2.240		2206	2.201		
7	2.5505	2.5287	2.5070	2.4855	2.4642	2.443		4220	2.401		00//
6	2.7785	2.7549	2.7315	2.7083	2.6852	2,662	2.	6396	2.617	2.5947	2.5725
- 5	3.0248	2.9993	2.9740	2.9489	2.9240	2.899		8747	2,850		
4	3.2907	3.2632	3.2359	3.2088	3.1819	3.155		1287	3,102		
3	3.5775	3.5479	3.5184	3.4892	3.4602	3.431	. -	4028	3.374		
2	3.8868	3.8548	3.8230	3.7916	3.7603	3.729		.6985	3.667		1
1	4.2199	4.1854	4.1513	4.1174	4.0837	4.050	2 4.	.0171	3.984 	3.9515	3.9190
- 0	4.5802	4.5428	4.5057	4.4690	4.4325	4.396	2 4.	3604	4.324	8 4.2896	4.2546

PRESSURE OF AQUEOUS VAPOR OVER WATER. METRIC MEASURES.

	METRIC MEASURES.											
Tem- pera- ture.	.0	.1	.2	3	.4	.5	.6	.7	.8	.9		
C.	mm.	mm.	mm.	mm.	mm,	mm.	mm.	mm.	mm.	mm.		
l o°	4.580	4.614	4.647	4.681	4.715	4.750	4.784	4.819	4.854	4.889		
I	4.924	4.060	4.996	5.032	5.068	5.105	5.142	5.179	5.216	5.254		
2	5.201	5.329	5.368	5.406	5.445	5.484	5.523	5.562	5.602	5.642		
3	5.682	5.723	5.763	5.804	5.846	5.887	5.929	5.971	6.013	6.056		
II 4	6.008	6.141	6.185	6.228	6.272	6.316	6.361	6.406	6.450	6.496		
11	,.		0.103	0.220	0.2/2	0.310	0.301	0.400	0.430	0.490		
5	6.541	6.587	6.633	6.680	6.726	6.773	6.820	6.868	6.916	6.964		
6	7.012	7.061	7.110	7.150	7.200	7.259	7.309	7.360	7.410	7.462		
7	7.513	7.565	7.617	7.660	7.722	7.775	7.828	7.882	7.936	7.991		
7 8	8.045	8.100	8.156	8.211	8.267	8.324	8.380	8.437	8.494	8.552		
9	8.610	8.669	8.727	8.786	8.846	8.906	8.966	0.026	0.087	9.148		
						1						
10	9.210	9.272	9.334	9.397	9.460	9.523	9.587	9.651	9.716	9.781		
11	9.846	9.912	9.978	10.044	10.111	10.178	10.246	10.314	10.382	10.451		
12	10.521	10.590	10.660	10.731	10.801	10.873	10.944	11.016	11.089	11.162		
13	11.235	11.309	11.383	11.458	11.533	11.608	11.684	11.761	11.837	11.915		
14	11.992	12.070	12.149	12.228	12.307	12.387	12.468	12.549	12.630	12.712		
II												
15	12.794	12.877	12.960	13.043	13.127	13.212	13.297	13.383	13.469	13.555		
16	13.642	13.729	13.817	13.906	13.995	14.084	14.174	14.265	14.356	14.447		
17	14.539	14.632	14.725	14.818	14.912	15.007	15.102	15.197	15.293	15.390		
18	15.487	15.585	15.683	15.782	15.882	15.981	16.082	16.183	16.285	16.387		
19	16.489	16.593	16.696	16.801	16.906	17.011	17.117	17.224	17.331	17.439		
20	T7 5 48	17.657	66	0	0-	_0	_0	_0	-0			
20	17.548 18.665	18.780	17.766	17.877	17.987	18.099	18.211	18.323	18.437	18.551		
21	10.844		18.896	19.012	19.129	19.247	19.365	19.484	19.603	τ9.723		
22	21.087	19.965	20.087	20.210	20.333	20.457	20.582	20.707	20.833	20.960		
23	22.398		21.344 22.660	21.473 22.805	21.604	21.734	21.866	21.998	22.131	22.264		
24	22.390	22.533	22.009	22.005	22.942	23.080	23.219	23.358	23.498	23.638		
25	23.780	23.022	·24.065	24.200	24.353	24.498	24.644	24.791	24.938	25.086		
26	25.235	25.385	25.535	25.687	25.839	25.991	26.145	26.299	26.455	26.610		
27	26.767	26.925	27.083	27.242	27.402	27.563	27.725	27.887	28.051	28.215		
28	28.380	28.546	28.712	28.880	29.048	29.217	29.387	29.558	29.730	20.213		
20	30.076	30.251	30.426	30.602	30.779	30.957	31.136	31.315	31.496	31.678		
	l	0 3	0	J	5119	0-1937	5-1-5-	3-3-3	32,490	32.070		
30	31.860	32.043	32.228	32.413	32.599	32.786	32.974	33.163	33.353	33-543		
31	33.735	33.928	34.121	34.316	34.512	34.708	34.906	35.104	35.303	35.504		
32	35.705	35.908	36.111	36.315	36.521	36.727	36.935	37.143	37-353	37.563		
33	37.775	37.987	38.201	38.415	38.631	38.848	39.065	39.284	39.504	39.725		
34	39.947	40.170	40.394	40.619	40.846	41.073	41.302	41.531	41.762	41.994		
				-								
35	42.227	42.461	42.696	42.932	43.170	43.408	43.648	43.889	44.131	44-374		
36	44.619	44.864	45.111	45.358	45.608	45.858	46.109	46.362	46.615	46.870		
37	47.127	47.384	47.643	47.902	48.163	48.426	48.689	48.954	49.220	49.487		
38	49.756	50.025	50.296	50.569	50.842	51.117	51.393	51.670	51.949	52.229		
39	52.510	52.793	53.077	53.362	53.649	53.937	54.226	54.516	54.808	55.101		
				46 -00	#6 c00	-6.00						
40	55.396	55.692	55.989	56.288	56.588	56.889	57.192	57.496	57.802	58.109		
41	58.417	58.727	59.038	59.351	59.665	59.981	60.298	60.616	60.936	61.257		
42	61.580 64.889	61.904	62.230	62.557	62.886 66.255	63.216	63.547	63.880	64.215	64.551		
43		65.228	65.569	65.911		66.600	66.947	07.295	07.045	67.997		
44	68.350	68.704	69.061	69.419	69.778	70.139	70.502	70.866	71.232	71.599		
45	71.968	72.339	72.712	73. 0 86	73.461	73.839	74.218	74.598	74.00-	75 26 -		
	75.751	76.138	76.527	76.918			78.101	78.499	74.981 78.898	75.365		
46	79.703	80.107	80.514	80.922	77.311 81.332	77.705 81.744	82.158	82.573	82.990	79.300		
47 48	83.830	84.253	84.677	85.104	85.532	85.062	86.394	86.828	87.263	83.409		
	88.140	88.581	89.024	89.470	89.916	90.365	90.816	91.269		87.701		
49	55.145	30.301	39.024	29.4/0	29.910	90.303	90.010	91,209	91.723	92.180		
50	92.639	93.099	93.562	94.026	94.492	94.961	95.431	95.903	96.378	96.854		
	I ' -09	70 -99	70.0-2	74.220	27.42-	27.30-	7J-TU-	20.20	<i>3310</i>	90.034		
			:									

PRESSURE OF AQUEOUS VAPOR OVER WATER. METRIC MEASURES.

Tarre										
Tem- pera- ture,	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
50°	92.64	93.10	93.56	94.03	94.49	94.96	95.43	95.90	96.38	96.85
51	97.33	97.81	98.30	98.78	99.27	99.76	100.25	100.74	101.23	101.73
52	102.23	102.73	103.23	103.74	104.25	104.75	105.27	105.78	106.30	106.81
53	107.33	107.86	108.38	108.91	109.44	109.97	110.50	111.04	111.57	112.11
54	112.66	113.20	113.75	114.30	114.85	115.40	115.96	116.51	117.07	117.64
55	118.20	118.77	119.34	119.91	120.49	121.06	121.64	122.22	122.81	123.39
56	123.98	124.57	125.16	125.76	126.36	126.96	127.56	128.17	128.77	129.38
57	130.00	130.61	131.23	131.85	132.47	133.10	133.73	134.36	134.99	135.62
58	136.26	136.90	137.54	138.19	138.84	139.49	140.14	140.80	141.46	142.12
59	142.78	143.45	144.12	144.79	145.46	146.14	146.82	147.50	148.19	148.88
60	149.57	150.26	150.95	151.65	152.35	153.06	153.77	154.48	155.19	155.90
бі	156.62	157.34	158.07	158.79	159.52	160.26	160.99	161.73	162.47	163.21
62	163.96	164.71	165.46	166.22	166.98	167.74	168.50	169.27	170.04	170.81
63	171.59	172.37	173.15	173.93	174.72	175.51	176.31	177.10	177.91	178.71
64	179.52	180.32	181.14	181.95	182.77	183.59	184.42	185.25	186.08	186.91
65	187.75	188.59	189.44	190.28	191.13	191.99	192.85	193.71	194.57	195.44
66	196.31	197.18	198.06	198.94	199.82	200.71	201.60	202.49	203.39	204.29
67	205.19	206.10	207.01	207.92	208.84	209.76	210.68	211.61	212.54	213.47
68	214.41	215.35	216.30	217.24	218.20	219.15	220.11	221.07	222.04	223.01
69	223.98	224.96	225.94	226.92	227.91	228.90	229.89	230.89	231.89	232.90
70	233.91	234.92	235.94	236.96	237.98	239.01	240.04	241.08	242.12	243.16
71	244.21	245.26	246.31	247.37	248.43	249.50	250.57	251.64	252.72	253.80
72	254.88	255.97	257.07	258.16	259.27	260.37	261.48	262.59	263.71	264.83
73	265.96	267.08	268.22	269.35	270.50	271.64 283.32	272.79 284.51	273.94 285.71	275.10 286.90	276.26 288.11
74	277.43	278.60	279.77			•			_	
75	289.32	290.53	201.74	292.97	294.19	295.42	296.65	297.89	299.13 311.80	300.38
76	301.63	302.89 315.68	304.15 316.99	305.41	306.68 319.61	307.95 320.93	309.23	310.51	324.91	313.09 326.25
77	314.38 327.59	328.93	330.28	331.64	333.00	334.36	335.73	337.10	338 48	339.86
79	341.25	342.65	344.04	345.44	346.85	348.26	349.68	351.10	352.53	353.96
80	355.40	356.84	358.28	359.73	361.19	362.65	364.11	365.58	367.06	368.54
81	370.03	371.52	373.01	374.51	376.02	377.53	379.05	380.57	382.09	383.62
82	385.16	386.70	388.25	389.80	391.36	392.92	394-49	396.06	397.64	399.22
83	400.81	402.40	404.00	405.61	407.22	408.83	410.45	412.08	413.71	415.35
84	416.99	418.64	420.29	421.95	423.61	425.28	426.95	428.64	430.32	432.01
85	433.71	435.41	437.12	438.83	440.55	442.28	444.01	445.75	447.49	449.24
86	450.99	452.75	454.51	456.28	458.06	459.84	461.63	463.42	465.22	467.03
87	468.84	470.66	472.48	474·3I	476.14	477.99	479.83	481.68	483.54	485.41
88	487.28	489.16	491.04	492.93	494.82	496.72	498.63	500.54	502.46	504.39
89	506.32	508.26	510.20	512.15	514.11	516.07	518.04	520.01	521.99	523.98
90	525.97	527.97	529.98	531.99	534.01	536.04	538.07	540.11	542.15	544.21
91	546.26	548.33	550.40	552.48	554.56	556.65	558.75	560.85	562.96	565.08
92	567.20	569.33	571.47	573.61	575.76	577.92	580.08	582.25	584.43	586.61
93	588.80	591.00	593.20	595.41	597.63	599.86	602.09	604.33	600.57	608.82
94	611.08	613.35	615.62	617.90	620.19	622.48	024.79	627.09	029.41	631.73
95	634.06	636.40	638.74	641.09	643.45	645.82	648.19	650.57	652.96	655.35
96	657.75	660.16	662.58	665.00	667.43	669.87	672.32	674.77	677.23	679.70
97	682.18	684.66	687.15	689.65	692.15	694.67	697.19	699.71	702.25	704.79
98	707.35	709.90	712.47	715.04	717.63	720.22	722.81	725.42	728.03	730.65
99	733.28	735.92	738.56	741.21	743.87	746.54	749.22	751.90	754-59	757.29
100	760.00	762.72	765.44	768.17	770.91	773.66	776.42	779.18	781.95	784.73
<u> </u>			<u>'</u>							

TABLE 72.

PRESSURE OF AQUEOUS VAPOR OVER WATER. METRIC MEASURES.

Temperature.	O°	1°	2°	3°	4 °	5°	6°	7°	8°	9°
C.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
100°	760.0	787.5	815.9	845.0	875.1	906.0	937.8	970.5	1004. 2	1038.8
110	1074.4	1111.0	1148.6	1187.2	1226.9	1267.7	1309.6	1352.6	1396.8	1442.1
120	1488.7	1536.4	1585.4	1635.7	1687.3	1740. 2	1794.4	1850.0	1907.0	1965.4
130	2025.2	2086.5	2149.3	2213.7	2270.6	2347.0	2416. I	2486.8	2559.2	2633.2
140	2709.0	2786.5	2865.8	2947.0	3029.9	3114.7	3201.4	3290. I	3380.7	3473 - 3
150°	3567.9	3664.6	3763.3	3864.2	3967.2	4072.4	4179.8	4289.5	4401.5	4515.7
160	4632.4	4751.4	4872.8	4996.7	5123.1	5252.0	5383.4	5517.5	5654.2	5793 - 5
170	5935.6	6080.4	6228.0		6531.7	6687.8	6846.9	7009.0	7174.0	7342.1
180	7513.3	7687.7	7865.2	8045.9	8229.8	8417.0	8607.6	8801.5	8998.9	9199.6
190°	9404	9612	9823	10038	10257	10479	10705	10935	11169	11407
200	11648	11894	12143	. 12397	12654	12916	13182	13452	13727	14006
210	14289	14577	14869	15165	15467	15772	16083	16398	16718	17043
220	17372	17707	18046	18391	18740	19095	19454	19819	20190	20565
230°	20946	21332	21724	22121	22524	22932	23347	23766	24192	24623
240	25061	25504	25953	26408	26870	27337	27811	28291	28778	29270
250	29770	30275	30787	31306	31832	32364	3 2 9 0 3	33449	34002	34562
260	35128	35702	36283	36872	37467	38070	38680	39298	39923	40556
270	41197	41845	42501	43165	43836	44516	45204	45899	46603	47316
280°	48036	48765	49503	50248	51003	51766	52538	53318	54108	54906
200	55714	56530	57356	58191	59035	59888	60751	61624	62506	63398
300	64299	65211	66132	67063	68005	68956	69918	70890	71872	72865
310	73869	74883	75907	76943	77990	79047	80116	81195	82286	83389
320	84503	85628	86765	87913	89074	90246	91430	92626	93835	95056
330°	ç628g	97534	98793	100060	101350			105280	106610	107960
340	109320	110700	112090	113490		116340		119240	120720	122210
350	123710	125220	126760	128310	129870			134640	136270	137900
360	139560	141230		144620		148070	149820	151590	153380	155180
370	157000	158840	160690	162560	164450					

WEIGHT OF A CUBIC FOOT OF SATURATED VAPOR. ENGLISH MEASURES.

Temper- aturs.		Tsmper- ature.	.0	.5	Tempera- ature.	.0	.2	.4	.6	.8
F.	Grains Troy.	F.	Grains Troy.	Grains Troy.	F.	Grains Troy,	Grains Troy.	Grains Troy.	Grains Troy.	Grains Troy,
-30°	0.095	+20°	1.244	1.273	+70°	8.066	8.117	8.170	8.223	8.276
20	0.100	21	1.301	1.332	71	8.329	8.383	8.437	8.491	8.546
28	0.106	22	1.362	1.393	72	8.600	8.656	8.711	8.766	8.823
27	0.112	23	1.425	1.457	73	8.879	8.936	8.992	9.050	9.107
26	0.119	24	1.490	1.524	74	9.165	9.223	9.281	9.341	9.400
25	0.126	+25	1.558	1.593	+75	9.460	9.519	9.579	9.640	9.700
24	0.134	26	1.629	1.666	76	9.761 10.072	9.823	9.885	9.947 10.263	10.009
23	0.141	27 28	1.703	1.741 1.810	7 7 78		10.135	10.199	10.587	10.653
22 2I	0.150 0.158	20	1.779 1.859	1.900	78 79	10.392 10.720	10.457	10.853	10.921	10.987
-20	0.167	+30	1.942	1.984	+80	11.056	11.124	11.193	.11.262	11.331
19	0.176	31	2.028	2.072	81	11.401	11.471	11.542	11. 613	11.685
18	0.187	32	2.118	2.159	82	11.756	11.828	11.900	11.974	12.047
17	0.197	33	2.200	2.242	83	12.121	12.195	12.269	12.344	12.419
16	0.208	34	2.286	2.330	84	12.494	12,570	12.646	12.723	12.800
-15	0.220	+35	2.375	2.420	+85	12.878	12.956	13.034	13.113	13.192
14	0.232	36	2.466	2.513	86	13.272	13.351	13.432	13.512	13.594
13	0.244	37	2.560	2.609	87	13.676	13.758	13.840	13.923	14.006
12	0.258	38	2.658	2.708	88	14.090	14.174	14.258	14.344	14.429
11	0.272	39	2.759	2.810	89	14.515	14.601	14.689	14.776	14.864
-10	0.286	+40	2.863	2.916	+90	14.951	15.040	15.129	15.219	15.309
9	0.302	41	2.970	3.026	gı	15.400	15.490	15.581	15.673	15.766
9 8	0.318	42	3.082	3.138	92	15.858	15.951	16.045	16.139	16.234
7	0.335	43	3.196	3.254	93	16.328	16.423	16.520	16.616	16.713
6	0.353	44	3.315	3.374	94	16.810	16.909	17.007	17.106	17.205
5	0.371	⊹4 5	3.436	3.499	+95	17.305	17.406	17.506	17.607	17.709
4	0.391	46	3.563	3.627	96	17.812	17.914	18.018	18.121	18.226
3	0.411	47	3.693	3.759	97	18.330	18.436	18.542	18.648	18.755
2	0.433	48	3.828	3.895	ģ8	18.863	18.971	19.079	19.188	19.298
- 1	0.455	49	3.965	4.036	99	19.407	19.518	19.629	19.741	19.853
± 0	0.479	+50	4.108	4.181	+100	19.966	20.079	20.193	20.307	20.422
+ I	0.503	51	4.255	4.331	101	20.538	20,654	20.770	20.887	21.005
2	0.529	52	4.407	4.485	102	21.123	21.242	21.362	21.481	21.602
3	0.556	53	4.564	4.644	103	21.723	21.845	21.967	22.090	22.213
4	0.584	54	4.725	4.807	104	22.337	22.462	22.588	22.714	22.839
5	0.613	+55	4.891	4.976	+105	22.966	23.095	23.223	23.351	23.481
6	0.644	56	5.062	5.149	10б	23.611	23.742	23.873	24.005	24.138
7 8	0.676	57	5.238	5.328	107	24.271	24.405	24.539	24.673	24.809
	0.709	58	5.420	5.513	108	24.946	25.082	25.220	25.358	25-597
9	0.744	59	5.607	5.703	109	25.636	25.776	25.917	26.058	26.201
10	0.780	+60	5.800	5.899	+110	26.343	25.486	26.630	26.775	26.920
11	0.818	61	5.999	6.099	III	27.066	27.213	27.360	27.508	27.657
12	0.858	62	6.203	6.306	112	27.807	27.956	28.107	28.259	28.411
13	0.900	63	6.413	6.521	113	28.563	28.717	28.871	29.026	29.181
14	0.943	64	6.630	6.740	114	29.338	29.495	29.653	29.812	29.970
15	0.988	+65	6.852	6.966	+ 115	30.130	30.291	30.452	30.614	30.777
16	1.035	66	7.082	7.198	116	30.940	31.104	31.270	31.435	31.601
17	1.084	67	7.317	7.437	117	31.768	31.937	32.106	32.274	32.445
18	1.135	68	7.560	7.683	118	32.616	32.787	32.960	33.133	33.307
+19	1.189	+69	7.809	7.937	+119	33.482	33.657	33.834	34.010	34.189

TABLE 74.

WEIGHT OF A CUBIC METER OF SATURATED VAPOR.

METRIC MEASURES,

					O WEA					
Temper- ature.		Temper- ature.	.0	.5	Temper- ature.	.0	.2	.4	.6	.8
G.	Grams.	G.	Grams.	Grams.	G.	Grams.	Grams.	Grams,	Grams.	Grams.
-29°	0.378	-17°	1.174	1.123	-5°	3.261	3.208	3.157	3.106	3.056
28	0.418	16	1.284	1.228	4	3.534	3.478	3.422	3.368	3.314
27	0.461	15	1.403	1.342	3	3.828	3.767	3.708	3.649	3.591
26	0.508	14	1.531	1.466	2	4.144	4.078	4.015	3.951	3.889
25	0.559	13	1.671	1.599	1	4.482	4.412	4.344	4.276	4.209
24	0.615	12	1.820	1.744	٥	4.847	4.771	4.697	4.624	4.553
-23	0.677	- 11	1.983	1.900	+0	4.847	4.914	4.982	5.051	5.121
22 21	0.743	10	2.158	2.069	1 2	5.192	5.264 5.634	5.336	5.409 5.789	5.483 5.868
20	0.894	9 8	2.347 2.551	2.25I 2.447	3	5.559	6.028	6.110	6.192	6.275
10	0.980	7	2.770	2.658	4	6.360	6.445	6.532	6.619	6.708
18	1.073	6	3.006	2.886	5	6.797	6.888	6.979	7.072	7.166
Temper- ature.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	Grams.	Grams.	Grams.	Grams.	Grams.	Grams.	Grams.	Grams.	Grams.	Grams.
+ 6°	7.261	7.309	7.357	7.405	7-453	7.502	7-552	7.601	7.651	7.701
7	7.751	7.802	7.853	7.904	7.956	8.007	8.059	8.112	8.164	8.217
8	8.271	8.324	8.378	8.432	8.487	8.542	8.597	8.652	8.708	8.764
9	8.821	8.877	8.934	8.991	9.049	9.106	9.165	9.223	9.282	9.341
+10	9.401	9.461	9.521	9.582	9.643	9.704	9.765	9.827	9.889	9.952
11	10.015	10.078	10.142	10.205	10.270	10.334	10.400	10.465	10.530	10.597
12	10.664	10.730	10.797	10.865	10.932	11.001	11.069	11.138	11.208	11.278
13	11.348	11.418	11.489	11.561	11.632	11.704	11.777	11.850	11.922	11.997
14	12.070	12.144	12.219	12.295	12.370	12.446	12.523	12.000	12.677	12.754
+15	12.832	12.911	12.990	13.068	13.148	13.229	13.309	13.390	13.472	13-553
16	13.635	13.718	13.801	13.885	13.969	14.053	14.139	14.224	14.309	14.395
17	14.482	14.569	14.657	14.744	14.833	14.922	15.011	15.101	15.191	15.282
18	15.373	15.465	15.557 16.505	15.650 16.603	15.743 16.701	15.836 16.799	15.931 16.898	16.998	16.121	16.216 17.198
19	16.311	10.409	10.303				10.090			
+20	17.300	17.401	17.503	17.606	17.708	17.812	17.917	18.021	18.126	18.232
21	18.338	18.445	18.553	18.660	18.768	18.878	18.987	19.097	19.207	19.319
22	19.430	19.542	19.655	19.769	19.882	19.996	20.112	20.227	20.343	20.461
23	20.578	20.695	20.814	20,933	21.053	21.173	21.295	21.416	21.538	21.660
24	21.783	21.907	22.032	22.157	22,202		22.536	22.003	22.791	22.920
+25	23.049	23.179	23.310	23.442	23.573	23.706	23.839	23.973	24.107	24.242
26	24.378	24.514	24.651	24.790	24.929	25.066	25.206	25.346	25.488	25.629
27	25.771	25.915	26.058	26.203	26.348	26.494	26.641	26.787	26.936	27.084
28	27.234	27.384 28.923	27.534 29.081	27.686 29.239	27.837 29.399	27.990 29.559	28.143 29.720	28.298 29.881	28.453 30.044	28.609 30.207
29	28.765	20.923	29.001	29.239	29.399	29.339	29.720	29.001	30.044	• •
+30	30.371	30.535	30.701	30.867	31.034	31.202	31.371	31.540	31.710	31.880
31	32.052	32.225	32.398	32.572	32.747	32.923	33.100	33.277	33.454	33.633
32	33.812	33.993	34.175	34.356	34.540	34.723 36.6 0 9	34.909 36.801	35.004	35.280	35.467
33	35.656	35.844 37.780	36.034	36.224 38.178	36.416 38.378	38.579	38.782	36.995 38.984	37.190 39.187	37.386
34	37.583	_ '	37.979			_		_		39-393
+35	39.599	39.805	40.013	40.221	40.430	40.640	40.851	41.064	41.277	41.491
36	41.706	41.921	42.139	42.356	42.575	42.795	43.015	43.237	43.459	43.683
37	43.908	44.134	44.360	44.587	44.815	45.046	45.277	45.507	45.740	45.973
38	46.208 48.6 0 9	46.443	46.680	46.918	47.156	47.396	47.636	47.878	48.121	48.365 50.861
39							-		_	
+40	51.117	51.373	51.631	51.890	52.150	52.410	52.673	52.936	53.200	53.466
L		·							<u> </u>	

HYGROMETRICAL TABLES.

Reduction of psychrometric observations — English measures.	
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Reduction of psychrometric observations — Metric Measures.	
Values of $e = e' - 0.000660 B (t - t') (1 + 0.00115 t')$.	TABLE 77
Relative humidity — Temperature Centigrade	TABLE 78
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Quantity of rainfall corresponding to given depths	TABLE 82

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 32}{1571}\right)$$

Pressure of Saturated Aqueous Vapor, e.

Tempera- ture.	0	1	2	3	4	5	6	7	8	9		
F.	Inches.	Inches.	Inches.	Inches.	Inches	Inches.	Inches.	Inches.	Inches.	Inches.		
-60°	.0010	20-0		6								
50 40	20 38	.0018 36	.0017	.0016	.0015	.0014 28	.0013 26	.0012	.0011	.0011		
30	71	66	33	31 59	29 55	52	49	24 46	23	2I 40		
20	.0127	.0120	.0113	.0107	.0101	.0095	.0090	.0084	.0080	.0075		
			l		J.,			,				
			e=e'			$(t')\left(\mathbf{I} + \mathbf{I}\right)$	$-\frac{t-32}{1571}$)				
	1				= 30.0 i	— t'						
t'	.0 .2 .4 .6 .8 1.0 1.2 1.4 1.6 1.8											
-20°	Inches.	Inches.	Inches.	Inches.	Inches.	Inches,	Inches.	Inches.	Inches.	Inches.		
10	.0127	.0106	.0085	.0063	.0042	.0021						
18	135 143	113 121	.0100	71	49		.0007		ĺ			
17	143	130	108	79 87	57 66	36 44	.0015	.0002		· i		
16	160	138	117	06	74	53	32	.0002				
		-3-	,	90	/-	33	32	.0010		1 3		
15	169	148	126	.0105	84	62	41	10		l i		
14	179	157	136	115	93	72	50	29	.0008			
13	189	168	146	125	.0103	82	61	39	.0018			
12	200	178	157	136	114	93	71	50	29	.0007		
11	211	190	168	147	125	.0104	83	61	40	.0018		
10	223	202	180	159	137	116	94	73	52	30		
9	236	214	193	171	150	128	.0107	73 85	64	43		
8	249	227	206	184	163	141	120	98	77	56		
7	263	241	220	198	177	155	134	.0112	91	6g		
6	277	256	234	213	191	170	148	127	.0105	84		
5	292	271	249	228	206	185	163	142	120			
4	308	287	265	244	222	201	179	158	136	.0099		
3	325	304	282	261	239	218	106	175	153	132		
2	343	321	300	278	257	235	214	192	171	149		
- I	361	340	318	297	275	254	232	210	189	167		
± 0	381	359	338	316	204	273	251	230	208	187		
+ 1	401	380	358	337	315	293	272	250	220	207		
2	423	401	379	358	336	315	293	271	250	228		
3	445	423	402	380	359	337	315	294	272	250		
4	468	447	425	404	382	360	339	317	295	274		
5	493	471	450	428	407	385	363	342	320	298		
6	519	497	476	454	432	411	389	367	346	324		
7	546	524	503	481	459	438	416	394	373	351		
8	574	552	531	509	487	466	444	422	401	379		
9	604	582	560	539	517	495	474	452	430	408		
10	.0635	.0613	.0591	.0569	.0548	.0526	.0504	.0483	.0461	.0439		
-20 { + 10 }	$\Delta e \times \Delta B$	+.0001	+.0001	+.0002	+.0003	+.0004	+.0004	+.0005	+.0006	+.0007		

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 32}{1571}\right)$$

B = 30.0 inches

					.o mcne					
	t - t'									
<i>t</i>	2.0	2.2	2.4	2.6	2.8	3.0	3.2	3.4	3.6	3.8
F. -10° 9 8 7	Inches. .0009 21 34 48 62	26	.0005	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
5 4 3 - 1	77 93 .0110 127 146	.0106	34 50 67 84 .0103	29 45 63	.0007 .0024 41 60	.0002 .0020 38	. 00 16			
± 0 + 1 2 3 4	165 185 207 229 252	185 207	122 142 163 186 209	164	79 99 .0120 142 166	57 78 .0099 .0121 144	36 56 77 99	.0014 34 55 78	.0013 34 56 79	.001 <i>2</i> 34 58
5 6 7 8 9	277 302 329 357 387	308 336	233 259 286 314 343	237 264	190 216 243 271 300	168 194 221 249 278	147 172 199 227 257	125 151 178 205 235	.0104 129 156 184 213	82 .0107 134 162 191
10 -10 \ Aa \ AB	.0417	.0396	.0374		.0331	.0309	.0287	.0266	.0244	.0222
$-10 \left\{ \Delta e \times \Delta B \right\}$	+.0007	+.0008	+.0009	+.0009	+.0010	+.0011	+.0012	+.0012	+.0013	+.0014
	t-t'									
t'	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.8
3° 4	Inches. .0013	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
5 6 7 8	60 86 .0113 140 170	39 64 91 .0119 148	.0017 42 69 97 .0126	.0021 47 75 .0105	.0026 54 83	.0004 32 61	.0010 40	.0018		
10	.0200	.0179	.0157		.0114	.0092	.0070	.0048	.0027	.0005
$+10 \Delta e \times \Delta B$	+.0014	+.0015	+.0016	+.0017	+.0017	+.0018	+.0019	+.0020	+.0020	+.0021

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.

Values of $e = e' - 0.000367 B(t - t') \left(1 + \frac{t' - 3^2}{1571}\right)$ B = 30.0 inches

B = 30.0 inches											
1-1'											
ť.	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	
IO°	$\Delta e \times \Delta B$	+.0004	+.0007	+-0011	+.0014	+.0018	+.0022	+.0025	+.0029	+.0033	
10°	0.063	0.053	0.042	0.031	0.020	0.009 .01 <i>2</i>	0.002				
11 12	67 70	56 50	45 48	34 37	23 27	16	1		ľ		
13	74	59 63	52	41	30	19	5 8				
14	77	66	56	45	34	23	.012	0.001			
15	81	70	59	49	38	27	16	5			
16	8.5	74	63 68	53	42	31	20	9	0.000		
17 18	89 94	79 83	72	57 61	46 50	35 39	24 28	.013 18	0.002		
10	.099	88	77	66	55	44	33	22	11	0.000	
20	.103	92	81	71	60	49	38	27	16	.005	
21	.108	97	86	76	65	54	43	32	21	.010	
22	.114	.103	92	81	70	59	43 48	37	26	15	
23	.119	.108 .114	97	86	75 81	64 70	53	42	32	21	
24	.125		.103	92			59	48	37	26	
25	.131 .137	.120 .126	.109	98 .104	87 93	76 82	65 71	54 60	43 49	32 38	
26 27	.143	.133	.122	.111	.100	89	78	67	56	45	
28	.150	.139	.128	.117	.106	95	84	73	62	51	
29	.157	.146	.135	.124	.113	.102	91	80	69	58	
30	.165	.154	.143	.132	.121	.110	99	88	77	66	
31	.172 .180	.161	.150	.139	.128	.117	.106	95	84	73 81	
32	.188	.169 .177	.158 .166	.147 .155	.136	.125 .133	.114	.103	92 .100	89	
33 34	.195	.184	.173	.162	.151	• .140	.129	.118	.107	96	
35	.203	.192	.181	.170	.159	.148	.137	.126	.115	.104	
36	.212	.201	.190	.179	.168	.157	.145	.134	.123	.112	
37	.220	.200	.198	.187	.176	.165	.154	.143	.132	.121	
38	.229	.218	.207 .216	.196	.185	.174 .183	.163 .172	.152 .161	.141 .150	.130	
39	.248			_	.203	_	.181		_	.139	
40	.258	·237 (246)	235	.215	.213	.192 .202	.101	.170	.159 .169	.148 .158	
41 42	.268	.257	.246	•234	.223	.212	.201	.190	.179	.168	
43	.278	.267	.256	.245	.234	.223	.212	.201	.190	.178	
44	.289	.278	.267	.256	.245	.234	.223	.211	.200	.189	
45	.300	.289	-278	.267	.256	.245	.234	.223	.211	.200	
46	.312 •324	.301	.290 .302	.279 .29I	.268 .280	.256 .268	.245	.234	.223	.212	
47 48	.336	.325	.314	.303	.292	.281	.270	.259	.248	.236	
49	·349	.338	.327	.316	. 305	.294	.283	.271	.260	.249	
50	.363	.351	-340	•329	.318	.307	.296	.285	.274	.262	
51	.376	.365	-354	-343	-332	.321	.309	.298	.287	.276	
52	.390	-379	.368	·357	.346	-335	•324	.312	.30 1 .316	.290	
53 54	.405 .420	•394 •409	•383 •398	•372 •387	.361 .376	•349 •364	•338 •353	•327 •342	.331	.305 .320	
55	.436	.425	.414	.402	.391	.380	.369	.358	-347	-335	
56	•452	.44I	.430	.419	.407	.396	.385	·374	.363	·353	
57	.469	.458	.446	·435	.424	.413	.402	-390	•379	.368	
58	.486	•475	.464	.452	.441	.430	.419	.408	.396	.385	
59	.504	•493	.481	.470	·459	.448	•437	.425	.414	.403	
60	0.522	0.511	0.500	0.488	0.477	0.466	0.455	0.444	0.432	0.421	
60	$\Delta e \times \Delta B$	+.0004	+.0007	+.0011	+.0015	+.0019	+.0022	+.0026	+.0030	+.0034	

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571} \right)$$

 $B = 30.00$

					t -	- t'				
t'	10	11	12	13	14	15	16	17	18	19
F. 30° Δε× ΔΒ	Inches. +.0037	Inches. +.0040	Inches. +.0044	inches. +.0048	Inches. +.0051	Inches. +.0055	Inches. +.0059	Inches. +.0062	Inches. +.0066	Inches. +.0070
22° 23 24	0.004 .010 15									
25 26 27 28 29	21 27 34 40 47	0.010 16 23 29 36	0.005 .012 18 25	0.001 7 .014	0.003	ì				
30 31 32 33 34	55 62 70 78 85	44 51 59 67 74	33 40 48 55 63	22 29 37 44 52	.011 18 26 33 41	0.000 .007 .015 22 30	0.004 11 19	0.000		
35 36 37 38 39	93 .101 .110 .119	82 90 99 .108 .117	71 79 88 96	60 68 77 85 94	49 57 66 74 83	38 46 55 63 72	27 35 43 52 61	.016 24 32 41 50	0.005 .013 21 30 39	0.002 .010 19 28
40 41 42 43 44	.137 .147 .157 .167 .178	.126 .136 .146 .156 .167	.115 .125 .135 .145	.104 .114 .124 .134	93 103 .113 .123	82 91 .101 .112	71 80 90 .101	60 69 79 90	49 58 68 79 89	37 47 57 68 78
45 46 47 48 49	.189 .201 .213 .225 .238	.178 .190 .202 .214	.167 .179 .191 .203 .216	.156 · .168 · .180 · .192 · .205	.145 .156 .168 .181	.134 .145 .157 .170	.123 .134 .146 .159 .171	.112 .123 .135 .147	.100 .112 .124 .136	89 .101 .113 .125
50 51 52 53 54	.251 .265 .279 .294 .309	.240 .254 .268 .282	.229 .243 .257 .271 .286	.218 .231 .246 .260	.207 .220 .234 .249 .264	.196 .209 .223 .238	.184 .198 .212 .227	.173 .187 .201 .216	.162 .176 .190 .204	.151 .165 .179 .193
55 56 57 58 59	.324 .340 .357 .374 .392	.313 .329 .346 .363 .381	.302 .318 .334 .352 .369	.29 1 .307 .323 .340	.280 .296 .312 .329 .347	.268 .285 .301 .318 .336	.257 .273 .290 .307 .325	.246 .262 .279 .296	.235 .251 .267 .284 .302	.224 .240 .256 .273
60	0.410	0.399	0.388	0.376	0.365	0.354	0.343	0.331	0.320	0.309
60 Δe× ΔB	+.0037	+.0041	+.0045	+.0049	+.0052	+ .0 056	+.0060	+.0064	+.0067	+.007

TABLE 75. REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

ENGLISH MEASURES.
Values of e=e'-0.000367 $B(t-t')\left(1+\frac{t'-32}{1571}\right)$ B=30.00

						t-t'				
ľ	20	21	22	23	24	25	26	27	28	29
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches,	Inches.	Inches.
40° Δ <i>e</i> × Δ <i>B</i>	+.0074	+.0077	+.0081	+.0085	+.0089	+.0092	+.0096	+.0100	+.0103	+.0107
38°	0.008		1				_			
39	.017	0.006					1			
40	26	.015	0.004							
41	36	25	.014	0.003						
42 43	46 56	35 45	24	.013	.012	0.001			ĺ	
43	67	56	34 45	34	23	.012	0.001			1
45	78	67	56	45	34	23	.012	0.001	·	
46	90	79	68	57 68	45	34	23	.012	0.001	1
47	.102	91	79		57	46	35	24	13	0.002
48	.114	.103	92	81	70	58	47	36	25	.014
49	.127	.116	.104	93	82	71	60	49	38	27
50 51	.140 .153	.129 .142	.118	.106	95 .109	84 98	73 87	62 75	51 64	40 53
52	.167	.156	.145	.134	.123	.112	.101	80	78	67
53	.182	.171	.160	.149	.137	.126	.115	.104	93	82
54	.197	.186	.175	.164	.152	.141	.130	.119	.108	97
55	.212	.201	.190	.179	.168	.157	.145	.134	.123	.112
56 57	.229	.218	.206	.195	.184	.173 .18g	.162	.150	.139	.128
57 58	.245	.234 .251	.223	.228	.217	.206	.195	.167 .184	.156 .173	.144 .161
59	.280	.269	.257	.246	.235	.224	.213	.201	.190	.179
60	0.298	0.287	0.275	0.264	0.253	0.242	0.231	0.219	0.208	0.197
$60 \Delta e \times \Delta B$	+.0075	+.0078	+.0082	+.0086	+.0090	+.0093	+.0097	+.0101	+.0105	+.0108
t'						t-t'				
	30	_31_	32	33	34	35	36	37	38	39
F.										
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
50°Δe×ΔB	+.0111	Inches. +.0115		Inches. +.0122	Inches. +.0126	Inches. +.0130	Inches. +.0134	Inches. +.0137		
50°Δe×ΔB 48°	+.0111 0.003	+.0115							Inches.	Inches.
50°Δe×ΔB 48° 49	+.0111 0.003 .015	+.0115 .004	+.0119						Inches.	Inches.
50°Δε×ΔΒ 48° 49 50	+.0111 0.003 .015	.004 .017	0.00 6	+.0122					Inches.	Inches.
50°Δe×ΔB 48° 49	+.0111 0.003 .015 29 42	.004 .017 .017	+.0119 0.006 .020	+.0122 0.009					Inches.	Inches.
50° Δε× ΔΒ 48° 49 50 51 52 53	+.0111 0.003 .015 29 42 56 70	.004 .017	0.006 .020 34 48	+.0122	+ .0 126	+.0130	+.0134 0.004		Inches.	Inches.
50° Δε× ΔΒ 48° 49 50 51 52 53 54	+.0111 0.003 .015 29 42 56 70 85	.004 .017 .31 .45 .59 .74	0.006 .020 34 48 63	0.009 .023 37 52	+.0126 0.011 26 41	0.000 .015 30	+.0134	+.0137 0.007	Inches. +.0141	Inches.
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55	+.0111 0.003 .015 29 42 56 70 85	+.0115 .004 .017 .31 45 59 74	0.006 .020 34 48 63 78	0.009 .023 37 52 67	+.0126 0.011 26 41 56	0.000 .015 30 45	+.0134 0.004 .018 34	+.0137 0.007 .023	Inches. +.0141	Inches. +.0145
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56	+.0111 0.003 .015 29 42 56 70 85 .101	+.0115 .004 .017 .31 45 59 74 90	0.006 .020 34 48 63 78 95	0.009 .023 37 52 67 83	+.0126 0.011 26 41 56 72	0.000 .015 30 45 61	0.004 .018 34 50	+.0137 0.007 .023 39	O.OII 28	o.ooo .o16
50° Δe × ΔB 48° 49 50 51 52 53 54 55 56 57	+.0111 0.003 .015 29 42 56 70 85 .101 .117	+.0115 .004 .017 .31 .45 .59 .74 .90 .106 .122	+.0119 0.006 .020 34 48 63 78 95	0.009 .023 .37 52 67 83 .100	+.0126 0.011 26 41 56 72 88	+.0130 0.000 .015 30 45 61 77	0.004 .018 34 50 66	+.0137 0.007 .023 39 55	O.OII 28 44	0.000 0.000
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56	+.0111 0.003 .015 29 42 56 70 85 .101	+.0115 .004 .017 .31 45 59 74 90	0.006 .020 34 48 63 78 95	0.009 .023 37 52 67 83	+.0126 0.011 26 41 56 72	0.000 .015 30 45 61	0.004 .018 34 50	+.0137 0.007 .023 39	O.OII 28	0.000 0.016 32 49
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59	+.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168	+.0115 .004 .017 .31 45 59 74 90 .106 .122 .139	0.006 .020 34 48 63 78 95 .111 .128	0.009 .023 37 52 67 83 .100	+.0126 0.011 26 41 56 72 88 .105	+.0130 0.000 .015 30 45 61 77 94	0.004 .018 34 50 66 83	+.0137 0.007 .023 39 55 72	0.011 28 44 61	0.000 .016 32 49 67
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60	+.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186	+.0115 .004 .017 .31 45 59 74 90 .106 .122 .139 .157	0.006 .020 34 48 63 78 95 .111 .128	0.009 .023 37 52 67 83 .100 .117 .134 0.152	+.0126 0.011 26 41 56 72 88 .105	+.0130 0.000 .015 30 45 61 77 94 .112	0.004 .018 34 50 66 83 .101	+.0137 0.007 .023 39 55 72 89	O.OII 28 44 61 78	0.000 0.016 32 49 67 0.085
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ	+.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186	+.0115 .004 .017 .31 45 59 74 90 .106 .122 .139 .157	0.006 .020 34 48 63 78 95 .111 .128 .145 0.163	0.009 .023 37 52 67 83 .100 .117 .134 0.152	+.0126 0.011 26 41 56 72 88 .105 .123 0.141	0.000 .015 30 45 61 77 94 .112 0.130 +.0131	0.004 .018 34 50 66 83 .101	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 .016 32 49 67
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60	+.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186	+.0115 .004 .017 .31 45 59 74 90 .106 .122 .139 .157	0.006 .020 34 48 63 78 95 .111 .128 .145 0.163	0.009 .023 37 52 67 83 .100 .117 .134 0.152	+.0126 0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 .015 30 45 61 77 94 .112 0.130 +.0131	0.004 .018 34 50 66 83 .101	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 0.016 32 49 67 0.085
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ t'	+.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112	+.0115 .004 .017 .31 45 59 74 90 .106 .122 .139 .157 0.175 +.0116	+.0119 0.006 .020 34 48 63 78 95 .111 .128 .145 0.163 +.0120	+.0122 0.009 .023 37 52 67 83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 .015 30 45 61 77 94 .112 0.130 +.0131	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 0.016 32 49 67 0.085
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ t' F.	+.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112	+.0115 .004 .017 .31 .45 .59 .74 .90 .106 .122 .139 .157 0.175 +.0116	+.0119 0.006 .020 34 48 63 78 95 .111 .128 .145 0.163 +.0120	+.0122 0.009 .023 37 52 67 83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 0.015 30 45 61 77 94 .112 0.130 +.0131 -t' 45	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 0.016 32 49 67 0.085
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ t' F. 56° 57	+.0111 0.003 015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112 40 Inches. 0.005	+.0115 .004 .017 .31 .45 .59 .74 .90 .106 .122 .139 .157 0.175 +.0116 41 Inches. 0.010	+.0119 0.006 .020 34 48 63 78 95 .111 .128 .145 0.163 +.0120 42 Inches.	+.0122 0.009 .023 37 52 67 83 .100 .117 .134 0.152 +.0123 43 Inches.	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 0.015 30 45 61 77 94 .112 0.130 +.0131 -t' 45	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 .016 32 49 67 0.085
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ ** ** ** ** ** ** ** ** ** *	+.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112	+.0115 .004 .017 .31 45 .59 .74 .90 .106 .122 .139 .157 0.175 +.0116 41 Inches. 0.010 .27	+.0119 0.006 .020 34 48 63 78 95 .111 .128 .145 0.163 +.0120 42 Inches.	+.0122 0.009 .023 37 52 67 83 .100 .117 .134 0.152 +.0123 1nches.	+.0126 0.011 26 41 56 72 88 .105 .123 0.141 +.0127 44 Inches.	0.000 0.015 30 45 61 77 94 .112 0.130 +.0131 -t' 45 Inches.	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 .016 32 49 67 0.085
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ *' F. 56° 57 58 59	+.OIII 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.OII2 40 Inches. 0.005 .021 38 56	+.0115 .004 .017 .311 .45 .59 .74 .90 .106 .122 .139 .157 0.175 +.0116	+.0119 0.006 .020 34 48 63 78 95 .111 .128 .145 0.163 +.0120 42 Inches. 0.016 33	0.009 .023 .37 .52 .67 .83 .100 .117 .134 0.152 +.0123 Inches.		0.000 0.015 30 45 61 77 94 .112 0.130 +.0131 -t' 45 Inches.	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 .016 32 49 67 0.085
50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ ** ** ** ** ** ** ** ** ** *	+.OIII 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.OII2 40 Inches. 0.005 .021 38 56 0.074	+.0115 .004 .017 .31 45 59 74 90 .106 .122 .139 .157 0.175 +.0116 41 Inches. 0.010 27 45 0.063	+.0119 0.006 .020 34 48 63 78 .111 .128 .145 0.163 +.0120 42 Inches. 0.016 33 0.051	+.0122 0.009 .023 37 52 67 83 .100 .117 .134 0.152 +.0123 Inches. 0.005 .022 0.040	+.0126 0.011 26 41 56 72 88 .105 .123 0.141 +.0127 44 Inches.	0.000 0.015 30 45 61 77 94 .112 0.130 +.0131 -t' 45 Inches.	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 .023 39 55 72 89 0.107	0.011 28 44 61 78 0.096	0.000 .016 32 49 67 0.085

REDUCTION OF PSYCHROMETRIC OBSERVATION. ENGLISH MEASURES,

Values of $e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 32}{1571} \right)$

B = 30.00

	t-t'										
t'	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0
F.	Inches,	Inches.	Inches,	Inches,	Inches.	Inches.	-	Inches,	Inchee,	Inches.	Inches.
60°	$\Delta e \times \Delta B$	+.0004						1	1	+.0034	1
60°	0.522	0.511	0.500	0.488	0.477	0.466	0.455	0.444	0.432	0.421	0.410
61	.541	.530	.518	.507	.496	.485	.474	.462	.451	.440	.429
62	.560	-549	.538	-527	.516	.504	•493	.482	.471	•459	.448
63	.580	569	.558	.547	.536	.524	.513	.502	.49I	-479	.468
64	.601	.590	.579	.568	.556	•545	-534	·523	.511	.500	.489
65 66	.623 .645	.633	.600	.589	.578	.566 .588	-555	.544	-533	.521	.510
67	.667	.656	.645	.634	.622	.500	.577	.566	·555 ·577	·543 ·566	·532 ·555
68	.691	.680	.668	.657	.646	.635	.623	.612	.601	.590	.578
69	.715	.704	.692	.681	.670	.659	.647	.636	.625	.614	.602
70	.740	.729	.717	.706	.695	.684	.672	.661	.650	.638	.627
71	.766	.754	.743	.732	.720	.709	.698	.687	.675	.664	.653
72	.792 .810	.781	.769	.758	-747	.735	.724	.713	.702	.690	.679
73 74	.847	.836	·797 .824	.785 .813	·774	.763 .791	.751 :779	.740 .768	.729 .757	.717 .745	.706
75	.876	.865	.853	.842	.831	.810	.808	·797	.786	.774	·734 ·763
76	.906	.804	.883	.872	.860	.840	.838	.826	.815	.804	.792
77	.936	.925	.914	.902	.891	.880	.868	.857	.846	.834	.823
78	.968	.956	945	-934	.922	.911	.900	.888	.877	.866	.854
79	1.000	.989	∙977	.966	.955	•943	.932	.921	.909	.898	.887
80	1.033	1.022	1.011	-999	.988	-977	.965	.954	.943	.931	.920
81 82	.068	.056	.045 .080	1.034 .069	.057	1.011 .046	-999	.988 1.023	.977	.965	.954
83	.139	.128	.116	.105	.037	.040	1.035	.060	.012	.037	.989 1.026
84	.176	.165	.154	.142	.131	.120	.108	.007	.086	.074	.063
85	1.215	1.204	1.192	1.181	1.160	1.158	1.147	1.135	1.124	1.112	1.101
86	.254	.243	.232	.220	.200	.197	.186	.175	.163	.152	.140
87 88	.295	.284	.272	.261	.249	.238	.227	.215	.204	.192	.181
	.336	.325 .368	.314	.302	.291	.279	.268	.257	.245 .288	.234	.222
89 90	. 379 1.423	1.412	·357	·345 1.380	·334 1.378	.322 1.366	.311	.300		.277	.265
90	.469	457	.446	.435	.423	.412	.400	1.343 .389	1.332 ·377	1.321 .366	1.309 •355
92	.515	.504	.492	.481	.470	.458	.447	435	.424	.412	.401
93	.563	.552	.540	.529	-517	.506	-494	.483	471	.460	-449
94	.612	.601	-589	.578	.566	-555	∙543	-532	.521	.509	.498
95	1.662	1.651	1.640	1.628	1.617	1.605	1.594	1.582	1.571	1.559	1.548
96	.714 .767	.703 .756	.691 •744	.68o •733	.668 .722	.657 .710	.646 .699	.634	.623	.611 .664	.600
97 98	.822	.811	799	.788	.776	.765	.753	.742	(.776) -730	.719	.653 .707
99	.878	.867	.855	.844	.832	.821	.800	.798	.786	.775	.763
ιοό	1.936	1.924	1.913	1.901	1.890	1.878	1.867	1.855	1.844	1.832	1.821
101	•994	983	.972	.960	-949	-937	.926	.914	.903	.891	-880
102	2.055	2.043	2.032	2.020	2.009	.997	.986	.974	.963	.951	.940
103	.117	.106	.094	.083	.071	2.060	2.048	2.037	2.025	2.014	2.002
104	.181	.169	.158	.146	.135	.123	.112	.100	.089	.077	.066
105 106	2.246 -314	.302	.200	.279	2.200	2.189 .256	2.177 -244	2.166	2.154	2.143	.198
100	-314 -382	.371	·359	.348	.336	.325	.313	.302	.200	.278	.267
108	·453	.441	.430	418	.407	•395	.384	.372	.361	-349	.337
109	.525	.514	.502	.491	.479	.467	.456	.444	•433	.421	.410
110	2.599	2.588	2.576	2.565	2.553	2.542	2.530	2.519	2.507	2.495	2.484
110	$\Delta e \times \Delta B$	+.0004	+.0008	+.0012	+.015	+.0019	+.0023	+.0027	+.0031	+.0035	
					!			<u></u>			

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571} \right)$$

					3 = 30.0			·			
t'			1	I 4.5		t-t'	1 4 5	· · · ·	1	1	
	0.0	11	12	13	14	15	16	17	18	19	20
F. 60°	Inches. $\Delta e imes \Delta B$	Inches. +.0041	Inches. +.0045	Inches. +.0049	Inches. +.0052	Inches. +.0056	Inches. +.0060	Inches. +.0063	Inches. +.0067	Inches. +.0071	Inche +.007
60°	0.522	0.399	0.388	0.376	0.365	0.354	0.343	0.331	0:320	0.309	0.298
61	.541	0.418	.406	-395	.384	-373	.361	.350	-339	.328	.317
62 63	.560 .580	.437	.426 .446	.415	.403	.392 .412	.381	.370	.358	347	.336
64	.601	.457 .478	.466	·435 ·455	·423 ·444	.433	.422	.390	378	.367	-356
65	.623	-499	.488	.476	.465	.454	443	.431	.420	.409	.398
66	.645	.521	.510	.498	.487	476	.465	453	.442	.431	.420
67	.667	-544	.532	.521	.510	·499	.487	.476	.465	-454	-442
68	.691	.567	.556	.544	·533	.522	.511	·499	.488	·477	.466
69 70	.715	.591	.580	.568	-557	.546	·535	.523	.512	.501	.490
70 71	.740 .766	.616 .641	.605 .630	·593 .619	.582 .608	.571 .596	·559 ·585	.548 .574	·537 ·562	.526 .551	.514
72	.792	.668	.656	.645	.634	.623	.611	.600	.589		.540
73	.819	.695	.684	.672	.661	.650	.638	.627	.616	·577 .604	.593
74	.847	.723	.71 1	*.700	.689	.678	.666	.655	.644	.632	.621
75	.876	-752	.740	.729	.718	.706	.695	.684	.672	.661	.650
76	.906	.781	.770	.758	-747	.736	.725	•7 ¹ 3	.702	.691	.679
77 78	.936 .968	.812 .843	.800 .832	.789 .820	.778 .809	.766 .798	·755	•744	.732 .764	.721	.710
70 79	1.000	.875	.864	.853	.841	.830	.819	·775 .807	.796	.752 .785	.74I .773
80	1.033	.000	.807	.886	.875	.863	.852	.841	.820	.818	.806
81	.068	.943	.931	.920	.909	.897	.886	.875	.863	.852	.841
82	.103	.978	.967	·955	944	.932	.921	.910	.898	.88 ₇	.876
83	.139	1.014	1.003	.991	.980	.969	-957	.946	.935	.923	.912
84	.176	.051	.040	1.029	1.017	1.006	-995	.983	.972	.960	-949
85	1.215	1.090	1.078	.1067	1.056	.083	1.033	1.02 I .06 I	1.010	·999	.987
86 87	.254	.129 .170	.118	.147	.095	.124	.072	.101	.049	.038	.067
87 88	.336	.211	.200	.188	.177	.165	.154	.143	.131	.120	.108
89	-379	.254	.242	.231	.220	.208	.197	.185	.174	.163	.151
90	1.423	1.298	1.286	1.275	1.264	1.252	1.241	1.229	1.218	1.206	1.195
91	.469	.343	.332	.320	.309	.297	.286	.275	.263	.252	.240
92	.515	.390	.378	.367	-355	•344	.332	.321	.310	.298	.287
93 94	.563 .612	.437 .486	.426 -475	.4 1 4 .463	.403 .452	.39 1 .440	.380	.369 .418	-357 -406	.346 .395	·334 ·383
95	1.662	1.537	1.525	1.514	1.502	1.491	1.479	1.468	1.456	1.445	1.433
96	.714	.588	·577	.565	·554	.542	.531	.520	.508	·497	.485
97	.767	.641	.630	.618	.607	.595	.584	.572	.561	.550	.538
98	.822	.696	.684	.673	.661	.650	.638	.627	.615	.604	•593
99	.878	.752	.740	.729	.717	.706	.694	.683	.671	.660	.648
100	1.936	1.809	1.798	1.786	1.775	1.763 .822	1.752	1.740	1.729	1.717	1.706
IOI IO2	.994 2.055	.868 .928	.857 .917	.845	.834 .894	.882	.811 .871	·799 .859	.788 .848	.776 .836	.765 .825
102	.117	.928	.979	.968	.956	.944	.933	.921	.910	.898	.887
104	.181	2.054	2.043	2.031	2.020	2.008	997	.985	.974	.962	.951
105	2.246	2.120	2.108	2.097	2.085	2.073	2.062	2.050	2.039	2.027	2.016
106	.314	.187	.175	.164	.152	.141	.129	.118	.106	094	.083
107	.382	-255	.244	.232	.221	.209	.198	.186	.175	.163	.152
108	•453	.326	.314	.302	.291	.280	.268	.257	·245	.234	.222
100	-525	.398	.387	-375	.364	.352	.340	.329	.317	.306	.294
110	2.599	2.472	2.461	2.449	2.438	2.426	2.414	2.403	2.391	2.380	2.368
110	$\Delta c \times \Delta B$	+.0042	+.0046	+.0050	+.0054	T.0058	T.0002	+.0065	7.0009	+.0073	+.007

Values of $e=e'-0.000367 B (t-t') \left(1 + \frac{t'-32}{1571}\right)$ B=30.00

ı E											
ı, l						t-t'		-			
	0.0	21	22	23	24	25	26	27_	28	29	30
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inchee.
60°	$\Delta e \times \Delta B$	+.0078	+.0082	+.0086				+.0101		+.0108	+.0112
60°	0.522	0.287	0.275	0.264	0.253	0.242	0.231	0.219	0.208	0.197	0.186
61	.541	0.305	.294	.283	.272	.261	.249	.238	.227	.216	.205
62	.560	·325	.314	.302	.291	.280	.269 .289	.257	.246	·235	.224
63 64	.580 .601	.345 .365	·334	.322 •343	.311 .332	.300	.309	.277 .298	.287	.255 .276	.244 .264
65	.623	.387	•354	.364	·353	.342	.330	.319	.308	.297	.285
66	.645	.408	∙375 •397	.386	·375	.363	.352	.341	.330	.319	.307
67	.667	.431	.420	.409	-397	.386	-375	.364	.352	.341	.330
68	.691	•454	-443	-432	.421	.409	.398	.387	.376	.364	-353
69	.715	.478	.467	.456	·445	-433	.422	.411	-399	.388	-377
70	.740	.503	.492	.481	.469	.458	-447	-435	.424	.413	.402
71	.766	.529	.517	.506	·495	.483	.472	.461	.450	.438	.427
72	.792	·5 <u>5</u> 5	•544	·532	.521	.510	.498	.487	.476	.464	-453
73	.819	.582	.571	-559	.548	·537	.525	.514	.503	.491	.480
74	847	.610	.598	.587 .616	.576	.564	·553	.542	531	.519	.508
75 -6	876	.638 .668	.627 .657	.645	.605 .634	•593 •623	.582 .611	.571 .600	·559 ·589	.548	·537 ·566
76	.906 .936	.698	.687	.676	.664	.653	.642	.630	.509	·577 .608	.596
77 78	.968	.730	.718	.707	.696	.684	.673	.662	.650	.639	.628
79	1.000	.762	.751	-739	.728	.717	.705	.694	.683	.671	.66o
80	1.033	•795	.784	.772	.761	.750	.738	.727	.716	.704	.693
81	.068	.829	.818	.806	·795	.784	.772	.761	.750	.738	.727
82	.103	.864	.853	.842	.830	.819	.808	.796	.785	·773	.762
83	.139	.900	.889	.878	.866	.855	.844	.832	.821	.810	.798
84	.176	.938	.926	.915	.904	.892	.881	.869	.858	.847	.835
85	1.215	.976	.965	.953	.942	.930	.919	.908	.896	.885	.873
86 87	.254	1.015 .056	1.004	.992 1.033	.981 1.021	.970 1.010	.958 .999	.947 .987	.935 .976	.924 .964	.913 ·953
88	.295 .336	.030	.044 .086	.074	.063	.051	1.040	1.029	1.017	1.006	.994
89	.379	.140	.128	.117	.106	.094	.083	.071	.060	.049	1.037
9ó	1.423	1.184	1.172	1.161	1.149	1.138	1.127	1.115	1.104	1.002	1.081
91	.469	.229	.217	.206	.195	.183	.172	.160	.149	.138	.126
92	.515	.275	.264	.252	.241	,230	.218	.207	.195	.184	.172
93	.563	•323	.311	.300	.288	•277	.266	.254	•243	.231	.220
94	.612	-372	.360	·349	•337	.326	.315	.303	.292	.280	.269
95	1.662	1.422	1.411	1.399	1.388	1.376	1.365	1.353	1.342	1.330	1.319
96	.714	•474	.462	.451 .504	.439 .492	.428 .481	.416 .469	.405 .458	·393 ·446	.382	.371
97 98	.767 .822	.527 .581	.515 .570	.558	.492	.535	.524	.512	.501	.435 .489	.423 .478
99	.878	.637	.625	.614	.602	.591	.580	.568	-557	.545	•534
100	1.936	1.694	1.683	1.671	1.660	1.648	1.637	1.625	1.614	1.602	1.591
101	.994	.753	.742	.730	.719	.707	.696	.684	.673	.661	.650
102	2.055	.813	.802	.790	.779	.767	.756	-744	•733	.721	.710
103	.117	.875	.864	.852	.841	.829	.818	.806	•795	.783	.772
104	.181	-939	.928	.916	.905	.893	.882	.870	.858	.847	.835
105	2.246	2.004	1.993	1.981	1.970	1.958	1.947	1.935	1.924	1.912	1.901
106	.314	.071	2.060	2.048	2.037	2.025	2.014	2.002	.991	.979	.968
107	.382	.140	.129	.117	.105	.094 .164	.082	.071	2.059	2.048	2.036
100	·453	.211	.199	.260	.170	.236	.153	.141	.130	.118	.107
	.525	_		2.334	2.322	2.310	2.299	2.287	2.276	2.264	}
110	2.599	2.357	2.345	1	_	-			i ·		2.253
110	$\Delta e \times \Delta B$	+.0081	7.0005	+.0089	T.0092	7.0090	7.0100	+.0104	1.0108	+.0112	+.0116

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571}\right)$$

 $B = 30.00$

					B=30	.00					
l'						t-t'					
	0.0	31	32	33	34	35	36	37	38	39	40
F. 60°	Inches, $\Delta e imes \Delta B$	Inches.	Inches. +.0120	Inches.	Inches. +.0127	Inches. +.0131	Inches. +.0134	Inches.	Inches. +.0142	Inches. +.0146	Inches. +.0149
60°	0.522	0.175	0.163	0.152	0.141	0.130	0.110	0.107	0.006	0.085	0.074
61	.541	.193	.182	.171	.160	.148	.137	.126	.115	.104	.092
62	.560	.213	.201	.190	.179	.168	.156	.145	.134	.123	.112
63 64	.580 .601	.232	.221	.210	.199	.188 .2 0 8	.176 .197	.165 .186	.154	.143	.131
65	.623	.274	.263	.252	.240	.229	.218	.207	.195	.184	.173
66	.645	.296	.285	.274	.262	.251	.240	.229	.217	.206	.195
67 68	.667	.318	.307	.296	.285	.273	.262	.251	.240	.228	.217
69	.691 .715	.342	.330 .354	.319 .343	.308	.297 .32I	.285	.274	.263	.252	.240
70	.740	.390	-379	.368	·357	·345	-334	-323	.311	.300	.289
71	.766	.416	.404	•393·	.382	.371	·359 .385	.348	.337	.325	.314
72	792	.442	.431	.419	.408	397		-374	.363	352	.340
73 74	.819 .847	.469 .496	.458 .485	.446 -474	.435 .463	.424 .451	.412 .440	.401 .429	.390 .418	·379 .4 0 6	·367 ·395
75	.876	.525	.514	.503	.491	.480	.460	·457	.446	·435	.424
76	.906	-555	•543	.532	.521	.500	.498	.487	.476	.464	·453
77	.936	.585	.574	.562	.551	.540	-529	.517	.506	495	.483
78	.968	.616	.605	-594	.582	.571	.560	.548	-537	.526	.514
79	1.000	.649	.637	.626	.615	.603	.592	.581	.569	.558	•547
80 81	.068	.682 .716	.670 .704	.659 .693	.648	.636 .670	.625 .659	.614 .648	.602 .636	.591 .625	.580 .613
82	.103	.751	.739	.728	.717	.705	.694	.683	.671	. 660	.648
83	.139	.787	.775	.764	·753	.741	.730	.719	.707	.696	.685
84	.176	.824	.813	.801	.790	.778	.767	.756	·744	-733	.722
85	1.215	.862	.851	.839	.828	.817	.805	.794	.782	.771	.760
86 87	.254 .295	.901	.890 .930	.878	.867 .907	.856 .8 0 6	.844 .885	.833 .873	.822 .862	.810 .850	·799 .839
88	.336	.983	.972	.960	.949	.937	.926	.915	.903	.892	.880
89	.379	1.026	1.014	1.003	.991	.980	.969	957	.946	.934	.923
90	1.423	1.069	1.058	1.047	1.035	1.024	1.012	1.001	.990	.978	967
91	.469	.115	.103	.092	.080	.069	.058	.046	1.035	1.023	1.012
92	.515 .563	.161	.150 .197	.138 .186	.127 .174	.115 .163	.104 .151	.092 .140	.081 .128	.070 .117	.058
93	.612	.257	.246	.234	.223	.212	.200	.189	.177	.166	.105
95	1.662	1.308	1.296	1.285	1.273	1.262	1.250	1.239	1.227	1.216	1.204
96	.714	-359	.348	.336	325	.313	.302	.290	.279	.267	.256
97	.767	.412	.401	.389	.378	.366	·355	-343	·332	.320	.309
98 99	.822 .878	.466	.455 .511	•443 •499	.432 .488	.420 .476	.409 .465	.398 -453	.386	· ·375 ·430	.363 .419
100	1.936	1.579	1.568	1.556	1.545	1.533	1.522	1.510	1.499	1.488	1.476
101	.994	.638	.627	.615	.604	.592	.581	.569	-558	-546	-535
102	2.055	.698	.687	.675	.664	.652	.641	.629	.618	.606	∙595
103	.117	.760 .824	.749 .812	.737 .801	.726 .789	.714 .778	.703 .766	.691 •755	.680	.668 .732	.657
104	.181	.88q	1.878	1.866	1.855	1.843	1.832	1.820	-743 1.808	.732 1.797	1.785
105 106	2.246 .314	.956	•945	-933	.922	.010	.898	.887	.875	.864	.852
107	.382	2.025	2.013	2.002	.990	·979	.967	955	944	.932	.921
108	·453	.095	.084	.072	2.c6o	2.049	2.037	2.026	2.014	2.003	.991
109	2.525	2.167	2.156	2.144	2.133	2.121	2.109	2.098	2.086	2.075	2.063
IIO	$\Delta e \times \Delta B$	+.0119	+.0123	+.0127	+.0131	+.0135	+.0139	+.0143	+ . 0146	+.0150	+.0154
L	•									·	

Values of $e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571}\right)$

B = 30.00

	<i>t</i> – <i>t'</i>											
	0.0	41	42	43	44	45	46	47	48	49	50	
F. 60°	In ches. $\Delta e imes \Delta B$	Inches. +.0153	Inches. +.0157	Inches. +.0161	Inches, +.0164	Inches. +.0168	Inches.	Inches. +.0176	Inches. +.0179	Inches. +.0183	Inches. +.0187	
60° 61 62	0.522 .541 .560	0.063 .081	0.051	0.040 .059	0.029 .048	0.018	0.007	0.014	0.003	0.011		
63 64	.580 .601	.120	.109 .129	.c98	.087	.055 .075 .096	.044 .064 .085	.033 .053 .073	.022 .042 .C62	.030	0.019 .040	
65 66 67 68	.623 .645 .667 .691	.162 .184 .206	.150 .172 .195 .218	.139 .161 .183 .207	.128 .150 .172 .195	.117 .139 .161 .184	.105 .127 .150 .173	.094 .116 .138 .162	.083 .105 .127 .150	.072 .094 .116	.061 .082 .105 .128	
69 70 71 72 73	.715 .740 .766 .792 .819	.253 .278 .303 .329 .356	.242 .266 .292 .318	.230 .255 .280 .306 .333	.219 .244 .269 .295	.208 .232 .258 .284	.197 .221 .246 .273 .299	.185 .210 .235 .261	.174 .199 .224 .250	.163 .187 .213 .239 .266	.152 .176 .201 .227 .254	
74 75 76 77 78 79	.847 .876 .906 .936 .968	.384 .412 .442 .472 .503	.372 .401 .430 .461 .492	.361 .390 .419 .449 .480	.350 .378 .408 .438 .469	.338 .367 .396 .427 .458 .490	·327 ·356 ·385 ·415 ·446 ·478	.316 ·344 ·374 ·404 ·435 ·467	.304 .333 .362 .393 .424 .456	.293 .322 .351 .381 .412	.282 .310 .340 .370 .401	
80 81 82 83 84	1.033 .068 .103 .139	.568 .602 .637 .673	.557 .591 .626 .662 .699	.546 .579 .614 .650 .687	.534 .568 .603 .639	.523 .557 .592 .628 .665	.511 .545 .580 .616 .653	.500 •534 •569 •605	.489 .523 .558 .594 .631	.477 .511 .546 .582 .619	.466 .500 .535 .571 .608	
85 86 87 88 89	1.215 .254 .295 .336 .379	.748 .787 .828 .869	.737 .776 .816 .858	.725 .765 .805 .846 .889	.714 .753 .793 .835 .877	.703 .742 .782 .823 .866	.691 .730 .771 .812 .855	.680 .719 .759 .801 .843	.669 .708 .748 .789 .832	.657 .696 .737 .778 .820	.646 .685 .725 .766 .809	
90 91 92 93 94	1.423 .469 .515 .563 .612	.955 1.000 .047 .094 .143	.944 .989 1.035 .083	.932 .978 1.024 .071	.921 .966 1.012 .060	.910 .955 1.001 .048 .097	.898 .943 .989 1.037 .086	.887 .932 .978 1.025	.875 .920 .967 1.014 .063	.864 .909 .955 1.003 .051	.853 .898 .944 .991	
95 96 97 98 99	1.662 .714 .767 .822 1.878	1.193 .244 .297 .352 1.407	1.182 .233 .286 .340 1.396	1.170 .222 .274 .329 1.384	1.159 .210 .263 .317 1.373	1.147 .199 .251 .306 1.361	1.136 .187 .240 .294 1.350	1.124 .176 .229 .283 1.338	1.113 .164 .217 .271 1.327	1.101 .153 .206 .260 1.316	1.090 .141 .194 .248 1.304	
100	$\Delta e \times \Delta B$	+.0157	+.0161	+.0165	+.0168	+.0172	+.0176	+0.180	+.0184	+.0188	+.0191	

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571} \right)$$

$$B = 30.00$$

t'						t-t'			·		
•	0.0	51	52	53	54	55	56	57	58	59	60
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inche
70°	$\Delta e \times \Delta B$	+.0192	+.0195	+.0199	+.0203	+.0207	+.0210	+.0214	+.0218	+.0222	+.02
62°	0.560										
63	.580	0.008									Į
64	.601	0.028	0.017	0.006							
65	.623	.049	.038	.027	0.016	o.co4					
66	.645	.071	.060	.049	.037	.026	0.015	0.004			
67	.667	.093	.082	.071	.060	.048	.037	.026	c.015	0.003	
68	.691	.116	.105	.094	.083	.071	.060	.049	.038	.026	0.01
69	.715	.140	.129	.118	.106	.095	.084	.073	.061	.050	.03
70	.740	.165	.154	.142	.131	.120	.108	.097	.0 86	.075	.06
71	.766	.190	.179	.167	.156	.145	.134	.122	.III	.100	.08
72	.792	.216	.205	.194	.182	.171	.160	.148	.137	.126	.II.
73	.819	.243	.232	.220	.209	.198	.186	.175	.164	.153	.14
74	.847	.271	.259	.248	-237	.225	.214	.203	.191	.180	.16
75	.876	.299	.288	.276	.265	·254	.243	.231	.220	.209	.19
76	.906	.328	.317	.306	.294	.283	.272	.260	.249	.238	.22
77 78	.936	-359	.347	.336	·325	.313	.302	.291	.279	.268	.25
	.968	.390	.378	.367	.356	-344	•333	.322	.310	.299	.28
79	1.000	.422	.410	-399	.388	.376	.365	∙354	.342	.331	.32
80	1.033	-455	•443	-432	.42I	.409	.398	.387	-375	.364	.35
8 1	.068	.489	.477	.466	·455	-443	432	.420	.409	.398	.38
82	.IC3	.524	.512	.501	.489	·478	.467	·455	•444	433	.42
83	.139	-559	.548	-537	.525	.514	.503	.491	.480	.469	.45
84	.176	.596	.585	-574	.562	.551	.540	.528	.517	.505	.49
85	1.215	.634	.623	.612	.600	.589	.578	.566	-555	·543	•53
86	.254	.673	.662	.651	.639	.628	617	.605	•594	.582	.57
87	.295	-714	.702	.691	.680	.668	.657	.645	.634	.623	.61
88	.336	.755	.744	.732	.721	.709	.698	.687	.675	.664	.65
89	1.379	0.798	0.786	0.775	0.763	0.752	0.740	0.729	0.718	0.706	0.69
90	$\Delta e \times \Delta B$	+.0104	+.0108	+.0202	+.0205	+.0200	+.0213	+.0217	+.0221	+,0225	+.02

RELATIVE HUMIDITY. TEMPERATURES FAHRENHEIT.

Alr Temper- ature.	RELATIVE HUMIDITY, OR PERCENTAGE OF SATURATION. 10 20 30 40 50 60 70 80 90 100										
	10	20	30	40	50	60	70	80	90	100	
F.					Vapor pres	sure (inche	s).				
-30°	0.0007	0.0014	0.0021	0.0028	0.0035	0.0042	0.0049	0.0056	0.0063	0.0071	
20	.0007	.0015	.0022	.0030	.0037	.0045	.0052	.0060	.0067	.0075	
28 27	8000. 8000.	.0016	.0024	.0032	.0040	.0048	.0056	.0064	.0072	.0080	
26	.0009	.0018	.0027	.0036	.0045	.0054	.0063	.0072	.0081	.0090	
-25	0.0010	0.0019	0.0029	0.0038	0.0048	0.0057	0.0067	0.0076	0.0086	0.0095	
24	.0010	.0020	.0030	.0040	.0050	.0060	.0071	.0081	.0091	1010.	
23	.0011	.0021	.0032	.0043	.0053	.0064	.0075	.0086	.0096	.0107	
22 2I	.0011	.0023	.0034	.0045	.0057	.0068	.0079	.0091	.0102	.0113	
-20	0.0013	0.0025	0,0038	0.0051	0.0064	0.0076	0.0080	0.0102	0.0114	0.0127	
19	.0013	.0027	.0040	.0054	.0067	.0081	.0094	.0108	.0121	.0135	
18	.0014	.0029	.0043	.0057	.0071	.0086	.0100	.0114	.0128	.0143	
17	.0015	.0030	.0045	.0060	.0076	.0091	.0106	.0121	.0136	.0151	
16	.0016	.0032	.0048	.0064	.0080	.0096	.0112	.0128	.0144	.0160	
-l5	0.0017	0.0034	0.0051	0.0068	0.0084	0.0101	0.0118	0.0135	0.0152	0.0169	
14	.0018	.0036	.0054	.0071	.0089	.0107	.0125	.0143	.0161 .0170	.0179	
12	.0020	.0040	.0060	.0080	.0100	.0120	.0132	.0150	.0170	.0200	
11	.0021	.0042	.0063	.0084	.0106	.0127	.0148	.0169	.0190	.0211	
-10	0.0022	0.0045	0.0067	0.0089	0.0112	0.0134	0.0156	0.0178	0.0201	0.0223	
9	.0024	.0047	.0071	.0094	.0118	.0141	.0165	.0188	.0212	.0236	
8	.0025	.0050	.0075	.0099	.0124	.0149	.0174	.0199	.0224	.0249	
7 6	.0026	.0053	.0079	.0105	.0131	.0158 .0166	.0184 .0194	.0210	.0236 .0240	.0263 .0277	
- 5	0.0020	0.0058	0.0088	0.0117	0.0146	0.0175	0.0205	0.0234	0.0263	0.0202	
4	.0031	.0062	.0093	.0123	.0154	.0185	.0216	.0247	.0278	.0308	
3	.0033	.0065	.0098	.0130	.0163	.0195	.0228	.0260	.0293	.0325	
2	.0034	.0069	.0103	.0137	.0171	.0206	.0240	.0274	.0309	.0343	
I	.0036	.0072	8010.	.0145	.0181	.0217	.0253	.0289	.0325	.0361	
±0	0.0038	0.0076	.0114	.0152	0.0190	0.0229	0.0267	0.0305	0.0343	0.0381	
1 2	.0042	.0085	.0127	.0160	.0211	.0241	.0206	.0321	.0361 .0380	.0401	
3	.0044	.0089	.0134	.0178	.0222	.0267	.0312	.0356	.0400	.0445	
4	.0047	.0094	.0141	.0187	.0234	.0281	.0328	.0375	.0422	.0468	
5	0.0049	0.0099	0.0148	0.0197	0.0247	0.0296	0.0345	0.0394	0.0444	0.0493	
6	.0052	.0104	.0156	.0208	.0259	.0311	.0363	.0415	.0467	.0519	
7 8	.0055	.0109	.0164	.0218	.0273 .0287	.0328	.0382 .0402	.0437	.0491	.0546	
9	.0057	.0115	.0172	.0230	.0302	.0344 .0362	.0402	.0459 .0483	.0517	.0574	
10	0.0063	0.0127	0.0190	0.0254	0.0317	0.0381	0.0444	0.0508	0.0571	0.0635	
11	.0067	.0133	.0200	.0267	.0334	.0400	.0467	.0534	.0600	.0667	
I 2	.0070	.0140	.0210	.0280	.0350	.0421	.0491	.0561	.0631	.0701	
13 14	.0074	.0147 .0155	.0221	.0295	.0368 .0387	.0442 .0464	.0515	.0589 .0619	.0663 .0696	.0736 .0773	
	0.0081	0.0162		0.0325	0.0406	0.0487	0.0568	0.0650	-		
1 5 16	.0085	.0170	.0256	.0341	.0426	.0512	.0597	.0682	.0767	.0812	
17	.0089	.0179	.0268	.0358	.0447	.0537	.0626	.0716	.0805	.0895	
18	.0094	.0188	.0282	.0376	.0470	.0563	.0657	.0751	.0845	.0939	
19	.0099	.0197	.0296	.0394	.0493	.0591	.0690	.0788	.0887	.0985	
20	0.0103	0.0207	0.0310	0.0413	0.0517	0.0620	0.0723	0.0827	0.0930	0.1033	

RELATIVE HUMIDITY. TEMPERATURES FAHRENHEIT.

Air Temper- ature.		F	ELATIVE	HUMIDI	TY, OR PI	ERCENTA	GE OF SA	TURATIO	N.	
	10	20	30	40	50	60	70	80	90	100
F.					Vapor pres	sure (inche	s).			
20°	0.010	0.021	0.031	0.041	0.052	0.062	0.072	0.083	0.093	0.103
21	.011	.022	.033	.043	.054	.065	.076	.087	.098	.108
22	.011 .012	.023	.034	.045	.057	.068	.080 .083	.001	.102 .107	.114
23 24	.012	.024	.036 .037	.048	.062	.071 .075	.087	.095	.112	.119
			0.039	_					_	
25 26	0.013 .014	0.026 .027	.041	0.052	0.065	0.078	.0092	0.105	.118	.137
27	.014	.020	.043	.057	.072	.086	.100	.115	.129	.143
28	.015	.030	.045	.oóo	.075	.090	.105	.120	.135	.150
29	.016	.c31	.047	.063	.079	.094	.110	.126	.142	.157
30	0.016	0.033	0.049	0.066	0.082	0.099	0.115	0.132	0.148	0.165
31	.017	.034	.052	.0 69	.086	.103	.121	.138	.155	.172
32	.018	.036	.054	.072	.000	.108	.126	-144	.162	.180
33 34	.019	.038 .039	.056 .059	.075 .078	.094 .098	.113 .117	.131 .137	.150 .156	.169 .176	.188
35	0,020	C.041	0.061	0.081	0.102	0.122	0.142	0.163	0.183	0.203
36	.021	.042	.064 .066	.085	.106	.127	.148	.169	.191	.212
37 38	.022	.044 .046	.060	.088	.110 .115	.132 .137	.154 .160	.176 .183	.198 .206	.220
39	.023	.048	.071	.095	.119	.143	.167	.103	.214	.238
40	0.025	0.050	0.074	0.099	0.124	0.149	0.173	0.198.	0.223	0.248
41	.026	.052 .054	.077 . 0 80	.103	.129	.155 .161	.180	.206	.232	.258
42	.027 .028	.054	.083	.107	.134 .139	.167	.187 .195	.214	.24I .250	.208
43 44	.029	.058	.087	.116	.145	.173	.202	.231	.260	.289
45	0.030	0.060	c.090	0.120	0.150	0.180	0.210	0.240	0.270	0.300
46	.031	.062 .065	.094	.125 .130	.156 .162	.187	.218	.250 .259	.281	.312
47 48	.032	.067	.101	.135	.168	.202	.236	.260	.292	.324
49	.035	.070	.105	.140	.175	.210	-245	.279	.314	-349
50	0.036	0.073	0.109	0.145	0.181	0.218	0.254	0.290	0.326	0.363
51	.038	.075	.113	.151	.188	.226	.263	.301	•339	.376
52 53	.039 .041	.078 .081	.117 .122	.156 .162	.195	.234	.273 .284	.312	.351 .365	.390 .405
54	.042	.084	.126	.168	.210	.252	.294	.336	.378	.420
55	0.044	0.087	0.131	0.174	0.218	0.262	0.305	0.349	0.392	0.436
56	.045	.000	.136	.181	.226	.271	.316	.362	.407	·452
57 58	.047 .040	.094	.141 .146	.187	.234	.281	.328	·375 ·389	.422 ·437	.469 .486
59	.050	.101	.151	.201	.252	.302	.340 .353	.403	·457	.504
60	0.052	0.104	0.157	0.200	0.261	0.313	0.365	0.418	0.470	0.522
61	.054	.108	.162	.216	.270	.325	•379	•433	.487	.541
62	.056 .058	.112 .116	.168 .174	.224	.280	.336 248	.392	.448 .464	.504 .522	.560 .580
63 64	.060	.120	.180	.232	.301	.348 .361	.406 .421	.481	.541	.601
65	0.062	0.125	0.187	0.249	0.311	0.374	0.436	0.498	0.560	0.623
66	.064	.129	.193	.258	.322	.387	.451	.516	.580	.645
67 68	.067 .060	.133	.200	.267	•334	.400 .415	.467 .484	-534	.601 .622	.667 .691
69	.009	.138	.207	.286	·345 ·358	.415	.500	·553 ·572	.644	.715
70	0.074	0.148	0.222	0.296	0.370	0.444	0.518	0.592	0.666	0.740
	0.0/4	0.140	0.222	0.290	0.370	J.444	0.310	0.392	5.500	0.740

RELATIVE HUMIDITY. TEMPERATURES FAHRENHEIT.

Air Temper- ature.]	RELATIVE	HUMIDI	TY, OR PI	ERCENTA	GE OF SA	TURATION	N.	
	10	20	30	40	50	60	70	80	90	100
F.					Vapor pres	sure (inches	i).	•		
70° 71 72 73 74	0.074 .077 .079 .082 .085	0.148 .153 .158 .164 .169	0.222 .230 .238 .246 .254	0.296 .306 .317 .328 -339	0.370 .383 .396 .410 .424	0.444 .459 .475 .491 .508	0.518 .536 .554 .573 .593	0.592 .612 .634 .655 .678	0.666 .689 .713 .737 .762	0.740 .766 .792 .819 .847
75 76 77 78 79	0.088 .091 .094 .097	0.175 .181 .187 .194 .200	0.263 .272 .281 .290 .300	0.350 .362 .374 .387 .400	0.438 .453 .468 .484 .500	c.526 .543 .562 .581 .600	0.613 .634 .655 .677	0.701 •724 •749 •774 •800	0.788 .815 .843 .871	0.876 .906 .936 .968
80 81 82 83 84	0.103 .107 .110 .114 .118	0.207 .214 .221 .228 .235	0.310 .320 .331 .342 .353	0.413 .427 .441 .456 .471	0.517 .534 .551 .570 588	0.620 .641 .662 .684 .706	0.723 .747 .772 .797 .824	0.827 .854 .882 .911	0.930 .961 .993 1.025 1.059	1.033 1.068 1.103 1.139 1.176
85 86 87 88 88 89	0.121 .125 .129 .134 .138	0.243 .251 .259 .267 .276	0.364 .376 .388 .401 .414	0.486 .502 .518 .535 .552	0.607 .627 .647 .668	0.729 .753 .777 .802 .828	0.850 .878 .906 .936 .966	0.972 1.003 1.036 1.069 1.104	1.093 1.129 1.165 1.203 1.241	1.215 1.254 1.295 1.336 1.379
90 91 92 93 94	0.142 .147 .152 .156 .161	0.285 .294 .303 .313 .322	0.427 .441 .455 .469 .484	0.569 .588 .606 .625	0.712 •734 •758 •782 •806	0.854 .881 .909 .938 .967	0.996 1.028 1.061 1.094 1.128	1.139 1.175 1.212 1.250 1.290	1.281 1.322 1.364 1.407 1.451	1.423 1.469 1.515 1.563 1.612
95 96 97 98 99	0.166 .171 .177 .182 .188	•343 •353 •364 •376	0.499 .514 .530 .547 .563	0.665 .686 .707 .729	0.831 .857 .884 .911	0.998 1.029 1.060 1.093 1.127	1.164 1.200 1.237 1.275 1.315	1.330 1.371 1.414 1.458 1.502	1.496 1.543 1.591 1.640 1.690	1.662 1.714 1.767 1.822 1.878
100 101 102 103 104	0.194 .199 .206 .212 .218	0.387 •399 •411 •423 •436	0.581 .598 .616 .635	0.774 .798 .822 .847 .872	0.968 •997 1.028 1.059 1.090	1.161 1.197 1.233 1.270 1.309	1.355 1.396 1.438 1.482 1.527	1.548 1.596 1.644 1.694	1.742 1.795 1.850 1.905 1.963	1.936 1.994 2.055 2.117 2.181
105 106 107 108 109	0.225 .231 .238 .245 .253	0.449 .463 .476 .491	0.674 .694 .715 .736 .758	0.899 .925 .953 .981 1.010	1.123 1.157 1.191 1.226 1.263	1.348 1.388 1.429 1.472 1.515	1.572 1.619 1.668 1.717 1.768	1.797 1.851 1.906 1.962 2.020	2.022 2.082 2.144 2.208 2.273	2.246 2.314 2.382 2.453 2.525
110 111 112 113 114	0.260 .268 .275 .283 .292	0.520 •535 •551 •567 •583	0.780 .803 .826 .850 .875	1.040 1.070 1.101 1.133 1.166	1.300 1.338 1.377 1.417 1.458	1.560 1.605 1.652 1.700 1.749	1.820 1.873 1.927 1.983 2.041	2.080 2.140 2.203 2.267 2.332	2.339 2.408 2.478 2.550 2.624	2.599 2.676 2.754 2.833 2.915
115 116 117 118 119	0.300 .309 .317 .326 .336	0.600 .617 .635 .653	0.900 .926 .952 .979 I.007	1.200 1.234 1.269 1.305 1.342	1.500 1.543 1.587 1.632 1.678	1.800 1.851 1.904 1.958 2.014	2.100 2.160 2.221 2.285 2.349	2.399 2.468 2.539 2.611 2.685	2.699 2.777 2.856 2.937 3.021	2.999 3.085 3.173 3.264 3.356
120	0.345	0.690	1.035	1.380	1.725	2.071	2.416	2.761	3.106	3.45 1

REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

METRIC MEASURES.

Values of e = e' - 0.000660 B (t - t') (1 + 0.00115 t')

Temper- ature.				PRESS	URE OF	AQUEOU	JS VAPO	OR, e.				
	0	1	2	3	4	5	·	6	7	8	9	
G.	mm.	mm.	mm.	mm.	mm.	mn		nm.	mm.	mm,	mm.	
-50° 40 30	0.029 0.096 0.288	0.026 0.086 0.259	0.023 0.076 0.233	0.020	0.06	0.0	54 0.	.048 0	0.012	0.010 0.037 0.121	o.oog o.o33 o.1o8	
	.1		e = e'	- 0.0006	660 B (t	-t') (1	1 + 0.00	115 t')				
				E	3 = 760	mm.						
t'						t-t'		r				
	.0 .1 .2 .3 .4 .5 .6 .7 .8 .9 1.0											
c. -30°	mm, $\Delta e imes \Delta B$											
-30°	0.288	0.239	0.191	0.143 .174 .208	0.094 .125 .160	0.046 .077	0.028 .063	0.014				
27 26	·354 ·392 ·434	.306 .344 .385	.257 .295 -337	.246	.198	.149	.101	.052				
-25 24 23 22 21	0.480 .530 .585 .646	0.431 .482 .537 .597	0.383 •433 •488 •548 •614	0.334 .384 .439 .499 .565	0.285 •335 •390 •450 •516	0.236 .286 .341 .401	0.188 .238 .292 .352 .418	0.139 .189 .244 .303 .369	0.090 .140 .195 .254	.091 .146 .206	0.043 .097 .157	
-20 19 18 17 16	0.783 .862 .947 1.041	0.734 .813 .898 .991 1.093	0.685 .764 .849 .942 1.044	0.636 .715 .800 .893	0.587 .666 .751 .844	0.538 .616 .702 .795 .896	0.489 .567 .653 .746 .847	0.440 .518 .604 .696		.420 .505 .598	0.293 .371 .456 .549 .650	
-15 14 13 12 11	1.252 1.373 1.503 1.644 1.798	1.203 1.323 1.453 1.595 1.748	1.154 1.274 1.404 1.545 1.699	1.105 1.225 1.355 1.496 1.649	1.055 1.175 1.305 1.447 1.600	1.006 1.126 1.256 1.397 1.550	0.957 1.076 1.206 1.348 1.501	1.027	0.858 .978 1.108 1.249 1.402	.928	0.760 .879 1.009 1.150 1.303	
-10 9 8 7 6	1.964 2.144 2.340 2.550 2.778	1.915 2.095 2.290 2.501 2.729	1.865 2.045 2.240 2.451 2.679	1.816 1.996 2.190 2.401 2.629	1.766 1.946 2.141 2.351 2.579	1.716 1.896 2.091 2.302 2.529	1.667 1.847 2.041 2.252 2.480	1.617 1.797 1.992 2.202 2.430	1.568 1.747 1.942 2.152 2.380	1.518 1.698 1.892 2.103 2.330	1.468 1.648 1.843 2.053 2.280	
-5 -5	3.025 Δe×ΔB	2.975 +0.007	2.925 +0.013	2.875 +0.020	2.825 +0.026	2.775 +0.033	2.726 +0.039	2.676 +0.046	2.626 +0.052	2.576 +0.059	2.526 +0.066	

Values of e = e' - 0.000660 B (t - t') (1 + 0.00115 t')

B = 760 mm.

					B = 700						
<i>t</i>						t-t'					
	0.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0
C. -20°	mm. Δe×ΔB	mm. +0.071	mm. +0.077	mm. +0.084	mm. +0.090	mm. +0.097	mm. +0.103	mm. +0.110	mm. +0.116	mm. +0.123	mm. +0.129
-25° 24 23 22 21	0.480 .530 .585 .646 .712	0.048 .108 .173	0.059	0.010							
-20 19 18 17 16	.783 .862 .947 1.041	.244 .322 .407 .500	.273 .358 .450	.146 .224 .309 .401	.097 * .175 .260 -352 -453	0.048 .126 .211 .303	0.077 .161 .254 .354	.112	0.063 .155 .256	0.014 .106 .207	0.057 .157
-15 14 13 12 11	1.252 1.373 1.503 1.644 1.798	.710 .830 .959 1.100	.910	.612 .731 .861 1.001	.562 .682 .811 .952 1.105	.513 .632 .762 .902	.464 .583 .712 .853 1.005	.414 .534 .663 .803	.365 .484 .614 .754 .906	.316 •435 •564 •705	.267 .386 .515 .655
-10 9 8 7 6	+1.964 2.144 2.340 2.550 2.778	1.419 1.598 1.793 2.003 2.231	1.743	1.320 1.499 1.693 1.904 2.131	1.270 1.450 1.644 1.854 2.081	1.400 1.594 1.804	1.171 1.350 1.544 1.754 1.981	1.495 1.705	1.072 1.251 1.445 1.655 1.882	1.022 1.201 1.395 1.605 1.832	.973 1.152 1.346 1.555 1.782
-5	3.025	2.476	2.426	2.376	2.327	2.277	2.227	2.177	2.127	2.077	2.027
-5	$\Delta e \times \Delta B$	+0.072	+0.079	+0.085	+0.092	+0.098	+0.105	+0.112	+0.118	+0.125	+0.131
						t-t'					
t'	0.0	2.1	2.2	2.3	2,4	2.5	2.6	2.7	2.8	2.9	3.0
C. -15°	mm. $\Delta e \times \Delta B$	mm. +0.136	mm. +0.143	mm. +0.149	mm. +0.156	mm. +0.162	mm. +0.169	mm. +0.175	mm. +0.182	mm. +0.188	mm. +0.195
-17°	1.041 1.142	0.008 0.108	0.059	0.010							
-I5 14 13 12	1.252 1.373 1.503 1.644 1.798	0.217 .336 .465 .606 .758	.168 .287 .416 .556 .708	.119 .237 .366 .507	0.069 .188 .317 .457 .609	0.020 .139 .268 .408 .560	0.089 .218 .358 .510	0.040 .169 .309 .461	0.119 .259 .411	0.070 .210 .362	0.021 .160 .312
- IO 9 8 7 6	1.964 2.144 2.340 2.550 2.778	.923 1.102 1.296 1.506 1.732	.873 1.052 1.246 1.456 1.683	.824 1.003 1.196 1.406 1.633	.774 .953 1.147 1.356 1.583	.725 .903 1.097 1.307	.675 .854 1.047 1.257 1.483	.626 .804 .998 1.207	.576 .755 .948 1.157 1.384	.526 .705 .898 1.108 1.334	.477 .655 .849 1.058
- 5 - 5	3.025 Δe×ΔB	1.977 +0.138	1.928 +0.144	1.878 +0.151	1.828 +0.157	1.778 +0.164	1.728 +0.171	1.678 +0.177	1.628 +0.184	1.579 +0.190	1.529 +0.197

TABLE 77.

Values of e=e'-0.000660 B (t-t') (1 + 0.00115 t')B=760 mm.

	D 700 IIII.									
t'					t	- t'		-		
	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	4.0
C. −10° Δe×ΔB	mm. +0.202	mm. +0.209	mm. +0.215	mm. +0.222	mm, +0.228	mm. +0.235	mm. +0.241	mm. +0.248	mm. +0.254	mm. +0.261
-I2°	0.111 .263	0.061	0.012 .164	0.114	0.065	0.015				
- IO 9 8 7 6	.427 .606 .799 1.008 1.234	.378 .556 .749 .958 1.184	.328 .506 .699 909	.278 .457 .650 .859	.229 .407 .690 .809	.179 •357 •550 •759 •985	.308 .501 .710	.258 .451 .660	.209 .401 .610	0.159 •352 •560 •786
−5 −5 Δe×ΔB	1.479 +0.203	1.429 +0.210	1.379	1.329	1.279 +0.230	1.229 +0.236		1.130 +0.249		1.030
t'		 			t-	- t'				
	4.1	4.2	4.3	4.4	4.5	4.6	4.7	4.8	4.9	5.0
$\begin{array}{ c c } & \textbf{C.} \\ & -8^{\circ} \ \Delta e \times \Delta B \end{array}$	mm. +0.268	mm. +0.275	mm, +0.281	mm. +0.288	mm. +0.294	mm. +0.301	mm. +0.307	mm. +0.314	mm. +0.320	mm. +0.327
-9° 8 7 6	0.109 0.302 .510 .736	0.060 0.252 .461 .686	0.010 .202 .411 .637	0.153 .361 .587	0.103 .311 .537	0.053 .262 .487	0.004 .212 ·437	0.162 .387	0.112 •338	0.063 .288
-5	0.980	0.930	0.880	0.830	0.781	0.731	0.681	0.631	0.581	0.531
-5 Δe×ΔB	+0.269	+0.276	+0.282	+0.289	+0.295	+0.302	+0.308	+0.315	+0.322	+0.328
t'					<i>t</i> -	- <i>t</i> ′				
	5.1	5.2	5.3	5-4	5.5	5.6	5.7	5.8	5.9	6.0
C, 7° 6	mm. 0.013	mm. 0.188	mm.	mm. 0.089	mm. 0.039	mm.	mm,	mm.	mm.	mm.
-5	0.481	0.431	0.382	0.332	0.282	0.232	0.182	0.132	0.082	0.033
-5 Δe×ΔB	+0.335	+0.341	+0.348	+0.354	+0.361	+0.367	+0.374	+0.381	+0.387	+0.394

Values of e = e' - 0.000660 B (t - t') (1 + 0.00115 t')

B = 760 mm.

1'	· · · · · · · · · · · · · · · · · · ·					t-t'					
	0	1	2	3	4	5	6	7	8	9	10
C	mm,	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
-5° -5°	$\Delta e \times \Delta B$	+0.07	+0.13	+0.20	+0.26	+0.33	+0.39	+0.46	+0.52	+0.59	+0.66
4	3.02 3.29	2.53 2.79	2.03	1.53 1.79	1.03	0.53	0.03				
3	3.58	3.08	2.58	2.08	1.58	1.08	0.58	0.08		ļ	
2 1	3.89 4.22	3.39 3.72	2.89 3.22	2.39 2.72	2.22	1.38 1.71	0.88	0.38	0.21		
±ο	4.58	4.08	3.58	3.08	2.57	2.07	1.57	1.07	0.57	0.07	
+1	4.92	4.42	3.92	3.42	2.92	2.41	1.91	1.41	0.91	0.40	
3	5.29 5.68	4.79 5.18	4.29 4.68	3.78 4.17	3.28 3.67	2.78 3.17	2.27	1.77 2.16	1.27 1.66	0.77 1.15	0.26
4	6.10	5.59	5.09	4-59	4.08	3.58	3.07	2.57	2.07	1.56	1.06
5 6	6.54	6.03 6.51	5.53 6.00	5.03	4.52	4.02	3.51	3.01	2.51	2.00	1.50
7 8	7.01 7.51	7.01	6.50	5.50 6.00	4.99 5.49	4.49 4.98	3.98 4.48	3.48 3.97	2.97 3.47	2.47 2.96	1.96 2.46
	8.05 8.61	7.54	7.03	6.53	6.02	5.51	5.01	4.50	4.00	3.49	2.98
9 10	9.21	8.10	7.60 8.20	7.69 7.69	6.58 7.18	6.08 6.67	5·57 6.17	5.66 5.66	4.56 5.15	4.05 4.64	3·54 4·14
11	9.85	9-34	8.83	8.32	7.81	7.31	6.80	6.29	5.78	5.27	4.77
12 13	10.52 11.24	10.01	9.50	9.00 9.71	8.49. 9.20	7.98 8.60	7.47 8.18	6.96 7.67	6.45 7. 1 6	5.94 6.65	5.44 6.14
14	11.99	11.48	10.97	10.46	9.95	9.44	8.93	8.42	7.91	7.41	6.90
15 16	12.79 13.64	12.28	11.77	11.26	10.75 11.60	10.24	9·73 10.58	9.22	8.71	8.20	7.69
17	14.54	14.03	13.52	13.00	12.49	11.09	11.47	10.07	9.56 10.45	9.04 9.94	8.53 9.42
18	15.49 16.49	14.98 15.98	14.46 15.46	13.95 14.95	13.44	12.93	12.42	11.90	11.39	10.88	10.37
19 20	17.55	17.03	16.52	16.01	14.44 15.50	13.93 14.98	13.41 14.47	13.96	12.39 13.44	11.88	11.36
21	18.66	18.15	17.64 18.82	17.12	16.61	16.10	15.58	15.07	14.56	14.04	13.53
22 23	19.84 21.09	19.33	20.06	18.30	17.79 19.03	17.27	16.76 18.00	16.24 17.48	15.73 16.97	15.22 16.45	14.70
24	22.40	21.88	21.37	20.85	20.34	19.82	19.31 20.68	18.79	18.27	17.76	17.24
²⁵ 26	23.78 25.24	23.26	22.75	22.23	21.72	21.20	22.14	20.17	19.65	20.59	18.62
27	26.77	26.25	25.73	25.22	24.70	24.18	23.66	23.15	22.63	22.11	21.60
28 29	28.38 30.08	27.86 29.56	27.34	26.83 28.52	26.31 28.00	25.79 27.48	25.27 26.97	24.76 26.45	24.24	23.72 25.41	23.20
30	31.86	31.34	30.82	30.30	29.78	29.27	28.75	28.23	27.71	27.19	26.67
31	33.74	33.22	32.70	32.18	31.66	31.14	30.62	30.10	29.58	29.06	28.54
32 33	35.70 37.78	35.18 37.25	34.66 36.73	34.14 36.21	33.62 35.69	33.10	32.58 34.65	32.06	31.54 33.61	31.02 33.09	30.50 32.57
34	39.95	39-43	38.90	38.38	37.86	37.34	36.82	36.30	35.78	35.26	34.73
35 36	42.23	41.71	41.18	40.66	40.14	39.62 42.01	39.10 41.48	38.57 40.06	38.05	37·53 39·92	37.01 39.40
37	47.13	46.60	46.08	45.56	45.04	44.51	43.99	43.47	42.94	42.42	41.90
38 39	49.76 52.51	49·23 51·99	48.71	48.19 50.94	47.66 50.41	47.14 49.89	46.61 49.37	46.09 48.84	45.57 48.32	45.04 47.79	44.52 47.27
39 40	55.40	54.87	54.35	53.82	53.30	52.77	52.25	51.72	51.20	50.67	50.15
41	58.42	57.89	57.37	56.84 60.00	56.32	55.79	55.27	54.74	54.21	53.69	53.16
42 43	61.58 64.89	61.05 64.36	60.53 63.84	63.31	59.48 62.78	58.95 62.26	58.43 61.73	57.90 61.20	57-37 60.68	56.85 60.15	56.32 59.62
44	68.35	67.82	67.30	66.77	66.24	65.72	65.19	64.66	64.13	63.61	63.08
45 45	71.97 Δe×ΔB	71.44 +0.07	70.91	70.39 +0.21	69.86	69. 3 3 +0. 3 5	68.80 +0.42	68.28 +0.49	67.75 +0.56	67.22 +0.62	66.69 +0.60
45		+0.07	T♥•14	∓0.21		T-0.35	T∪.42	₹9.49	+0.50	70.02	+0.09

Values of $e = e' - 0.000660 \ B \ (t - t') \ (1 + 0.00115 \ t')$ $B = 760 \ \mathrm{mm}.$

) = 700						
ť						t-t'					
	О	11	12	13	14	15	16	17	18	19	20
C. +5°	mm. $\Delta e \times \Delta B$	mm. +0.73	mm. +0.80	mm, +0.86	mm. +0.93	mm. +1.00	mm. +1.06	mm. +1.13	mm. +1.19	mm. +1.26	mm. +1.33
+3° 4 5	5.68 6.10 6.54	0.15 0.56 0. 99	0.05 0.49								
6 7 8 9 10	7.01 7.51 8.05 8.61 9.21	1.46 1.95 2.48 3.04 3.63	0.95 1.45 1.97 2.53 3.12	0.45 0.94 1.46 2.02 2.61	0.43 0.96 1.52 2.11	0.45 1.01 1.60	0.50 1.09	0. 58	0.08		
II 12 13 14 15	9.85 10.52 11.24 11.99 12.79	4.26 4.93 5.63 6.39 7.18	3.75 4.42 5.13 5.88 6.67	3.24 3.91 4.62 5.37 6.16	2.73 3.40 4.11 4.86 5.65	2.23 2.89 3.60 4.35 5.14	1.72 2.38 3.09 3.84 4.63	1.21 1.88 2.58 3.33 4.12	0.70 1.37 2.07 2.82 3.61	0.20 0.86 1.56 2.31 3.10	0.35 1.05 1.80 2.59
16 17 18 19 20	13.64 14.54 15.49 16.49 17.55	8.02 8.91 9.86 10.85 11.90	10.34	7.00 7.89 8.83 9.83 10.88	6.49 7.38 8.32 9.31 10.36	5.98 6.87 7.81 8.80 9.85	5.47 6.36 7.30 8.29 9.34	4.96 5.85 6.78 7.78 8.82	4.45 5.33 6.27 7.26 8.31	3.94 4.82 5.76 6.75 7.80	3.43 4.31 5.25 6.24 7.29
2! 22 23 24 25	18.66 19.84 21.09 22.40 23.78	13.01 14.19 15.42 16.73 18.10	14.91 16.21	11.99 13.16 14.39 15.70	11.47 12.64 13.88 15.18 16.56	10.96 12.13 13.36 14.67 16.04	10.45 11.62 12.85 14.15 15.52	9.93 11.10 12.33 13.64 15.01	9.42 10.59 11.82 13.12 14.49	8.90 10.07 11.30 12.60 13.98	8.39 9.56 10.79 12.09 13.46
26 27 28 29 30	25.24 26.77 28.38 30.08 31.86	19.55 21.08 22.68 24.37 26.15	19.04 20.56 22.17 23.86 25.63	18.52 20.04 21.65 23.34 25.11		17.49 19.01 20.61 22.30 24.08	16.97 18.49 20.10 21.78 23.56	16.45 17.98 19.58 21.26 23.04	15.94 17.46 19.06 20.75 22.52	15.42 16.94 18.54 20.23 22.00	14.90 16.42 18.02 19.71 21.48
31 32 33 34 35	33.74 35.70 37.78 39.95 42.23	28.02 29.98 32.05 34.21 36.49	31.53 33.69	26.98 28.94 31.01 33.17 35.44	28.42 30.49 32.65	25.94 27.90 29.97 32.13 34.40	25.42 27.38 29.44 31.61 33.88	24.90 26.86 28.92 31.09 33.36	24.38 26.34 28.40 30.57 32.83	23.86 25.82 27.88 30.04 32.31	23.34 25.30 27.36 29.52 31.79
36 37 38 39 40	44.62 47.13 49.76 52.51 55.40	38.87 41.37 44.00 46.74 49.62	46.22	37.83 40.33 42.95 45.70 48.58	45.17	36.78 39.28 41.90 44.65 47.53	36.26 38.76 41.38 44.12 47.00	35.74 38.24 40.86 43.60 46.48	35.22 37.71 40.33 43.08 45.95	34.69 37.19 39.81 42.55 45.43	34.17 36.67 39.29 42.03 44.90
41 42 43 44 45	58.42 61.58 64.89 68.35 71.97	52.64 55.80 59.10 62.55 66.16	55.27	51.59 54.74 58.05 61.50 65.11	54.22 57.52 60.97	50.54 53.69 56.99 60.45 64.05	50.01 53.17 56.47 59.92 63.53	49.49 52.64 55.94 59.39 63.00	48.96 52.12 55.41 58.86 62.47	48.44 51.59 54.89 58.34 61.94	47.91 51.06 54.36 57.81 61.42
45	$\Delta e \times \Delta B$	+0.76	+0.83	+0.90	+0.97	+1.04	+1.11	+1.18	+1.25	+1.32	+1.39

Values of $e = e' - 0.000660 \ B \ (t - t') \ (1 + 0.00115 \ t')$ $B = 760 \ \mathrm{mm}.$

					700						
t'						t-t'					
	0	21	22	23	24	25	26	27	28	29	30
C.	mm.	mm.	mm,	mm.	mm.						
+15°	$\Delta e \times \Delta B$			+0.154	+0.161	+0.168	+0.175	+0.181	+0.188	+0.195	+0.201
13°	11.24 11.99	1.29	0.03	0.27		1			1		,
15	12.79	2.08	1.57	1.06	p.55	0.04					
+16	13.64	2.01	2.40	1.89	1.38	0.87	0.36				
17 18	14.54 15.49	3.80 4.74	3.29 4.22	2.78 3.71	2.27 3.20	1.75 2.69	2.18	0.73	0.22	0.64	0.13
19	16.49	5.73	5.21	4.70	4.19	3.68	3.16	2.65	2.14	1.62	1.11
20	17.55	6.77	6.26	5.75	5.23	4.72	4.21	3.69	3.18	2.67	2.15
+2I	18.66 19.84	7.88	7.36 8.53	6.85 8.02	6.34 7.50	5.82 6.99	5.31 6.47	4.79 5.96	4.28 5.44	3.77 4.93	3.25 4.42
23	21.09	10.27	9.76	9.25	8.73	8.22	7.70	7.19	6.67	6.16	5.64
24 25	22.40 23.78	11.57	11.06	10.54	10.03	9.51 10.88	9.00 10.36	8.48 9.85	7.97 9.33	7·45 8.82	6.93 8.30
+26	25.24	14.39	13.87	13.35	12.84	12.32	11.80	11.20	10.77	10.25	0.74
27	26.77	15.91	15.39	14.87	14.35	13.84	13.32	12.80	12.20	11.77	11.25
28 20	28.38 30.08	17.51	16.99	16.47	15.95 17.64	15.44 17.12	14.92 16.60	14.40 16.08	13.88	13.37	12.85
3ó	31.86	20.96	20.44	19.93	19.41	18.89	18.37	17.85	17.33	16.81	16.29
+31	33.74	22.83	22.31	21.79	21.27	20.75	.20.23	19.71	19.19	18.67	18.15
32	35.70 37.78	24.78 26.84	24.26 26.32	23.74 25.80	23.22 25.28	22.70 24.76	22.18	21.66	21.14	20.62	20.10 22.16
34	39.95	29.00	28.48	27.96	27.44	26.92	26.40	25.87	25.35	24.83	24.31
35	42.23	31.27	30.75	30.23	29.70	29.18	28.66	28.14	27.62	27.10	26.57
+36 37	44.62 47.13	33.65 36.15	33.13 35.62	32.60 35.10	32.08 34.58	31.56 34.05	31.04 33.53	30.52 33.01	29.99 32.48	29.47 31.96	28.95 31.44
38	49.76	38.76	38.24	37.72	37.19	36.67	36.14	35.62	35.10	34.57	34.05
39 40	52.51 55.40	41.50	40.98 43.85	40.46 43.33	39.93 42.80	39.41 42.28	38.88 41.75	38.36 41.23	37.84 40.71	37.31 40.18	36.79 39.66
+40	$\Delta e \times \Delta B$								+0.193		
			'		-		-				
ť						t-t'	,				
		31	32	33	34	35		37	38	39	40
C.	$\Delta e \times \Delta B$	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
+20°	ΔεχΔΒ			+0.223	+0.230	+0.230	+0.243	+0.250	+0.257	+0.203	+0.270
20		0.60 1.64	0.09	0.61	0.10						
- 21		2.74	2.23	1.71	1.20	0.69	0.17				
22		3.90	3·39 4.61	2.87	2.36	1.84 3.07	1.33	0.82	0.30	1.01	0.40
23 24		5.13 6.42	5.90	4.10 5.39	3.58 4.87	4.36	2.55 3.84	3.33	1.52 2.81	2.30	0.49 1.78
25		7.78	7.27	6.75	6.24	5.72	5.20	4.69	4.17	3.66	3.14
+26		9.22	8.70 10.22	8.19	7.67	7.15 8.67	6.64	6.12	5.60	5.09 6.60	4.57 6.08
27 28		10.73	11.81	9.70 11.29	9.18 10.78	10.26	8.15 9.74	7.63 9.22	7.11 8.71	8.19	7.67
29		14.01	13.49	12.97	12.45	11.93	11.42	10.00	10.38	9.86	9.34
30 + 30	$\Delta e \times \Delta B$	15.77	15.26	14.74	14.22	13.70	13.18	12.66	12.14	11.62 ±0.266	11.10
T30		70.212	70.210	₩-0.225	⊤0.232	T0.239	T0.240	~ 0.253	+0.259	₩,200	+0.273

RELATIVE HUMIDITY. TEMPERATURE CENTIGRADE.

_ Air		R	ELATIVE	HUMIDI	Y, OR PE	RCENTAC	GE OF SA	T URATIO	4.	
Temper- ature.	10	20	30	40	50	60	70	80	90	100
G.				Vap	or pressure	(millimete	rs).			
-45° , 44 , 43 , 42 , 41	0.01 0.01 0.01 0.01	0.0I 0.0I 0.0I 0.02 0.02	0. 02 0. 02 0. 02 0. 02 0. 02	0.02 0.02 0.03 0.03 0.03	o. c3 o. o3 o. o3 o. o4 o. o4	0.03 0.04 0.04 0.05 0.05	0.04 0.04 0.05 0.05 0.06	0.04 0.05 0.05 0.06 0.07	0.05 0.05 0.06 0.07 0.08	0.05 0.06 0.07 0.08 0.09
-40 39 38 37 36	0.0I 0.0I 0.0I 0.0I 0.02	0. 02 0. 02 0. 02 0. 03 0. 03	0.03 0.03 0.04 0.04 0.05	0.04 0.04 0.05 0.05 0.06	0.05 0.05 0.06 0.07 0.08	o. o6 o. o6 o. o7 o. o8 o. o9	0.07 0.08 0.08 0.09 0.11	0.08 0.09 0.10 0.11	0.09 0.10 0.11 0.12 0.14	0. 10 0. 11 0. 12 0. 14 0. 15
-35 34 33 32 31	0.02 0.02 0.02 0.02 0.03	0. 03 0. 04 0. 04 0. 05 0. 05	o. o5 o. o6 o. o6 o. o7 o. o8	0.07 0.08 0.08 0.09 0.10	0.08 0.09 0.10 0.12 0.13	0. I0 0. I1 0. I3 0. I4 0. I6	0.12 0.13 0.15 0.16 0.18	0.13 0.15 0.17 0.19 0.21	0. 15 0. 17 0. 19 0. 21 0. 23	0.17 0.19 0.21 0.23 0.26
-30 29 28 27 26	0.03 0.03 0.04 0.04 0.04	o. o6 o. o6 o. o7 o. o8 o. o9	0.09 0.10 0.11 0.12 0.13	0. 12 0. 13 0. 14 0. 16 0. 17	0. 14 0. 16 0. 18 0. 20 0. 22	0. 17 0. 19 0. 21 0. 24 0. 26	0. 20 0. 22 0. 25 0. 27 0. 30	0. 23 0. 26 0. 28 0. 31 0. 35	0. 26 0. 29 0. 32 0. 35 0. 39	0. 29 0. 32 0. 35 0. 39 0. 43
-25 24 23 22 21	0.05 0.05 0.06 0.06	0. 10 0. 11 0. 12 0. 13 0. 14	0. 14 0. 16 0. 18 0. 19 0. 21	0. 19 0. 21 0. 23 0. 26 0. 28	0. 24 0. 27 0. 29 0. 32 0. 36	0. 29 0. 32 0. 35 0. 39 0. 43	0.34 0.37 0.41 0.45 0.50	0. 38 0. 42 0. 47 0. 52 0. 57	0. 43 0. 48 0. 53 0. 58 0. 64	0.48 0.53 0.59 0.65 0.71
-20 19 18 17 16	0.08 0.09 0.09 0.10 0.11	0. 16 0. 17 0. 19 0. 21 0. 23	0. 24 0. 26 0. 28 0. 31 0. 34	0. 31 0. 34 0. 38 0. 42 0. 46	0. 39 0. 43 0. 47 0. 52 0. 57	0.47 0.52 0.57 0.62 0.69	o. 55 o. 60 o. 66 o. 73 o. 80	o. 63 o. 69 o. 76 o. 83 o. 91	0.71 0.78 0.85 0.94 1.03	0.78 0.86 0.95 1.04 1.14
- 15 14 13 12 11	0.13 0.14 0.15 0.16 0.18	o. 25 o. 27 o. 30 o. 33 o. 36	0. 38 0. 41 0. 45 0. 49 0. 54	0. 50 0. 55 0. 60 0. 66 0. 72	o. 63 o. 69 o. 75 o. 82 o. 90	0.75 0.82 0.90 0.99 1.08	0.88 0.96 1.05 1.15 1.26	1.00 1.10 1.20 1.32 1.44	1.13 1.24 1.35 1.48 1.62	1.25 1.37 1.50 1.64 1.80
- 10 9 8 7 6	0. 20 0. 21 0. 23 0. 26 0. 28	0. 39 0. 43 0. 47 0. 51 0. 56	0. 59 0. 64 0. 70 0. 77 0. 83	0.79 0.86 0.94 1.02 1.11	0.98 1.07 1.17 1.28 1.39	1.18 1.29 1.40 1.53 1.67	1.38 1.50 1.64 1.79 1.94	1.57 1.72 1.87 2.04 2.22	1.77 1.93 2.11 2.30 2.50	1.96 2.14 2.34 2.55 2.78
- 5 4 3 2 1	0.30 0.33 0.36 0.39 0.42	o. 60 o. 66 o. 72 o. 78 o. 84	0.91 0.99 1.07 1.17 1.27	1. 21 1. 32 1. 43 1. 55 1. 69	1.51 1.65 1.79 1.94 2.11	1.81 1.97 2.15 2.33 2.53	2.12 2.30 2.50 2.72 2.95	2.42 2.63 2.86 3.11 3.38	2.72 2.96 3.22 3.50 3.80	3. 29 3. 58 3. 89 4. 22
± 0 + 1 2 3 4	0.46 0.49 0.53 0.57 0.61	0.92 0.98 1.06 1.14 1.22	1.37 1.48 1.59 1.70 1.83	1.83 1.97 2.12 2.27 2.44	2. 29 2. 46 2. 65 2. 84 3. 05	2.75 2.95 3.17 3.41 3.66	3.21 3.45 3.70 3.98 4.27	3.66 3.94 4.23 4.55 4.88	4. 12 4. 43 4. 76 5. 11 5. 49	4. 58 4. 92 5. 29 5. 68 6. 10
+ 5	0.65	1.31	1.96	2.62	3.27	3.92	4.58	5.23	5.89	6. 54

RELATIVE HUMIDITY. TEMPERATURE CENTIGRADE.

Air Temper- ature.			RELATIV	E HUMID	ITY, OR	PERCENT	AGE OF	SATURAT	ion.	
	10	20	30	40	50	60	70	80	90	100
C.				Vapor p	ressure (m	illimeters).				
5° 6 7 8	0.7 0.7 0.8 0.8 0.9	1.3 1.4 1.5 1.6	2.0 2.1 2.3 2.4 2.6	2.6 2.8 3.0 3.2 3.4	3.3 3.5 3.8 4.0 4.3	3.9 4.2 4.5 4.8 5.2	4.6 4.9 5.3 5.6 6.0	5.2 5.6 6.0 6.4 6.9	5.9 6.3 6.8 7.2 7.7	6.5 7.0 7.5 8.0 8.6
10 11 12 13 14	0.9 1.0 1.1 1.1	1.8 2.0 2.1 2.2 2.4	2.8 3.0 3.2 3.4 3.6	3.7 3.9 4.2 4.5 4.8	4.6 4.9 5.3 5.6 6.0	5·5 5·9 6·3 6·7 7·2	6.4 6.9 7.4 7.9 8.4	7·4 7·9 8·4 9·0 9·6	8.3 8.9 9.5 10.1 10.8	9. 2 9. 8 10. 5 11. 2 12. 0
15 16 17 18 19	1.3 1.4 1.5 1.5	2.6 2.7 2.9 3.1 3.3	3.8 4.1 4.4 4.6 4.9	5. I 5. 5 5. 8 6. 2 6. 6	6.4 6.8 7.3 7.7 8.2	7.7 8.2 8.7 9.3 9.9	9.0 9.5 10.2 10.8 11.5	10. 2 10. 9 11. 6 12. 4 13. 2	11.5 12.3 13.1 13.9 14.8	12.8 13.6 14.5 15.5 16.5
20 21 22 23 24	1.8 1.9 2.0 2.1 2.2	3.5 3.7 4.0 4.2 4.5	5.3 5.6 6.0 6.3 6.7	7.0 7.5 7.9 8.4 9.0	8.8 9.3 9.9 10.5	10.5 11.2 11.9 12.7 13.4	12.3 13.1 13.9 14.8 15.7	14.0 14.9 15.9 16.9	15.8 16.8 17.9 19.0 20.2	17.5 18.7 19.8 21.1
25 26 27 28 29	2.4 2.5 2.7 2.8 3.0	4.8 5.0 5.4 5.7 6.0	7.1 7.6 8.0 8.5 9.0	9.5 10.1 10.7 11.4 12.0	11.9 12.6 13.4 14.2 15.0	14.3 15.1 16.1 17.0 18.0	16.6 17.7 18.7 19.9 21.1	19.0 20.2 21.4 22.7 24.1	21.4 22.7 24.1 25.5 27.1	23.8 25.2 26.8 28.4 30.1
30 31 32 33 34	3.2 3.4 3.6 3.8 4.0	6.4 6.7 7.1 7.6 8.0	9.6 10.1 10.7 11.3 12.0	12.7 13.5 14.3 15.1 16.0	15.9 16.9 17.9 18.9 20.0	19. 1 20. 2 21. 4 22. 7 24. 0	22.3 23.6 25.0 26.4 28.0	25.5 27.0 28.6 30.2 32.0	28.7 30.4 32.1 34.0 36.0	31.9 33.7 35.7 37.8 39.9
35 36 37 38 39	4.2 4.5 4.7 5.0 5.3	8.4 8.9 9.4 10.0	12.7 13.4 14.1 14.9 15.8	16.9 17.8 18.9 19.9 21.0	21.1 22.3 23.6 24.9 26.3	25.3 26.8 28.3 29.9 31.5	29.6 31.2 33.0 34.8 36.8	33.8 35.7 37.7 39.8 42.0	38.0 40.2 42.4 44.8 47.3	42. 2 44. 6 47. 1 49. 8 5 ² · 5
40 41 42 43 44	5.5 5.8 6.2 6.5 6.8	11.1 11.7 12.3 13.0 13.7	16.6 17.5 18.5 19.5 20.5	22. 2 23. 4 24. 6 26. 0 27. 3	27.7 29.2 30.8 32.4 34.2	33. 2 35. I 36. 9 38. 9 41. 0	38.8 40.9 43.1 45.4 47.8	44.3 46.7 49.3 51.9 54.7	49.9 52.6 55.4 58.4 61.5	55.4 58.4 61.6 64.9 68.4
45 46 47 48 49	7. 2 7. 6 8. 0 8. 4 8. 8	14.4 15.2 15.9 16.8 17.6	21.6 22.7 23.9 25.1 26.4	28.8 30.3 31.9 33.5 35.3	36.0 37.9 39.9 41.9 44.1	43.2 45.5 47.8 50.3 52.9	50.4 53.0 55.8 58.7 61.7	57.6 60.6 63.8 67.1 70.5	64.8 68.2 71.7 75.4 79.3	72.0 75.8 79.7 83.8 88.1
50 51 52 53 54	9.3 9.7 10.2 10.7 11.3	18.5 19.5 20.4 21.5 22.5	27.8 29.2 30.7 32.2 33.8	37.1 38.9 40.9 42.9 45.1	46.3 48.7 51.1 53.7 56.3	55.6 58.4 61.3 64.4 67.6	64.8 68.1 71.6 75.1 78.9	74. I 77. 9 81. 8 85. 9 90. I	83.4 87.6 92.0 96.6 101.4	92.6 97.3 102.2 107.3 112.7
55	11.8	23.6	35.5	47.3	59. I	70.9	82.7	94.6	106.4	118.2

TABLE 79. RATE OF DECREASE OF VAPOR PRESSURE WITH ALTITUDE FOR MOUNTAIN STATIONS.

(According to the empirical formula of Dr. J. Hann.)

$$\frac{e}{e} = 10^{-\frac{h}{6200}}$$

 $e, e_0 =$ Vapor pressures at an upper and a lower station respectively. h = Difference of altitude in meters.

Difference (of Altitude.	$\frac{e}{e_{\circ}}$.	Difference of Altitude.		$\frac{e}{e_{\circ}}$.	Difference	of Altitude.	$\frac{e}{e_{\circ}}$.
Meters. 200 400 600 800	Feet. 656 1312 1968 2625	0.93 .86 .80 .75	Meters. 1800 2000 2200 2400	Feet. 5905 6562 7218 7874	0. 52 . 48 . 45 . 42	Meters. 3400 3600 3800 4000	Feet. .11155 .11811 .12467 .13123	0. 29 . 27 . 25 . 23
1000 1200 1400 1600	3281 3937 4593 5249	0.69 .64 .60 .56	2600 2800 3000 3200	8530 9186 9842 10499	0.39 .36 .33 .31	4500 5000 5500 6000	14764 16404 18045 19685	0. I9 . I6 . I3 . II

TABLE 80.

DEPTH OF WATER CORRESPONDING TO THE WEIGHT OF A
CYLINDRICAL SNOW CORE 2.655 INCHES IN DIAMETER.

(One-fifth pound equals 1 inch.)

Weight lbs.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	Inches.	Inches.	Inches.	Inches,	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
.0	0.00	0.05	0.10	0.15	0.20	0.25	0.30	0.35	0.40	0.45
. I	0.50	0.55	0.60	0.65	0.70	0.75	0.80	0.85	0.90	0.95
. 2	1.00	1.05	1.10	1.15	1.20	1.25	1.30	1.35	1.40	1.45
.3	1.50	1.55	1.60	1.65	1.70	1.75	1.80	1.85	1.90	1.95
.4	2.00	2.05	2.10	2.15	2.20	2.25	2.30	2.35	2.40	2.45
· 5 .6	2.50	2.55	2.60	2.65	2.70	2.75	2.80	2.85	2.90	2.95
	3.00	3.05	3.10	3.15	3.20	3.25	3.30	3.35	3.40	3 - 45
.7	3.50	3.55	3.60	3.65	3.70	3.75	3.80	3.85	3.90	3.95
.8	4.00	4.05	4.10	4.15	4.20	4.25	4.30	4.35	4.40	4.45
.9	4.50	4.55	4.60	4.65	4.70	4 · 75	4.80	4.85	4.90	4.95
1.0	5.∞	5.05	5.10	5.15	5.20	5 · 25	5.30	5.35	5.40	5.45
I.I	5.50	5.55	5.60	5.65	5.70	5 · 75	5.80	5.85	5.90	5.95
1.2	6.00	6.05	6. 10	6.15	6.20	6. 25	6.30	6.35	6.40	6.45
1.3	6.50	6.55	6.60	6.65	6.70	6.75	6.80	6.85	6.90	6.95
1.4	7.∞	7.05	7. 10	7.15	7.20	7 · 25	7.30	7.35	7.40	7-45
1.5	7.50	7 - 55	7.60	7.65	7.70	7.75	7.80	7.85	7.90	7.95
1.6	8.00	8.05	8. 10	8.15	8.20	8.25	8.30	8.35	8.40	8.45
1.7	8.50	8.55	8.60	8.65	8.70	8.75	8.80	8.85	8.90	8.95
1.8	9.00	9.05	9. 10	9.15	9.20	9.25	9.30	9.35	9.40	9.45
1.9	9.50	9.55	9.60	9.65	9.70	9.75	9.80	9.85	9.90	9.95
2.0	10.00	10.05	10.10	10.15	10. 20	10. 25	10.30	10.35	10.40	10.45
2. I	10.50	10.55	10.60	10.65	10.70	10.75	10.80	10.85	10.00	10.95
2.2	11.00	11.05	11.10	11.15	11.20	11.25	11.30	11.35	11.40	11.45
2.3	11.50	11.55	11.60	11.65	11.70	11.75	11.80	11.85	11.90	11.95
2.4	12.00	12.05	12.10	12.15	12.20	12.25	12.30	12.35	12.40	12.45
2.5	12.50	12.55	12.60	12.65	12.70	12.75	12.80	12.85	12.90	12.95
2.6	13.00	13.05	13.10	13.15	13.20	13.25	13.30	13.35	13.40	13.45
2.7	13.50	13.55	13.60	13.65	13.70	13.75	13.80	13.85	13.90	13.95
2.8	14.00	14.05	14.10	14.15	14. 20	14.25	14.30	14.35	14.40	14.45
2.9	14.50	14.55	14.60	14.65	14.70	14.75	14.80	14.85	14.90	14.95
<u> </u>		·			<u>'</u>					

Table 81.

DEPTH OF WATER CORRESPONDING TO THE WEIGHT OF SNOW. (OR RAIN) COLLECTED IN AN 8-INCH CAGE. (One pound equals 0.5507 inch.)

Weight Pounds.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	Inch.	Inch.	Inch,	Inch,	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
.0	.00	.01	.01	. 02	. 02	. 03	. 03	. 04	. 04	. 05
.1	. 06	. 06	. 07	. 07	. 08	. 08	.00	. 00	. 10	. 10
. 2	. 11	. I 2	. 12	. 13	. 13	.14	.14	. 15	. 15	. 16
.3	. 17	. 17	. 18	. 18	.19	. 19	. 20	. 20	.21	. 22
-4	. 22	. 23	. 23	. 24	. 24	. 25	.25	. 26	. 26	. 27
.5	. 28	. 28	. 29	. 29	.30	.30	.31	.31	. 32	.33
.6	. 33	-34	.34	-35	.35	. 36	. 36	37	. 38	. 38
.7	. 39	.39	. 40	.40	.41	.41	.42	. 43	.43	-44
.8	. 44	·45	.45	.46	.46	.47	.47	. 48	.49	.49
.9	. 50	. 50	.51	.51	. 52	. 52	- 53	. 54	. 54	-55
					1				l	

Table 82. QUANTITY OF RAINFALL CORRESPONDING TO GIVEN DEPTHS.

Denth of rain-	Cubic inches per		Gallons	per acre.	Tono nor nore (2000
fall, inches.	acre,	Gubic feet per acre.	United States or Queen Anne.	Imperial (BritIsh).	Tone per acre (2000 pounds). (62° F.)
0.01	62726.4	36.3	271.5	226	1.1
0.02	I25453.	72.6	543	452	2.3
0.03	188179.	108.9	815.	678	3.4
0.04	250005.	145.2	1086.	904	4.5
0.05	313632.	181.5	1358.	1130	5.6
0.06	376358.	217.8	1629.	1356	6.8
0.07	439084.	254. I	1900.	1582	7.9
0.08	501810.	290.4	2171.	1808	9.0
0.00	564536.	326.7	2442.	2034	IO. I
0.10	627264. •	363.0	2715.	2261	11.3
0.25	1568160.	907.5	6789.	5652	28.
0.50	3136320.	1815.	13577.	11303	56.
0.75	4704480.	2722.	20366.	16955	85.
1.00	6272640.	3630.	27154.	22607	113.
1.25	7840800.	4538.	33943.	28259	141.
1. 50	9408960.	5445.	40371.	33911	170.
1.75	10977120.	6352.	47520.	39563	198.
2.00	12545280.	7260.	54309.	45214	226.
2.25	14113440.	8168.	61097.	50866	255.
2.50	15681600.	9075.	67866.	56517	283.
2.75	17249760.	9982.	74674.	62169	311.
3.00	18817920.	10890.	81463.	67821	339.
4.co	25090560.	14520.	108617.	90428	452.
5.00	31363200.	18150	135772.	113035	565.
6.00	37635840.	21780.	162926.	135642	678.

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VALUE OF GRAVITY ON THE EARTH AT SEA LEVEL.

 $g_{\phi} = 978.039 \; (1 + 0.005294 \; sin^2 \phi - 0.000007 \; sin^2 2 \phi)$ = 980.621 $(1 - 0.002640 \; cos \; 2 \phi + 0.000007 \; cos^2 \; 2 \phi)$

ф	g_{ϕ}	ф	g_{ϕ}	ф	g_{ϕ}	ф	g_{ϕ}	ф	g_{ϕ}
,	Dynes.	0 /	Dynes.	o ,	Dynes.	0 ,	Dynes.	۰,	Dynes.
0 0	978.039	20 00	978.642	37 o o	979.908	54 00	981.422	71 00	982.665
[0	.041	20	.661	20	.937	20	.450	20	. 684
2 0	. 045	40	.681	40	. 966	40	.479	40	. 702
3 0	.053	21 00	.701	38 00	.995	55 00	. 507	72 00	.720
4 0	. 064	20	.721	20	980.024	20	- 535	20	. 738
5 00	. 078	22 00	. 762	39 00	. 054	40 56 00	. 564	40	.755
20	. 084	20	. 783	20	.113	20	.620	73 00	· 772
40	. 080	40	. 805	40	. 142	40	.647	40	.805
6 00	. 005	23 00	.826	40 00	.172	57 00	.675	74 00	.822
20	.102	20	. 848	20	. 201	20	. 703	20	.837
40	. 108	40	.870	40	. 231	40	. 730	40	.853
7 00	. 115	24 00	. 892	41 00	. 261	58 00	.757	75 00	. 868
20	. 123	20	.914	20	. 291	20	. 784	20	. 883
40	. 131	40	.937	40	.321	40	.811	40	.898
8 00	. 139	25 00	. 960	42 00	. 350	59 00	. 838	76 00	.912
20	. 147	20	. 983	20	. 380	20	.865	20	.926
40	. 156	40	979.006	40	.410	40	. 891	40	.940
900	. 165	26 00	. 030	43 00	- 440	60 00	.917	77 00	-953
20	. 174	20	. 054	20	.471	20	.943	20	.966
40	. 184	40	.077	40	. 501	40	.969	40	.979
10 00	. 194	27 00	. 102	44 00	. 531	61 00	.995	78 oo	.992
20	. 205	20	. 126	20	. 561	20	982.020	20	983.004
40 II 00	.215	28 oo	.151	40	.59I .62I	40 62 00	.046	40	.016
20	.238	20 00	. 175	45 00 20	.651	20	. 071 . 006	79 00 20	.027
40	. 250	40	. 226	40	.681	40	. 121		. 039
12 00	, 262	20 00	. 251	46 00	.711	63 00	.121	40 80 00	. 049 . 060
20	. 274	20	. 277	20	.741	20	. 160	20	.070
40	. 287	40	.302	40	.772	40	. 194	40	- 080
13 00	. 300	30 00	.328	47 00	. 802	64 00	.217	81 00	. 000
20	.313	20	.354	20	. 832	20	. 241	20	. 000
40	. 327	40	. 381	40	.862	40	. 265	40	. 108
14 00	.341	31 00	. 407	48 00	. 892	65 00	. 288	82 00	. 116
20	.355	20	. 434	20	. 922	20	.311	20	. 124
40	. 369	40	.460	40	.952	40	-334	40	. 132
15 00	. 384	32 00	. 487	49 00	.981	66 00	. 356	83 00	. 140
20	- 399	20	.515	20	981.011	20	.379	20	. 147
40	.415	40	. 542	40	. 041	40	. 401	40	. 153
16 00	.430	33 00	. 569	50 00	.071	67 00	. 423	84 00	. 160
20	.447	20	. 597	20	.100	20	.445	20	. 166
17 00	. 463 . 479	40 34 00	. 624 . 652	40 51 00	. 130 . 160	68 oo	. 466	40	. 172
20	.479	20	. 68o	20	. 189	20	. 487	85 00	. 177
40	. 514	40	. 708	40	. 218	40	. 508 . 528	20	. 182 . 187
18 00	. 531	35 00	. 736	52 00	. 248	60 00	. 549	40	.107
20	. 549	20	. 765	20	. 277	20	. 569	86 00	. 192
40	.567	40	. 793	40	. 306	40	. 589	87 00	. 203
19 00	. 585	36 00	. 822	53 00	. 335	70 00	. 608	88 00	. 210
20	. 604	20	.850	20	. 364	20	.628	80 00	. 215
40	978.623	40	979.879	40	981.393	40	982.647	90 00	983.217
<u></u>									

TABLE 84.
RELATIVE ACCELERATION OF GRAVITY AT DIFFERENT LATITUDES.

Ratio of the acceleration of gravity at sea level for each 10' of latitude, to its acceleration at latitude 45° .

$$\frac{g_{\phi}}{g_{45}} = I - 0.002640 \cos 2 \phi + 0.000007 \cos^2 2 \phi$$

Latitude.	0'	10′	20′	30′	40′	50′
o°	0.997367	0.997367	0.997367	0.997367	0.997368	0.997368
l i	.997369	.997369	.997370			
2				.997371	.997371	.997372
	· 997373	.997374	.997376	.997377	.997378	.997380
3	.997381	.997383	.997385	.997387	. 997388	.997390
4	. 997393	•997395	.997397	-997399	.997402	.9974 0 4
5	0.997407	0.997410	0.997412	0.997415	0.997418	0.997421
6	.997424	. 997428	.997431	.997434	. 997438	. 99744 1
7 8	.997445	-997449	-997453	. 997456	. 997460	.997465
8	. 997469	.997473	.997477	.997482	. 997486	.997491
9	. 997496	. 997500	- 997505	.997510	.997515	.997520
10	0.997525	0.997531	0.997536	0.997541	0.997547	0.997553
II	. 997558	. 997564	.997570	.997576	. 997582	. 997588
12	.997594	.997600	. 997607	.997613	.997620	. 997626
13	.997633	.997640	. 997646	. 997653	.997660	. 997667
14	. 997674	.997682	. 997689	. 997696	. 997704	.997711
15	0.997719	0.997727	0.997734	0.997742	0.997750	0.997758
16	. 997766	.997774	.997783	.997791	.997799	.997808
17	.997816	.997825	.997833	.997842	.997851	.997860
18	. 997869	.997878	.997887	.997896	.997905	.997915
10	.997924	997934	.997943	.997953	.997962	.997973
19	.99/924	1997934			.997902	.997972
20	0.997982	0.997992	0.998002	0.998012	0.998022	0.998032
21	. 998042	. 998052	. 998 0 63	.998073	. 998084	. 998094
22	. 998104	.998115	.998126	.998137	.998148	. 998159
23	.998170	. 998181	.998192	. 998203	.998214	. 998225
24	. 998237	. 998248	.998260	.998271	. 998283	. 998294
25	0.998306	0.998318	0.998330	 0.998341	0.998353	0.998365
26	. 998377	. 998389	. 998402	. 998414	.998426	.998438
27	.998451	. 998463	. 998476	. 998488	.998501	.998513
28	.998526	.998539	.998551	. 998564	.998577	.998590
20	.998603	.998616	. 998629	.998642	.998655	.998669
30	0.008680	0.998695	0.998708	0.998722	0.998735	2 228212
	0.998682 .998762	. 998776	.998789	. 998803	.998817	0.998749
31			.998789			
32	. 998844	.998858		. 998886	.998899	.998913
33	. 998927	.998941	. 998956	.998970	.998984	. 998998
34	.999012	. 999026	. 999041	.999055	. 999 0 69	. 999 0 84
35	0.999098	0.999112	0.999127	0.999141	0.999156	0.999170
36	. 999185	.999199	. 999214	. 999229	.999243	. 999258
37	.999273	. 999 288	. 999302	.999317	.999332	. 999347
38	. 999362	.999377	. 999392	.9994 0 6	.999421	. 999436
39	.99945፤	. 999466	. 999482	- 999497	.999512	-999527
40	0.999542	0.999557	0.999572	0.999587	0.999602	0.999618
41	. 999633	. 999648	. 999663	.999678	. 999694	. 999709
42	.999724	. 999739	.999755	.999770	.999785	. 999801
43	.999816	. 999831	. 999847	. 999862	.999877	.999893
44	. 999908	. 999923	. 999939	.999954	. 999969	.999985
45	1.000000	1.000015	1.000031	1.000046	1.000061	1.000077
<u> </u>					I	

TABLE 84.

RELATIVE ACCELERATION OF CRAVITY AT DIFFERENT LATITUDES.

Ratio of the acceleration of gravity at sea level for each 10' of latitude, to its acceleration at latitude 45° .

$$\frac{g_{\phi}}{g_{45}} = 1 - 0.002640 \cos 2 \phi + 0.000007 \cos^2 2 \phi$$

Latitude. ϕ	0′	10′	20′	30′	40′	50′
45	1.000000	1.000015	1.000031	1.000046	1.000061	1.000077
46	092	108	123	138	153	169
47	184	200	215	230	246	261
48	276	291	307	322	337	352
49	368	383	398	413	428	444
50	1.000459	1.000474	1.000489	1.000504	1.000519	1.000534
51	549	564	579	594	609	624
52	639	654	669	684	699	713
53	728	743	758	773	787	802
54	816	831	846	860	875	889
55	1.000904	1.000918	1.000933	1.000947	1.00096 1	1.000976
56	0990	1004	1018	1033	1047	1061
57	1075	1089	1103	1117	1131	1145
58	1159	1173	1186	1200	1214	1227
59	1241	1255	1268	1282	1295	1308
60	1.001322	1.001335	1.001348	1.001362	1.001375	1.001388
61	1401	1414	1427	1440	1453	1466
62	1478	1491	1504	1517	1529	1542
63	1554	1567	1579	1591	1604	1 616
64	1628	1640	1652	1664	1676	1688
65	1.001700	1.001712	1.001723	1.001735	I.CO1747	1.co1758
66	1770	1781	1792	1804	1815	1826
67	1837	1848	1859	1870	1881	1892
68	1903	1913	1924	1935	1945	1955
69	1966	1976	1986	1996	2007	2017
70	1.002026	1.002036	1.002046	1.002056	1.002066	1.002075
71	2085	2094	2104	2113	2122	2131
72	2140	2149	2158	2167	2176	2185
73	2194	2202	2211	2219	2227	2236
74	2244	2252	2260	2268	2276	2284
75	1.002292	1.002299	1.002307	1.002314	1.002322	1.002329
76	2336	2344	2351	2358	2365	2372
77	2378	2385	2392	2398	2405	2411
78	2418	2424 2460	2430	2436	2442	2448
79	2454	2400	2465	2471	2476	2482
80	1.002487	1.002492	1.002497	1.002502	1.002507	1.002512
81	2517	2522	2527	2531	2536	2540
82	2544	2548	2553	2557	2561	2564
83	2568	2572	2576	2579	2582	2586
84	2589	2592	2595	2598	2601	2604
85	1.002607	1.002609	1.002612	1.002614	1.002617	1.002619
86	2621	2623	2625	2627	2629	263 1
87	2632	2634	2636	2637	2638	2639
88	2641	2642	2643	2643	2644	2645
89	2645	2646	2646	2647	2647	2647
90	1.002647					
				l		

LENGTH OF ONE DEGREE OF THE MERIDIAN AT DIFFERENT LATITUDES.

Latitude.	Meters.	Statute Miles.	Geographic Miles. 1' of the Eq.	Latitude.	Meters.	Statute Miles.	Geographic Miles. 1' of the Eq.
0 ° 1 2 3	110 568.5 110 568.8 110 569.8 110 571.5	68.703 68.704 68.705 68.706	59.594 59.594 59.595 59.596	45° 46 47 48	111 132.1 111 151.9 111 171.6 111 191.3	69.054 69.067 69.079 69.091	59.898 59.908 59.919 59.929
4	110 573.9	68.707	59.597	49	111 210.9	69.103	59.940
5 6 7 8	110 577.0 110 580.7 110 585.1	68.709 68.711 68.714	59.598 59.600 59.603	50 51 52	111 230.5 111 249.9 111 269.2	69.115 69.127 69.139	59.951 59.961 59.972
9	110 590.2 110 595.9	68.717 68.721	59.606 59.609	53 54	111 288.3	69.151 69.163	59.982 59.992
10 11 12 13 14	110 602.3 110 609.3 110 617.0 110 625.3 110 634.2	68.725 68.729 68.734 68.739 68.745	59.612 59.616 59.620 59.625 59.629	55 56 57 58 59	111 326.0 111 344.5 111 362.7 111 380.7 111 398.4	69.175 69.186 69.198 69.209 69.220	60.002 60.012 60.022 60.032 60.041
15 16 17 18 19	110 643.7 110 653.8 110 664.5 110 675.7 110 687.5	68.751 68.757 68.763 68.770 68.778	59.634 59.640 59.646 59.652 59.658	60 61 62 63 64	111 415.7 111 432.7 111 449.4 111 465.7 111 481.5	69.230 69.241 69.251 69.261 69.271	60.051 60.060 60.069 60.077 60.086
20 21 22 23 24	110 699.9 110 712.8 110 726.2 110 740.1	68.786 68.794 68.802 68.810 68.819	59.665 59.672 59.679 59.686 59.694	65 66 67 68 69	111 497.0 111 512.0 111 526.5 111 540.5 111 554.1	69.281 69.290 69.299 69.308 69.316	60.094 60.102 60.110 60.118 60.125
25 26 27 28 29	110 769.2 110 784.5 110 800.2 110 816.3 110 832.8	68.829 68.838 68.848 68.858 68.868	59.702 59.710 59.719 59.727 59.736	70 71 72 73 74	111 567.1 111 579.7 111 591.6 111 603.0 111 613.9	69.324 69.332 69.340 69.347 69.354	60.132 . 60.139 60.145 60.151 60.157
30 31 32 33 34	110 849.7 110 866.9 110 884.4 110 902.3 110 920.4	68.879 68.889 68.900 68.911 68.923	59·745 59·755 59·764 59·774 59·784	75 76 77 78 79	111 624.1 111 633.8 111 642.8 111 651.2 111 659.0	69.360 69.366 69.372 69.377 69.382	60.163 60.168 60.173 60.177 60.182
35 36 37 38 39	110 938:8 110 957.4 110 976.3 110 995.3	68.934 68.946 68.957 68.969 68.981	59.794 59.804 59.814 59.824 59.834	80 81 82 83 84	111 666.2 111 672.6 111 678.5 111 683.6 111 688.1	69.386 69.390 69.394 69.397 69.400	60. 186 60. 189 60. 192 60. 195 60. 197
40 41 42 43 44	111 033.9 111 053.4 111 073.0 111 092.6 111 112.4	68.993 69.005 69.017 69.029 69.042	59.845 59.855 59.866 59.876 59.887	85 86 87 88 89	111 691.9 111 695.0 111 697.4 111 699.2 111 700.2	69.402 69.404 69.405 69.407 69.407	60.199 60.201 60.202 60.203 60.204
45	111 132.1	69.054	59.898	90	111 700.6	69.407	60.204

LENGTH OF ONE DEGREE OF THE PARALLEL AT DIFFERENT LATITUDES.

Latitude.	Meters.	Statute Miles.	Geographic Miles. 1' oi the Eq.	Latitude.	Meters.	Statute Miles,	Geographic Miles. 1' of the Eq.
0° 1 2 3	111 321.9	69.171	60.000	45°	78 850.0	48.995	42.498
	111 305.2	69.162	59.991	46	77 466.5	48.135	41.753
	111 254.6	69.130	59.964	47	76 059.2	47.261	40.994
	111 170.4	69.078	59.918	48	74 628.5	46.372	40.223
5 6	111 052.6 110 901.2 110 716.2 110 497.7	69.005 68.911 68.796 68.660	59.855 59.773 59.673	49 50 51 52	73 174.9 71 698.9 70 200.8 68 681.1	45.469 44.552 43.621 42.676	39.440 38.644 37.837 37.018
7 8 9	110 497.7 110 245.8 109 960.5	68.503 68.326 68.128	59.556 59.420 59.266 59.095	52 53 54 55	67 140.3 65 578.8 63 997.1	41.719 40.749 39.766	36.187 35.346 34.493
11	109 290.1	67.909	58.905	56	62 395.7	38.771	33.630
12	108 905.2	67.670	58.697	57	60 775.1	37.764	32.757
13	108 487.3	67.411	58.472	58	59 135.7	36.745	31.873
14	108 036.6	67.131	58.229	59	57 478.1	35.715	30.979
15	107 553.1	66.830	57.969	60	55 802.8	34.674	30.076
16	107 037.0	66.510	57.690	61	54 110.2	33.622	29.164
17	106 488.5	66.169	57.395	62	52 400.9	32.560	28.243
18	105 907.7	65.808	57.082	63	50 675.4	31.488	27.313
19	105 294.7	65.427	56.751	64	48 934.3	30.406	26.374
20	104 649.8	65.026	56.404	65	47 178.0	29.315	25.428
21	103 973.2	64.606	56.039	66	45 407.1	28.215	24.473
22	103 265.0	64.166	55.657	67	43 622.2	27.106	23.511
23	102 525.4	63.706	55.259	68	41 823.8	25.988	22.542
24	101 754.6	63.227	54.843	69	40 012.4	24.862	21.566
25	100 953.0	62.729	54.411	70 71 72 73 74	38 188.6	23.729	20.583
26	100 120.6	62.212	53.963		36 353.0	22.589	19.593
27	99 257.8	61.676	53.498		34 506.2	21.441	18.598
28	98 364.8	61.121	53.016		32 648.6	20.287	17.597
29	97 441.9	60.548	52.519		30 780.9	19.126	16.590
30	96 489.3	59.956	52.006	75	28 903.6	17.960	15.578
31	95 507.3	59.345	51.476	76	27 017.4	16.788	14.562
32	94 496.2	58.717	50.931	77	25 122.8	15.611	13.541
33	93 456.3	58.071	50.371	78	23 220,4	14.428	12.515
34	92 387.9	57.407	49.795	79	21 310.8	13.242	11.486
35	91 291.3	56.726	49.204	80	19 394.6	12.051	10.453
36	90 166.8	56.027	48.598	81	17 472.4	10.857	9.417
37	89 014.8	55.311	47.977	82	15 544.7	9.659	8.378
38	87 835.6	54.578	47.341	83	13 612.2	8.458	7.337
39	86 629.6	53.829	46.691	84	11 675.5	7.255	6.293
40	85 397.0	53.063	46.027	85	9735.1	6.049	5.247
41	84 138.4	52.281	45.349	86	7791.7	4.841	4.200
42	82 854.0	51.483	44.656	87	5845.9	3.632	3.151
43	81 544.2	50.669	43.950	88	3898.3	2.422	2.101
• 44	80 209.4	49.840	43.231	89	1949.4	1.211	1.051
45	78 850.0	48.995	42.498	90	0.0	0.000	0.000

Declination				LATIT	UDE NO	RTH.			
of the Sun.	0°	5°	10°	15°	20°	25°	30°	35°	40°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
-23°27′	12 7	11 50	II 32	11 14	10 55	10 35	10 13	9 48	9 19
-23°20	12 7	11 50	II 32	11 14	10 56	10 36	10 14	9 49	9 20
-23°0	12 7	11 50	II 33	11 15	10 57	10 37	10 15	9 51	9 23
-22 40	12 7	11 50	11 33	11 16	10 58	10 38	10 17	9 53	9 26
-22 20	12 7	11 51	11 34	11 17	10 59	10 40	10 19	9 55	9 29
-22 0	12 7	11 51	11 34	11 18	11 0	10 41	10 20	9 58	9 31
-21 40	12 7	11 51	11 35	II 19	II I	10 43	10 22	10 0	9 34
-21 20	12 7	11 52	11 35	II 19	II 2	10 44	10 24	10 2	9 37
-21 0	12 7	11 52	11 36	II 20	II 4	10 46	10 26	10 4	9 40
-20 40 -20 20 -20 0	12 7 12 7 12 7	11 52 11 52 11 53	11 37 11 37 11 38	II 2I II 22 II 23	11 5 11 6 11 7	10 47 10 49 10 50	10 28 10 29 10 31	10 6 10 11	9 4 2 9 45 9 47
-19 40 -19 20 -19 0	12 7 12 7 12 7	11 53 11 53 11 53	11 38 11 39 11 39	11 23 11 24 11 25	11 9 11 10	10 51 10 53 10 54	10 33 10 35 10 37	10 13 10 15 10 17	9 50 9 53 9 55
-18 40	12 7	11 54	II 40	11 26	II II	10 55	10 38	10 19	9 58
-18 20	12 7	11 54	II 40	11 27	II I2	10 57	10 40	10 21	10 1
-18 0	12 7	11 54	II 41	11 28	II I3	10 58	10 42	10 23	10 3
-17 40	12 7	11 54	II 4I	11 28	11 14	IO 59	10 43	10 26	10 5
-17 20	12 7	11 55	II 42	11 29	11 15	II I	10 45	10 28	10 8
-17 0	12 7	11 55	II 42	11 30	11 16	II 2	10 47	10 30	10 10
-16 40 -16 20 -16 0	12 7 12 7 12 7	11 55 11 55 11 56	II 43 II 44	11 31 11 31 11 32	11 17 11 18 11 19	11 4 11 5 11 6	10 49 10 50 10 52	10 32 10 34 10 36	10 13 10 16 10 18
-15 40 -15 20 -15 0	12 7 12 7 12 7	11 56 11 56 11 56	11 44 11 45 11 45	II 33 II 34 II 34	II 20 II 2I II 22	11 9 11 10	10 53 10 55 10 57	10 38 10 40 10 42	10 20 10 23 10 25
-14 40	12 7	11 57	11 46	11 35	II 23	11 11	10 59	10 44	10 28
-14 20	12 7	11 57	11 46	11 36	II 25	11 13	11 0	10 46	10 30
-14 0	12 7	11 57	11 47	11 37	II 26	11 14	11 2	10 48	10 32
-13 40	12 7	11 57	11 47	11 37	11 27	11 16	11 4	10 50	10 35
-13 20	12 7	11 58	11 48	11 38	11 28	11 17	11 5	10 52	10 37
-13 0	12 7	11 58	11 48	11 39	11 29	11 18	11 7	10 54	10 40
-12 40	12 7	11 58	11 49	11 40	II 30	11 19	11 10	10 56	10 42
-12 20	12 7	11 58	11 49	11 40	II 31	11 21		10 58	10 44
-12 0	12 7	11 58	11 50	11 41	II 32	11 22		11 0	10 47
- 11 40	12 7	11 59	11 50	11 42	11 33	11 23	11 13	11 2	10 49
- 11 20	12 7	11 59	11 51	11 43	11 34	11 25	11 15	11 4	10 52
- 11 0	12 7	11 59	11 51	11 43	11 35	11 26	11 16	11 6	10 54
-10 40	12 7	11 59	11 52	11 44	11 36	11 27	II 18	11 8	10 56
-10 20	12 7	12 0	11 52	11 45	11 37	11 28	II 20	11 10	10 59
-10 0	12 7	12 0	11 53	11 46	11 38	11 30	II 21	11 12	11 1
- 9 40	12 7	12 O	11 53	11 46	11 39	II 3I	II 23	11 14	11 3
- 9 20	12 7	12 O	11 54	11 47	11 40	II 32	II 24	11 16	11 5
- 9 0	12 7	12 I	11 54	11 47	11 41	II 34	II 26	11 17	11 8
- 8 40	12 7	12 I	11 55	11 48	11 42	11 35	II 28	11 19	II IO
8 20	12 7	12 I	11 55	11 49	11 43	11 36	II 29	11 21	II I2
8 0	12 7	12 I	11 56	11 50	11 44	11 37	II 3I	11 23	II I4

Declination				I,	ATITUD:	E NORT	т.		· · · · · · · · · · · · · · · · · · ·	
the Sun.	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
-23°27′	9 7	8 53	8 38	8 22	8 4	7 44	7 22	6 56	6 27	5 52
-23°20	9 8	8 54	8 39	8 23	8 5	7 45	7 24	6 58	6 29	5 54
-23°0	9 11	8 58	8 43	8 28	8 10	7 50	7 29	7 4	6 36	6 2
-22 40	9 14	9 I	8 46	8 31	8 14	7 55	7 34	7 10	6 43	6 9
-22 20	9 17	9 4	8 50	8 35	8 18	8 0	7 39	7 16	6 49	6 17
-22 0	9 20	9 7	8 53	8 38	8 22	8 4	7 44	7 22	6 55	6 25
-21 40	9 23	9 IO	8 57	8 42	8 26	8 9	7 49	7 27	7 I	6 32
-21 20	9 26	9 I3	9 1	8 46	8 30	8 13	7 54	7 32	7 8	6 38
-21 0	9 28	9 I7	9 4	8 50	8 34	8 18	7 59	7 38	7 I4	6 46
-20 40	9 31	9 20	9 7	8 53	8 38	8 22	8 4	7 43	7 20	6 52
-20 20	9 34	9 23	9 11	8 57	8 42	8 26	8 8	7 49	7 25	6 59
-20 0	9 37	9 26	9 14	9 I	8 46	8 31	8 13	7 54	7 31	7 5
-19 40	9 40	9 29	9 17	9 4	8 50	8 35	8 18	7 59	7 37	7 12
-19 20	9 43	9 32	9 20	9 7	8 54	8 39	8 23	8 4	7 43	7 18
-19 0	9 46	9 35	9 24	9 II	8 58	8 43	8 27	8 9	7 48	7 25
-18 40	9 48	9 38	9 27	9 15	9 2	8 47	8 32	8 14	7 54	7 3 ¹
-18 20	9 51	9 41	9 30	9 19	9 6	8 52	8 36	8 19	7 59	7 37
-18 0	9 54	9 44	9 34	9 22	9 IO	8 56	8 41	8 24	8 5	7 43
-17 40	9 56	9 47	9 37	9 25	9 13	9 0	8 45	8 29	8 10	7 49
-17 20	9 59	9 50	9 40	9 29	9 17	9 4	8 50	8 34	8 15	7 55
-17 0	10 2	9 53	9 43	9 32	9 21	9 8	8 54	8 38	8 20	8 1
-16 40	10 5	9 56	9 46	9 35	9 25	9 12	8 58	8 43	8 26	8 6
-16 20	10 7	9 59	9 49	9 39	9 28	9 16	9 2	8 47	8 31	8 12
-16 0	10 10	10 1	9 52	9 43	9 32	9 20	9 7	8 52	8 36	8 17
-15 40	10 12	10 4	9 55	9 46	9 35	9 24	9 II	8 57	8 41	8 23
-15 20	10 15	10 7	9 58	9 49	9 39	9 28	9 I5	9 2	8 46	8 29
-15 0	10 18	10 10	10 1	9 52	9 43	9 31	9 I9	9 6	8 51	8 34
-14 40	IO 20	10 13	IO 4	9 56	9 46	9 35	9 23	9 II	8 56	8 40
-14 20	IO 23	10 16	IO 7	9 59	9 49	9 39	9 28	9 I5	9 I	8 45
-14 0	IO 26	10 19	IO IO	10 2	9 53	9 43	9 32	9 I9	9 6	8 50
-13 40	10 28	IO 2I	10 13	10 5	9 56	9 47	9 36	9 24	9 11	8 56
-13 20	10 31	IO 24	10 16	10 8	10 0	9 50	9 40	9 28	9 16	9 1
-13 0	10 33	IO 26	10 19	10 11	10 3	9 54	9 44	9 33	9 20	9 6
-12 40	10 36	10 29	10 22	10 15	10 7	9 58	9 48	9 37	9 25	9 11
-12 20	10 38	10 32	10 25	10 18	10 10	10 1	9 52	9 41	9 30	9 17
-12 0	10 41	10 35	10 28	10 21	10 13	10 5	9 56	9 46	9 35	9 22
- II 40	10 44	10 38	10 31	10 25	10 17	10 9	10 0	9 50	9 39	9 27
- II 20	10 46	10 40	10 34	10 28	10 20	10 13	10 4	9 55	9 44	9 32
- II 0	10 49	10 43	10 37	10 31	10 23	10 16	10 8	9 59	9 49	9 37
-10 40	10 51	10 46	10 40	10 34	IO 27	IO 19	10 12	10 3	9 53	9 42
-10 20	10 53	10 49	10 43	10 37	IO 3I	IO 23	10 16	10 7	9 58	9 47
-10 0	10 56	10 51	10 46	10 40	IO 34	IO 27	10 19	10 11	10 3	9 52
- 9 40	10 59	10 54	10 49	10 43	IO 37	IO 3I	10 23	10 16	10 7	9 57
- 9 20	11 1	10 56	10 52	10 46	IO 40	IO 34	10 27	10 20	10 11	10 2
- 9 0	11 3	10 59	10 55	10 49	IO 44	IO 37	10 31	10 24	10 16	10 7
- 8 40	11 6	II 2	10 57	10 52	10 47	10 41	10 34	10 28	10 20	10 11
- 8 20	11 8	II 4	11 0	10 55	10 50	10 44	10 38	10 32	10 25	10 16
- 8 0	11 10	II 7	11 3	10 58	10 53	10 48	10 42	10 36	10 29	10 21

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Declination of				ĻATI'	TUDE NO	ORTH.			
the Sun.	0°	5°	10°	15°	20°	25°	30°	35°	40°
-8° 0′	h. m. 12 7	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
-7 40	12 7	12 I	11 56	11 50	11 45	11 38	11 32	11 25	II 17
-7 20	12 7	12 I	11 56	11 51	11 46	11 40	11 34	11 27	II 19
-7 0	12 7	12 2	11 57	11 52	11 47	11 41	11 35	11 29	II 22
-6 40	12 7	12 2	11 57	11 53	11 48	11 42	11 37	11 31	11 24
-6 20	12 7	12 2	11 58	11 53	11 49	11 43	11 38	11 32	11 26
-6 0	12 7	12 2	11 58	11 54	11 50	11 45	11 40	11 34	11 28
-5 40	12 7	12 3	11 59	11 55	11 51	11 46	11 41	11 36	11 31
-5 20	12 7	12 3	11 59	11 55	11 52	11 47	11 43	11 38	11 33
-5 0	12 7	12 3	12 0	11 56	11 53	11 49	11 44	11 40	11 35
-4 40	12 7	12 3	12 O	11 57	11 54	11 50	11 46	11 42	II 37
-4 20	12 7	12 4	12 I	11 58	11 55	11 51	11 47	11 44	II 40
-4 0	12 7	12 4	12 I	11 58	11 56	11 52	11 49	11 46	II 42
-3 40	12 7	12 4	12 2	11 59	11 57	11 53	11 51	11 47	11 44
-3 20	12 7	12 4	12 2	12 0	11 58	11 55	11 52	11 49	11 46
-3 0	12 7	12 5	12 3	12 1	11 58	11 56	11 54	11 51	11 49
-2 40	12 7	12 5	12 3	12 I	11 59	11 58	11 55	11 53	11 51
-2 20	12 7	12 5	12 4	12 2	12 0	11 59	11 57	11 55	11 53
-2 0	12 7	12 5	12 4	12 3	12 1	12 0	11 58	11 57	11 55
- I 40	12 7	12 5	12 4	12 4	12 2	12 I	12 0	11 59	II 58
- I 20	12 7	12 6	12 5	12 4	12 3	12 2	12 2	12 1	I2 0
- I 0	12 7	12 6	12 5	12 5	12 4	12 4	12 3	12 2	I2 2
-0 40	12 7	12 6	12 6	12 5	12 5	12 5	12 5	12 4	12 4
-0 20	12 7	12 6	12 6	12 6	12 6	12 6	12 6	12 6	12 7
0 0	12 7	12 7	12 7	12 7	12 7	12 7	12 8	12 8	12 9
+0 20	12 7	12 7	12 7	12 8	12 8	12 8	12 9	12 10	12 11
0 40	12 7	12 7	12 8	12 8	12 9	12 10	12 11	12 12	12 13
I 0	12 7	12 7	12 8	12 9	I2 I0	12 11	12 13	12 14	12 15
I 20	12 7	12 8	12 9	12 10	I2 II	12 13	12 14	12 16	12 17
I 40	12 7	12 8	12 9	12 10	I2 I2	12 14	12 16	12 17	12 20
2 0	12 7	12 8	12 IO	12 11	12 13	12 15	12 17	12 19	12 22
2 20	12 7	12 8	12 IO	12 12	12 14	12 16	12 19	12 21	12 25
2 40	12 7	12 9	12 II	12 13	12 15	12 17	12 20	12 23	12 27
3 0	12 7	12 9	12 11	12 13	12 16	12 19	12 22	12 25	12 29
3 20	12 7	12 9	12 12	12 14	12 17	12 20	12 23	12 27	12 31
3 40	12 7	12 9	12 12	12 15	12 18	12 21	12 25	12 29	12 33
4 0	12 7	12 IO	12 13	12 16	12 19	12 22	12 26	12 31	12 35
4 20	12 7	12 IO	12 13	12 16	12 20	12 23	12 28	12 32	12 38
4 40	12 7	12 IO	12 14	12 17	12 21	12 25	12 29	12 34	12 40
5 0	12 7	12 10	12 14	12 18	12 22	12 26	12 31	12 36	12 43
5 20	12 7	12 10	12 15	12 19	12 23	12 28	12 32	12 38	12 45
5 40	12 7	12 11	12 15	12 19	12 24	12 29	12 34	12 40	12 47
6 0	12 7	12 II	12 16	12 20	12 25	12 30	12 35	12 42	12 49
6 20	12 7	12 II	12 16	12 21	12 26	12 31	12 37	12 44	12 52
6 40	12 7	12 II	12 16	12 22	12 27	12 32	12 39	12 46	12 54
7 0	12 7	12 12	12 17	12 22	12 28	12 34	12 40	12 48	12 56
7 20	12 7	12 12	12 17	12 23	12 29	12 35	12 42	12 50	12 58
7 40	12 7	12 12	12 18	12 23	12 30	12 36	12 43	12 52	13 1
8 0	12 7	12 13	12 18	12 24	12 31	12 38	12 45	12 53	13 3

					* 144 Ware					
Declination of		1		1,,	ATITUDI	E NORT	н.			
the Sun.	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
-8° 0′	h. m. II II	h. m.	h. m.	h. m. 11 58	h. m. 10 53	h. m. 10 48	h. m. 10 43	h. m. 10 36	h. m. 10 30	h. m. IO 21
-7 40	11 13	II IO	11 5	11 I	10 57	10 52	10 46	10 40	10 34	10 26
-7 20		II I2	11 8	11 4	11 0	10 55	10 50	10 44	10 38	10 31
-7 ° -6 40	11 19	11 15	11 11	11 7	II 3 II 7	10 59	10 54	10 48	10 42	10 35
-6 20 -6 0	II 23 II 26	II 20 II 23	II 17 II 20	11 13	11 10	11 5	11 1	10 56 11 0	10 51	10 45 10 50
-5 40	11 28	11 25	II 23	11 19	11 16	11 13	11 8	11 4	10 59	10 55
-5 20	11 31	11 28	II 25	11 22	11 19	11 16	11 13	11 8	11 4	10 59
-5 0	11 33	11 31	II 28	11 25	11 23	11 19	11 16	11 12	11 8	11 4
-4 40	11 35	11 33	11 31	11 28	11 26	11 23	II 20	11 16	II 13	11 8
-4 20	11 38	11 36	11 34	11 31	11 29	11 26	II 23	11 20	II 17	11 13
-4 0	11 40	11 38	11 37	11 34	11 32	11 30	II 27	11 24	II 21	11 18
-3 40	11 43	11 41	11 39	11 37	11 35	11 33	11 31	11 28	11 26	II 22
-3 20	11 45	11 43	11 42	11 40	11 38	11 37	11 35	11 32	11 30	II 27
-3 0	11 47	11 46	11 45	11 43	11 42	11 40	11 38	11 36	11 34	II 32
-2 40	11 50	11 49	11 47	11 46	11 45	II 44	11 42	11 40	11 38	11 37
-2 20	11 52	11 51	11 50	11 49	11 48	II 47	11 46	11 44	11 43	11 41
-2 0	11 55	11 54	11 53	11 52	11 52	II 50	11 49	11 48	11 47	11 46
- I 40	11 57	11 56	11 55	11 55	11 55	11 54	11 53	11 52	11 51	11 50
- I 20	11 59	11 59	11 58	11 58	11 58	11 57	11 57	11 56	11 56	11 55
- I 0	12 2	12 2	12 1	12 1	12 1	12 1	12 1	12 0	12 0	11 59
-0 40	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 4
-0 20	12 7	12 7	12 7	12 7	12 7	12 7	12 8	12 8	12 8	
+0 0	12 9	12 9	12 10	12 10	12 IO	12 11	12 11	12 12	J2 I3	12 13
0 20	12 11	12 12	12 13	12 13	12 I4	12 14	12 15	12 16	I2 I7	12 18
0 40	12 14	12 14	12 15	12 16	12 I7	12 17	12 19	12 20	I2 2I	12 23
I 0	12 16	12 17	12 18	12 19	12 20	12 21	12 22	12 24	12 25	12 27
I 20	12 19	12 20	12 20	12 22	12 23	12 25	12 26	12 28	12 29	12 32
I 40	12 21	12 22	12 23	12 25	12 26	12 28	12 30	12 32	12 34	12 37
2 0	12 23	12 25	12 26	12 28	12 29	12 31	12 34	12 36	12 38	12 41
2 20	12 26	12 28	12 29	12 31	12 32	12 35	12 37	12 40	12 43	12 46
2 40	12 28	12 30	12 32	12 34	12 36	12 38	12 41	12 44	12 47	12 50
3 0	12 31	12 32	12 35	12 37	12 39	12 41	12 44	12 48	12 51	12 55
3 20	12 33	12 35	12 37	12 40	12 42	12 45	12 48	12 52	12 55	13 0
3 40	12 35	12 38	12 40	12 43	12 46	12 49	12 52	12 56	13 0	13 4
4 0	12 38	12 40	12 43	12 46	12 49	12 52	12 56	13 0	13 4	13 9
4 20	12 40	12 43	12 46	12 49	12 52	12 55	12 59	13 4	13 8	13 14
4 40	12 43	12 46	12 49	12 52	12 55	12 59	13 3	13 8	13 13	13 19
5 0	12 45	12 48	12 51	12 55	12 58	13 2	13 7	13 12	13 17	13 23
5 20	12 47	12 51	12 54	12 58	13 2	13 6	13 11	13 16	13 22	13 28
5 40	12 50	12 53	12 57	13 1	13 5	13 10	13 14	13 20	13 26	13 33
6 0	12 53	12 56	12 59	13 4	13 8	13 13	13 18	13 24	13 31	13 38
6 20	12 55	12 59	13 2	13 7	13 11	13 16	13 22	13 28	13 35	13 43
6 40	12 58	13 1	13 5	13 10	13 14	13 20	13 26	13 32	13 39	13 47
7 0	13 0	13 4	13 8	13 13	13 18	13 23	13 29	13 36	13 44	13 52
7 20	13 2	13 7	13 11	13 16	13 21	13 27	13 33	13 40	13 48	13 57
7 40	13 5	13 9	13 14	13 19	13 25	13 31	13 37	13 44	13 53	14 2
8 0	13 7	13 12	13 17	13 22	13 28	13 34	13 41	13 48	13 57	14 7

Declination				L ATI	TUDE NO	ORTH.			
of the Sun.	0°	5°	10°	15°	20°	25°	30°	35°	40°
+8° 0′	h. m.	h. m.	h. m.	h. m.	h. m. 12 31	h. m. 12 38	h. m.	h. m.	h. m.
8 20 8 40	12 7 12 7	12 13	12 19 12 19	12 25 12 26	12 32 12 33	12 39 12 40	12 47 12 48	12 55 12 57	13 5
9 0	12 7	12 13	12 20	12 26	12 34	12 41	12 50	12 59	13 10
9 20	12 7	12 13	12 20	12 27	12 35	12 43	12 52	13 1	13 13
9 40	12 7	12 14	12 21	12 28	12 36	12 44	12 53	13 3	13 14
10 0	12 7	12 I4	12 21	12 29	12 37	12 45	12 55	13 5	13 17
10 20	12 7	12 I4	12 22	12 29	12 38	12 47	12 56	13 7	13 19
10 40	12 7	12 I4	12 22	12 30	12 39	12 48	12 58	13 9	13 22
11 0	12 7	12 15	12 23	12 31	12 40	12 49	12 59	13 11	13 24
11 20	12 7	12 15	12 23	12 32	12 41	12 50	13 1	13 13	13 26
11 40	12 7	12 15	12 24	12 32	12 42	12 52	13 2	13 15	13 29
12 0	12 7	12 15	12 24	12 33	12 43	12 53	13 4	13 17	13 31
12 20	12 7	12 16	12 25	12 34	12 44	12 55	13 6	13 19	13 34
12 40	12 7	12 16	12 25	12 35	12 45	12 56	13 8	13 21	13 36
13 0	12 7	12 16	12 26	12 35	12 46	12 57	13 9	13 23	13 38
13 20	12 7	12 16	12 26	12 36	12 47	12 58	13 11	13 25	13 41
13 40	12 7	12 17	12 27	12 37	12 48	13 0	13 13	13 27	13 43
14 0	12 7	12 17	12 27	12 38	12 49	13 I	13 14	13 29	13 46
14 20	12 7	12 17	12 28	12 39	12 50	13 2	13 16	13 31	13 48
14 40	12 7	12 17	12 28	12 40	12 51	13 4	13 17	13 33	13 51
15 0	12 7	12 18	12 29	12 40	12 52	13 5	13 19	13 35	13 53
15 20	12 7	12 18	12 29	12 41	12 53	13 7	13 21	13 37	13 56
15 40	12 7	12 18	12 30	12 41	12 54	13 8	13 23	13 39	13 58
16 0	12 7	12 19	12 30	12 42	12 55	13 9	13 25	13 41	14 1
16 20	12 7	12 19	12 31	12 43	12 56	13 11	13 26	13 43	14 3
16 40	12 7	12 19	12 31	12 44	12 58	13 12	13 28	13 45	14 6
17 0	12 7	12 19	12 32	12 45	12 59	13 13	13 29	13 47	14 8
17 20	12 7	12 20	12 32	12 46	13 0	13 15	13 31	13 50	14 11
17 40	12 7	12 20	12 33	12 46	13 1	13 16	13 33	13 52	14 14
18 0	12 7	12 20	12 33	12 47	13 2	13 17	13 35	13 54	14 16
18 20	12 7	12 20	12 34	12 48	13 3	13 19	13 37	13 56	14 19
18 40	12 7	12 21	12 34	12 49	13 4	13 20	13 38	13 58	14 22
19 0	12 7	12 21	12 35	12 50	13 5	13 22	13 40	14 0	14 24
19 20	12 7	12 21	12 35	12 51	13 6	13 23	13 42	14 2	14 26
19 40	12 7	12 22	12 36	12 52	13 7	13 25	13 44	14 5	14 29
20 0	12 7	12 22	12 36	12 52	13 8	13 26	13 46	14 7	14 32
20 20	12 7	12 22	12 37	12 53	13 10	13 28	13 47	14 10	14 35
20 40	12 7	12 22	12 37	12 54	13 11	13 29	13 49	14 12	14 37
21 0	12 7	12 23	12 38	12 55	13 12	13 31	13 51	14 14	14 40
21 20	12 7	12 23	12 39	12 56	13 13	13 32	13 53	14 16	14 43
21 40	12 7	12 23	12 39	12 56	13 14	13 34	13 55	14 19	14 46
22 0	12 7	12 24	12 40	12 57	13 16	13 35	13 56	14 21	14 49
22 20	12 7	12 24	12 41	12 58	13 17	13 37	13 58	14 23	14 52
22 40	12 7	12 24	12 41	12 59	13 18	13 38	14 0	14 25	14 54
23 0	12 7	12 25	12 42	13 O	13 19	13 40	14 2	14 28	14 57
23 20	12 7	12 25	12 42	13 I	13 20	13 41	14 4	14 30	15 0
23 27	12 7	12 25	12 43	13 I	13 20	13 41	14 5	14 31	15 1

Declination				Ļ	ATITUDI	e nort	н,			
of the Sun.	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
+8° 0′	13 7	13 12	13 17	13 22	13 28	13 34	13 41	13 49	13 58	14 7
8 20	13 10	13 14	13 20	13 25	13 31	13 38	13 45	13 53	14 2	14 12
8 40	13 12	13 17	13 23	13 28	13 34	13 41	13 49	13 57	14 6	14 17
9 0	13 15	13 20	13 25 13 28	13 31	13 38 13 41	13 45 13 49	13 53 13 56	14 I 14 5	14 11	14 22 14 26
9 40 10 0	13 20 13 22	13 25 13 28	13 31	13 38	13 44	13 52 13 56	14 0	14 10	14 20	14 31
10 20	13 25	13 31	13 37	13 44	13 51	13 59	14 8	14 18	14 29	14 41
10 40	13 28	13 34	13 40	13 47	13 55		14 12	14 22	14 34	14 47
II 0	13 30	13 36	13 43	13 50	13 58	14 7	14 16	14 27	14 38	14 52
II 20	13 32	13 39	13 46	13 53	14 I	14 10	14 20	14 31	14 43	14 57
11 40 12 0	13 35 13 38	13 41	13 49 13 52	13 56 14 0	14 5	14 14	14 24	14 35	14 48	15 2 15 8
12 20	13 40	13 47	13 55	14 3	14 12	14 22	14 32	14 44	14 58	15 13
12 40	13 43	13 50	13 58	14 6	14 16	14 25	14 37	14 49	15 2	15 18
13 0	13 46	13 53	14 1	14 10	14 19	14 29	14 41	14 53	15 7	15 23
13 20	13 48	13 56	14 4	14 13	14 22	14 33	14 45	14 58	15 13	15 29
13 40	13 50	13 58	14 7	14 16	14 26	14 37	14 49	15 2	15 17	15 35
14 0	13 53	14 1	14 10	14 19	14 29	14 41	14 53	15 7	15 22	15 40
14 20	13 56	14 4	14 13	14 23	14 33	14 45	14 57	15 11	15 28	15 46
14 40	13 59	14 7	14 16	14 26	14 37	14 49	15 2	15 16	15 33	15 51
15 0	14 I	14 10	14 19	14 29	14 40	14 52	15 6	15 21	15 38	15 57
15 20	14 4	14 13	14 22	14 33	14 44	14 56	15 10	15 26	15 43	16 2
15 40	14 7	14 16	14 26	14 36	14 48	15 0	15 14	15 30	15 48	16 8
16 0	14 10	14 19	14 29	14 40	14 52	15 4	15 19	15 35	15 53	16 14
16 20	14 12	14 22	14 32	14 43	14 55	15 8	15 23	15 40	15 59	16 20
16 40	14 15	14 25	14 35	14 46	14 59	15 13	15 28	15 45	16 4	16 26
17 0	14 17	14 28	14 38	14 50	15 3	15 17	15 32	15 50	16 10	16 32
17 20	14 20	14 31	14 41	14 53	15 7	15 21	15 37	15 55	16 15	16 38
17 40	14 23	14 34	14 45	14 57	15 10	15 25	15 41	16 0	16 20	16 45
18 0	14 26	14 37	14 48	15 1	15 14	15 29	15 46	16 5	16 26	16 51
18 20	14 29	14 40	14 52	15 4	15 18	15 34	15 50	16 10	16 32	16 58
18 40	14 32	14 43	14 55	15 8	15 22	15 38	15 55	16 15	16 38	17 4
19 0	14 35	14 46	14 58	15 11	15 26	15 42	16 0	16 20	16 44	17 11
19 20	14 37	14 49	15 1	15 15	15 30	15 46	16 5	16 25	16 50	17 17
19 40	14 40	14 52	15 5	15 19	15 34	15 51	16 10	16 31	16 56	17 24
20 0	14 43	14 55	15 8	15 22	15 38	15 55	16 15	16 37	17 2	17 31
20 20	14 46	14 58	15 11	15 26	15 42	16 0	16 20	16 42	17 8	17 38
20 40	14 49	15 2	15 15	15 30	15 46	16 4	16 25	16 47	17 14	17 46
21 0	14 52	15 5	15 19	15 34	15 50	16 9	16 30	16 53	17 20	17 53
21 20	14 55	15 8	15 22	15 38	15 55	16 13	16 35	16 59	17 27	18 1
21 40	14 58	15 11	15 26	15 42	15 59	16 18	16 40	17 5	17 34	18 8
22 0	15 I	15 14	15 29	15 46	16 3	16 23	16 45	17 11	17 40	18 16
22 20	15 4	15 18	15 33	15 49	16 7	16 28	16 50	17 17	17 47	18 24
22 40	15 7	15 22	15 37	15 53	16 12	16 32	16 56	17 23	17 54	18 32
23 0	15 10	15 25	15 40	15 57	16 16	16 37	17 I	17 29	18 I	18 41
23 20	15 13	15 28	15 44	16 1	16 21	16 42	17 7	17 35	18 8	18 49
23 27	15 14	15 29	15 46	16 3	16 23	16 44	17 9	17 37	18 II	18 52

Declination	LATITUDE NORTH.										
of the Sun.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	70°
	h. m.	h. m.	h. m.								
-23° 27′ -23 20 -23 0	5 52 5 55 6 2	5 31 5 34 5 43	5 8 5 12 5 21	4 42 4 46 4 56	4 11 4 16 4 28	3 34 3 40 3 53	2 46 2 53 3 11	1 29 1 41 2 11			
-22 40 -22 20 -22 0	6 10 6 17 6 25	5 51 5 59 6 7	5 30 5 39 5 47	5 6 5 16 5 25	4 39 4 50 5 1	4 7 4 20 4 32	3 27 3 43 3 58	2 35 2 56 3 14	0 59 1 43 2 13		
-21 40	6 32	6 14	5 56	5 34	5 11	4 43	4 11	3 31	2 38	1 1	
-21 20	6 39	6 22	6 4	5 43	5 20	4 55	4 24	3 47	2 59	1 45	
-21 0	6 46	6 29	6 12	5 5 ²	5 30	5 5	4 36	4 1	3 18	2 16	
-20 40	6 52	6 37	6 20	6 1	5 40	5 16	4 48	4 16	3 35	2 41	I 2
-20 20	6 59	6 44	6 27	6 9	5 49	5 26	4 59	4 29	3 51	3 2	I 47
-20 0	7 5	6 51	6 34	6 17	5 58	5 35	5 10	4 41	4 6	3 22	2 19
-19 40	7 12	6 58	6 42	6 25	6 6	5 45	5 21	4 53	4 20	3 39	2 44
-19 20	7 18	7 4	6 49	6 33	6 14	5 54	5 31	5 5	4 34	3 55	3 6
-19 0	7 25	7 11	6 56	6 41	6 23	6 3	5 41	5 16	4 47	4 11	3 26
-18 40	7 3 ¹	7 17	7 4	6 48	6 31	6 12	5 5 1	5 26	4 59	4 25	3 44
-18 20	7 37	7 24	7 10	6 55	6 39	6 20	6 1	5 37	5 11	4 39	4 1
-18 0	7 43	7 31	7 17	7 3	6 47	6 29	6 10	5 47	5 22	4 52	4 16
-17 40	7 49	7 37	7 24	7 10	6 55	6 38	6 19	5 57	5 33	5 5	4 31
-17 20	7 55	7 43	7 31	7 17	7 2	6 46	6 28	6 7	5 43	5 17	4 45
-17 0	8 1	7 49	7 37	7 24	7 9	6 53	6 36	6 16	5 54	5 28	4 58
-16 40	8 6	7 55	7 44	7 3 ¹	7 17	7 I	6 44	6 26	6 4	5 40	5 11
- 16 20	8 12	8 1	7 50	7 3 ⁸	7 24	7 9	6 52	6 35	6 14	5 51	5 23
- 16 0	8 17	8 7	7 56	7 44	7 3 ¹	7 I7	7 1	6 44	6 24	6 2	5 35
-15 40	8 23	8 13	8 2	7 51	7 3 ⁸	7 25	7 9	6 52	6 34	6 12	5 47
-15 20	8 29	8 19	8 8	7 58	7 45	7 32	7 17	7 1	6 43	6 22	5 59
-15 0	8 34	8 25	8 15	8 4	7 5 ²	7 39	7 25	7 9	6 52	6 32	6 10
-14 40 -14 20 -14 0	8 40 8 45 8 50	8 31 8 36 8 42	8 21 8 27 8 33	8 10 8 17 8 23	7 59 8 5 8 12	7 46 7 53 8 1	7 32 7 40 7 47	7 17 7 26 7 34	7 I 7 I 7 I 7 I 8	6 42 6 51 7 1	6 20 6 31 6 41
-13 40	8 56	8 47	8 38	8 29	8 19	8 7	7 55	7 4 ¹	7 26	7°10	6 51
-13 20	9 1	8 53	8 44	8 35	8 25	8 14	8 2	7 49	7 35	7 19	7 1
-13 0	9 6	8 58	8 50	8 41	8 32	8 21	8 10	7 57	7 43	7 28	7 10
-12 40	9 11	9 4	8 56	8 47	8 38	8 28	8·17	8 5	7 51	7 37	7 20
-12 20	9 17	9 10	9 2	8 53	8 44	8 34	8 24	8 12	7 59	7 45	7 29
-12 0	9 22	9 15	9 7	8 59	8 50	8 41	8 31	8 20	8 7	7 53	7 38
-11 40	9 27	9 20	9 13	9 Š	8 <u>5</u> 6	8 47	8 38	8 27	8 15	8 2	7 47
-11 20	9 32	9 25	9 19	9 II	9 3	8 54	8 44	8 34	8 23	8 10	7 56
-11 0	9 37	9 31	9 24	9 I7	9 9	9 0	8 51	8 41	8 31	8 18	8 5
-10 40	9 42	9 36	9 29	9 22	9 15	9 7	8 58	8 49	8 38	8 26	8 14
- 10 20	9 47	9 41	9 35	9 28	9 21	9 13	9 5	8 56	8 46	8 34	8 22
- 10 0	9 52	9 46	9 40	9 34	9 27	9 19	9 11	9 3	8 53	8 42	8 31
- 9 40	9 57	9 51	9 46	9 40	9 33	9 26	9 18	9 10	9 0	8 50	8 39
- 9 20	10 2	9 56	9 51	9 45	9 39	9 32	9 25	9 16	9 8	8 58	8 47
- 9 0	10 7	10 2	9 56	9 50	9 44	9 38	9 31	9 23	9 15	9 5	8 55
- 8 40	10 11	10 7	10 2	9 56	9 50	9 44	9 37	9 30	9 22	9 13	9 3
- 8 20	10 16	10 12	10 7	10 2	9 56	9 50	9 44	9 37	9 29	9 21	9 11
- 8 0	10 21	10 17	10 12	10 7	10 2	9 56	9 50	9 43	9 36	9 28	9 19

Declination	LATITUDE NORTH.									
of the Sun.	71°	72°	73°	74°	75°	76°	77°	78°	79°	80°
-23°27′ -23°20 -23°0	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
-22 40 -22 20 -22 0										
-21 40 -21 20 -21 0										
-20 40 -20 20 -20 0		i								
-19 40 - 19 20 - 19 0	I 3 I 50 2 22								l	
- 18 40 - 18 20 - 18 0	2 47 3 10 3 30	1 5 1 52 2 25								
-17 40 -17 20 -17 0	3 49 4 6 4 22	2 52 3 14 3 35	1 6 1 55 2 29							
- 16 40 - 16 20 - 16 0	4 37 4 52 5 6	3 54 4 12 4 28	2 56 3 20 3 4I	1 8 1 58 2 32						
- 15 40 - 15 20 - 15 0	5 19 5 3 ² 5 44	4 44 4 59 5 ¹ 3	4 I 4 I9 4 36	3 I 3 25 3 47	1 10 2 2 2 37					
-14 40 -14 20 -14 0	5 56 6 8 6 19	5 27 5 40 5 52	4 52 5 7 5 21	4 7 4 26 4 43	3 6 3 31 3 54	1 13 2 5 2 42				
-13 40 -13 20 -13 0	6 29 6 40 6 51	6 5 6 17 6 29	5 35 5 49 6 2	5 0 5 16 5 31	4 14 4 34 4 52	3 12 3 38 4 2	1 15 2 10 2 48			
- 12 40 - 12 20 - 12 0	6 I 7 II 7 2I	6 40 6 50 7 I	6 15 6 27 6 39	5 45 5 59 6 13	5 9 5 25 5 41	4 23 4 43 5 2	3 19 3 46 4 10	1 18 2 15 2 55		
-II 40 - II 20 - II 0	7 3 ¹ 7 40 7 50	7 12 7 23 7 33	6 51 7 3 7 14	6 26 6 38 6 51	5 56 6 11 6 25	5 19 5 38 5 54	4 32 4 53 5 13	3 27 3 55 4 20	1 21 2 20 3 2	
-10 40 -10 20 -10 0	7 59 8 8 8 17	7 43 7 53 8 3	7 25 7 35 7 46	7 3 7 15 7 27	6 34 6 52 7 4	6 9 6 23 6 38	5 31 5 49 6 6	4 43 5 5 5 25	3 35 4 5 4 31	1 25 2 27 3 10
- 9 40 - 9 20 - 9 0	8 26 8 35 8 44	8 13 8 22 8 31	7 56 8 7 8 17	7 38 7 50 8 1	7 17 7 29 7 41	6 52 7 6 7 20	6 22 6 38 6 53	5 44 6 3 6 21	4 56 5 19 5 40	3 46 4 17 4 44
- 8 40 - 8 20 - 8 0	8 53 9 I 9 IO	8 41 8 50 8 59	8 27 8 37 8 47	8 11 8 22 8 33	7 53 8 5 8 17	7 33 7 46 7 59	7 8 7 22 7 36	6 38 6 55 7 11	6 0 6 19 6 38	5 10 5 34 5 56

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

Declination of		٠			LATIT	UDE N	ORTH.				
the Sun.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	70°
-8° 0′	h. m. 10 21	h. m. 10 17	h. m. 10 12	h. m.	h. m. IO 2	h. m. 956	h. m. 9 50	h. m. 9 43	h. m. 9 36	h. m. 9 28	h. m.
-7 40	10 26	10 22	10 17	10 13	10 8	10 2	9 56	9 50	9 43	9 35	9 2 7
-7 20	10 31	10 27	10 23	10 18	10 13	10 8	10 3	9 57	9 50	9 43	9 35
-7 0	10 35	10 32	10 28	10 23	10 19	10 14	10 9	10 4	9 57	9 50	9 43
6 40	10 40	10 37	10 33	10 29	10 25	10 20	10 15	10 10	10 4	9 57	9 51
6 20	10 45	10 42	10 38	10 34	10 31	10 26	10 22	10 16	10 11	10 5	9 58
6 0	10 50	10 47	10 43	10 40	10 36	10 32	10 28	10 23	10 18	10 12	10 6
-5 40	10 55	10 52	10 49	10 45	10 41	10 38	10 34	10 29	10 25	10 19	10 14
-5 20	10 59	10 56	10 54	10 50	10 47	10 44	10 40	10 36	10 31	10 26	10 21
-5 0	11 4	11 1	10 59	10 56	10 53	10 50	10 46	10 42	10 38	10 34	10 29
-4 40 -4 20 -4 0	11 13 11 18	11 16 11 11	11 4 11 9 11 14	II I II 7 II I2	10 58 11 4 11 10	10 55 11 1 11 7	10 52 10 58 11 4	10 49 10 55 11 1	10 45 10 52 10 58	10 41 10 48 10 55	10 36 10 44 10 51
-3 40 -3 20 -3 0	II 22 II 27 II 32	11 21 11 26 11 31	11 19 11 24 11 29	11 17 11 22 11 28	11 15 11 20 11 26	11 13 11 19 11 24	II IO II 16 II 22	11 8 11 14 11 20	11 5 11 18	11 2 11 9 11 16	10 59 11 6 11 13
-2 40	11 37	11 35	11 34	11 33	11 31	11 30	11 28	11 27	11 25	11 23	11 21
-2 20	11 41	11 40	11 39	11 38	11 37	11 36	11 34	11 33	11 32	11 30	11 28
-2 0	11 46	11 45	11 44	11 43	11 43	11 41	11 40	11 40	11 38	11 37	11 35
-1 40	11 50	11 50	11 49	11 49	11 48	11 47	11 46	11 46	11 45	11 44	11 43
-1 20	11 55	11 55	11 54	11 54	11 53	11 53	11 52	11 52	11 52	11 51	11 50
-1 0	11 59	11 59	11 59	11 59	11 59	11 59	11 58	11 58	11 58	11 58	11 58
-0 40	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 5	12 5	12 5
-0 20	12 9	12 9	12 9	12 IO	12 IO	12 10	12 IO	12 11	12 11	12 12	12 12
0 0	12 13	12 14	12 14	12 15	12 15	12 16	12 16	12 17	12 18	12 19	12 19
+0 20	12 18	12 19	12 19	12 20	12 20	12 22	12 22	12 23	12 25	12 26	12 27
0 40	12 22	12 23	12 24	12 25	12 26	12 27	12 28	12 29	12 31	12 33	12 34
I 0	12 27	12 28	12 29	12 31	12 32	12 33	12 34	12 36	12 38	12 40	12 41
I 20	12 32	12 33	12 34	12 36	12 37	12 39	12 40	12 42	12 44	12 47	12 49
I 40	12 37	12 38	12 39	12 41	12 43	12 44	12 46	12 49	12 51	12 54	12 56
2 0	12 41	12 43	12 44	12 46	12 48	12 50	12 52	12 55	12 58	13 I	13 4
2 20	12 46	12 47	12 49	12 52	12 53	12 56	12 59	13 1	13 4	13 8	13 11
2 40	12 50	12 52	12 54	12 57	12 59	13 2	13 5	13 7	13 11	13 15	13 19
3 0	12 55	12 57	12 59	13 2	13 5	13 8	13 11	13 14	13 17	13 22	13 26
3 20	13 0	13 2	13 5	13 7	13 10	13 13	13 17	13 20	13 24	13 29	13 34
3 40	13 4	13 7	13 10	13 13	13 16	13 19	13 23	13 27	13 31	13 36	13 41
4 0	13 9	13 12	13 15	13 18	13 22	13 25	13 29	13 33	13 38	13 43	13 49
4 20	13 14	13 17	13 20	13 23	13 27	13 31	13 35	13 40	13 45	13 50	13 56
4 40	13 19	13 22	13 25	13 29	13 32	13 37	13 41	13 46	13 52	13 58	14 4
5 0	13 23	13 27	13 30	13 34	13 38	13 43	13 47	13 53	13 58	14 5	14 11
5 20	13 28	13 32	13 35	13 40	13 44	13 49	13 54	13 59	14 5	14 12	14 19
5 40	13 33	13 37	13 41	13 45	13 50	13 55	14 0	14 6	14 12	14 19	14 27
6 0	13 38	13 42	13 46	13 50	13 55	14 I	14 6	14 13	14 19	14 26	14 35
6 20	13 43	13 47	13 51	13 56	14 1	14 7	14 12	14 19	14 26	14 34	14 43
6 40	13 47	13 52	13 56	14 1	14 7	14 I3	14 18	14 26	14 33	14 42	14 51
7 0	13 52	13 57	14 1	14 7	14 12	14 19	14 25	14 32	14 40	14 49	14 59
7 20	13 57	14 2	14 7	14 13	14 18	14 25	14 31	14 39	14 48	14 57	15 7
7 40	14 2	14 7	14 12	14 18	14 24	14 31	14 38	14 46	14 55	15 4	15 15
8 0	14 7	14 12	14 17	14 2 3	14 30	14 37	14 45	14 52	15 2	15 12	I5 23

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

Declination of				I,	ATITUDI	e nort	rH.			
the Sun.	`71°	72°	73°	74°	75°	76°	77°	78°	79°	80°
-8° 0′	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
	9 10	8 59	8 47	8 33	8 17	7 58	7 37	7 10	6 38	5 56
-7 40	9 18	9 08	8 56	8 43	8 28	8 11	7 50	7 26	6 56	6 18
-7 20	9 26	9 17	9 6	8 53	8 39	8 23	8 4	7 41	7 14	6 38
-7 0	9 35	9 26	9 16	9 3	8 50	8 35	8 17	7 56	7 31	6 58
-6 40	9 43	9 34	9 25	9 14	9 I	8 47	8 30	8 11	7 47	7 17
-6 20	9 51	9 43	9 34	9 24	9 I2	8 59	8 43	8 25	8 3	7 36
-6 0	9 59	9 52	9 43	9 34	9 23	9 11	8 56	8 39	8 19	7 54
-5 40	10 7	10 I	9 53	9 44	9 34	9 22	9 9	8 53	8 34	8 11
-5 20	10 15	10 9	10 2	9 53	9 44	9 34	9 22	9 7	8 50	8 28
-5 0	10 23	10 I7	10 11	10 3	9 55	9 45	9 34	9 20	9 5	8 46
-4 40	10 31	10 26	10 20	IO I3	10 5	9 56	9 46	9 34	9 19	9 2
-4 20	10 39	10 34	10 29	IO 22	10 15	10 7	9 58	9 47	9 34	9 18
-4 0	10 47	10 43	10 38	IO 32	10 26	10 18	10 10	10 0	9 49	9 34
-3 40	10 55	10 51	10 46	10 41	10 36	10 29	10 22	10 13	10 3	9 50
-3 20	11 3	10 59	10 55	10 51	10 46	10 40	10 34	10 26	10 17	10 6
-3 0	11 11	11 8	11 4	11 0	10 56	10 51	10 45	10 39	10 31	10 22
-2 40	11 19	11 16	11 13	II 10	11 6	II 2	10 57	10 52	10 45	10 37
-2 20	11 26	11 24	11 22	II 19	11 16	II 13'	11 8	11 4	10 59	10 52
-2 0	11 34	11 32	11 31	II 28	11 26	II 23	11 20	11 17	11 13	11 8
-I 40	11 42	11 41	11 39	11 38	11 36	11 34	11 32	11 29	11 26	11 23
-I 20	11 49	11 49	11 48	11 47	11 46	11 45	11 43	11 42	11 40	11 38
-I 0	11 57	11 57	11 56	11 56	11 56	11 55	11 55	11 55	11 54	11 53
-0 40	12 5	12 5	12 5	12 5	12 6	12 6	12 7	12 7	12 8	12 8
-0 20	12 13	12 13	12 14	12 15	12 16	12 17	12 18	12 20	12 21	12 23
0 0	12 20	12 22	12 22	12 24	12 26	12 28	12 29	12 32	12 35	12 38
+0 20	12 28	12 30	12 31	12 34	12 36	12 38	12 41	12 44	12 49	12 53
0 40	12 36	12 38	12 40	12 43	12 46	12 49	12 53	12 57	13 2	13 9
I 0	12 44	12 46	12 49	12 52	12 56	13 O	13 5	13 10	13 16	13 24
I 20	12 52	12 55	12 58	13 2	13 6	13 II	13 16	13 2 3	13 30	13 40
I 40	12 59	13 3	13 7	13 11	13 16	13 22	13 28	13 36	13 44	13 55
2 0	13 7	13 11	13 16	13 20	13 26	13 32	13 40	13 49	13 59	14 11
2 20	13 15	13 19	13 25	13 30	13 36	13 43	13 52	14 1	14 13	14 27
2 40	13 23	13 28	13 33	13 40	13 46	13 54	14 4	14 14	14 28	14 43
3 0	13 31	13 36	13 42	13 49	13 57	14 5	14 16	14 28	14 42	14 59
3 20	13 39	13 44	13 51	13 59	14 7	14 17	14 28	14 41	14 56	15 16
3 40	13 47	13 53	14 1	14 8	14 17	14 28	14 40	14 55	15 11	15 33
4 0	13 55	14 2	14 10	14 18	14 28	I4 40	14 53	15 8	15 27	15 50
4 20	14 3	14 10	14 19	14 28	14 38	I4 5I	15 5	15 22	15 43	16 7
4 40	14 11	14 19	14 28	14 38	14 49	I5 2	15 18	15 36	15 58	16 25
5 0	14 19	14 28	14 37	14 48	15 O	15 14	15 31	15 50	16 14	16 44
5 20	14 27	14 37	14 46	14 58	15 II	15 26	15 44	16 5	16 31	17 3
5 40	14 35	14 45	14 56	15 8	15 22	15 38	15 57	16 20	16 47	17 22
6 0	I4 44	14 54	15 5	15 19	15 33	15 50	16 11	16 35	17 5	17 43
6 20	I4 52	15 3	15 15	15 29	15 44	16 3	16 25	16 51	17 23	18 5
6 40	I5 I	15 12	15 25	15 40	15 56	16 16	16 39	17 7	17 41	18 2 7
7 0	15 10	15 22	15 35	15 50	16 8	16 2 9	16 53	17 23	18 I	18 50
7 20	15 18	12 31	15 45	16 1	16 20	16 42	17 8	17 40	18 2I	19 16
7 40	15 27	15 40	15 55	16 12	16 32	16 55	17 2:	17 58	18 42	19 44
8 0	15 35	15 50	16 5	16 23	16 44	17 9	17 39	18 16	19 5	20 15

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

Declination					Latit	UDE N	ORTH.				
of the Sun.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	70°
	h. m.	h. m.	h. m.								
+ 8° 0′	14 7	14 12	14 17	14 23	14 30	14 37	14 45	14 53	15 2	15 12	15 23
8 20	14 12	14 1;	14 23	14 29	14 36	14 43	14 52	15 0	15 10	15 20	15 32
8 40	14 17	14 22	14 28	14 35	14 42	14 50	14 58	15 7	15 17	15 28	15 40
9 0	14 22	14 27	14 34	14 41	14 48	14 56	15 5	15 14	15 25	15 36	15 49
9 20	14 27	14 32	14 39	14 46	14 54	15 2	15 11	15 21	15 32	15 44	15 57
9 40	14 32	14 38	14 45	14 52	15 0	15 9	15 18	15 28	15 40	15 52	16 6
10 0	14 37	14 43	14 50	14 58	15 6	15 15	15 25	15 35	15 47	16 0	16 15
10 20	14 42	14 49	14 56	15 4	15 13	15 22	15 32	15 43	15 55	16 8	16 24
10 40	14 47	14 54	15 2	15 10	15 19	15 28	15 39	15 5 0	16 3	16 17	16 33
11 0	14 52	14 59	15 7	15 16	15 25	15 35	15 46	15 58	16 11	16 26	16 42
11 20	14 57	15 5	15 13	15 22	15 31	15 41	15 53	16 5	16 19	16 34	16 52
11 40	15 2	15 10	15 19	15 28	15 38	15 48	16 0	16 13	16 27	16 43	17 1
12 0	15 8	15 16	15 25	15 34	15 44	15 55	16 7	16 21	16 35	16 52	17 11
12 20	15 13	15 21	15 31	15 40	15 50	16 2	16 15	16 29	16 44	17 1	17 21
12 40	15 18	15 27	15 36	15 46	15 57	16 9	16 22	16 37	16 53	17 11	17 31
13 0	15 23	15 33	15 42	15 53	16 4	16 16	16 30	16 45	17 2	17 20	17 41
13 20	15 29	15 39	15 48	15 59	16 11	16 23	16 37	16 53	17 10	17 30	17 52
13 40	15 35	15 44	15 55	16 5	16 17	16 31	16 45	17 1.	17 19	17 40	18 3
14 0	15 40	15 50	16 1	16 12	16 24	16 38	16 53	17 10	17 29	17 50	18 14
14 20	15 46	15 56	16 7	16 19	16 31	16 46	17 1	17 19	17 38	18 0	18 26
14 40	15 51	16 2	16 13	16 25	16 38	16 53	17 9	17 28	17 48	18 11	18 38
15 0	15 57	16 8	16 19	16 32	16 46	17 1	17 17	17 37	17 58	18 22	18 50
15 20	16 2	16 14	16 26	16 39	16 53	17 9	17 26	17 46	18 8	18 33	19 3
15 40	16 8	16 20	16 32	16 46	17 1	17 17	17 35	17 55	18 18	18 45	19 16
16 0	16 14	16 26	16 39	16 53	17 8	17 25	17 44	18 5	18 29	18 57	19 30
16 20	16 20	16 32	16 46	17 0	17 16	17 33	17 53	18 15	18 40	19 10	19 45
16 40	16 26	16 39	16 52	17 7	17 23	17 41	18 2	18 25	18 51	19 23	20 1
17 0	16 32	16 45	16 59	17 14	17 31	17 50	18 11	18 35	19 3	19 36	20 17
17 20	16 38	16 52	17 6	17 22	17 39	17 59	18 21	18 46	19 15	19 50	20 35
17 40	16 45	16 58	17 13	17 29	17 47	18 8	18 31	18 57	19 28	20 6	20 55
18 0	16 51	17 5	17 20	17 37	17 56	18 17	18 41	19 8	19 41	20 22	21 17
18 20	16 58	17 12	17 28	17 45	18 5	18 26	18 52	19 2 0	19 55	20 40	21 42
18 40	17 4	17 19	17 35	17 53	18 14	18 36	19 3	19 33	20 10	20 59	22 13
19 0	17 11	17 26	17 43	18 2	18 23	18 46	19 14	19 46	20 26	21 20	22 58
19 20	17 17	17 33	17 51	18 10	18 32	18 56	19 25	20 0	20 44	21 45	
19 40	17 24	17 41	17 59	18 19	18 41	19 7	19 37	20 14	21 3	22 16	
20 0 20 20 20 40	17 31 17 38 17 45	17 48 17 56 18 4	18 7 18 15 18 23	18 28 18 37 18 46	18 51 19 1 19 12	19 19 19 30 19 42	19 50 20 4 20 19	20 30 20 47 21 5	21 23 24 47 22 17	22 59	
21 0 21 20 21 40	17 52 18 0 18 8	18 11 18 20 18 28	18 32 18 41 18 50	18 56 19 6 19 16	19 23 19 34 19 46	19 25 20 8 20 22	20 34 20 50 21 8	21 26 21 50 22 19	23 I		
22 0 22 20 22 40	18 16 18 24 18 32	18 37 18 46 18 55	19 0 19 10 19 20	19 27 19 38 19 50	19 58 20 11 20 25	20 37 20 53 21 11	21 29 21 52 22 21	23 2			
23 0 23 20 23 27	18 41 18 49 18 52	19 4 19 13 19 17	19 31 19 41 19 46	20 2 20 14 20 19	20 40 20 56 21 2	21 31 21 54 22 3	23 3				

DIFFERENT LATITUDES.

DURATION OF SUNSHINE AT DECLINATION OF THE SUN FOR THE YEAR 1899.

	-	M-M		an Mark	
Declination of the Sun.		LATI1	UDE NO	JRTH.	
the sun.	71°	72°	73°	74°	75°
+ 8° 0′	h. m. 15 35 15 44	h, m. 15 50 15 59	h. m. 16 5 16 16	h. m. 16 23 16 35	h, m. 16 44 16 57
8 40 9 0 9 20 9 40	15 53 16 3 16 12 16 22	16 19 16 29 16 39	16 26 16 37 16 48 16 59	16 46 16 58 17 10 17 23	17 10 17 23 17 37 17 51
10 0 10 20 10 40	16 31 16 41 16 50	16 50 17 0	17 11 17 22 17 34	17 35 17 49 18 2	18 5 18 20 18 36
II 0 II 20 II 40	17 I 17 II 17 22	17 22 17 34 17 45	17 47 17 59 18 13	18 16 18 31 18 46	18 52 19 9 19 2 7
12 0 12 20 12 40	17 32 17 43 17 55	17 57 18 9 18 22	18 26 18 40 18 55	19 1 19 18 19 35	19 46 20 7 20 29
13 0 13 20 13 40	18 6 18 18 18 30	18 35 18 49 19 2	19 11 19 26 19 43	19 54 20 14 20 35	20 55 21 23 21 59
14 0 14 20 14 40	18 43 18 56 19 10	19 17 19 33 19 49	20 I 20 20 20 4I	21 0 21 28 22 2	22 50
15 0 15 20 15 40	19 24 19 40 19 55	20 7 20 26 20 46	2I 5 2I 32 22 5	22 52	
16 0 16 20 16 40	20 13 20 31 20 51	21 10 21 36 22 8	22 54		
17 0 17 20 17 40	21 13 21 39 22 11	22 56		-	
	76°	77°	78°	·79°	80°
+ 8° 0′ 8 20 8 40	17 9 17 23 17 38	17 39 17 55 18 12	18 16 18 35 18 56	19 5 19 29 19 56	20 15 20 50 21 33
9 0 9 20 9 40	17 53 18 8 18 25	18 30 18 48 19 8	19 17 19 41 20 6	20 25 20 59 21 40	22 35
10 0 10 20 10 40	18 41 18 59 19 18	19 28 19 50 20 15	20 31 21 6 21 46	22 39	
11 0 11 20 11 40	19 38 19 59 20 23	20 41 21 13 21 50	22 43		
12 0 12 20 12 40	20 49 21 19 21 55	22 46			

Day of	Zan	. 1	Feb		Ма	
Day of Month.	Jan	.				_
1 4 7 10 13	23° 22 22 21 21	o' 44 22 57 28	-17° 16 15 14	4' 12 16 19	7° 6 5 4 2	33' 24 14 4 53
16 19 21 24 27 30	20 20 19 19 18	55 19 53 11 26 38	12 11 10 9 8	15 14 31 25 18	- o + o I 2 3	42 31 16 27 38 48
	Apı	<i>r</i> .	Ma	ν.	Jun	e.
1 4 7 10	+ 4° 5 6 7	34' 43 51 58 4	+15° 15 16 17 18	6/ 59 50 38 24	+22° 22 22 23 23	4' 27 46 1
16 19 21 24 27 30	10 11 11 12 13	9 12 53 53 51 48	19 19 20 20 21 21	7 47 12 47 19 47	23 23 23 23 23 23	22 26 27 25 20 11
	Jul	γ.	Au	g.	Sep	ot.
1 4 7 10	+23° 22 22 22 21	7' 53 36 15 50	+ 18° 17 16 15	1/ 15 26 34 40	+ 8° 7 6 4 3	17' 11 4 56 47
16 19 21 24 27 30	21 20 20 19 19 18	22 51 29 52 13 31	13 12 12 11 10	41 46 7 6 4 0	2 1 + 0 - 0 1 2	38 28 42 29 39 49
	Oct	t.	No	ν.	De	ec.
1 4 7 10 13	- 3° 4 5 6 7	12' 22 31 40 48	-14° 15 16 17 18	24 18 10 0	-21° 22 22 22 23	16 38 56 10
16 19 21 24 27 30	8 10 10 11 12 13	55 0 43 47 48 49	18 19 19 20 21 21	46 29 56 35 9 40	23 23 23 23 23 23 23	20 26 27 26 20 10

DURATION OF ASTRONOMICAL TWILIGHT.

(Interval between sunrise or sunset and the time when the true position of the sun's center is 18° below the horizon.)

D-4-												•	N	ORI	н	LAT	ri]	ומטי	€.											
Date,	6)°	1	O°	2	20°	2	25°	3	o°	3	2°	3	4°	3	6°	3	8°	4	ł0°	4	ŀ2°	4	4°	4	6°	4	18°	Ę	50°
Jan. 1	1	m. 14		m.	1	· m.	1	m. 2I	1			m. 28	1	m. 29				. m. 34	1	. m.	1	m. 41		. m.			1	. m.	1	. m.
11 21		14 13		14 13				21 20				27 25						33 32		36 34				43 41		47 45	I	52 49	I	57 54
Γeb. 1	1	I 2 I I I O	1	I 2 I 2 I I	1	14	1	18 17 16	I	21	1		τ		1	27	I	29	1	33 32 31	1	36 34 33	I	39 37 36	1	43 41 40	1	47 45 44	I	52 49 48
Mar. 1	I	09	I	10	1	13	1		1	19	Ι	21	I	23	I	25	1	28	Ι	30 30 31	Ι	33	1	36	1	39 39 41	1	43	I	48 48 50
Apr. 1	1		I	11	1	15	1	17 18 20	1	22	I	24	1		I	30	1	33	I	33 36 39	1	39	1	40 43 48	1	44 48 54	1		2	54 00 08
May 1	I	- 1	I	13 14 15	1	19	1	22 24 26	Ι	30	1	33	1		1	40	I		1	43 48 54	1		2	54 01 10	2	01 10 20	2	10 20 35	2	20 35 58
June 1	I		r	17	Ι		I	28 29 29	1		1	40	I		I	49	I	55	2	59 02 03	-2	12	2		2	31 40 44	3	11		
July 1 11 21	1	15 14 13	1	16	1	24 23 21	1	29 28 26	I	35	1	38	I	41	1	46	1	55 52 48	I	6 2 59 54	2		2	23 18 10	2	40 31 21	2	54		00
Aug. 1	I	12	1	14 13 12	I	18	Į	22	1	27	1	30	I	33	I	36	1	39	1	48 43 39	I	48	I	02 54 48	2	10 01 54	2	10	2	35 20 09
Sept. 1 11 21	1		I		1	14 13 13	1	18 17. 16	I	2 I	Ι	23	1	25	1	27	I	30	I	36 33 31	Ι		I	43 39 37	I	48 44 41	I	53 49 45	1	00 54 50
Oct. 1	1	- 1	I	10 11	I	13 13 13	I	16 16	1	19	1	21	I		Ι	25	Ι		1	30 30 31	I	33	1		I		I	43	I	48 48 48
Nov. 1 11 21	I	12	I	12	1	16	I	18	Ι	22	Ι	24	Ι	26	I	28	τ	30	1	32 33 35	Ι	36	Ι	40	Ι	43	1	47	I	49 52 55
Dec. 1	I	14	I		I	18 18 19	I	22	1	26	Ι	28	1	30	Ι	32	1	34	I	36 37 38	I	41	1	44 45 45	I		1	53	I	57 59 59

SMITHSONIAN TABLES.

DURATION OF CIVIL TWILIGHT.

(Interval between sunrise or sunset and the time when the true position of the sun's center is 6° below the horizon.)

[Minutes.]

Date.		NORTH LATITUDE.													
pate.	,O _o	10°	20°	25°	30°	32°	34°	36°	38°	40°	42°	44°	46°	48°	50°
Jan. 1	22	22	24	25	27	27	28	28	29	30	32	33	34	36	39
11 21	22	22 22	24 23	25 24	26 26	27 26	28 27	28 27	29 28	30 29	31 30	32 32	33 33	35 34	38 37
Feb. 1	22	22	23	24	25	26	27	27	27	28	29	31	32	34	35
11 21	22 2I	22 22	22 22	23 23	25 24	26 25	26 25	27 26	27 27	28 28	29 28	30 29	31 30	33 32	34 33
Mar. 1	21	22	22	23	24	24	25	26	27	28	28	29	30	31	33
11 21	2I 2I	2 I 2 I	22	23 23	24 24	24 24	25 25	26 26	26 26	27 27	27 27	29 28	30 30	31 31	3 ² 33
Apr. 1	21	21	-22	23	24	25	25	26 26	27	28 28	28 28	29	30	32	33
1 I 2 I	2I 22	22	22 22	23 23	24 25	25 25	26 26	27	27 28	28	20 29	29 30	31 32	32 34	34 35
Мау т	22	22	23	24	25 26	26	27 28	28	28	29	30	32	33	35	36
11 21	22 22	22 22	23 24	24 25	27	27 28	28	29 29	29 30	30 31	33	33 35	35 36	36 38	39 41
June I	22 22	22	24 24	25 26	27 28	28 28	28 20	29 30	31 31	32 33	34	36 36	37 38	40 41	43
21	22	23 23	25	26 26	28	29	29	30	31	33	34 34	36	38	42	44 44
July 1	22 22	23 22	24 24	26 25	28 27	28 28	29 28	30 20	31 31	33 32	34 34	36 36	38	41 40	44
21	22	22	24	25	27	28	28	29	30	3 ²	33	35	37 36	38	43 41
Aug. 1	22 22	22	23 23	24 24	26 25	27 26	28 27	29 28	29 28	30 20	31 30	33 32	35	36 35	39 36
21	22	22	22	23	25	25	26	28	28	28	29	30	33 32	34	35
Sept. 1	2I 2I	22 2I	22	23 23	24 24	25 25	26 25	26 26	27 27	28 28	28 28	29 20	31 30	32 31	34 33
21	21	21	22	23	24	24	25	26	26	27	27	29	30	31	32
Oct. 1	2I 2I	2I 22	22	23 23	24 24	24 24	25 25	26 26	26 27	27 28	27 28	29 20	30 30	31 31	3 ² 33
21	21	22	22	23	24	25	25	26	27	28	28	29	30	32	33
Nov. 1	22 22	22	22 23	23 24	25 25	25 26	26 27	27 28	28 28	28 20	29 30	30 • 31	3I 32	33 33	34 35
2 I	22	22	23	24	26	26	27	28	28	29	30	32	33	33 34	37
Dec. 1	22 22	2 ['] 2 22	24 24	25 25	26 27	27 27	28 28	28 28	29 29	30 30	31 32	33 33	34 34	35 36	38 39
21	22	23	24	25 25	27	27	28	28	29	31	32	33	34	37	39

SMITHSONIAN TABLES.

RELATIVE INTENSITY OF SOLAR RADIATION.

Mean intensity J for 24 hours of solar radiation on a horizontal surface at the top of the atmosphere and the solar constant A, in terms of the mean solar constant A₀.

		R	elati	VE M	EAN	Verti	CAL I	NTEN	SITY	$\left(\frac{J}{A_{\circ}}\right)$) ·	
Date.	Longitude of the Sun.				I,A	TITUD	E NOR	тн.				$\frac{A}{A_{\circ}}$.
		0°	10°	20°	30°	40°	50°	60°	70°	80°	90°	
Jan. 1	o:99 15.78	o.303 .307	0.265 .271	0.220	o. 169 . 180	0.117	o.o66 .o78	0.018				1.0335 1.0324
Feb. 1	31.54 45.34	.312	.282 .293	.244 .261	.200	.150 .177	.100	.048 .075	0.006			1.0288
<i>Mar</i> . 1	59.14 73.93	.320 .321	.303	.279 .296	.245 .270	.204 .236	.158	.108	.056	0.013		1.0173
<i>Apr.</i> 1	89.70 104.49	.317 .311	.319	.312	.295 .315	.269 .297	.235 .271	.195 .238	.148	.101	0.082	1.0009 0.9923
May 1	119.29 134.05	.303 .294	.318	.330 .333	.329 .339	.320 -337	.302	.278 .312	.253 .298	.255 .317	.259	0.9841 0.9772
June 1	149.82 164.60	.287 .283	.315	·334 ·334	·345 ·348	·349 ·354	·345 ·353	·337 ·348	·344 .361	.360 .378	.366 .384	0.9714 0.9679
July 1 16	179.39 194.13	.283 .287	.312 ·314	·333 ·332	·347 ·342	·352 ·345	.351 .340	·345 ·329	.356 .331	·373 ·347	·379 ·352	0.9666 0.9674
Aug. 1	209.94 224.73	.294 .303	.316 .318	.330 .325	·334 ·322	.330	.318 .291	.300 .264	.282 .234	.295	.300	0.9709 0.9760
Sept. 1 16	240.50 255.29	.310 .315	.318 .315	.316 .305	.305 .284	.285 .256	.256	.220 .178	,180 .130	.139	.140	0.98 2 8 0.9909
<i>Oct</i> . 1	270.07 284.86	.317 .316	.308 .298	.289 .271	.261 .236	.225	.183	.135 .097	.084 .047	.06 <u>5</u>		0.9995 1.0080
<i>Nov</i> . 1	300.63 315.42	.312	.286 .276	.251 .235	.211 .190	.164 .140	.114	.063 .040	.018			1.0164 1.0235
<i>Dec</i> . 1	330.19 344.98	.304 .302	.267 .263	.224 .218	.175 .167	.124	.072 .064	.024				1.0288
Year		0.305	0.301	0.289	0.268	0,241	0.209	0.173	0.144	0.133	0.126	

TABLE 92.

RELATIVE AMOUNTS OF SOLAR RADIATION RECEIVED ON A

HORIZONTAL SURFACE DURING THE YEAR AT DIFFERENT LATITUDES.

Latitude.					
(North.)	1.0	0.9	0.8	0.7	0.6
Equator.	439	374	316	262	213
l0°	433	368	310	257	209
20°	416	350	293	242	195
30°	386	322	266	213	171
30° 40°	347	284	231	185	144
50°	301	239	190	149	114
60°	249	191	148	113	84
70° 80°	207	152	113	83	60
80°	192	134	94	64	43
90°	181	125	94 85	56	35

TABLE 93.

AIR MASS, M, CORRESPONDING TO DIFFERENT ZENITH DISTANCES

OF THE SUN.

				sun's z	ENITH DI	STANCE.				
Sun'a zenith	o°	1°	2°	3 °	4 °	5°	6°	7°	8°	9°
distance.					AIR MA	SS.				
0	1.00									
10	1.02					1.04				
20	1.06	1.07	1.08	1.09	1.09	1.10	1.11	I, I2	1.13	1.14
30	1.15	1.17	1.18	1.19	1.20	1.22	1.24	1.25	1.27	1.28
40	1.30	1.32	1.34	1.37	1.39	1.41	1.44	1.46	1.49	1.52
50	1.55	1.59	1.62	1.66	1.70	1.74	1.78	1.83	1.88	1.94
60	2.00	2.06	2.12	2.20	2.27	2.36	2.45	2.55	2.65	2.7
70	2.90	3.05	3.21	3.39	3.59	3.82	4.08	4.37	4.72	5. 1:
80	5.60	6.18	6.88	7 - 77	8.90	10.39	12.44	15.36	19.79	26.90

TABLE 94.

RELATIVE ILLUMINATION INTENSITIES.

Source of illumination.	Intensity.	Ratio to zenithal full moon.
Zenithal sun Sky at sunset Sky at end of civil twilight Zenithal full moon Quarter moon Starlight	0.40 0.02 0.002	465000.0 1650.0 20.0 1.0 0.1

MISCELLANEOUS TABLES.

WEIGHT IN GRAMS OF A	CUBIC CENTIMETER OF AIR:	
English measures —	Temperature term Table	95
	Humidity term; auxiliary table Table	96
	Humidity and pressure terms, combined Table	97
Metric measures —	Temperature term Table	98
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	Humidity and pressure terms, combined TABLE I	:OC
Atmospheric water-vapo	r lines in the visible spectrum TABLE I	01
Atmospheric water-vapo	r bands in the infra-red spectrum . TABLE I	02
Transmission percentage	s of radiation through moist air TABLE I	03
International Meteorolog	gical Symbols Table 1	04
International Cloud Class	esification Table 1	05
Beaufort Weather Notat	ion TABLE I	06
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WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Temperature term: $\delta_t = \frac{0.00129305}{1 + 0.0020389 (t - 32^\circ)}$. Fahrenheit temperatures.

1 cubic centimeter of dry air at the temperature 32° F. and pressure 760 mm., under the standard value of gravity and sea-level, weighs 0.00129305 gram.

standard varue of gravity and sea-level, weighs 0.00129305 gram.								
Temper- ature.	δ_{t}	Log δ_t	Temper- ature.	δ_{t}	Log δ _t	Temper- ature.	δ_{t}	Log δ _t
F.	0.00	– 10	F.	0.00	– 10	F.	0.00	7.0
-45°	15339	7.18579	30°	0.00	7.11339	75°	11888	7.07512
- 40	15155	.18056	31	12957	.11250	76	11866	.07430
-35	14977	.17541	32	12931	.11162	77	11844	.07349
- 30	14802	.17031	33	12904	.11073	78	11822	.07268
- ž ₅	14631	.16527	34	12878	.10985	79	11800	.07187
	0.00			0.00			0.00	' '
-20	14464	7.16029	35	12852	7.10897	80	11778	7.07107
- 18	14398	.15831	36	12826	.10809	81	11756	.07026
- 16	14333	.15634	37 38	12800	.10721	82	11734	.06946
- 14	14269	.15439		12774	.10633	83	11713	.06865
- 12	14205	.15244	39	12749	.10546	84	11691	.06785
-10	0.00 14142	7.15050	40	0.00 12723	7.10459	85	0.00 11670	7.06705
- 8	14079	.14856	41	12/23	.10372	86	11648	.06625
- 6	14017	.14664	42	12672	.10285		11627	.06546
- 4	13955	.14472	43	12647	80101.	87 88	11605	.06466
- 2	13894	.14282	44	12622	.10112	89	11584	.06387
ti	0.00		1	0.00	l		0.00	
+ 0	13833	7.14092	45	12597	7.10025	90	11563	7.06307
1 .	13803	.13997	46	12572	.09939	91	11542	.06228
2	13773	.13903	47	12547	.09853	92	11521	.06149
3	13743	.13808	48	12522	.09767	93	11500	.06070
4	13713	.13714	49	12497	.09682	94	11479	.05992
5	13684	7.13621	50	0.00	7.09596	95	0.00 11458	7.05913
6	13654	.13527	51	12473 12448	.09511	96	11438	.05835
	13625	.13434	52	12424	.09426	97	11418	.05757
7 8	13596	13340	53	12400	.09341	98	11397	.05678
9	13567	.13247	54	12375	.09256	99	11376	.05600
1	0.00			0.00	-		0.00	
10	13538	7.13155	55	12351	7.09171	100	11356	7.05523
II	13509	.13062	56	12327	.09087	IOI	11336	.05445
12	13480	.12970	57 58	12303	.09002	102	11315	.05367
13 14	13452 13423	.12877		12280	.08918	103	11295	.05290
1 -4	0.00	.12/05	59	0.00	.00034	104	0.00	.05213
15	13395	7.12694	60	12232	7.08750	105	11255	7.05136
16	13367	.12602	61	12209	.08667	106	11235	.05058
17	13338	.12510	62	12185	.08583	107	11215	.04982
18	13310	.12419	63	12162	.08500	ю8	11196	.04905
19	13282	.12328	64	12138	.08416	109	11176	.04828
20	0.00			0.00		1	0.00	
20 21	13255	7.12237	65	12115	7.08334	110	11156	7.04752
21 22	13227 13200	.12147	66	12092	.08251 .08168	112	11117	.04599
23	13200	.12056	67 68	12069 12046	.08085	114 116	11078	.04447
24	13145	.11876	69	12040	.08003	118	11040	.04290
-	0.00	,	29	0.00		1.0	0.00	•~4.43
25	13118	7.11786	70	12001	7.07921	120	10963	7.03994
26	13091	.11696	71	11978	.07839	125	10870	.03621
27	13064	.11606	72	11956	.07757	130	10776	.03248
28	13037	.11517	73	11933	.07675	135	10686	.02883
29	13010	.11428	74	11910	.07593	140	10597	.02518

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity term: Values of 0378 e.

Auxiliary to Table 97.

e = Vapor pressure in inches.

(See Tables 69 and 70.)

Temperature by normal hydrogen thermometer.

Dew- Point.	e Vapor Pressure. (Ice.)	0.378 e	Dew- Point.	Vapor Pressure. (*)	0.378 €	Dew- Point,	Vapor Pressure. (Water.)	0.378 e	Dew- Point.	Vapor Pres- sure. (Water.)	0.378 e
F.	Inch.	Inch.	F.	Inch.	Inch.	F.	Inch.	Inch.	F.	Inches.	Inches.
−60°	0.0010	0.000	~ 10°	0.0223	6.008	40°	0.2477	0.094	90°	1.423	0.538
59	.0011	,000	9 8	.0236	.009	41	.2575	.097	91	1.469	-555
58	.0011	.000		.0249	.009	42	.2677	.101	92	1.515	.573
57 56	.0012	.000	7 6	.0263	.010.	43 44	.2782	.106	93 94	1.563	.591
-55	0.0014	0.001	5	0.0202	0.011	45	0.3003	0.114	95	1.662	0.628
-55 54	.0015	100.0	4	.0308	.012	46	.3120	.114	96	1.714	.648
53	.0016	.001	3	.0325	.012	47	.3240	.122	97	1.767	.668
52	.0017	.001	2	.0343	.013	48	.3365	.127	98	1.822	.689
51	.0018	.001	I	.0361	.014	49	•3493	.132	99	1.878	.710
-50	0.0020	0.001	± 0	0.0381	0.014	50	0.3626	0.137	100	1.936	0.732
49	.0021	.001	+ I	.0401	.015	51	.3763	.142	101	1.994	•754
48	.0023	100.	2	.0423	.016	52	.3905	.147	102	2.055	.800
47 46	.0024	.001	3 4	.0445	.017	53 54	.4052	.153	103	2.117	.824
-45	0.0028	0.001	+ 5	0.0493	0.010	55	-	0.165	105	2.246	0.849
44	.0020	.001	T 6	.0519	.020	56	0.4359 .4521	.171	106	2.314	.875
43	.0031	.001	7	.0546	.021	57	.4687	.177	107	2.382	.900
42	.0033	.001	8	.0574	.022	58	.4859	.184	108	2.453	.927
41	.0036	.001	9	.0604	.023	59	.5037	.190	109	2.525	.954
-40	0.0038	0.001	+ 10	0.0635	0.024	60	0.5220	0.197	110	2.599	0.982
39	.0040	.002	11	.0667	.025	61	.5409	.204	III	2.676	1.012
38	.0043	.002	12	.0701	.027	62 63	.5804	.212	112 113	2.754 2.833	1.041
37 36	.0040	.002	13 14	.0730	.020	64	.6013	.227	113	2.033	1.102
-35	0.0052	0.002	+15	0.0812	0.031	65	0.6226	0.235	115	2.999	1.134
34	.0055	.002	16	.0852	.032	66	.6447	.244	116	3.085	1.166
33	.0059	.002	17	.0895	.034	67	.6674	.252	117	3.173	1.199
32	.0062	.002	18	.0939	035	68	.6909	.261	118	3.264	1.234
31	.0066	.003	19	.0985	.037	69	.7150	.270	119	3.356	1.269
-30	0.0070	0.003	+20	0.1033	0.039	70	0.7399	0.280	120	3.451	1.304
29	.0075	.003	21	.1084	.041	71	.7655	.289	121 122	3.548	1.341
28	.0080	.003	22	.1136	.043	72 73	.7919	.299	122	3.647	1.417
26	.0000	.003	23 24	.1248	.047	74	.8471	.320	124	3.853	1.456
-25	0.0095	0.004	+25	0.1308	0.049	75	0.8760	0.331	125	3.960	1.497
24	.0101	.004	26	.1370	.052	76	.9056	•343	126	4.069	1.538
23	.0107	.004	27	.1435	.054	77 78	.9362	-354	127	4.180	1.580
22	.0113	.004	28	.1502	.057		.9677	.366	128	4.294	1.623
21	.0120	.005	29	.1573	.059	79	1.0001	.378	129	4.412	1.668
-20	0.0127	0.005	+30	0.1646	0.062	80	1.0334	0.391	130	4.531	1.713
19 18	.0135	.005	31	.1723	.065	81 82	1.0676	.404	131	4.654	1.759
17	.0143	.005	32	.1803	.071	83	1.1392	.431	133	4.779	1.855
16	.0151	.006	33 34	.1954	.074	84	1.1765	•445	134	5.038	1.904
~15	0.0169	0.006	+35	0.2034	0.077	85	1.2140	0.459	135	5.172	1.955
14	.0179	.007	36	.2117	.080	86	1.2543	474	136	5.309	2.007
13	.0189	.007	37	.2202	.083	87	1.2949	.489	137	5.449	2.060
I 2	.0200	.008	38	.2291	.087	88	1.3365	.505	138	5.592	
11	.0211	.008	39	.2382	.090	89	1.3794		139	5.739	
10	10 0.0223 0.008 40 0.2477 0.094 90 1.4234 0.538 140 5.889 2.226										
		* V	alues for	temperatu	res less th	nan 32° F	'. refer to v	apor over	ice.		

WEIGHT IN CRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined: $\frac{\delta}{\delta_o} = \frac{h}{29.921} = \frac{B - 0.378 \, e}{29.921}$.

B = Barometric pressure in inches; e = Vapor pressure in inches.

h.	<u>h</u> 29.921	Log h 29.921	h.	<u>h</u> 29.291	Log h 29.921	h.	h 29.921	Log h 29.921
Inch's. 0.0 10.1 10.2 10.3 10.4	0.3342 .3376 .3409 .3442 .3476	- 10 9.52402 .52835 .53262 .53686 .54106	Inches. 15.0 15.1 15.2 15.3 15.4	0.5013 •5047 •5080 •5113 •5147	- 10 9.70012 .70300 .70587 .70871 .71154	Inches. 20.0 20.1 20.2 20.3 20.4	0.6684 .6718 .6751 .6784 .6818	- 10 9.82505 .82722 .82938 .83152 .83365
10.5	0.3509	9.54521	15.5	0.5180	9.71435	20.5	0.6851	9.83578
10.6	•3543	·54933	15.6	.5214	.71715	20.6	.6885	.83789
10.7	•3576	·55341	15.7	.5247	.71992	20.7	.6918	.83999
10.8	•3609	·55745	15.8	.5281	.72268	20.8	.6952	.84209
10.9	•3643	·56145	15.9	.5314	.72542	20.9	.6985	.84417
11.0	0.3676	9.56542	16.0	0.5347	9.72814	21.0	0.7018	9.84624
11.1	.3710	·56935	16.1	.5381	.73085	21.1	.7052	.84831
11.2	.3743	·57324	16.2	.5414	.73354	21.2	.7085	.85036
11.3	.3777	·57710	16.3	.5448	.73621	21.3	.7119	.85240
11.4	.3810	·58093	16.4	.5481	.73887	21.4	.7152	.85444
11.5	0.3843	9.58472	16.5	0.5515	9.74151	21.5	0.7186	9.85646
11.6	.3877	.58848	16.6	•5548	•74413	21.6	.7219	.85848
11.7	.3910	.59221	16.7	•5581	•74674	21.7	.7252	.86048
11.8	.3944	.59591	16.8	•5615	•74933	21.8	.7286	.86248
11.9	.3977	.59957	16.9	•5648	•75191	21.9	.7319	.86447
12.0	0.4011	9.60321	17.0	0.5682	9.75447	22.0	0.7353	9.86645
12.1	.4044	.60681	17.1	.5715	.75702	22.1	.7386	.86842
12.2	.4077	.61038	17.2	.5748	.75955	22.2	.7420	.87038
12.3	.4111	.61393	17.3	.5782	.76207	22.3	.7453	.87233
12.4	.4144	.61745	17.4	.5815	.76457	22.4	.7486	.87427
12.5	0.4178	9.62093	17.5	0.5849	9.76706	22.5	0.7520	9.87621
12.6	.4211	.62439	17.6	.5882	.76954	22.6	•7553	.87813
12.7	.4244	.62782	17.7	.5916	.77200	22.7	•7587	.88005
12.8	.4278	.63123	17.8	.5949	.77444	22.8	•7620	.88196
12.9	.4311	.63461	17.9	.5982	.77687	22.9	•7653	.88386
13.0 13.1 13.2 13.3 13.4	0.4345 .4378 .4412 .4445 .4478	9.63797 .64130 .64460 .64788 .65113	18.0 18.1 18.2 18.3 18.4	0.6016 .6049 .6083 .6116	9.77930 .78170 .78410 .78648 .78884	23.0 23.1 23.2 23.3 23.4	0.7687 .7720 .7754 .7787 .7821	9.88575 .88764 .88951 .89138 .89324
13.5	0.4512	9.65436	18.5	0.6183	9.79120	23.5	0.7854	9.89509
13.6	•4545	.65756	18.6	.6216	•79354	23.6	.7887	.89693
13.7	•4579	.66074	18.7	.6250	•79587	23.7	.7921	.89877
13.8	•4612	.66390	18.8	.6283	•79818	23.8	.7954	.90060
13.9	•4646	.66704	18.9	.6317	•80049	23.9	.7988	.90242
14.0	0.4679	9.67015	19.0	o.6350 ·	9.80278	24.0	0.8021	9.90424
14.1	.4712	.67324	19.1	.6383	.80506	24.1	.8054	.90604
14.2	.4746	.67631	19.2	.6417	.80733	24.2	.8088	.90784
14.3	.4779	.67936	19.3	.6450	.80958	24.3	.8121	.90963
14.4	.4813	.68239	19.4	.6484	.81183	24.4	.8155	.91141
14.5	0.4846	9.68539	19.5	0.6517	9.81406	24.5	0.8188	9.91319
14.6	.4879	.68837	19.6	.6551	.81628	24.6	.8222	.91496
14.7	.4913	.69134	19.7	.6584	.81849	24.7	.8255	.91672
14.8	.4946	.69429	19.8	.6617	.82069	24.8	.8289	.91848
14.9	.4980	.69721	19.9	.6651	.82288	24.9	.8322	.92022

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined: $\frac{\delta}{\delta_o} = \frac{h}{29.921} = \frac{B - 0.378\,e}{29.921}$.

B = Barometric pressure in inches; e = Vapor pressure in inches.

h.	<u>h</u> 29.921	Log h 29.921	h.	<u>h</u> 29.921	Log h 29.921	h.	<u>h</u> 29.921	Log h_29.921
Inches.		_ 10	Inches.		- 10	Inches.		- 10
25.00	0.8355	9.92196	27.25	0.9107	9.95939	29.50	0.9859	9.99385
25.05	.8372	.92283	27.30	.9124	.96019	29.55	.9876	.99458
25.10	.8389	.92370	27.35	.9141	.96098	29.60	.9893	.99532
25.15	.8405	.92456	27.40	.9157	.96177	29.65	.9909	.99605
25.20	.8422	.92542	27.45	•9174	.96256	29.70	.9926	.99678
25.25	0.8439	9.92628	27.50	0.9191	9.96336	29.75	0.9943	9.99751
25.30	.8456	.92714	27.55	.9208	.96414	29.80	.9960	.99824
25.35	.8472	.92800	27.60	.9224	.96493	29.85	.9976	.99897
25.40	.8489	.92886	27.65	.9241	.96572	29.90	.9993	.99970
25.45	.8506	.92971	27.70	.9258	.96650	29.95	1.0010	0.00042
25.50	0.8522	9.93056	27.75	0.9274	9.96728	30.00	1.0026	0.00115
25.55	.8539	.93141	27.80	.9291	.96807	30.05	1.0043	.00187
25.60	.8556	.93226	27.85	.9308	.96885	30.10	1.0060	.00259
25.65	.8573	.93311	27.90	.9325	.96963	30.15	1.0076	.0033T
25.70	.8589	.93396	27.95	.9341	.97040	30.20	1.0093	.00403
25.75	o.8606	9.93480	28.00	0.9358	9.97118	30.25	1.0110	0.00475
25.80	.8623	.93564	28.05	-9375	.97195	30.30	1.0127	.00547
25.85	.8639	.93648	28.10	.9391	.97273	30.35	1.0143	.00618
25.90	.8656	.93732	28.15	.9408	.97350	30.40	1.0160	.00690
25.95	.8673	.93816	28.20	-9425	.97427	30.45	1.0177	.00761
26.00 26.05 26.10 26.15 26.20	o.8690 .8706 .8723 .8740 .8756	9.93900 .93983 .94066 .94149 .94233	28.25 28.30 28.35 28.40 28.45	0.9441 .9458 .9475 .9492 .9508	9.97504 .97581 .97657 .97734 .97810	30.50 30.55 30.60 30.65 30.70	1.0193 1.0210 1.0227 1.0244 1.0260	0.00832 .00903 .00975 .01045
26.25	o.8773	9.94315	28.55	0.9525	9.97887	30.75	1.0277	0.01187
26.30	.8790	.94398	28.55	•9542	.97963	30.80	1.0294	.01257
26.35	.8806	.94480	28.60	•9558	.98039	30.85	1.0310	.01328
26.40	.8823	.94563	28.65	•9575	.98115	30.90	1.0327	.01398
26.45	.8840	.94645	28.70	•9592	.98191	30.95	1.0344	.01468
26.50	0.8857	9.94727	28.75	0.9609	9.98266	31.00	1.0361	0.01539
26.55	.8873	.94809	28.80	.9625	.98342	31.05	1.0377	.01608
26.60	.8890	.94891	28.85	.9642	.98417	31.10	1.0394	.01678
26.65	.8907	.94972	28.90	.9659	.98492	31.15	1.0411	.01748
26.70	.8924	.95054	28.95	.9675	.98567	31.20	1.0427	.01818
26.75 26.80 26.85 26.90 26.95	0.8940 .8957 .8974 .8990	9.95135 .95216 .95297 .95378 .95458	29.00 29.05 29.10 29.15 29.20	0.9692 .9709 .9726 .9742 .9759	9.98642 .98717 .98792 .98866 .98941	31.25 31.30 31.35 31.40 31.45	1.0444 1.0461 1.0478 1.0494 1.0511	0.01887 .01957 .02026 .02095 .02164
27.00	0.9024	9.95539	29.25	0.9776	9.99015	31.50	1.0528	0.02233
27.05	.9040	.95619	29.30	•9792	.99089	31.55	1.0544	02302
27.10	.9057	.95699	29.35	•9809	.99163	31.60	1.0561	.02371
27.15	.9074	.95779	29.40	•9826	.99237	31.65	1.0578	.02439
27.20	.9091	.95 ⁸ 59	29.45	•9843	.99311	31.70	1.0594	.02508

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Temperature term: $\delta_{t, 760} = \frac{0.00129305}{1 + 0.003670 t}$. Centigrade temperature.

1 cubic centimeter of dry air at the temperature o° C. and pressure 760 mm., under the standard value of gravity and sea-level, weighs 0.00129305 gram.

		<u> </u>	1					
t.	δ _{t, 760}	Log δ _{t, 760}	t.	δ _{t, 760}	Log δ _{t, 760}	t.	δt, 760	Log δ _{t, 760}
c.	0.00	– 10	c.	0.00	– 10	c.	0.00	– 10
- 34°	14774	7.16950	- 4°5	13148	7.11885	18%	12129	7.08383
- 33	14712	.16768	- 4.0	13123	.11804	18.5	12108	8309
-33	14651	.16587	- 3.5	13099	.11723	19.0	12088	8234
-31	14590	.16407	– 3.0	13074	.11612	19.5	12067	8160
] 3-	0.00	110407	3.0	0.00		19.0	0.00	1
- 30	14530	7.16227	- 2.5	13050	7.11562	20.0	12046	7.08085
– 29	14471	.16049	- 2.0	13026	.11481	20.5	12026	8011
- 28	14412	.15871	- 1.5	13002	.11401	21.0	12005	7937
– 2 7	14353	.15693	- 1.0	12978	.11321	21.5	11985	7863
i — 26	14295	.15517	- 0.5	12954	.11241	22.0	11965	7789
	0.00			0.00	1 .		0.00	ا ہا
- 25	14237	7.15341	0.0	12931	7.11162	22.5	11944	7.07716
- 24	14179	.15166	+ 0.5	12907	.11082	23.0	11924	7642
- 23	14123	.14991	1.0	12884	.11006	23.5	11904	7569
- 22	14066	.14818	1.5	12860	.10923	24.0	11884	7496
— 21	14010	.14645	2.0	12836	.10844	24.5	11864	7422
-20.0	0.00	7 74470	2 =	0.00	7 70765	25.0	0.00	7 07240
- 20.0 - 19.5	13955 13927	7.1447 2 .14386	2.5	12813	7.10765		11844 118 24	7.07349
— 19.5	1392/	.14301	3.0	12790 12766	.10607	25.5 26.0	11804	7204
- 18.5	13872	.14215	3.5			26.5	11784	7131
- 18.0	13845	.14130	4.0 4.5	12744 12720	.10529 .10450	27.0	11765	7058
1 - 10.0	0.00	.14130	4.5	0.00	.10450	27.0	0.00	7030
-17.5	13818	7.14044	5.0	12698	7.10372	27.5	11745	7.06986
- 17.0	13791	13959	5.5	12675	.10294	28.0	11726	6913
- 16.5	13764	13874	6.0	12652	.10216	28.5	11706	6841
- 16.0	13737	.13790	6.5	12629	.10138	29.0	11687	6769
- 15.5	13710	.13705	7.0	12607	.10069	29.5	11667	6697
	0.00	0.0	,	0.00		- 5.5	0.00	''
-15.0	13684	7.13621	7.5	12584	7.09982	30.0	11648	7.06625
– 14.5	13657	.13536	8.0	12562	9905	30.5	11629	6554
– 14.0	13631	.13452	8.5	12539	9828	31.0	11610	6482
— 13.5	13604	.13368	9.0	12517	9750	31.5	11591	6411
– 13.0	13578	.13285	9.5	12495	9673	32.0	11572	6340
ll	0.00			0.00			0.00	
-12.5	13552	7.13201	10.0	12473	7.09596	32.5	11553	7.06268
- I2.0	13526	.13117	10.5	12451	9519	33.0	11534	6197
- 11.5	13500	.13034	11.0	12429	9443	33.5	11515	6126
- 11.0 - 10.5	13473	.12951	11.5	12407	9366	34.0	11496	6055
10.5	13449	1 .12000	12.0	12385	9290	34.5.	0.00	5984
-10.0	13423	7.12785	12.5		7 00374	35.0		7.05072
– 9.5	13398	.12703	13.0	12363	7.09214	Et	11459	7.05913 5843
– 9.0	13372	.12620	13.5	12342	9137	35·5 36.0	11440	5772
- 8.5	13347	.12538	14.0	12320	8986	36.5	11403	5702
- 8.0	13322	.12456	14.5	12277	8910	37.0	11385	5632
	0.00		1 -7.5	0.00		3/.5	0.00	3-3-
- 7.5	13297	7.12374	15.0	12256	7.08834	37.5	11366	7.05562
- 7.0	13271	.12292	15.5	12235	8759	38.0	11348	5492
- 6.5	13246	.12210	16.0	12213	8683	38.5	11330	5422
– 6.0	13222	.12128	16.5	12192	8608	39.0	11311	5352
− 5.5	13197	.12047	17.0	12171	8533	39.5	11293	5282
	0,00			0.00		l i	0.00	
- 5.0	13172	7.11966	17.5	12150	7.08458	40.0	11275	7.05213
	<u> </u>		<u> </u>	<u> </u>		I	<u> </u>	

SMITHSONIAN TABLES.

TABLE 98. WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Temperature term. (Continued.)

t.	δ _{t, 760}	Log δ _{t, 760}	t.	δt, 760	Log δ _{t, 760}	t.	δ _{t, 760}	Log δ _{t, 760}
C.	0.00	-1c	c.	0.00	-10	c.	0.00	-10
40°	11275	7.05213	50°	10926	7.03845	60°	10597	7.02518
41	11239	.05074	51	10892	.03710	6 r	10565	.02388
42	11204	. 04936	52	10858	. 03576	62	10534	. 02258
43	11168	. 04798	53	10825	. 03443	63	10502	.02128
44	11133	. 04660	54	10792	. 03300	64	10471	. 01999
	0.00			0.00	1 1		0.00	
45	11098	7.04523	55	10759	7.03177	65	10440	7.01870
46	11063	. 04387	56	10726	. 03044	66	10409	.01742
47	11028	.04251	57	10694	.02912	67	10379	.01614
47 48	10994	.04115	58	10661	. 02780	68	10348	.01486
49	10960	. 03980	59	10629	.02649	69	10318	.01358
	1							

TABLE 99.

Humidity term : Values of 0.378 e. Auxiliary to Table 100. e = Vapor pressure in mm. (See Tables 71 and 72.)

	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$							
		0.378 <i>e</i>	Dew- point.	e Vapor Pressure (Water).	0.378e			0.378 e
G.	mm.	mm.	G.	mm.	mm.	C.	mm.	mm.
-50	0.029	0.01	l o°	4. 580		30°	31.860	12.04
-45	0.054	0.02					, ,	
-40	o. o g6	0.04	2	5.29 1	2.00			13.50
-35			3			33	37.775	14. 28
-30	0.288	0.11	4	6.098	2.31	34	39.947	15.10
-25	0.480	o. 18	5	6.541	2.47	35	42.227	15.96
24			ll .			36	44.619	
			7					
		0.24			3.04	38	49.756	
21	0.712	0.27	9	8.610	3.25	39	52.510	19.85
-20	0.783	0.30	10	9.210	3.48	40	55.396	20.94
19	v. 862	0.33	11	9.846	3.72	41	58.417	22.08
18	0.947	0.36	12	10.521	3.98	42	61.580	23.28
17	1.041	0.39	13	11.235	4.25	43	64.889	24.53
16	1.142	0.43	14	11.992	4.53	44	68.350	25.84
-15	1.252	0.47	15	12.794	4.84	45	71.968	27.20
14	1.373	0.52	16	13.642	5.16	46	75.75I	28.63
13	1.503	0.57	17	14.539	5.50	47	79.703	30.13
12	1.644	0.62	18	15.487	5.85	48	83.830	31.69
11	1.798	o. 68	19	16.489	6.23	49	88. 140	33.32
-10	1.964	0.74	20	17.548	6.63	50	492.64	35.02
	2.144	0.81	21	18.665	7.06	51	97.33	36.79
9 8	2.340	o. 88	22	19.844	7.50	52	102.23	38.64
7	2.550	0.96	23	21.087	7.97	53	107.33	40.57
6	2.778	1.05	24	22.398	8.47	54	112.66	42.59
-5	3.025	1.14	25	23.780	8.99	55	118.20	44.68
4	3.291	1.24	26	25.235	9.54	56	123.98	46.86
3	3.578	1.35	27	26.767	10.12	57	130.00	49.14
2	3.887	1.47	28	28.380	10. 73	58	136.26	51.51
I	4.220	1,60	29	30.076	11.37	59	142.78	53.97
0	4.580	1.73	30	31.860	12.04	60	149.57	56.54

WEIGHT IN CRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined : $\frac{\delta}{\delta_0} = \frac{h}{760} = \frac{B - 0.378e}{760}$.

B = Barometric pressure in mm.; e = Vapor pressure in mm.

h.	760	Log h 760.	h.	<u>h</u> 760·	Log h .	h.	760 ·	Log h/760.
mm.		– 10	mm.		– 10	mm.		– 10
300	0.3947	9.59631	400	0.5263	9.72125	450	0.5921	9.77240
302	•3974	.59919	401	.5276	-72233	451	•5934	.77336
304 306	.4000 .4026	.60206 .60491	402 403	.5289 .5303	.72341 .72449	452 453	.5947 .5961	.77432 .775 2 8
308	.4053	.60774	404	.5316	.72557	454	•5974	.77624
310	0.4079	9.61055	405	0.5329	9.72664	455	0.5987	9.77720
312	.4105	.61334	406	5342	.72771	456	.6000	.77815
314 316	.4132	.61612 .61887	407	•5355	.72878	457	.6013 .6026	.77910 .78005
318	.4158 .4184	.62161	408 409	.5369 .538 2	.72985 .73091	458 459	.6040	.78100
320	0.4211	9,62434	410	0.5395	9.73197	460	0.6053	9.78194
322	.4237	.62704	411	.5408	.73303	461	.6066	.78289
324	.4263	.62973	412	.5421	.73408	462	.6079 .6092	.78383 .78477
326 328	.4289 .4316	.63240 .63506	413 414	•5434 •5447	.73514 .73619	463 464	.6105	.78570
330	0.4342	9.63770	415	0.5461	9.73723	465	0.6118	9.78664
332	.4368	.64032	416	.5474	.73828	466	.6132	78757
334	·4395 ·4421	.64293	417 418	.5487	.73932 .74036	467 468	.6145 .6158	.78850 .78943
336 338	•4447	.64552 .64810	419	.5500 .5513	.74140	469	.6171	.79036
340	0.4474	9.65066	420	0.5526	9.74244	470	0.6184	9.79128
342	.4500	.65321	421	.5540	74347	471	.6197	.79221
344	.4526	.65574 .65826	422	•5553	-74450	472	.6210 .6224	.79313 .79405
346 348	•4553 •4579	.66076	423 424	.5566 ·5579	-74553 -74655	473 474	.6237	.79496
350	0.4605	9.66325	425	0.5592	9.74758	475	0.6250	9.79588
352	.4632	.66573	426	.5605	.74860	476	.6263	.79679
354 356	.4658 .4684	.66819 .67064	427 428	.5618 .5632	.74961 .75063	477 478	.6276 .6289	.79770 .79861
358	.4711	.67307	429	.5645	.75164	479	.6303	.79952
360	0.4737	9.67549	430	0.5658	9.75265	480	0.6316	9.80043
362	.4763	.67790 .68029	431	.5671	.75366	481 482	.6329 .6342	.80133 .80223
364 366	.4789 .4816	.68267	432 433	.5684 .5697	.75467 .75567	483	.6355	.80313
368	.4842	.68503	434	.5711	.75668	484	.6368	.80403
370	0.4868	9.68739	435	0.5724	9.75768	485	0.6382	9.80493
372	.4895 .4921	.68973	436	•5737	.75867	486 487	.6395 .6408	.80582 .80672
374 376	·4947	.69437	437 438	.5750 .5763	.75967 .76066	488	.6421	.80761
378	•4974	1.69668	439	.5776	.76165	489	.6434	.80850
380	0.5000	9.69897	440	0.5790	9.76264	490	0.6447	9.80938
382 384	.5026 •5053	.70125 .70352	441 442	.5803 .5816	.76362 .76461	491 492	.6461 .6474	.81027 .81115
386	•5079	.70577	443	.5829	.76559	492	.6487	.81203
388	.5105	.70802	444	.5842	.76657	494	.6500	.81291
390	0.5132	9.71025	445	0.5855	9.76755	495	0.6513	9.81379
392	.5158 .5184	.71247 .71468	446	.5868 .588 2	.76852 .76949	496 497	.6526 .6540	.81467 .81556
394 396	.5211	.71688	447 448	.5895	.77046	497	.6553	.81642
398	•5237	.71907	449	.5908	.77143	499	.6566	.81729
		II			<u> </u>	JI	<u> </u>	:

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined : $\frac{\delta}{\delta_0} = \frac{\hbar}{760} = \frac{B - 0.378e}{760}$.

B = Barometric pressure in mm.; e = Vapor pressure in mm.

h.	<u>h</u> .	Log h 760.	h,	<u>h</u> 760⋅	Log _h .	h.	<u>h</u> 760 ·	Log + 760
mm, 500 501 502	0.6579 .6592 .6605 .6618	- 10 9.81816 .81902 .81989	mm. 550 551 552	0.7237 .7250 .7263	- 10 9.85955 .86034 .86112	mm. 600 601 602	0.7895 .7908 .7921	- 10 9.89734 .89806 .89878
503 504 505 506 507	.6632 0.6645 .6658 .6671	.82075 .82162 9.82248 .82334 .82419	553 554 555 556 557	.7276 .7290 0.7303 .7316 .7329	.86191 .86270 9.86348 .86426	603 604 605 606 607	.7934 .7947 o.7961 .7974 .7987	.89950 .90022 9.90094 .90166 .90238
508 509 510 511 512	.6684 .6697 o.6711 .6724 .6737	.82505 .82590 9.82676 .82761 .82846	558 559 560 561 562	.7342 .7355 0.7368 .7382 .7395	.86582 .86660 9.86737 .86815 .86892	608 609 610 611 612	.8000 .8013 0.8026 .8040	.90309 .90380 9.90452 .90523 .90594
513 514 515 516 517 518	.6750 .6763 0.6776 .6789 .6803	.82930 .83015 9.83099 .83184 .83268 .83352	563 564 565 566 567 568	.7408 .7421 0.7434 .7447 .7461 .7474	.86969 .87046 9.87123 .87200 .87277 .87353	613 614 615 616 617 618	.8066 .8079 0.8092 .8105 .8118	.90665 .90735 9.90806 .90877 .90947 .91017
519 520 521 522 523	.6829 0.6842 .6855 .6869	.83435 9.83519 .83602 .83686 .83769	569 570 571 572 573	.7474 .7487 0.7500 .7513 .7526 .7540	9.87506 .87582 .87658 .87734	619 620 621 622 623	.8145 0.8158 .8171 .8184 .8197	.91017 .91088 9.91158 .91228 .91298
524 525 526 527 528	.6895 o.6908 .6921 .6934 .6947	.83852 9.83934 .84017 .84100	574 575 576 577 578	•7553 •.7566 •7579 •7592 •7605	.87810 9.87885 .87961 .88036 .88111	625 626 627 628	.8211 0.8224 .8237 .8250 .8263	9.91507 9.91507 .91576 .91645
529 530 531 532 533	.6961 0.6974 .6987 .7000 .7013	.84264 9.84346 .84428 .84510 .84591	579 580 581 582 583	.7618 0.7632 .7645 .7658 .7671	.88186 9.88261 .88336 .88411 .88486	629 630 631 632 633	.8276 0.8289 .8303 .8316 .8329	.91784 9.91853 .91922 .91990
534 535 536 537 538	.7026 0.7040 .7053 .7066 .7079	.84673 9.84754 .84835 .84916 .84997	584 585 586 587 588	.7684 0.7697 .7711 .7724 .7737	.88560 9.88634 .88708 .88782 .88856	634 635 636 637 638	.8342 0.8355 .8368 .8382 .8395	.92128 9.92196 .92264 .92332 .92401
539 540 541 542 543	.7092 0.7105 .7118 .7132 .7145	.85078 9.85158 .85238 .85318 .85399	589 590 591 592 593	.7750 0.7763 .7776 .7789 .7803	.88930 9.89004 .89077 .89151 .89224	639 640 641 642 643	.8408 0.8421 .8434 .8447 .8461	.92469 9.92537 .92604 .92672 .92740
544 545 546 547 548 549	.7158 0.7171 .7184 .7197 .7211	.85478 9.85558 .85638 .85717 .85797 .85876	594 595 596 597 598 599	.7816 0.7829 .7842 .7855 .7868	.89297 9.89370 .89443 .89516 .89589 .89662	644 645 646 647 648 649	.8474 o.8487 .8500 .8513 .8526 .8539	.92807 9.92875 .92942 .93009 .93076

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined : $\frac{\delta}{\delta_0} = \frac{h}{760} = \frac{B - 0.378e}{760}$.

B = Barometric pressure in mm.; e = Vapor pressure in mm.

h.	<u>h</u> 760	Log h 760	h.	<u>h</u> 760·	Log h/760.	h.	_h_ 760	Log h/760.
mm.		- 10	mm.		IO	mm.		- 10
650 651 652 653 654	0.8553 .8566 .8579 .8592 .8605	9.93210 .93277 .93341 .93410	700 701 702 703 704	0.9211 .9224 .9237 .9250 .9263	9.96428 .96490 .96552 .96614 .96676	750 751 752 753 754	0.9868 .9882 .9895 .9908 .9921	9.99425 .99483 .99540 .99598 .99656
655 656 657 658 659	0.8618 .8632 .8645 .8658 .8671	9.93543 .93609 .93675 .93741 .93807	705 706 707 708 709	0.9276 .9289 .9303 .9316 .9329	9.96738 .96799 .96860 .96922 .96983	755 756 757 758 759	0.9934 •9947 •9961 •9974 •9987	9.99713 .99771 .99828 .99886 .99943
660 661 662 663 664	0.8684 .8697 .8711 .8724 .8737	9.93873 .93939 .94004 .94070	710 711 712 713 714	0.9342 •9355 •9368 •9382 •9395	9.97044 .97106 .97167 .97228 .97288	760 761 762 763 764	1.0000 .0013 .0026 .0039 .0053	0.00000 .00057 .00114 .00171 .00228
665 666 667 668 669	0.8750 .8763 .8776 .8790 .8803	9.94201 .94266 .94331 .94396 .94461	715 716 717 718 719	0.9408 .9421 .9434 .9447 .9461	9.97349 .97410 .97470 .97531 .97592	765 766 767 768 769	1.0066 .0079 .0092 .0105 .0118	0.00285 .00342 .00398 .00455 .00511
670 671 672 673 674	0.8816 .8829 .8842 .8855 .8869	9.94526 .94591 .94656 .94720	720 721 722 723 724	0.9 47 4 .9487 .9500 .9513 .9526	9.97652 .97712 .97772 .97832 .97892	770 771 772 773 774	1.0132 .0145 .0158 .0171 .0184	o.oo568 .oo624 .oo680 .oo736 .oo793
675 676 677 678 679	0.8882 .8895 .8908 .8921 .8934	9.94849 .94913 .94978 .95042 .95106	725 726 727 728 729	0.9539 •9553 •9566 •9579 •9592	9.97952 .98012 .98072 .98132 .98191	775 776 777 778 779	1.0197 .0211 .0224 .0237 .0250	0.00849 .00905 .00961 .01017
680 681 682 683 684	0.8947 .8960 .8974 .8987 .9000	9.95170 •95233 •95297 •95361 •95424	730 731 732 733 734	0.9605 .9618 .9632 .9645 .9658	9.98250 .98310 .98370 .98429 .98488	780 781 782 783 784	1.0263 .0276 .0289 .0303 .0316	0.01128 .01184 .01239 .01295
685 686 687 688 689	0.9013 .9026 .9039 .9053 .9066	9.95488 •95551 •95614 •95677 •95740	735 736 737 738 739	0.9671 .9684 .9697 .9711 .9724	9.98547 .98606 .98665 .98724 .98783	785 786 787 788 789	1.0329 .0342 .0355 .0368 .0382	0.01406 .01461 .01516 .01571 .01626
690 691 692 693 694	0.9079 .9092 .9105 .9118 .9132	9.95804 .95866 .95929 .95992 .96054	740 741 742 743 744	0.9737 •9750 •9763 •9776 •97 ⁸ 9	9.98842 .98900 .98959 .99018 .99076	790 791 792 793 794	1.0395 .0408 .0421 .0434 .0447	0.01681 .01736 .01791 .01846 .01901
695 696 697 698 699	0.9145 .9158 .9171 .9184 .9197	9.96117 .96180 .96242 .96304 .96366	745 746 747 748 749	0.9803 .9816 .9829 .9842 .9855	9.99134 .99192 .99251 .99309 .99367	795 796 797 798 799	1.0461 .0474 .0487 .0500 .0513	0.01955 .02010 .02064 .02119

		14	1		
Wave lengths	Num-	Inten-	Warra lamatha	Num-	Inten-
Wave lengths	ber of	sity.	Wave lengths	ber of	sity.
in Ångströms.	lines.	sity.	in Ångströms.	linee.	SILY.
	·		Y	[]	
5202 2 5226 2	ا د ا		FOT 7.6	1 1	1
5292 3-5296.0 5861.8-5870.0	4?	00 CO	5915.146		1
5861.8-5870.864	7	I	5915 650		I
5870.804 5871.3-5876 0	8	00	5915.840 5916.0-5918.2.		00
5876.338	ا " ا	I	5918.635.	[4
5876.6-5879.4	4	00	5919.175		000
5879.820		ī	5919 276		5
5879.945	ا ا	ī	5919.860		7
580.7-5881.0	2	ō	5920 395		00
5881.147		1	5920.776		1
5881.320		0	5921.3-5922.6	3	0
5882.084		1	5922.735		2
5882.2-5883 2	3	0	5922.9-5923.4	2	0
5884 120		5	5923.865		1
5884.4-5885.8	3	00	5924.040		2
5886.193		5	5924.490	· • • • • •	4
5886.560		I	5924.975		coo
5886.6-5886.9	2	0	5925.220	• ••••	2
5887.445		5	5926.835	[]	000
5887.880		3	5928 510		00
5888.056		00	5929.0-5931.2	5	1
5888 920	[· · · · · · · · ·	2 CO	59 32. 306 5932.998	[5 2
5889.303			5932.998 5933.2–5940 2	14	000
5889 855		3 2	5933.2-5940.2		I
5890.100 5890.4-5890.9		00	5941.091		00
5890.4-5890.9		1 00	5941.290		5
5891.720	1	o	5941.470		000
5891.720	L .	4	5941.845		2
5892.608		3	5942.500		000
5893.268		ŏ	5942.635		1
5893.725		1	5942 789		3
5894.6-5896.6	5	0	5944.530		I
5896 710		1	5944-945		I
5897.047		2	5945.4-5915 5		00
5897.3-5898.2		00	5945.865		I
5898.378		4	5946.223		3
5898.6-5899.0		00	5946.864		000
5899.215		00	5947.062 5947.283		2
5899.752		2	5947.6-5949.2		000
5900.135		4	5949.399	14	2
5900.260 5900 6-5901.5		co	5949.8-5954.6		00
5901.682	1	6	5955.170		I
5902.238		000	5956.0-5956.6.	4	000
5902.363			5958 098		
5903 035		1 1	5958.460		I
5903 748			5961.6-5966 6	. 5	00
5903.9-5907.7	13	00	5966.885		
5908 070			5967.540		QO
5908.425		. I	5968.058		
5909.213	. .	. 3	5968.280		000
5909 668		. 00	5968.495		
5910.398	.	. I	5969.2-5970.9		00
5910.5-5910.9	. 3	00	5971 557		
5910.987	• ••••	. 2	5975 330	1	1 00
5911.1-5912.9	. 7	00	5976.694		00
5913.212	.	. 3	5977.252 5977.6-6479.7	73	000
5914 430		"	37/1.0 -04/9./	13	
			(1)	<u></u>	

ATMOSPHERIC WATER-VAPOR LINES IN THE VISIBLE SPECTRUM.

Wave lengths in Ångströms.	Num- ber of lines.	Intensity.	Wave lengths in Ångströms.	Num- ber of lines.	Inten- sity.
6480.285 6480.4-6483.3 6483.468	4	I 0000	6941.475 6942.402		000 I 2
6483.6–6490 9 6491 015 6493.1–6493 5	II	000 I	6942.630 6944.0 6 0 6947.782		ι 3 5
6194.725 6496 082		I 2	6947.863 6949.240 6949 310		00 I I
6497.8-6514.5 6514.956 6516 080	7	00 2 000	6951 010 6953.828	2	I I OO
	3	I 2 00	6954.0-6955.9 6956.660 \ 6956.746 \		4 1
6519.682 6522.1–6523.9 6524.080		0000 T	6959.704 6961.515 6964.812		3 4 1
6526.0-6530 8	2	000 I 2	6971.135 6977.715		0 3 1
6534.8-6542.6 6544.140	3	000	6985.220 6986.833 6988 125		3 0
6552 865		I 00	6989.237 6990.632		3 1 2
6554.025 6556.308 6557.4–6558 4		00? I 0	6994.360 6998.978		I 0 2
6560 800 6563.7-6569.0 6572.330	4	00 I }	6999.223 7004.575 7004.995		0 2
6575.085 6580.4–6929.6 6934.075	11	I 000 2	7016.330		0 2 I
6937 957 6938 520 6939 875		2 I 2	7016.675 7023.770 7027.213		3 2 0
6940.436		2	7027.740	ļ. 	2

TABLE 102.
ATMOSPHERIC WATER-VAPOR BANDS IN THE INFRA-RED SPECTRUM.

Name of band.	Wave- lengths.	Transmission coefficient a.	of numerous fin apparatus does r Wide bands o	oands may perhate lines which the lines which the lines sparately different found in lines.	ne bolographic stinguish. ospheric water-
d	o.718 o.814 o.896	0.9I 0.92 0.90	Name.	Wave lengths.	Absorption at Washington.
$egin{array}{ccccc} ho & & & & & & \\ \sigma & & & & & & \\ \hline \sigma & & & & & & \\ \Phi_1 & & & & & & \\ \Phi_2 & & & & & & \\ \hline & & & & & & \\ & & & & &$	0.933 0.945 0.974 1.119 1.134 1.172 1.331	0.63 0.69 0.91 0.54 0.60 0.92 0.74 0.36 0.35	ρστ Φ Υ X See Vol. I. Anna sonian Institution.	ils Astrophysical Ob	0.3 to 0.5 0.5 to 0.8 0.7 to 1.0 0.9 to 1.0 1 o { Partly } CO ₂ }

TRANSMISSION PERCENTACES OF RADIATION THROUGH MOIST AIR.

Rang Wave-le			PRECIPITABLE WATER IN CENTIMETERS.											
μ	μ	.001	.003	.006	.01	.03	.06	.10	.25	.50	1.0	2,0	6.0	10.0
0.75 t	0.1.0				100	99	99	98	97	95	93	90	83	78
1.0	1.25				99	99	98	97	95	92	89	85	74	69
1.25	1.5		ŀ		96	92	84	80	66	57	51	44	31	28
1.5	2.0				98	97	94	88	79	73	70	66	δo	57
* 2.	3.	96	92	87	84	77	70	64	' '	'	1			•
3.	4.	95	88	84	78	72	66	63]
* 4.	5. 6.	92	83	76	71	65	бо	53						
5•	6.	95	82	75	68	56	51	47	35		İ			
6.	7. 8.	85	54	50	31	24	8	4	3	2	0	0	0	0
7· 8.	8.	94	84	76	68	57	46	35	16	10	2	0	0	0
8.	9.	100	100	100	99	98	96	94	65					
† 9 .	10.	100	100	100	100	100	100	100	100	100	100	100		
†10.	II.	100	100	100	100	100	100	100	100	100	100	100		1
II.	12.	100	100	100	100	100	99	98	96	95	93			1
12.	13.	100	100	100	100	99	99	97	86	82				
*13.	14.	100	100	100	99	97	94	90	80	60				
*14.	15.			96	93	80	75	50	15	0	0	0	0	0
*15.	16.					70	55	40	0	0	0	0	0	0
16.	17.						50	20	0	0	0	0	0	0
17.	18.	l .					25	10	0	0	0	0	0	0
18.		٥	0	0	0	٥	0	0	0	0	0	0	0	0

^{*} These places require multiplication by the following factors to allow for losses in CO2 gas. Under average sea-level outdoor conditions the CO_2 (partial pressure = 0.0003 atmos.) amounts to about 0.6 grams per cu.m. Paschen gives 3 times as much for indoor conditions. 2μ to 3μ , for 2 grams in m^2 path (93); for 140 grams in m^2 path (93); $4m^2 + 5m^2 + m^2

4 5, sight allowance to be made; 14 15, 80 grams in m² path reduces energy to zero; 15 16, ""..."

F. Paschen gives (Annalen d. Physik. u. Chemie, 51, p. 14, 1894) the absorption of the radiation from a blackened strip at 500° C. by a layer 33 centimeters thick of water vapor at 100° C. and atmospheric pressure as follows:

Wave length	μ μ	μ μ	μ μ
	2.20-3.10	5.33-7.67	7.67-10 (?)
Percentage absorption	80	94	94-13

The following table, due to Rubens and Aschkinass (Annalen d. Physik u. Chemie, 64, p. 598, 1898), gives the absorption of radiation from a zircon burner by a layer 75 centimeters thick of water vapor saturated at 100° C. This amount of vapor is about equivalent to a layer of water 0.45 millimeter thick or to 1.5% of the water in a total vertical atmospheric column whose dewpoint at sea-level is 10° C. The region of spectrum examined includes most of the region of terrestrial radiation.

Wave length	μ	д	μ μ	μ	μ	μ	μ
	7. 0	8. о	9.0-12.0	12.4	12.8	13.4	14.0
Percentage absorption	75	40	6	20	13	28	22
Wave length	μ	μ	μ	μ	μ	μ	μ
	14. 3	15.0	15.7	16. o	17.5	18.3	20. 0
Percentage absorption	43	35	65	52	88	80	100

[†] These places require multiplication by 0.90 and 0.70 respectively for one air mass and 0.85 and 0.65 for two air masses to allow for ozone absorption when the radiation comes from a celestial body.

INTERNATIONAL METEOROLOGICAL SYMBOLS.

The International Meteorological Symbols were adopted at the Vienna meteorological congress of 1873. A few additions and modifications have been made at subsequent international meteorological meetings. The forms of these symbols are more or less flexible. Those shown in the accompanying table are the forms which have generally been used in the United States, and with two exceptions ("wet fog" and "zodiacal light") are identical with those used by the Prussian Meteorological Institute and given in the German editions of the International Meteorological Codex. The principal variants found in the meteorological publications of the different countries are given in the Monthly Weather Review (Wash., D.C.), May, 1916, p. 268.

Exponents.—An exponent added to a symbol indicates the degree of intensity, ranging from ° weak (light, etc.) to ² strong (heavy, etc.). Thus, •°, light rain; •², heavy rain. German and French observers use the exponent ¹ to denote medium intensity, in accordance with the German and French versions of the report of the Vienna congress, and the German editions of the Codex. The English version of the above-mentioned report and the English edition of the Codex provide for the use of only two exponents, ° and ²; hence in English-speaking countries the omission of the exponent indicates medium intensity.

Time of occurrence. — When hours of occurrence are added to symbols, the abbreviation a is used for a.m., and p for p.m. Thus, a 10a — 4p denotes "rain from 10 a.m. to 4 p.m." 12a = noon; 12p = midnight. The abbreviation n means "during night." Stations taking tri-daily observations may use a to mean between the first and second observation; p, between the second and third; and n, between the third and the first.

For further information concerning the International Symbols and other meteorological symbols, see "Meteorological Symbols," by C. Fitzhugh Talman, *Monthly Weather Review* (Wash., D.C.), May, 1916, pp. 265-274.

SMITHSONIAN TABLES.

Symbol.	Meaning.	Remarks.
0	Rain.	
*	Snow.	
IĞ.	Thunderstorm.	Thunder and lightning.
Τ	Thunder.	Without lightning.
∢	Lightning.	Without thunder; "heat-lightning."
•	Hail.*	, , , , , , , , , , , , , , , , , , , ,
	Graupel.	Sometimes called "soft hail." French, grésil. Resembles little snow-pellets.
=	Fog.	
	Ground fog.	Not exceeding the height of a man.
=≕	Wet fog.	One which wets exposed surfaces.
	Hoarfrost.	
	Dew.	
V	Rime.	A rough frost deposit from fog.
2	Glaze; Glazed frost.†	Ice coating due to rain, "ice-storm." In America often called "sleet."
- +→	Driving snow.	Ger., Schneegestöber; Fr., bourrasque de neige.
_ ←	Ice-crystals.	Ice-needles sometimes seen floating or slowly falling in the air in clear, cold weather.
\boxtimes	Snow on ground.	Ground near station more than half covered.
	Gale.	Wind of force 8-12, Beaufort scale. (Rept. Int. Met'l Comm., Berlin, 1910, English ed., p. 17.) Formerly used for
O	Sunshine.	"strong wind." A 3-barbed arrow is introduced in the 2d German ed. of the Int. Met'l Codex to denote "strong wind," but no authority is cited. According to the Observer's Handbook of the British Met'l Office "the number of barbs on the arrow may conveniently be made to represent the strongest wind force noted," but there is no international sanction for such variants. In German edition of Int. Met'l Codex, but has never been definitely recognized by the international organization. (See Rept. Int. Met'l Comm., Southport, 1903, Engl. ed., p. 19 and 101.) Widely used in German and Austrian publications.
⊕⊖Ӈ∋Ҁ∛҅ҩ҄8	Solar halo. Solar corona. Lunar halo. Lunar corona. Rainbow. Aurora. Zodiacal light. Haze.	Due to fine dust, or to the disturbance of atmospheric transparency by air-currents of different densities ("optical turbidity"), and not to water-drops. In practice, this is often difficult to distinguish from light fog (== °), or "mist" of British observers. Prussian and Austrian observers underscore this symbol (\sigma) to denote a definitely smoky atmosphere ("Moorrauch").
	1	l:

^{*} True hail, which occurs chiefly with summer thunderstorms, should be distinguished from the snowy pellets, like miniature snowballs, known as graupel, or soft hail (A): also from the small particles of clear ice, called sleet by the U.S. Weather Bureau, for which there is no international symbol. On the history of the word sleet see Monthly Weather Review, May, 1916, pp. 281-286.

† Glaze is the official term in the United States; glazed frost in Great Britain.

INTERNATIONAL CLOUD CLASSIFICATION.

The International Conference of Meteorologists held at Munich in 1891 recommended the following classification of clouds, elaborated by Messrs. Abercromby and Hildebrandsson:

- Detached clouds with rounded upper outlines (most frequent in dry weather). b. Clouds of great horizontal extent suggesting a layer or sheet (wet weather).
- A. Upper Clouds, average altitude 0000^m .

 - a. 1. Cirrus. b. 2. Cirro-stratus.
- B. Intermediate Clouds, between 3000^m and 7000^m .
 - a. { 3. Cirro-cumulus. 4. Alto-cumulus. b. 5. Alto-stratus.
- C. Lower Clouds, below 2000m.
 - a. 6. Strato-cumulus. b. 7. Nimbus.
- D. Clouds of diurnal ascending currents.

 - a. 8. Cumulus; top '1800m; hase 1400m.
 b. 9. Cumulo-nimbus; top 3000m to 8000m; base 1400m.
- E. High Fogs, under 1000^m.
 - 10. Stratus.

DEFINITIONS AND DESCRIPTIONS OF CLOUD FORMS.

- 1. Cirrus (Ci.). Detached clouds of delicate and fibrous appearance, often showing a featherlike structure, generally of a whitish color. Cirrus clouds take the most varied shapes, such as isolated tufts, thin filaments on a blue sky, threads spreading out in the form of feathers. curved filaments ending in tufts, sometimes called Cirrus uncinus, etc.; they are sometimes arranged in parallel belts which cross a portion of the sky in a great circle, and by an effect of perspective appear to converge towards a point on the horizon, or, if sufficiently extended. towards the opposite point also. (Ci.-St. and Ci.-Cu., etc., are also sometimes arranged in similar bands.)
- 2. Cirro-stratus (Ci.-St.). A thin, whitish sheet of clouds sometimes covering the sky completely and giving it only a milky appearance (it is then called Cirro-nebula), at other times presenting, more or less distinctly, a formation like a tangled web. This sheet often produces halos around the Sun and Moon.
- 3. Cirro-cumulus (Ci.-Cu.). Mackerel sky. Small globular masses or white flakes without shadows, or showing very slight shadows, arranged in groups and often in lines.
- 4. Alto-stratus (A.-St.). A thick sheet of a gray or bluish color, sometimes forming a compact mass of dark gray color and fibrous structure. At other times the sheet is thin, resembling thick Ci.-St., and through it the Sun or the Moon may be seen dimly gleaming as through ground glass. This form exhibits all changes peculiar to Ci.-St., but from measurements its average altitude is found to be about one half that of Ci.-St.
- 5. Alto-cumulus (A.-Cu.). Largish globular masses, white or grayish, partially shaded. arranged in groups or lines, and often so closely packed that their edges appear confused. The detached masses are generally larger and more compact (resembling St.-Cu.) at the center of the group, but the thickness of the layer varies. At times the masses spread themselves out and assume the appearance of small waves or thin slightly curved plates. At the margin they form into finer flakes (resembling Ci.-Cu.). They often spread themselves out in lines in one or two directions.
- 6. Strato-cumulus (St.-Cu.). Large globular masses or rolls of dark clouds often covering the whole sky, especially in winter. Generally St.-Cu. presents the appearance of a gray layer irregularly broken up into masses of which the edge is often formed of smaller masses, often of wavy appearance resembling A.-Cu. Sometimes this cloud-form presents the characteristic appearance of great rolls arranged in parallel lines and pressed close up against one another. In their centers these rolls are of a dark color. Blue sky may be seen through the intervening spaces which are of a much lighter color. (Roll-cumulus in England, Wulstcumulus in Germany.) St.-Cu. clouds may be distinguished from Nb. by their globular or rolled appearance, and by the fact that they are not generally associated with rain.
- 7. Nimbus (Nb.), Rain Clouds. A thick layer of dark clouds, without shape and with ragged edges, from which steady rain or snow usually falls. Through the openings in these clouds an upper layer of Ci.-St. or A.-St. may be seen almost invariably. If a layer of Nb.

separates up in a strong wind into shreds, or if small loose clouds are visible floating underneath a large Nb., the cloud may be described as Fracto-nimbus (Fr.-Nb.) (" Scud " of sailors).

8. Cumulus (Cu.), Wool pack Clouds. — Thick clouds of which the upper surface is dome-shaped and exhibits protuberances while the base is horizontal. These clouds appear to be formed by a diurnal ascensional movement which is almost always noticeable. When the cloud is opposite the Sun, the surfaces facing the observer have a greater brilliance than the margins of the protuberances. When the light falls aslant, as is usually the case, these clouds throw deep shadows; when, on the contrary, the clouds are on the same side of the observer as the Sun, they appear dark with bright edges.

True cumulus has well defined upper and lower limits, but in strong winds a broken cloud resembling Cumulus is often seen in which the detached portions undergo continual change.

This form may be distinguished by the name Fracto-cumulus (Fr.-Cu.).

9. Cumulo-nimbus (Cu.-Nb.), The Thunder-Cloud; Shower-Cloud.—Heavy masses of cloud rising in the form of mountains, turrets or anvils, generally surmounted by a sheet or screen of fibrous appearance (false Cirrus) and having at its base a mass of cloud similar to nimbus. From the base local showers of rain or snow, (occasionally of hail or soft hail) usually fall. Sometimes the upper edges assume the compact form of cumulus, and form massive peaks round which delicate "false Cirrus" floats. At other times the edges themselves separate into a fringe of filaments similar to Cirrus clouds. This last form is particularly common in spring showers.

The front of thunder-clouds of wide extent frequently presents the form of a large arc

spread over a portion of a uniformly brighter sky.

10. Stratus (St.). — A uniform layer of cloud resembling a fog but not resting on the ground. When this sheet is broken up into irregular shreds in a wind, or by the summits of mountains, it may be distinguished by the name Fracto-stratus (Fr.-St.).

During summer all low clouds tend to assume forms resembling Cumulus, and may be described accordingly as Stratus cumuliformis, Nimbus cumuliformis, etc.

The term Mammato-cumulus is applied to a cloud having a mammillated lower surface. occurring especially in connection with severe local storms.

The ovoid form, with sharp edges, assumed by certain clouds, particularly during the occurrence of sirocco, mistral or foehn, is indicated by the adjective lenticularis, e.g., Cumulus lenticularis (Cu. lent.), Stratus lenticularis (St. lent.). Such clouds frequently show iridescence.

For pictures of typical cloud forms see "International Cloud Atlas," 2d ed., Paris, 1910; also U.S. Weather Bureau, "Classification of Clouds for the Guidance of Observers," Washington, D.C., 1911, and Gt. Britain, Meteorological Office, "Observer's Handbook," London (annual).

BEAUFORT WEATHER NOTATION.

Especially intended for the use of mariners, but sometimes used at land stations. The original notation was devised in 1805 by Admiral Sir F. Beaufort; it has since been slightly altered and amplified by British and American meteorologists. The following symbols are used by the marine observers of the U.S. Weather Bureau: -

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Upper Atmosphere:
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- b. Blue sky.
- c. Cloudy sky.
- o. Overcast sky.

Lower Atmosphere:

- v. Visibility (exceptionally clear).
- z. Haze.
- m. Mist. f. Fog.
- Precipitation:
 - d. Drizzling.
 - p. Passing showers.
 - r. Rain.
 - s. Snow.
 - h. Hail.

Electric phenomena:

- l. Lightning.t. Thunder.

Wind:

q. Squally.

The British Meteorological Office also uses the following: -

- e. Wet air without rain.
- g. Gloom.
- \tilde{u} . Ugly or threatening appearance of the weather.

"The letters b, c, o are intended to refer only to the amount of cloud visible, and not to its density, form or other quality. They have gradually come to be regarded as corresponding to the following cloud amounts in the scale o-ro: b = 0 to 3; bc or cb = 4 to 6; c = 7 or 8; o = o or 10." — Marine Observer's Handbook, Lond., 1915, p. 82.

U.S. Weather Bureau Observers use a line (light or heavy) under the symbol, British observers a dot or two dots, to indicate great intensity. Thus, U.S., r heavy rain, r, very heavy rain. British, r, heavy rain; r, very heavy rain.

SMITHSONIAN TABLES.

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

NORTH AMERICA.	Longitude Letitude, from Greenwich.		Нві	ght.
GREENLAND. *Angmagsalik. *Godthaab. Ivigtut. *Jacobshavn. *North Star Bay. *Upernivik.	65° 37′ N. 64 11 61 12 69 13 76 30 72 47	37° 34′ W. 51 44 48 10 51 2 68 55 56 7	Feet. 104 30 16 41 2 44	m. 32 9 5 13 6
ICELAND.				
*Berufjord. *Grimsey (Akureyi). *Stykkisholm. *Vestmanno.	64 40 N. 66 33 65 5 63 26	14 19 W. 17 58 22 46 20 15	59 22 37 23	18 7 11 8
FÄRO ISLANDS.	62 2 N.	6 45 W.	20	26
*ThorshavnALASKA.	02 2 N.	6 45 W.	30	20
*Dutch Harbor *Eagle Juneau *Nome *Sitka *Tanana *Valdez	53 54 N. 64 46 58 18 64 30 57 4 65 12 61 6	166 32 W. 141 12 134 24 165 24 135 20 152 00 146 13	13 814 80 23 88	4 248 24 7 27 ?
CANADA.				:
Banff *Barkerville. *Belle Isle. *Berens River *Calgary *Carcross. *Davis Inlet. *Dawson. Father Point. *Fort Chippewyan. *Fort Hope. *Fort Resolution. *Fort Simpson. Fredericton. Halifax *Hay River. *Kamloops. Kingston. *Macleod. *Minnedosa. Montreal. *Moose Factory. *Nain. Parry Sonnd. *Point Riche. *Prince Albert. *Prince Rupert.	51 10 N. 53 2 51 55 52 18 51 2 60 11 55 50 64 4 48 31 58 42 51 32 61 00 61 52 45 57 44 39 60 51 50 41 44 13 49 44 50 15 50 41 50 45 50 45 50 45 51 16 56 33 45 19 50 42 51 18	115 34 W. 121 35 55 20 97 23 114 2 134 34 60 50 139 20 68 19 111 10 87 48 113 00 120 43 66 36 63 36 115 20 120 29 76 29 113 24 99 50 73 35 80 56 61 41 80 00 57 25 106 00 130 18	4521 4180 436 709 3389 2172 1053 20 715 787 423 164 88 525 1243 285 3130 1699 187 30 13 635 36 1430 171	1378 1274 133 216 1033 662 ? 321 6 218 ? 240 129 50 29 161 379 87 954 518 57 9 4 193 11 436 52

Note. — Stations with asterisk appear in the 'Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

CANADA.	Latitude.	Longitude from Greenwich.	Helgt	nt.
(Continued.) *Qu'Appelle. Quebec. *Sable Island. *St. John, N.B. *St. Johns, Newfoundland. *S.W. Point, Anticosti. Sydney. *Toronto. *Victoria. *Winnepeg. Woodstock. *York factory.	50° 30′ N. 46 48 43 57, 45 17 47 34 49 24 46 10 43 40 48 24 49 53 43 8 57 00	103° 47′ W. 71 13 60 6 66 4 52 42 63 35 60 10 79 24 123 19 97 7 80 47 92 28	Feet. 2116 296 26 119 125 30 48 379 230 760 980	m. 645 90 8 36 38 9 11 116 70 232 299 11
*Abilene Albany Alpena Amarillo Asheville Atlanta Atlantic City Augusta Baltimore Binghamton Binghamton Binghamton Bismarck Block Island Blue Hill Boise Boston Buffalo Cairo Cape Henry *Charleston Charlotte Chattanooga *Cheyenne *Chicago Cincinnati Cleveland Columbia, Mo Columbia, S.C. Columbus Concord Corpus Christi Davenport	32 23 N. 42 39 45 5 35 13 35 36 33 45 33 22 33 28 39 17 42 6 46 47 41 10 42 12 43 37 42 21 42 53 37 36 56 32 47 35 13 35 4 41 53 37 6 41 53 39 6 41 30 38 57 34 12 27 49 41 30	99 40 W. 73 45 83 30 101 50 82 32 84 23 74 25 81 54 76 37 75 55 100 38 71 36 71 6 116 3 71 4 78 53 89 10 76 0 76 0 79 56 80 51 85 14 104 48 87 37 84 30 81 42 92 20 81 3 83 0 71 32 97 25 90 38	1738 97 6009 3676 2255 1174 52 180 123 875 1674 26 640 2739 125 767 356 18 48 779 702 6088 823 628 762 784 351 824 288 20 606	530 30 186 1120 687 358 16 55 37 267 510 8 105 835 38 234 108 5 15 237 232 232 1855 251 191 232 239 107 251 88 6
*Desveror Parents Parents Person Pers	39 45 41 35 42 20 37 45 41 20 42 30 46 47 44 54 38 53 31 47 42 7	93 37 83 3 100 0 96 16 90 44 92 6 66 59 79 49 106 30 80 5	5291 861 730 2509 1299 698 1133 76 1940 3762 714	1613 262 222 765 396 213 345 23 591 1147 217

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

	Latitude.	Longitude from	Heigh	ıt.	
UNITED STATES.		Greenwich.			
(Continued.)			Feet.	m,	
Escanaba	45° 48′ N.	87° 5′ W.	612	187	
Eureka	40 48	124 11	62	19	
Evansville	37 58	87 33	431	131	
Fort SmithFort Worth	35 22	94 24	457 670	139 204	
Fresno	32 43 36 43	97 15 119 49	330	101	
*Galveston	29 18	94 50	54	16	
Grand Haven	43 5	86 13	632	193	
Grand Junction	39 9	108 33	4608	1404	
Green Bay	44 31 40 16	88 o 76 52	617 374	188 114	
Hartford	41 46	72 40	150	48	
Havre	48 34	109 40	2505	764	
*Helena	46 34	112 4	4110	1253	
HoughtonHouston	47 7 20 47	88 34 95 24	668 138	204 42	
Huron	29 47 44 21	95 24 98 14	1306	398	
Indianapolis	39 46	86 10	822	251	
Ithaca	42 27	76 29	836	255	
Jacksonville	30 20 48 10	81 39 114 25	43 2973	906	
Kansas City	39 5	94 37	963	293	
*Key West	24 33	8 1 48	22	7	
Knoxville	35 56	83 58	996	304	
La Crosse	43 49	91 15	714	218	
Lander Lansing	42 50 42 44	108 45 84 26	5372 878	1637 268	
Lewiston	46 25	117 2	757	231	
Lexington	38 2	84 33	989	30 1	
Lincoln	40 49	96 45	1189	362	
Little RockLos Angeles	34 45	92 6 118 1 5	357 338	109	
Louisville	34 3 38 15	85 45	525	160	
Lynchburg	37 25	79 9	681	207	
Macon	32 50	83 38	370	113	
Madison	43 5 46 34	89 23 87 24	974 734	297 224	
Marquette Memphis	46 34 35 9	90 3	399	122	
Meridan	32 21	88 40	375	114	
Milwaukee	43 2	87 54	681	207	
Minneapolis	44 59	93 18 88 2	918 57	280 17	
*Mobile Montgomery	30 41 32 23	86 18	223	68	
Moorhead	46 52	96 44	935	285	
Mount Tamalpais	37 56	122 35	2375	724	
Mount Weather	39 4	77 55	1726	526	
Nantucket*	41 17 36 10	70 6 86 47	12 546	4 166	
New Haven	41 18	72 56	106	32	
*New Orleans	29 58	90 4	53	16	
*New York	40 43	74 0	314	111	
Norfolk	36 51 46 16	76 17 124 4	91 211	28 64	
North Head* *North Platte	41 08	100 45	2821	860	
Northfield	44 10	72 41	876	267	
Oklahoma City	35 26	97 33	1214	370	
Omaha	41 16	95 56	1105	337	
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Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

UNITED STATES.	Latitude.	Longitude from Greenwich.	Helg	ht.
(Continued.)				
(Continued.) Oswego. Parkersburg. Pensacola. Philadelphia Phœnix Pike's Peak Pittsburg. Pocatello. Port Huron. Portland, Me. *Portland, Oreg. Providence. Pueblo. Raleigh. Richmond. Rochester. Roseburg. Sacramento. *St. Louis. St. Paul. Salt Lake City. San Antonio. *San Diego.	43° 29' N. 39 16 30 25 39 57 33 28 38 50 40 32 42 52 43 0 43 39 45 32 41 50 38 18 35 45 37 32 43 8 43 13 38 35 38 35 44 58 40 46 29 27 32 43	76° 35′ W. 81 36 87 13 75 9 112 0 105 2 80 2 112 29 82 26 70 15 122 41 71 25 104 36 78 37 77 42 123 20 121 30 90 12 93 3 111 30 98 28 117 10	Feet. 335 638 56 117 1108 14134 842 4477 638 103 153 160 4685 376 144 523 510 69 568 837 4360 693 87	m. 102 194 17 36 338 4308 257 1365 194 47 49 1428 115 44 159 155 21 173 255 1329 211 26
Sandusky *San Francisco *Santa Fé Sault Ste. Marie Savannah Scranton Seattle. Shreveport Spokane. Springfield, Ill. Springfield, Mo Syracuse. Tacoma Tampa. Tatoosh Island Taylor Toledo Topeka. Valentine Vicksburg *Washington City Wichita. Williston Wilmington Wytheville Yankton	32 24 47 38 32 30 47 38 32 30 47 48 32 24 47 38 32 30 47 40 39 48 37 12 43 2 47 16 27 57 48 23 30 35 41 40 39 35 41 40 39 48 37 12 48 23 30 35 41 40 39 48 37 12 48 23 30 35 41 40 39 48 37 12 48 23 30 35 41 40 48 25 48 26 48 50 49 50 40 30 40 50 40	82 40 122 26 105 57 84 21 81 5 75 42 122 20 93 40 117 25 89 39 93 18 76 10 122 23 82 27 124 44 97 20 83 34 95 41 100 32 90 53 77 3 97 20 103 35 77 57 81 5 97 28	629 155 7013 614 65 805 125 249 1929 644 1324 597 213 35 86 583 628 987 2598 247 112 1358 1878 78 2304 1233	192 47 2138 187 20 245 38 76 588 196 403 182 65 11 26 178 191 301 792 75 34 414 572 24 702 376
MEXICO, CENTRAL AMERICA AND WEST INDIES. *Barbados (Windward Islands) Basseterre (St. Kitts) *Belize (Brit. Honduras)	13 8 N. 17 18 19 29 32 17	59 36 W. 62 43 88 12 64 46	180 29 6 151	55 9 2 46

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

MEXICO, CENTRAL AMERICA AND WEST INDIES.	Latitude.	Longitude from Greenwich.	Heig	tht.
(Continued.) Bridgetown (Barbados). Camp Jacob (Guadeloupe). Cienfuegos (Cuba) Montserrat. Colon (Panama). *Culebra (Panama). Fort de France (Martinique). Grand Turk (Turks Is.). *Grenada (Richmond Hill). Guanajuato (Mexico). Guatemala. *Havana (Cuba). *Jamaica (Negril Point). Kingston (Jamaica). *Leon (Mexico). *Morelia (Mexico). *Morelia (Mexico). *Nassau (Bahamas). *Oaxaca (Mexico). *Port au Prince (Haiti). Port of Spain (Trinidad). Puelba (Mexico). Puerto Principe (Cuba). Roseau (Dominica). *St. Croix (Christiansted). St. Thomas (Virgin Is.). *Salina Cruz (Mexico). San Jomingo (San Domingo). San José (Costa Rico). San Juan (Porto Rico). San Luis Potosi (Mexico). *San Salvador (Central America). Santiago de Cuba (Cuba). Tacubaya (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico). *Zacatecas (Mexico).	13° 4′ N. 16 00 22 8 9 23 9 10 14 36 21 21 12 3 21 00 14 37 23 8 18 15 17 58 21 7 23 11 19 26 19 14 25 5 17 4 18 34 10 35 19 2 21 23 15 17 17 45 18 13 16 12 25 5 17 45 18 13 16 12 25 5 18 28 9 56 18 29 9 56 18 29 19 24 19 55 19 24 19 55 19 24 19 38	59° 37′ W. 62 2 80 26 79 23 79 40 61 5 71 7 61 45 101 15 90 31 82 22 78 23 76 48 101 41 106 25 99 8 100 7 77 21 96 44 72 22 61 30 98 11 77 56 61 23 64 42 64 29 95 16 100 56 69 93 84 8 66 07 100 59 89 9 75 50 99 12 96 8 68 56 102 35 103 37	Feet. 30 1650 98 36 404 13 11 508 6640 4888 57 33 286 5899 25 7480 6342 26 5128 118 40 7116 352 25 23 27 184 5399 57 3724 82 7621 23 75 8015 5016	m. 9 503 30 11 123 4 3 155 2024 1490 24 100 87 1799 8 2280 1933 8 1563 37 12 2169 107 8 8 56 1645 18 1135 25 1890 657 25 2323 7 23 2610 1529
SOUTH AMERICA. Andalgalá (Argentina). Aracajú (Brazil). *Arequipa (Peru). Asuncion (Paraguay). *Bahía Blanca (Argentina). Bello Horizonte (Brazil). Bogotá (Colombia). *Buenos Aires (Argentina). Caldera (Chile). *Caracas (Venezuela). Catamarca (Argentina). *Cayenne (French Guiana). Ceres (Argentina). Chaco (Paraguay). Concordia (Argentina).	27 30 S. 10 55 16 22 25 32 38 45 19 54 4 35 34 36 27 3 10 31 N. 28 27 S. 4 56 N. 29 55 S. 23 23 31 23	66 26 W. 37 4 71 33 57 48 62 15 43 30 74 14 58 22 70 53 66 56 65 47 52 21 61 58 58 25 58 2	3517 14 8041 312 82 2812 8579 72 98 3419 1673 20 285 361 79	1072 4 2451 95 25 857 2615 22 30 1042 510 6 87 110 24

TABLE 107. LIST OF METEOROLOGICAL STATIONS.

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

SOUTH AMERICA.	Latitude,	Longitude from Greenwich.	Heig	ht.
Coquimbo (Chile) *Córdoba (Argentina) Corrientes (Argentina) *Curityba (Brazil) *Cuyaba (Brazil) *El Misti (Peru). Summit Station Mt. Blanc station *El Peru (Brazil) *Fernando Noronha (Brazil) *Georgetown (Brit. Guinea) *Goya (Argentina) Iquique (Chile) Isla Chañaral (Chile) *Islota de los Evangelistas (Chile) Juan Fernandez (Chile) La Plata (Argentina) Lima (Peru) *Manaos (Brazil) *Montevideo (Uruguay) *Paramaribo (Dutch Guinea) Paraná (Argentina) *Porto Alegre (Brazil) Potosi (Bolivia) *Puerto de Antofagasta (Chile) *Puerto de Antofagasta (Chile) *Puerto de Punta Arenas (Chile) *Punta Angeles (Chile) *Punta Carranza (Chile) *Punta Galera (Chile) *Punta Galera (Chile) *Punta Gelra (Chile) *Punta Tortuga (Chile) *Punta Grande do Sul (Brazil) *Rio Grande do Sul (Brazil) *Rosario (Paraguay) San Juan (Argentina) *Santiago (Chile) *Sao Paulo (Brazil) Observatorio *Sucre (Bolivia) Torre do Recife (Pernambuco, Brazil)	29° 56′ S. 31 25 27 27 25 26 15 36 16 16 16 7 30 N. 29 9 S. 20 12 29 1 52 24 33 37 34 9 4 3 8 8 34 54 N. 41 43 S. 30 2 19 38 23 39 18 28 23 39 18 28 53 10 33 1 52 24 40 1 29 56 0 14 29 56 0 14 29 56 0 14 32 2 32 2 33 37 33 34 35 36 41 2 32 32 33 37 34 38 38 38 38 38 38 38 38 38 38 38 38 38	71 ° 21 'W. 64 12 58 49 49 16 56 00 71 30 71 30 62 00 32 25 58 12 59 15 70 11 71 37 75 6 78 50 57 9 56 12 55 9 56 12 55 9 56 12 55 9 56 25 70 25 70 20 70 54 71 38 72 38 72 38 73 50 68 25 73 44 71 21 78 32 43 10 52 6 60 38 68 42 70 42 46 38 67 17 34 53	Feet. 82 1388 177 2979 771 19200 15700 7984 312 6 210 33 157 180 33 60 520 105 96 13 256 85 13287 16 33 131 98 82 16 131 98 82 16 131 98 82 16 131 98 82 16 131 98 82 16 131 98 82 9337 197 7 85 2168 1706 2690 9331	m. 25 423 54 908 235 5852 4785 7300 95 2 64 10 48 55 10 18 158 32 29 4 78 78 26 4050 5 10 4 40 30 25 5 40 25 2846 61 2 26 664 520 820 2844
Valparaiso (Chile) Villa Colon (Uruguay) Observatorio	33 I	71 38	131	40
Prado EUROPE. NORWAY AND SWEDEN.	34 51	56 19	95	29
*Bergen (Norway) *Berufjord (Sweden). *Bodö (Norway) Carlshamn (Sweden) Christiania (Norway) *Christiansund (Norway)	60 24 N. 64 40 67 17 56 10 59 55 63 7	5 19 E. 14 19 12 24 14 52 10 43 7 45	144 59 67 39 82 59	44 18 21 12 25 18

Note. — Stations with asterisk appear in the "Réseau Mondial" in the British Meteorological Office for 1912. (London, 1917.)

	Latitude.	Longitude from	Height.	
NORWAY AND SWEDEN. (Continued.)		Greenwich.		
Dovre (Norway) Florö (Norway) *Gjesvaer (Norway) *Harparanda (Sweden) Härnösand (Sweden) *Mehavn (Norway) Skudenes (Norway) Stockholm (Sweden) *Trondhjem (Norway) *Upsala (Sweden) *Vardö (Norway)	62° 5′ N. 61 36 71 6 65 50 62 37 71 1 59 9 59 21 63 26 59 51 70 22	62° 5′ W. 5 2 25 22 24 9 17 57 27 47 5 16 18 4 10 25 17 38 31 8	Feet. 2113 26 20 30 66 20 12 144 131 79 33	m. 644 7 6 9 20 6 4 44 40 224
RUSSIA.				}
RUSSIA. (WITH SIBERIA AND FINLAND.) Akhtuba. *Akmolinsk. *Arkhangelsk. Askhabad. *Astrakhan. *Barnaoul. Batoum. Belagatchskoe Zimovie. *Berezov. *Blagoveskchensk. *Blagoveskchensk Priisk. Bogoslovsk. Choucha. Dorpat. Derkoulskoe verderie. *Doudinka. *Ekaterinburg. Elatma. Elisavetgrad. *Eniseisk. *Fort Alexandrovsk. Golooustnoe. Goudaour. *Helsingfors. *Iakontsk. *Irgiz. *Irkutsk. *Jurjev. Kamenaïa Steppe. Kansk. Kargopol. Kars. Kazalinsk. *Kazan. Kem. Kerki.	64 33 37 57 46 21 53 20 41 40 51 00 63 56 59 45 59 45 59 45 59 45 59 45 59 45 58 22 49 3 69 7 56 58 48 31 58 27 44 31 58 27 44 31 58 27 58 30 69 50 5	46 9 E. 71 23 40 32 58 23 48 2 83 47 41 38 80 18 65 4 127 38 114 17 60 1 46 45 26 43 39 48 87 00 60 38 41 45 32 17 92 11 50 16 105 27 44 28 24 57 129 43 61 16 104 19 26 43 40 42 95 39 38 57 49 43 61 19 26 43 40 42 95 39 38 57 49 8 34 39 65 13	16 ?1138 22 741 -46 558 10 1043 131 ?525 ?1608 636 4487 243 499 ?66 948 459 403 276 79 1529 7231 38 354 367 1532 246 623 715 420 5731 230 262 41 804	5 ?347 7 226 -14 170 3 318 40 ?160 ?490 194 1368 74 152 ?20 289 140 123 84 24 466 2204 112 ?108 112 112 112 112 112 112 112 11
*Kharkov (University) *Kiev. *Kirensk. *Kola. *Krasnovodsk.	50 00 50 27 57 47 68 53 40 00	36 14 30 30 108 7 33 1 52 59	459 600 886 22 -49	140 183 270 7 -15

TABLE 107. LIST OF METEOROLOGICAL STATIONS.

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

RUSSIA.	Latitude,	Longitude from Greenwich.	Height,				
(Continued.)			Feet.	m.			
*Kuopio	62° 54′ N.	27° 40′ E.	328	100			
Kursk		36 12	•	236			
*Lenkoran	51 45 38 46	48 52	774 -62	-I9			
Libava	56 31	21 1	16	5			
Lubny (Gymnasium)	50 1	33 22	541	165			
Lugansk	48 35	39 20	148	45			
Magaratch	44 32	34 13	262	80			
*Malye Karmakouly	72 23	52 43	48	15			
Mariupolskoe verderie	47 39	37 30	gig	280			
Mezen	65 50	44 16	53	16			
*Minousinsk	53 43	91 41	837	7255			
*Moscow	55 45	37 34	512	156			
*Narynskoe	41 26	76 2	512 ?661 1	72015			
*Nertchinsk	51 59	116 35	1588	484			
Nertchinski Zavod	51 19	119 37	2041	622			
Nijni Novgorod	56 20	44 00	518	158			
*Nikolaevsk-um-Amour	53 8	140 45	69	21			
Nikolaief	46 58	31 58	64	20			
Nikolsk	59 32	45 27	508	156			
Novaia Alexandria* *Novorossiisk	51 25	21 57	482	147			
*Obdorsk	44 40	37 49	121	37			
*Odessa (University)	66 31	66 35	86	24			
*Okhotsk	46 29	30 46	213	65			
*Olekminsk	59 21	143 17	20	6			
*Omsk	60 . 22	120 26	7663	7202 88			
Orel	54 58	73 23	289 600				
*Orenburg	52 58 51 45	36 4 55 6		183			
*Oust-Maïskoe	51 45 60 25	55 6 134 29	374 7328	?100			
*Oust-Tsylma	65 27	52 10	782	725			
*Paikanskii Sklad	50 11	130 7	?55I	?168			
Pamirski Post	38 11	74 2	711042	73640			
Pavlovsk	59 41	30 29	130	40			
Pensa.	53 II	45 1	706	215			
*Perm	58 1	56 15	535	163			
Pernov	58 23	24 30	32	10			
*Petrograd	59 56	30 16	1 6	5			
*Petropavlosk	52 53	158 47	285	87			
*Petrozavodsk	61 47	34 23	128	39			
Pinsk	52 7	26 6	466	142			
Ploti	47 57	29 10	468	143			
Polibino	53 44	52 56	355	108			
*Port Arthur	48 27	89 12	643	196			
Povenets	62 51	34 49	141	43			
Rostov on Don	47 13	39 43	161	49			
Rykovskoe	50 47	142 55	410	125			
SagunySamarkand	50 36	39 43	685	200			
Sarapul	39 39	66 57	2369	722			
*Saratov	56 28	53 49	39 7	121			
Smolensk	51 32	46 3	197	60			
Sodankylä	54 47	32 4 26 36	79I	241			
*Sourgout	67 25 61 15		590	180			
Stavropol.		73 24	7131	740			
Surgut	45 3 61 15	41 59 73 24	1909	582			
*Tachkent	41 20	73 24 69 18	472 1568	42			
*Tchita	51 2	113 30	2211	478 674			
	J- 2	3 30	2211	0/4			
1		<u> </u>					

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

RUSSIA.	Latitude.	Longitude from Greenwich,	Height.	
(Continued.) Termez. *Tiflis. Tiumen. *Tobolsk. *Tomsk. Totaikoi. *Touroukhanst. Troitskosavsk. *Troitsko-Petcherskoe. Tulun. *Tygan Ourkan. Ufa. Uman. Uralsk. Uspenskaia. Valaam. Varshava (Warsaw) (University). Vasilevitchi. Velikiia Louki. *Velsk. Verkhniaia Michikha. *Verkhoïansk. *Vernyï. Viatka. Vilno. *Vladivostok. Vlotslavsk. Vologda. Vycknii Volotchok. Zlatoust.	37° 12′ N. 41 43 57 10 58 12 56 30 44 54 65 55 50 22 64 33 54 43 51 12 56 38 61 23 52 16 51 30 67 33 43 16 61 5 51 30 67 33 43 16 58 36 58 36 59 44 43 7 52 40 59 14 57 35 55 10	67° 15′ E. 44 48 65 32 68 14 84 58 34 11 87 38 106 27 56 13 100 22 124 46 55 56 30 13 51 22 39 12 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 31 29 48 30 57 21 1 29 48 30 57 21 1 29 48 30 57 21 1 29 48 30 57 21 1 29 48 30 57 21 1 29 48 30 57 21 1 29 48 30 57 21 1 29 48 30 57 30 58 31 32 44 76 53 49 41 25 18 131 54 19 4 39 53 34 34 59 41	Feet. 1017 1342 292 354 400 994 7131 2520 404 1617 71214 571 709 124 783 122 394 440 341 7285 4199 328 2566 607 486 88 213 407 548 1502	m. 310 409 89 108 122 303 740 768 7123 493 7370 174 216 38 239 37 120 134 104 787 1280 100 782 185 148 27 65 124 167 458
FRANCE. Bagnères-de-Bigorre Besançon (Observatoire) Bordeaux Brest Chamonix Cherbourg Dunkerque Langres Lyon (Saint-Genis-Laval) *Marseille Mont Blanc (Grands Mulets) Mont Blanc (Chamonix) Mont Blanc (Chamonix) Mont Blanc (Sommet) Mont Ventoux Montpellier *Nantes Nice (Observatoire) Paris (Central Meteo. Bureau) *Paris (Eiffel) Paris (Montsouris) Perpignan	43 4 N. 47 15 44 50 48 23 45 55 49 39 51 2 47 52 45 41 43 18 45 52 45 55 45 59 44 10 43 37 47 15 43 43 48 52 48 48 48 52 48 49 42 42	o 9 E. 5 59 0 31 W. 4 30 7 2 E. 1 38 W. 2 22 E. 5 20 4 47 5 23 6 51 6 51 6 51 5 16 3 53 1 34 W. 6 78 E. 2 18 2 30 2 18 2 20 2 53	1795 1020 243 200 3406 43 23 1529 981 246 9908 3405 14301 15781 6234 118 135 1115 108 164 1027 253 102	547 311 74 61 1038 13 7 466 299 75 3020 1038 4359 4810 1900 36 41 340 33 50 313 77 31

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

FRANCE.	Latitude.	Longitude from Greenwich.	Heig	ht.
(Continued.)			Feet.	m.
Pic du Midi de Bigorre	42° 56′ N. 45 46 45 46 49 5 43 37	o° 8' E. 2 86 2 57 0 30 W. 1 67	9380 1309 4813 387 636	2859 399 1467 118 194
GERMANY.				
GERMANY. Aachen (Prussia). Ansbach (Bavaria) Altenberg (Saxony) Augsburg (Bavaria) Bad Elster (Saxony) Bamberg (Bavaria) Bautzen (Saxony) Bayreuth (Bavaria) Berlin (Prussia) Berlin (Prussia) Brokum (Prussia) Brokum (Prussia) Brocken (Prussia) Brocken (Prussia) Brocken (Prussia) Bromberg (Prussia) Chemnitz (Saxony) Dresden (Saxony) Erfurt (Prussia) Freiberg (Saxony) Friedrichshafen (Württemberg) Grosser Belchen (Alsace) *Hamburg Helgoland (North Sea) Höchenschwand (Baden) Hohenheim (Württemberg) Hohenspeissenberg (Bavaria) Kahl a. M. (Bavaria) Kaiserlautern (Bavaria) Kaiserlautern (Bavaria) Keitum (Prussia) Kiel (Prussia) Königsberg (Prussia) Landshut (Bavaria) Leipzig (Saxony) Ludwigshafen (Bavaria) Mügdeburg (Prussia) München (Bavaria) Münster (Westfalen) Neufahrwasser (Prussia) Nürnberg (Bavaria) Passau (Bavaria) Passau (Bavaria) Passau (Bavaria) Posen (Prussia) *Potsdam observatory (Prussia) Regensburg (Bavaria) Regensburg (Bavaria) Regensburg (Bavaria)	50 47 8 50 17 51 11 49 57 52 30 55 50 55 50 55 50 55 50 55 60 60 60 60 60 60 60 60 60 60 60 60 60	6 6 E. 10 33 13 46 10 54 12 15 10 53 14 26 11 34 13 25 6 40 8 48 17 2 10 37 18 0 12 55 13 44 13 27 15 37 7 68 9 14 17 7 46 8 22 10 9 20 30 12 10 12 23 8 26 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 38 21 7 11 32 11 38 21 7 11 32 11 3	672 1437 2481 1640 1644 943 669 1190 125 26 52 482 3766 177 1092 361 718 1336 1338 4573 85 144 3296 1319 3261 374 794 416 26 155 33 1305 391 329 177 33 1726 210 15 1014 1015 279 1161 2551	205 438 756 500 288 204 363 38 16 147 1148 54 333 110 219 407 408 1394 26 44 1005 402 994 1114 242 127 8 8 47 10 398 110 54 398 110 54 398 110 54 398 110 54 398 110 54 398 110 54 398 110 54 54 54 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 88 84 77 86 86 86 86 86 86 86 86 86 86 86 86 86
Schneekoppe (Prussia)	54 20 50 36 50 44	10 23 12 38 15 44	1452 5282	3 443 1610

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

GERMANY.	Latitude.	Longitude from Greenwich.	Heigh	ıt.
(Continued.) Strassburg (Alsace). Stuttgart (Württemberg). Swinemünde (Prussia). Villingen (Baden). Wiesbaden (Prussia). Wilhelmshaven (Oldenburg). Würzburg (Bavaria). Wustrow (Mecklenburg). Zittau (Saxony).	48° 35′ N. 48 47 53 56 48 4 50 5 53 32 49 48 54 21 51 54	7° 46' E. 9 .11 14 16 8 27 8 14 8 9 9 56 12 24 14 49	Feet. 471 883 33 2342 374 28 588 23 827	m. 144 269 10 714 114 8 179 7 252
HOLLAND. Amsterdam. *De Bilt. Groningen Helder. Maastricht. Rotterdam. Vlissingen.	52 23 N. 52 6 53 13 5 52 58 50 51 51 54 51 26	4 55 E. 5 11 6 33 4 45 5 41 4 29 3 34	9 45 29 18 167 66 26	2 3 9 6 61 4 8
BELGIUM. Arlon Bruxelles Furnes Liège Macseyck Ostende *Uccle	50 37 51 6 51 14	5 48 E. 4 22 2 40 5 34 5 48 2 55 4 22	1450 131 20 246 115 23 328	442 40 6 75 35 7
*Aberdeen Armagh Ben Nevis. Bidston (Liverpool) Deerness, Orkney Is. Falmouth. Fort William Glasgow *Greenwich Holyhead (Harbour office) Kew *Lerwick London (Westminster) Malin Island. Oxford. Scilly Islands, St. Mary's. Shields North. Southport. Stonyhurst College Stornoway. Sumburgh head. *Valencia. Yarmouth.	58 56 50 99 56 49 55 53 51 28 53 18 60 30 55 23 51 46 49 56 49 56 55 39 53 51 58 11 59 51 59 51	2 6 W. 6 39 5 00 3 4 2 45 5 .4 5 7 4 18 0 00 4 39 0 19 1 8 0 8 7 24 1 16 6 18 1 27 2 59 2 28 6 22 1 17 10 15 1 43	88 200 4405 188 164 167 39 180 157 57 18 59 76 208 208 131 96 37 375 51 112 46 17	27 61 1343 57 50 51 12 55 48 17 6 18 23 63 63 40 29 11 114 16 34 14 5

SPAIN AND PORTUGAL.	2° 10′ E. 6 18 W. 8 25 28 38 15 26	Feet. 138 46 459 98 30	m. 42 14
Valencia (Spain) 39 28 ITALY	16 54 3 41 3 25 8 36 5 48 2 42 E. 25 40 W. 16 32 0 25 7 35 16 30	312 82 2149 1903 328 801 7 56 7328 92 4547 454	140 30 95 25 655 580 100 244 7 7100 28 1386 138
Alessandria 44 54 N. Asti 44 54 56 Belluno 46 8 Benevento 41 7 Bergamo 45 42 Bologna 44 30 Caserta 41 3 Castellaneta 40 38 *Catania (Bened.) 37 30 Conegliano 45 53 Cremona 45 8 Desenzano 45 8 Elena 41 12 Ferrara 44 51 Firenze 43 46 Foggia 41 27 Forli 44 13 Genova 44 25	o 22 W.	23	7
Ischia. 40 44 Lecce. 40 22 Livorno. 43 33 Messina. 38 12 Milano (Brera) 45 28 Modena. 44 54 Moncalieri. 45 0 Napoli. 40 52 Padova. 45 24 Palermo. 38 6 Pavia. 45 11 Perugia. 43 7	8 77 E. 8 13 14 45 12 14 14 48 9 81 11 21 13 82 16 56 14 65 12 19 10 3 10 72 13 35 13 43 11 77 11 15 15 31 12 2 8 95 13 54 17 72 10 18 15 33 9 11 12 29 7 77 13 76 11 92 12 80 9 10 12 23	321 465 1871 1325 558 1267 279 250 780 213 279 222 344 147 919 131 238 287 163 177 106 236 78 197 482 167 848 489 103 268 1706	98 142 570 404 170 386 85 76 238 65 85 68 105 45 280 47 73 87 50 147 51 258 149 31 71 82 520

ITALY.	Latitude.	Longitude from Greenwich.	Helgh	nt.
(Continued.)				
	g (137	0 45	Feet.	m.
Pistoia Prato	43° 56′ N.	10° 95′ E.	282 246	86 75
Reggio, Calabria	43 53 38 8	15 39	48	15
Riposto	37 41	14 72	46	14
Roca di Papa* *Roma, Collegio Romano	41 46	12 43	2493	760
Rovigo	41 54 45 3	12 29 11 87	207 60	63 21
Salo	45 36	10 71	328	100
SassariSestola	40 44	8 75	735	224
Siena	44 15 43 19	10 87 11 20	3585 1143	1092 348
Siracusa	37 3	16 75	76	23
Teramo	42 40	13 43	945	288
TorinoVenezia	45 4	7 82 12 20	907 70	276 21
venezia	45 26	12 20	70	21
SWITZERLAND.				
Alstätten	1, 0	93 3 E. 8 39	1476	450
AltdorfBasel	46 53	• •	1493 912	455 278
Bern	47 33 46 57	7 35 7 26	1877	572
Castasegna	46 20	9 31	2297	700
Chaumont	47 I	6 59	3701	1128
Davos Platz		9 49 6 9	5118 1329	405
Lugano	46 o	8 57	902	275
Neuenburg		6 57 8 16	160 1 6781	488 2067
Pilatus-Kulm	46 59 47 3	8 16 8 30	5863	1787
Säntis	47 15	9 20	8202	2500
Sils-Maria	46 26	9 46	5951	1814
St. Bernhard* *Zürich*		7 II 8 33	8123 1687	2476 493
	47 23	0 33	1007	493
AUSTRIA-HUNGARY.		F	208	01
Arco	45 55 N. 50 40	10 53 E.	528	161
Bielitz	49 49	19 3	1125	343
Bruck a.d. Mur	47 25	15 17	1591	485
Brünn	49 11 47 8	16 33 12 58	679 3947	207 1203
Bucheben*Budapest	47 8 47 30	19 2	369	112
Dobogókö	47 44	18 54	2290	698
Döllach	40 58	12 54	3359 308	1024 94
GörzGraz	45 57 47 4	13 37 15 28	300 1211	369
Gries b. Bozen	46 30	II 20	932	284
Gvertvó-Szt. Miklos	46 43	25 36	2670	814 227
Herény	47 10	16 36 11 24	744 1903	58o
Innsbruck	46 37	14 18	1476	450
Krakan	50 4	19 57 14 8	722	220
Kremsmünster	48 4	14 8 16 26	1260 62	384 19
Lesina Lussinpiccolo	43 IO 44 32	14 28	10	3
Lussimpiecolo	-17 J-			l

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

AUSTRIA-HUNGARY.	Latitude.	Longitude from Greenwich.	Heig	ght.	
(Continued.)				1	
Marburg Mariahrunn Nagyszeben Obir (Berghaus) Obir (Hannwarte) O-Gyalla Osielec Pécs Pelagosa Prag (Petrinwarte) Prag (Sternwarte) Prerau Rothholz Schmittenhöhe Sonnblick St. Katharein a. d. Lamming St. Pölten Tarnopol Tragöss Turkeve Ungvár Weiswasser *Wien (Hohe Warte) Wiener Neustadt Zágrah Zell am See Zsomholya	46° 34' N. 48 12 45 47 46 30 46 30 47 52 49 41 46 6 42 23 50 5 50 5 49 27 47 23 47 28 48 12 49 33 47 28 48 12 49 33 47 3 47 7 46 36 50 30 48 15 47 49 45 49 45 49 45 47	15° 39′ E. 16 14 24 19 14 29 18 12 19 47 18 14 16 16 14 25 17 27 11 48 12 57 15 10 15 37 25 36 15 5 20 45 22 18 14 48 16 22 16 15 15 58 12 48 20 43	Feet. 886 751 1358 6716 7021 394 1378 499 302 1066 646 696 1758 6456 10190 2083 899 1063 2510 288 433 964 666 869 531 2503 269	m. 270 229 415 2044 2140 120 420 152 92 325 197 212 536 1968 3106 635 274 324 765 88 132 294 203 265 162 763 82	
BALKAN PENINSULA AND ASIATIC TURKEY. *Athens (Greece). *Baghdad (Asiatic Turkey). *Beirut (Asiatic Turkey). Belgrad (Servia). Boulouk-Dere (Asiatic Turkey). *Bucharest (Roumania). *Busrah (Asiatic Turkey). Constantinople (European Turkey). El-Athroun (Palestine). *Hehron (Palestine). Jerusalem (Palestine). Kazanlyk (Bulgaria). Le Krey (Asiatic Turkey). Mamouret-ul-Aziz (Asiatic Turkey) Monastir (Servia). Saloniki (Greece). Sarona (Palestine). Scutari (Albania). Sinaia (Roumania).	37 38 N. 33 21 33 54 44 48 41 10 44 25 30 31 41 2 31 50 58 12 31 48 42 37 33 49 38 30 41 1 40 39 32 5 42 3 45 30	23 43 E. 44 28 35 28 20 27 29 3 26 6 47 53 28 58 34 60 62 21 35 11 25 24 35 40 39 22 19 3 23 7 34 47 19 3	351 128 108 453 384 269 26 246 656 49 2447 1220 3330 73281 2024 6 66 30 2821	107 39 33 138 117 82 8 75 200 15 746 372 1015 ?1000 617 2 20 9	
Sinape (Asiatic Turkey). Sivas (Asiatic Turkey). Sofia (Bulgaria). Smyrna (Asiatic Turkey). Sulina (Roumania).	45 30 42 I 39 43 42 42 38 26 45 9	25 34 35 19 34 50 23 20 24 49 29 40	759 4331 1804 6 6	500 ?18 1320 550 2 2	

SMITHSONIAN TABLES.

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

	Latitude.	Longitude from Greenwich.	Helé	ght.
MEDITERRANEAN. Canea (Crete) *Gibraltar. Kyrenia (Cyprus) Mahon (Minorca) *Malta *Nicosia (Cyprus)	35° 30′ N. 36 6 35 21 39 53 35 54 35 12	24° 00′ E. 5 21 W. 33 19 E. 1 57 14 31 33 24	Feet. 105 52 52 141 194 72	m. 32 16 16 43 59 22
ASIA. INDIA (WITH NEIGHBORING COUNTRIES).				
*Aden (Arabia) Agra Ajmer Akola *Akyab (Burma) *Allahabad Amini Divi (Lakkadives) Bangalore Batticaloa (Ceylon) Belgaum Bellary Berhampore *Bombay Burdwan *Bushire (Persia) *Calcutta *Cherrapunji Chittagong Cochin *Colombo (Ceylon) *Cothin Cuttack Dacca Darjeeling Deesa *Dehra Dun Dhurbi Diamond Island (Burma) Durbhunga Enzeli (Persia) *Galle (Ceylon) *Gauhati Hambantota (Ceylon) Hazaribagh Hoshangabad *Hyderabad Jacobabad Jaffna (Ceylon) *Jaipur *Jask (Persia) Jubbulpore *Kandy (Ceylon) *Karwar Katmandu	12 45 N. 27 10 26 27 20 42 20 11 25 25 11 6 12 58 7 43 15 52 15 9 18 18 54 23 16 28 59 22 36 25 15 22 21 9 58 6 56 10 00 20 48 23 43 27 3 24 14 30 20 26 2 15 52 26 10 37 30 20 6 1 26 8 6 7 23 59 24 24 28 24 29 46 25 44 29 40 26 56 25 44 28 10 7 18 14 48 27 42	45 3 E. 78 5 74 44 77 4 492 56 81 51 72 45 77 37 81 44 74 34 76 57 84 51 72 49 87 54 50 53 88 23 91 42 91 53 76 21 85 54 88 18 72 13 78 00 2 94 19 86 00 49 28 86 46 87 21 87 25 77 45 88 18 87 25 77 45 88 18 89 49 49 89 49 89 59 55 89 49 89 49 89 49 89 49 89 49 89 49 89 49 89 59 59 89 49 89	94 555 1632 930 208 13 2982 26 2524 1455 67 37 102 14 20 4308 87 10 23 10 80 35 6960 474 2234 115 41 166 69 20 48 194 40 2014 1004 95 186 9 1431 13 13 13 13 13 16 16 16 16 16 16 16 16 16 16	29 169 497 283 6 91 4 909 8 769 4443 20 11 31 4 6 1313 26 3 7 3 24 11 2121 144 681 355 12 51 21 6 15 59 12 61 305 29 57 3 436 4 408 504 13 1337

TABLE 107. LIST OF METEOROLOGICAL STATIONS.

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

INDIA.	Latitude.	Longitude from Greenwich.	Heig	ht.	
(Continued.) Khandwa *Kodaikanal observatory. *Kurrachee *Lahore. *Leh Lucknow Ludhiana *Madras Malacca (Straits Settlements) Meerut Mercara Mergui *Meshed (Persia) Mooltan Mount Abu Murree *Mysore *Nagpur Nuwara Eliya (Ceylon) Nowgong Patna *Penang (Straits Settlements) Periyakulam observatory Peshawar Poona *Port Blair (Andaman Is.) Province Wellesley (Straits Settlements *Quetta (Baluchistan) Raipur *Rangoon Ranikhet Ratnagiri	21° 50′ N. 10 13 24 53 31 34 34 10 26 55 30 55 13 4 2 12 29 1 112 26 112 27 36 16 30 12 24 36 33 55 12 18 21 8 6 46 25 3 20 42 5 34 10 9 34 2 18 31 11 40 5 21 30 11 21 15 16 46 29 40 17 8 20 52	76° 23′ E. 77 28 66 57 74 21 77 42 80 59 75 54 80 14 102 14 77 45 75 47 98 35 59 35 71 31 72 45 73 27 76 40 79 5 80 47 79 30 83 10 100 20 77 32 71 37 73 55 92 40 100 25 67 3 81 41 95 48 79 33 73 19	Feet. 1037 7688 13 732 11503 369 806 22 23 738 3721 96 3105 420 3945 6333 2520 1017 6240 757 179 16 944 1110 1992 59 57 5502 970 20 6069 110 887	m. 316 2343 4 223 3506 112 246 7 7 225 1134 29 946 128 1202 1930 768 310 1902 231 54 55 288 338 607 18 17 1677 296 6 1850 34	
Roorkee Salem Saugor Island Secunderabad *Seychelles *Shillong Sholapur Sibsagar Silchar *Simla *Singapore (Straits Settlements) Sutna. Trichinopoli Trincomalee (Ceylon) Vizagapatam *Waltair Wellington CHINA AND INDO-CHINA. Cap-Saint Jacques (Indo-China).	29 52 11 39 21 40 17 27 4 37 25 33 17 40 26 59 24 50 31 7 1 17 24 34 10 50 8 33 17 42 17 45 11 22	77 53 78 12 88 10 78 33 55 27 91 48 75 56 94 41 92 51 77 8 103 55 78 46 81 15 83 20 83 16 76 50	887 940 6 1787 16 4921 1585 333 89 7224 6 1040 272 12 30 30 6200	270 286 2 545 5 1500 483 101 27 2204 2 317 83 4 9 9 1800	
*Hang Kow (China)	30 35 21 2 45 43	114 17 105 50 126 28	121 43 502	37 13 153	

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

CHINA AND INDO-CHINA.	Latitude,	Longitude from Greenwich.	Heig	ht,
(Continued.) *Hongkong (China) Kashgar (China) Lang-biam (Indo-China) *Moncay (China) *Mukden (China) *Nha-Trang (Indo-China) Pekin (China) *Phu Lien (China) Pnom-Penh (Indo-China) Pulo-Condor (Indo-China)	22° 18′ N. 39 25 12 2 21 31 41 48 12 16 39 57 20 48 11 35 8 16	114° 10′ E. 76 7 108 20 107 51 123 23 108 72 116 28 106 37 104 56 106 35	Feet. 108 3999 4606 33 144 23 125 380 26 21	m. 33 1219 1404 10 44 7 38 116 8 6
*Saigon (Indo-China) *Shanghai (China) Zi-Ka-Wei *Tiensin (China) Tsingtau (Kiao-chau) Urga (China) JAPAN AND KOREA.	10 46 31 12 39 10 36 4 47 55	106 42 121 26 117 10 120 19 106 50	36 23 16 259 ?4447	7 5 79 ?1325
*Chemulpo (Korea) Fusan (Korea) Hakodate Hirosima Hukuoka *Joshin (Korea) *Kioto Kobe Kumamoto Matuyama *Miyako *Nagasaki *Naha Nagoya *Nemuro *Ochiai Osaka Sapporo Tadotu *Taihoku *Tokio Tokusima Tsukubasan PHILIPPINES AND HAWAIIAN ISLANDS.	37 29 N. 35 7 41 46 34 23 33 35 40 40 35 1 34 41 32 49 33 50 38 32 44 26 13 35 10 43 20 47 20 34 39 43 47 25 2 35 41 34 3 36 13	126 32 E. 129 5 140 44 132 27 130 25 129 11 135 46 135 11 130 42 132 45 141 59 129 52 127 41 136 55 144 244 135 26 141 21 133 46 141 21 133 46 121 31 139 45 134 33 140 6	223 49 13 10 20 13 161 191 129 106 98 436 34 50 10 55 16 30 70 13 2854	68 15 4 3 6 4 49 58 39 32 30 133 10 27 15 3 17 5 9 21 4 870
Aparri (Luzon) Altimonan (Luzon) Baguio (Benguet) *Bolinao (Luzon) Cebu (Cebu) Dagupan (Luzon) *Honolulu (Hawaii) Iloilo (Panay) Legaspi (Luzon) *Manila (Luzon) Midway Island *Ormoc (Leyte)	18 22 N. 14 00 16 25 16 24 10 18 16 3 21 19 10 42 13 9 14 34 28 13 11 00	121 38 E. 121 55 120 36 119 53 123 54 120 20 157 52 W. 122 34 E. 123 45 120 58 177 22 124 36	16 13 4961 33 30 10 39 20 20 46 19	5 4 1512 10 9 3 12 6 6 6 14 6

SMITHSONIAN TABLES.

PHILIPPINES AND HAWAIIAN ISLANDS. (Continued.)	Latitude.	Longitude from Greenwich.	Heigh	it.
*Surigao (Mindanao) *Tagbilaran (Bohol) *Vigan (Luzon)	9° 48′ N. 9 38 17 34	125° 29′ E 123 51 120 23	Feet. 20 85 49	m. 6 26 15
EAST INDIES.				
*Batavia (Java) *Christmas Island. *Cocos Keeling Island. *Kajoemas (Java) *Kota Radja (Sumatra). *Medan (Sumatra). *Padang (Sumatra). *Pontianak (Borneo). *Port Moresby (New Guinea). Samarai. *Sandakan (Borneo).	6 II S. 10 25 12 5 7 56 5 32 3 35 0 56 7 38 0 I 9 29 10 3.7 5 49	106 50 E. 105 43 96 54 114 9 95 20 98 41 100 22 112 55 109 20 147 9 150 40 118 12	26 20 16 3117 23 79 23 16 10 128 20	8 6 5 950 7 24 7 5 3 39 6
AUSTRALASIA.				
*Adelaide (South Australia) Albany (West Australia) *Alice Springs (South Australia). *Alice Springs (South Australia). *Boulia (Queensland) *Bourke (New South Wales) *Brisbane (Queensland) Burketown (Queensland) Camooweal (Queensland) *Christchurch (New Zealand) Cooktown (Queensland) *Coolgardie (Western Australia). *Daly Waters (Northern Territory). *Danger Point (New South Wales) *Derby (Western Australia) *Dunedin (New Zealand) *Eucla (Western Australia) *Bourdin (New Zealand) *Eucla (Western Australia) *Hall's Creek (Western Australia) *Hall's Creek (Western Australia) *Katanning (Western Australia) *Katanning (Western Australia) *Launceston (Tasmania) *Launceston (Tasmania) *Laverton (Western Australia) *Mein (Queensland) *Mein (Queensland) *Mein (Queensland) *Melbourne (Victoria) *Mitchell (Queensland) *Melbourne (Victoria) *Melbourne (Victoria) *Melbourne (Victoria) *Peak Hill (Western Australia) *Peak Hill (Western Australia) *Perth (Western Australia) *Port Darwin (Northern Territory) Richmond (Queensland) *Rockhampton (Queensland) *Streaky Bay (South Australia)	34 56 S. 35 2 23 38 36 50 22 55 30 13 27 28 17 45 19 57 43 32 15 28 30 57 16 16 34 37 17 18 45 52 31 45 52 31 45 23 18 23 42 21 53 33 42 21 53 21 43 25 38 21 53 21 43 25 38 21 43 25 38 21 43 21 43 22 44 23 44	138 35 E. 117 50 123 37 174 50 139 38 145 58 145 58 143 2 139 33 138 17 172 38 145 17 121 10 133 23 19 18 123 40 170 31 128 58 143 33 127 46 147 20 147 35 147 10 117 35 147 10 1122 23 149 13 142 57 144 59 147 59 147 59 147 59 147 59 147 59 147 59 147 59 147 59 147 59 148 47 118 47 118 57 118 47 118 47 115 51 130 51 143 10 150 30 153 16 134 13	141 41 1926 125 479 360 137 27 758 27 17 1388 699 66 53 295 15 990 1224 160 1017 30 1463 36 400 115 1110 1270 13 1929 197 98 697 37 330 43	43 12 587 38 146 110 42 8 8 231 8 5 423 213 20 16 90 5 302 373 49 310 9 466 118 122 35 337 386 4 588 60 30 212 11 100 13

AUSTRALASIA.	Latitude.	Longitude from Greenwich.	Heigi	nt.
*Sydney (New South Wales) Thargomindah (Queensland) Thursday Island (Queensland) Townsville Pilot Station (Queens-	33° 52′ S. 27 58 10 34	151° 12′ E. 143 43 142 12	Feet. 146 402 17	m. 44 122 5
land). *Wellington (New Zealand). *William Creek (South Australia) Windorah (Queensland)	19 14 41 16 28 55 25 26	146 51 174 46 136 21 142 36	73 6 249 390	22 2 76 119
*Ambon . *Apia (Samoa) . *Alofi (Niue Is.) . *Chekhar Lland	3 42 S. 13 48 19 2	128 10 W. 171 46 169 55	13 16 121	4 5 37
*Chatham Island *Fanning Island. Gomen (New Caledonia) *Guam (Ladrones Is.) *Koepang *Lord Howe Island *Malden Island. *Moure (Easter Is.) *Norfolk Island. *Noumea (New Caledonia) *Ocean Island. *Rarotonga (Cook Is.) *Rendova (Solomon Is.) *Suva (Fiji) *Tahiti (Low Arch.) *Tulagi (Solomon Is.) *Uyelang. *Yap.	43 52 3 55 N. 20 21 S. 18 24 N. 10 10 S. 31 32 27 10 29 4 S. 22 16 0 52 21 12 8 24 18 8 8 15 47 9 5 9 42 9 29	170 42 159 23 164 10 E. 144 38 123 34 159 4 155 00 W. 109 26 167 58 E. 166 27 169 36 159 47 W. 157 19 E. 178 26 148 14 160 8 161 2 138 8	190 13 66 10 26 98 ? 30 92 ? ? 13 154 6 333 105	58 4? 20 3? 8 3? 98 ? 47 20 32
*AFRICA. *Accra (Brit. Guinea)	5 35 N. 9 1 31 9 36 47 24 2 13 24 32 7 37 17 20 10 S. 30 4 N. 29 52 5 5 5 35 47 33 56 S. 33 37 36 22 9 31 36 22 25 30 6 49 S. 9 4 29 51	o 6 W. 38 43 E. 29 54 2 64 32 53 16 36 W. 20 2 E. 9 50 28 40 31 17 31 20 1 13 W. 5 55 18 29 E. 7 35 W. 19 20 E. 13 43 W. 6. 37 E. 29 00 39 18 143 13 31 00	59 7874 105 125 328 16 30 30 4469 108 380 7 191 30 56 1493 52 2105 426 26 262	18 2400 32 38 100 5 9 - 1362 33 116 ? 58 9 17 455 16 660 130 8 8 80

AFRICA:	Latitude.	Longitude from Greenwich.	Heig	ht.	
(Continued.)			F4		
*East London (Cape Colony) El-Djem (Algeria) *El Obeid (Brit. Sudan) *Entebbe (Brit. East Africa) Fort Napier (Natal) Fort National (Algeria) Geryville (Algeria) Grahamstown (Cape Colony) *Gwelo (South Rhodesia) *Harrar (Ahyssinia) *Heidelberg (Transvaal) *Insalah (Sahara) Ismailia (Egypt) *Johannesburg (Transvaal) *Kadugli (Brit. Sudan) *Kafia Kingi (Brit. Sudan) *Katagum (Nigeria) Kenilworth (Kimberley) *Khartoum (Egypt) *Kimberley (Cape Colony) *Kontagora (Nigeria) Laghouat (Algeria) Laghouat (Algeria) *Lagos (Nigeria) *Lamu (Brit. East Africa) *Libreville (Fr. Congo) *Loango (Fr. Congo) *Loango (Fr. Congo)	33° 2′ S. 355 21 N. 13 11 0 5 S. 36 38 N. 33 41 S. 19 42 N. 34 5 S. 27 17 N. 30 36 S. 11 2 N. 9 22 17 S. 12 17 S. 12 17 S. 12 17 S. 13 37 N. 28 42 S. 15 37 N. 28 43 N. 33 48 6 22 16 S. 0 23 N. 4 38 S. 25 58	27° 55′ E. 10 38 30 14 32 29 30 23 3 72 1 00 26 32 29 49 42 30 20 58 2 27 31 76 28 4 29 45 20 45 21 27 32 33 24 46 5 24 27 32 33 24 46 5 24 27 32 33 28 40 54 9 26 11 50 32 36	Feet. 33 541 1919 3862 2200 3051 4281 1800 4646 6089 5056 1083 30 6148 1650 1955 102 3950 1309 4042 1312 2559 26 10 115 7164 194	m. 10 165 585 1177 671 930 1305 540 1416 1856 1541 330 9 1874 503 596 31 1204 390 1232 400 780 8 3 35 750 59	
*McCarthy Is. (Gambia). *Maiduguri (Port. East Africa). *Mauritius (Royal Alfred Observatory). Mayumba (Fr. Congo). Mojunga (Madagascar). Mozambique (East Africa). *Nairobi (Brit. East Africa). *Nairobi (Brit. East Africa). Oran (Algeria). Ouargla (Algeria). Port Elizabeth (Cape Colony). Port Said (Egypt). Porto Novo (Dahomey). *Pretoria (Transvaal). Queenstown (Cape Colony). St. Denis (Réunion). *St. Helena. St. Louis (Senegal). St. Paul de Loanda (Angolo). *St. Vincent (C. Verde Is.). *Sainte-Croix-des-Eshiras (Fr. Congo). *Salisbury (Rhodesia). *San Tiago (C. Verde Is.). *Ségou (Fr. West Africa). *Sierra Leone (Sierra Leone). *Sokoto (Nigeria). *Tamatave (Madagascar). *Tananarivo (Madagascar).	13 .42 N. 11 .48 20 6 S. 3 23 15 45 1 18 0 2 N. 35 42 31 55 8 S. 31 58 S. 31 54 20 51 15 57 N. 8 47 S. 16 54 N.	34 46 W. 13 12 E. 57 33 10 31 46 19 49 44 36 59 35 5 0 39 W. 4 70 E. 25 37 31 79 2 40 28 11 26 52 55 30 5 40 W. 16 31 13 13 E. 25 4 W. 10 21 E. 31 3 W. 6 17 13 9 5 14 E. 32 32 49 26 47 43	13 1214 177 200 134 13 5446 6594 174 407 181 14 65 5170 3500 102 2073 6 194 36 640 4878 112 7892 223 1161 10 13 4593	54 370 54 61 41 6 1660 2010 53 124 55 4 20 1576 1067 31 632 2 59 11 195 1487 34 ?272 68 354 3 4 1400	

Note. — Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1912. (London, 1917.)

AFRICA.	Latitude.	Longitude from Greenwich.	Height.	
(Continued.) Tangier (Morocco) *Timbouctoo (Fr. West Africa) *Tunis (Tunis) Upper Sheikh (East Africa) Vivi (Congo) *Wadi Halfa (Egypt) *Wau (Brit. Sudan) *Windhuk (Ger. South West Africa) *Yola (Nigeria) *Zanzibar (Brit. East Africa) *Zomba (Nyasaland Prot.) *Zungeru (Nigeria)	9 12 N. 6 10 S. 15 23	5° 49′W. 2 92 10 10 E. 45 11 13 49 31 20 28 3 17 5 12 30 39 11 35 18 6 10	Feet. m. 246 75 820 250 141 43 4593 1400 364 111 420 128 1444 440 5463 1665 850 259 73 22 2949 899 426 130	
ARCTIC AND ANTARCTIC. (See also Greenland, Iceland, Russia, etc.) Bossekop. *Cape Evans (McMurdo Sound). *Cape Pembroke. Dicksonhavn. Fort Rae. *Framheim. Jan Mayen. Kingua-Fjord (Cumberland Sound). Lady Franklin Bay. Novaya Zemlya. Orange Bay. Point Barrow. Sagastyr. *Spitsbergen Advent Bay. Green Harbour. *South Georgia. *South Orkneys.	51 41 73 30 N. 62 39 78 38 S. 70 59 N. 66 36 81 44 72 30 55 31 S. 71 23 N. 73 23 78 2 78 2 78 2 78 2 54 14 S.	23 15 E. 166 24 57 42 W. 81 00 E. 115 44 W. 163 37 8 28 67 9 64 45 52 45 E. 70 25 W. 156 40 124 5 E. 15 6 14 14 36 33 W. 44 39	7	

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